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CAMBRIA STEEL

TO THE HONORABLE
MEMBERS OF THE
HOUSE OF REPRESENTATIVES
IN SENATE CHAMBERS
WASHINGTON, D. C.

FOR THE YEAR 1904

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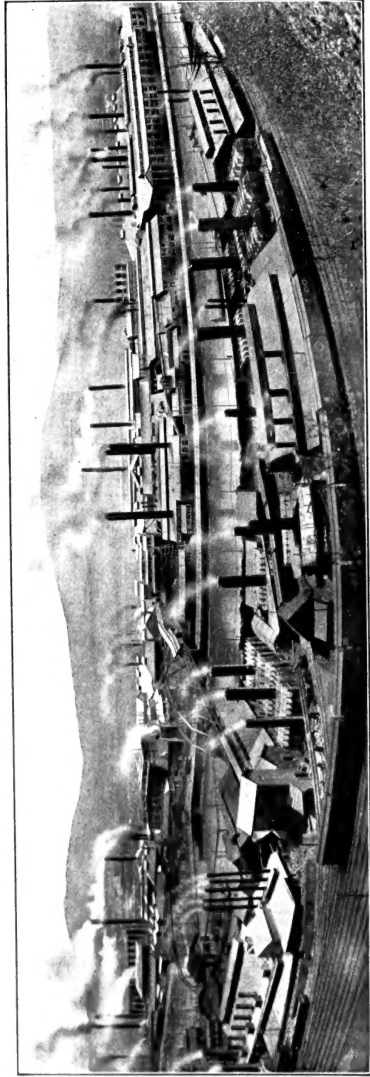
S/A 77

CONSOLIDATED STEEL CORPORATION
TORONTO, ONT.

CAMBRIA STEEL COMPANY'S WORKS

JOHNSTOWN, PA.

CAMBRIA PLANT



← ONE MILE →

BLAST FURNACES 1-4

FOUNDRY

PAINT, CAR REPAIR AND PATTERN SHOPS

ROLL SHOP

MACHINE SHOP

AXLE SHOP

RAIL AND SHAPE MILLS

COAL STORAGE

BLAST FURNACES 5 AND 6

BLOOMING, BILLET AND BEAM MILLS

BESSEMER STEEL WORKS O. H. STEEL WORKS

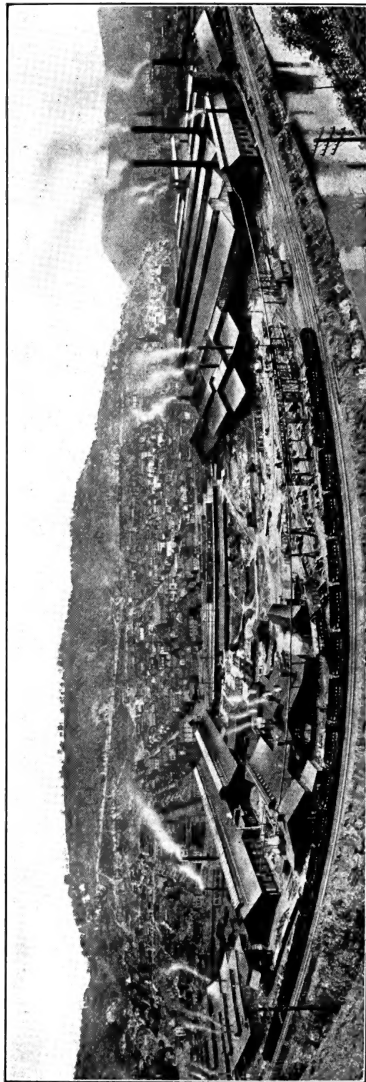
COAL BRIDGE

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COAL BRIDGE

GAUTIER PLANT



COLD ROLL SHOP

9" MILL

BAR MILL

PLATE MILLS

RAKE SHOP

MACHINE SHOP

DISC SHOP

UNIVERSAL PLATE MILL

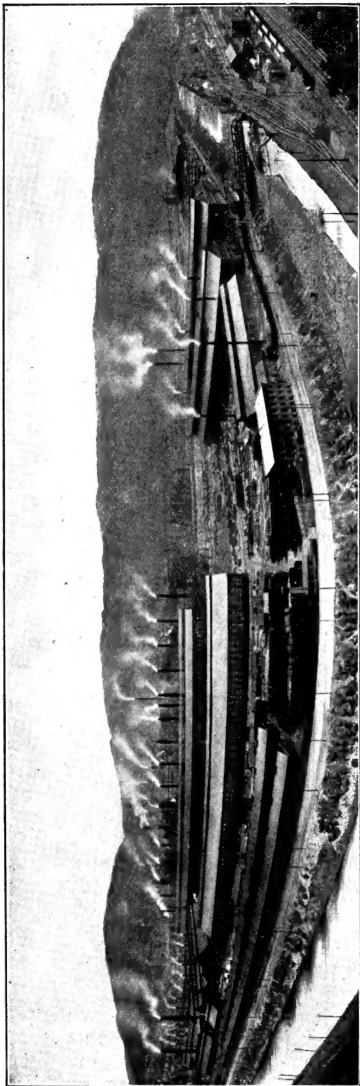
10" MILL

14" MILL

8" MILL

ROLL SHOP

FRANKLIN PLANT



BLOOMING MILLS
SLABBING MILL
CAR PAINT SHOP

COKE PLANT
BLAST FURNACES 7 AND 8
O. H. STEEL WORKS
134" PLATE MILL

POWER PLANT

CAR SHOP
FORGE SHOP
BOLT SHOP

STRUCTURAL SHOP
BEAM YARD

GENERAL SALES OFFICES: PHILADELPHIA, PA., U. S. A.

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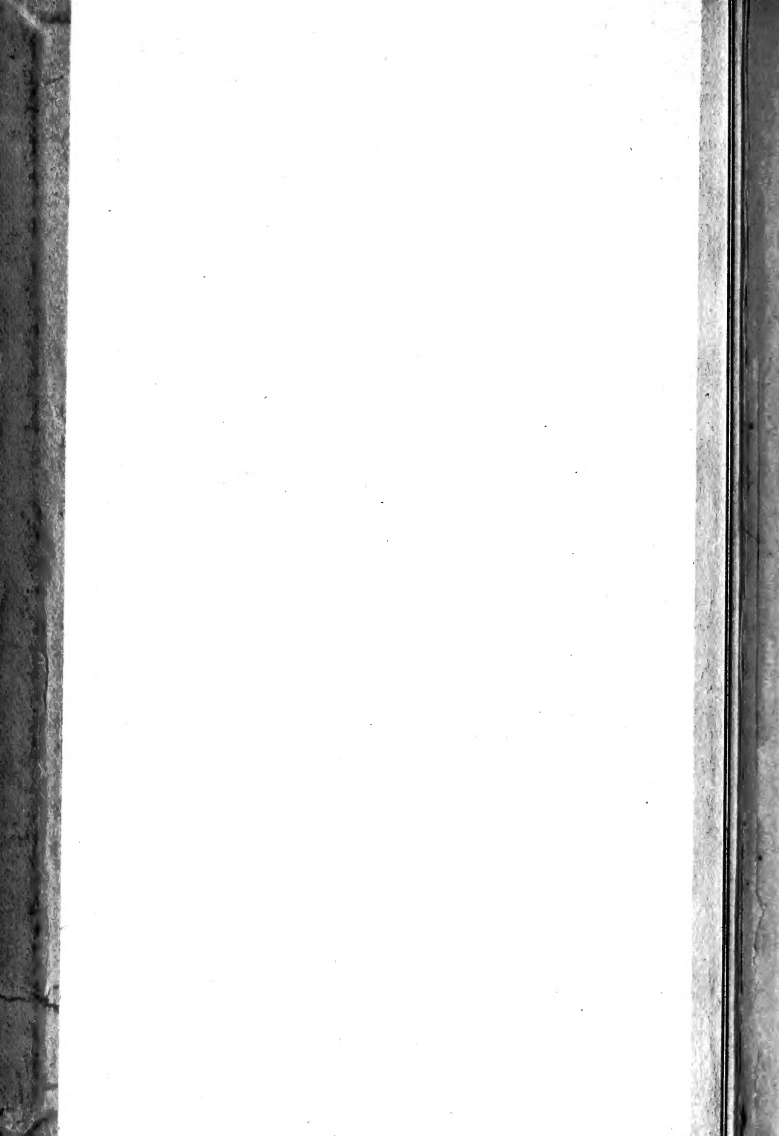
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CAMBRIA STEEL

A HANDBOOK OF INFORMATION
RELATING TO

STRUCTURAL STEEL

MANUFACTURED BY THE
CAMBRIA STEEL COMPANY

CONTAINING USEFUL TABLES, RULES,
DATA, AND FORMULÆ FOR
THE USE OF

ENGINEERS, ARCHITECTS,
BUILDERS AND MECHANICS

PREPARED AND COMPILED BY
GEORGE E. THACKRAY, C. E.
SPECIAL ENGINEER, CAMBRIA STEEL CO.

GENERAL OFFICES: PHILADELPHIA, PA.
WORKS AT JOHNSTOWN, PA.
U. S. A.

2) 1919

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Price, \$1.50



PREFACE TO TWELFTH EDITION.

This edition introduces much new matter thought useful, and revises, to a considerable extent, the data of the prior edition, to conform to current practice and a wider range of structural products.

The table of steel ingots is greatly amplified by the addition of more sizes and styles.

Cuts and properties of many new sections are introduced, among which are bulb angles, top-guard bulb angles, 3-inch and 4-inch channels for cars, 12-inch ship channels, and some seventeen T-bars of considerable range in dimensions.

Three sizes of rolled steel car stakes are also included.

Drawings and tabulations of standard ship sections including ship channels, bulb angles and one Z-bar hatch section, together with the equal leg and unequal leg angles selected as standards for ship building, which were adopted on November 20, 1918, are now given.

Rolled safety floor plates and buckle plates are newly listed in most convenient sizes.

In view of well-recognized practice, the standard connection angles formerly shown have been superseded by new standards and all tables relating thereto are correspondingly modified.

Additional new tables believed of value have been incorporated. These refer to Flat and Corrugated Steel Sheeting; Roof Truss Dimensions and Stresses; Moments of Inertia of Rectangles; Sizes of Wrought Spikes and Wood Screws; Wire Gauges shown in Combined Table; Decimal Equivalents of Non-Binary Fractions; Square Roots and Cube Roots of Fractions; Weights of Circular Steel Plates; Trigonometrical Formulæ; Squares and Cubes of Numbers and Fractional Intervals; Combinations and Factors of π ; Relations in Circular Segments; Volumes and Surfaces of Solids; Minutes and Seconds expressed in Decimals of a Degree and vice versa; Metric and Customary Measure Conversions, etc.

The tables of weights for various substances and materials have been considerably augmented.

Specifications for Structural and Boiler Steel have undergone slight revision to bring these up to date.

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GENERAL INFORMATION.

Our products are principally steel, made by the Bessemer or Open Hearth process, as required, and of all qualities from the softest rivet stock to high carbon special spring material.

Our Beams and Channels are made to conform to the American Standards, adopted January, 1896, in which the flanges have a uniform slope of one to six, and the dimensions, proportions and weights are determined by a regular schedule, as shown on the diagrams on pages 28 and 29. The standard proportions of beams and channels are further shown on page 27.

The principal structural angles now made are limited in number to conform to the American Standards, as revised May 21, 1910, and include eight base, or a total of fifty-four sizes for equal leg angles, and nine base, or a total of fifty-seven sizes of unequal leg angles, all varying in thickness by one-sixteenth inch, as shown on pages 17 and 18 and tables herein. It is believed that these standard angles include a sufficient range of sizes to meet all usual structural requirements, but, at the same time, we will continue the manufacture of angles of special sizes and proportions for those who require them, as shown on page 19.

The weights of angles, now given, are those adopted as American Standards in May, 1910.

The standard ship sections adopted November 20, 1918, comprising ship channels, bulb angles and one Z-bar hatch section are now shown and tabulated herein for the first time, and these standards also include certain equal leg and unequal leg angles, which were adopted on the same date, as standards for ship building, all of which are shown and indicated herein by a dagger. Although the drawings of standard structural sections herein show the minimum sizes, the drawings of standard bulb angles and ship channels are made to indicate the sizes of the British standard sections, which form the basis of these ship section standards.

During the time when rolls are being prepared for the new ship channels and bulb angles, our older sections of these shapes shown herein will be furnished, but as the new rolls become ready, the standard sections will be supplied and the prior shapes will be obsolete.

The method of increasing the sectional area of shapes from the minimum or base sizes to intermediate and maximum sizes, is

shown approximately on page 26. For beams and channels the increase from the minimum adds equally to the web thickness and flange width, the weight of the increase being equal to that of a plate of the same depth as the section, and of a thickness equal to the increase of the dimensions stated.

The method of increasing the thickness of angles from the minimum has the effect of adding to the length of the legs, as shown on page 26, so that for intermediate and maximum sizes the legs will be somewhat longer than the minimum or nominal dimensions, except in the cases for which we have finishing grooves. The plates of drawings of sections, pages 2 to 26 inclusive, show the minimum or base sizes of the various shapes, except in cases of standard ship channels and bulb angles as heretofore noted. Sections shown on the plates or lists for which more than one weight is stated can be rolled of different thicknesses to produce the stated weights. Others for which only one weight is given cannot be varied. Each section shown herein is numbered, both in the plates and tables, for convenience in reference and ordering.

I-Beams and Channels should be ordered of weights shown in the tables. Orders and inquiries concerning 12 in. 40 lb., 15 in. 60 lb., and 15 in. 80 lb. I-Beams should also specify these by Section Number.

Orders for angles and plates should specify either the thickness or the weight, but not both.

Orders for universal or edged plates should specify the width and thickness in inches and the length in feet and inches, whereas orders for sheared plates should give all the dimensions in inches.

All weights are stated in pounds per lineal foot of section, except in the table of rails on page 214, in which the weights are given in pounds per yard, as is customary. Weights of rolled sections are calculated on the basis of 489.6 pounds per cubic foot of steel, and 3.4 times the sectional area in square inches equals the weight in pounds per lineal foot. In calculating the weights, areas, and properties of I-Beams, Channels, and Angles for the lists and tables herewith, the fillets and smaller rounded corners were not considered.

The dimensions of all steel material herein are theoretical, as they are subject to customary rolling variations.

Structural Angles, I-Beams and Channels, unless otherwise ordered, will be cut to length with variation not to exceed $\frac{3}{8}$ inch more or less than that specified. For cutting to exact lengths, or with less variation than $\frac{3}{8}$ inch, an extra price will be charged.

All sections shown herein are steel.

**OFFICES FOR SALE OF
CAMBRIA STEEL COMPANY PRODUCTS.**

**GENERAL OFFICES: WIDENER BUILDING,
PHILADELPHIA, PA., U. S. A.**

- ATLANTA.....Candler Building, 129 Peachtree Street.
BOSTON.....Scolly Building, 40 Court Street.
CHICAGO.....McCormick Building, Corner of Michigan
Avenue and Van Buren Street.
CINCINNATI.....Union Trust Building, Corner of Fourth and
Walnut Streets.
CLEVELAND.....Swetland Building, 1010 and 1012 Euclid
Avenue.
DETROIT.....Penobscot Building, 45 Fort Street, West.
NEW YORK.....City Investing Building, 165 Broadway.
PHILADELPHIA.....Widener Building, Chestnut and Juniper
Streets.
PITTSBURGH.....Oliver Building, Smithfield Street.
ST. LOUIS.....Chemical Building, Corner of Eighth and
Olive Streets.
SALT LAKE CITY....Newhouse Building, Corner of Main Street
and Exchange Place.
SAN FRANCISCO....Monadnock Building, 681 Market Street.
SEATTLE.....Colman Building, Corner of First Avenue
and Marion Street.
WASHINGTON, D. C..Woodward Building, Corner of Fifteenth
and H Streets, N. W.

**WORKS AT
JOHNSTOWN, PA.
U. S. A.**

CAMBRIA STEEL COMPANY PRODUCTS.**STRUCTURAL STEEL WORK.**

Finished Steel Work for Buildings, including Beams, Girders, Columns, Roof Trusses, etc., fitted complete and ready for erection.

STEEL CARS.

Gondola, Hopper-Gondola, Hopper, Flat, Tank, Mine, etc., Underframes and Trucks.
Freight, Passenger, Electric and Industrial Car Wheels.
Draft Gears, Forged and Pressed Steel Car Parts.

STEEL RAILS.

Steel T-Rails, 12 lbs. to 150 lbs. per yard.
Angle, Plain and Special Type Splice Bars.
Standard and Special Track Bolts and Nuts.
For detailed information, see Rail and Splice Catalogue.

STEEL AXLES.

Passenger Car, Freight Car, Tender Truck, Engine Truck, Driving, Electric Car, Street Car, Mine Car, etc.

CRANK PINS, PISTON RODS, BRIDGE PINS.

Made to any requirement.

**MACHINE BOLTS, NUTS, RIVETS, AND PIPE OR TANK BANDS
WITH ROLLED THREADS.****FORGINGS.**

Axles, Crank Pins, Piston Rods and Forgings in general furnished of carbon steel, annealed, or treated by our Coffin toughening process (patented) as specified.
Crank Pins and Piston Rods also furnished oil-tempered and annealed; other small Forgings will be, if desired.
For small car forgings and pressed steel parts, see list on pages 30 and 31 herein.

ANNULAR ROLLED SECTIONS.

Car Wheels, Crane Track Wheels, Blanks for Cylindrical Wheels, Gears, Sprockets, Band Wheel Flanges, Pipe Flanges, Bevel Rollers, and Automobile Fly Wheels, etc.

MERCHANT BAR STEEL.

Including Tire, Toe Calk, Machinery, Automobile Spring, Carriage Spring, Baby Carriage Spring, Railroad Spring, Hoe, Rake, Fork, Forging, Bolt, Rivet, etc.
Special Sections.
Automobile and Motor Truck Rim Sections.

STEEL SPECIALTIES.

Mine Ties, Fence Posts, Reinforcing Bars, etc.

AGRICULTURAL STEEL AND SHAPES.

Finger Bars, Knife Backs, Rake Teeth, Bundle Carrier Teeth, Tedder Forks and Springs, Spring Harrow Teeth, Harrow (Drag) Teeth, Seat Springs, etc.

FLOW STEEL.

Bars and Slabs (Pen and Pernot), Flat Plow Shapes, Digger Blades, Hammered Lay, Rolled Lay, etc.

COLD ROLLED AND COLD DRAWN STEEL.

Rounds, Squares, Hexagons, Flats, Shafting and Special Shapes.

STEEL DISCS WITH ROLLED BEVEL.

10" to 20" diameter dished for Harrows, Drills, Cultivators, etc.

23" to 28 $\frac{1}{4}$ " diameter dished for Plows.

8" to 26" diameter flat for Rolling Coulters.

PRESSED STEEL SEATS FOR AGRICULTURAL IMPLEMENTS.**WIRE RODS, WIRE AND WIRE PRODUCTS.**

Wire Rods. Bolt, Screw and Rivet Wire.

Bright and Annealed Wire.

Galvanized Coiled Steel Spring Wire.

Barbed Wire, Galvanized or Painted.

Wire Nails, Bright or Galvanized.

Cement Coated Nails.

Fence Wire and Wire Fence. Fence and Poultry Netting Staples.

Bale Ties—Single Loop.

NON-STEEL PRODUCTS.

Cinder, Slag and Coal Derivatives.

Limestone Ballast and Screenings.

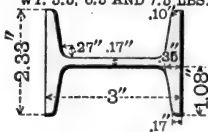
FOR PRODUCTS NOT LISTED HEREIN, SEE SPECIAL CATALOGUES.

SECTIONS
OF
STRUCTURAL STEEL SHAPES
MANUFACTURED BY
CAMBRIA STEEL COMPANY

STANDARD BEAMS.

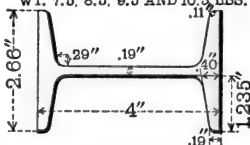
B. 5

WT. 5.5, 6.5 AND 7.5 LBS.



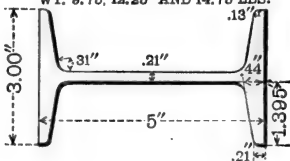
B. 9

WT. 7.5, 8.5, 9.5 AND 10.5 LBS.



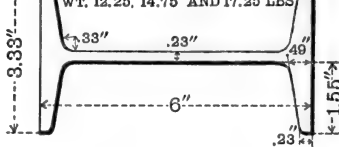
B. 13

WT. 9.75, 12.25 AND 14.75 LBS.



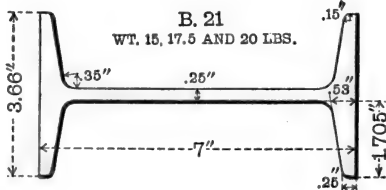
B. 17

WT. 12.25, 14.75 AND 17.25 LBS.

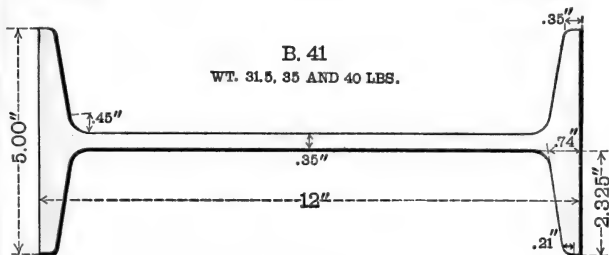
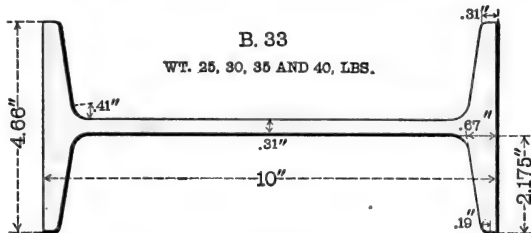
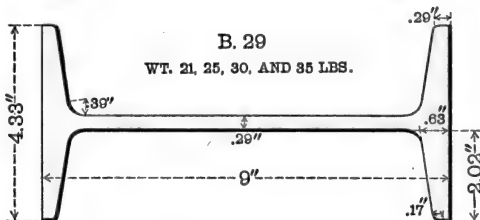
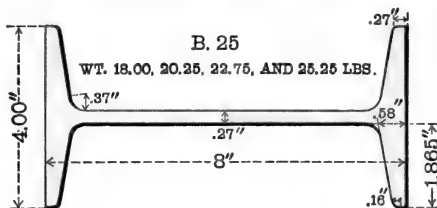


B. 21

WT. 15, 17.5 AND 20 LBS.

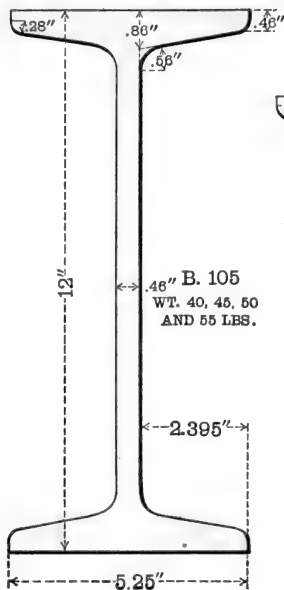


STANDARD BEAMS.

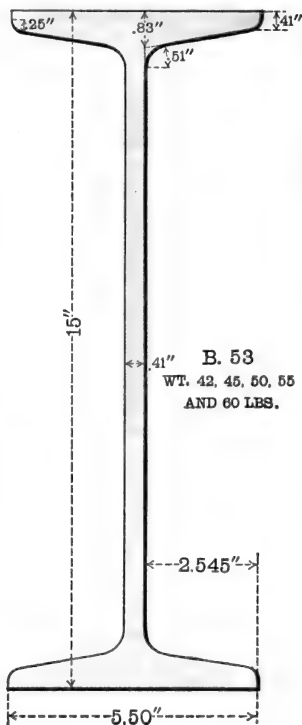


BEAMS.

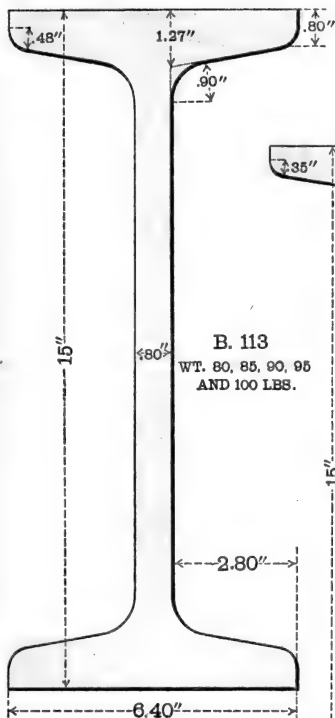
SPECIAL 12" BEAM.



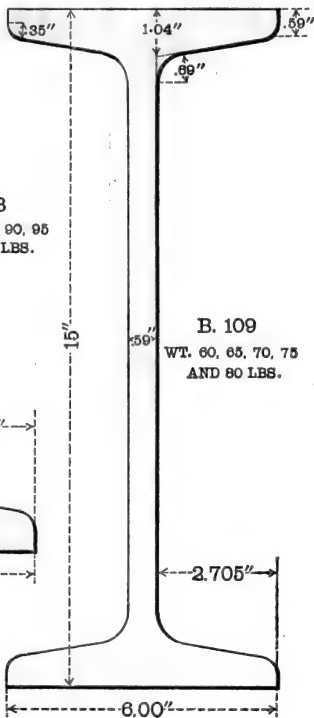
STANDARD 15" BEAM.



SPECIAL BEAMS.

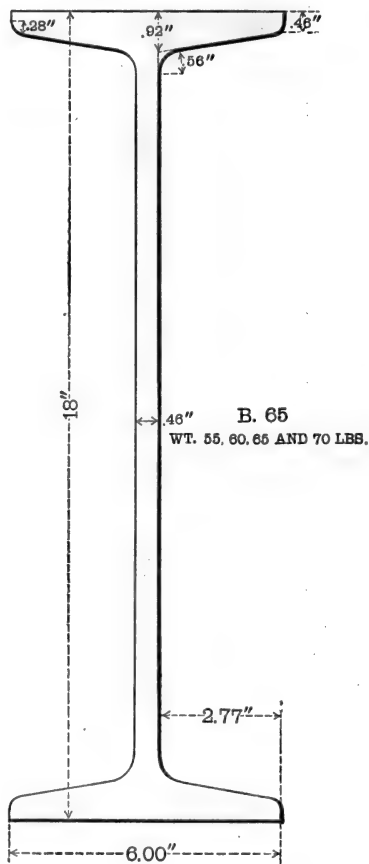


B. 113
WT. 80, 85, 90, 95
AND 100 LBS.

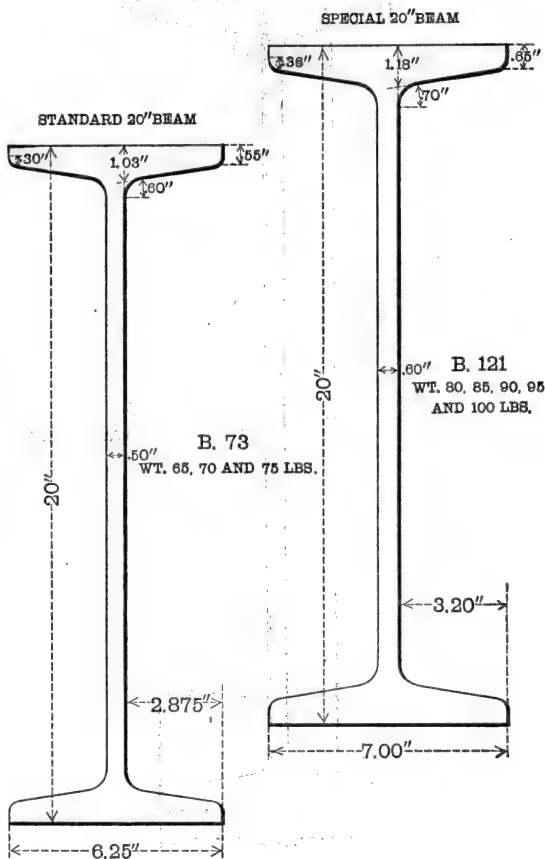


B. 109
WT. 60, 65, 70, 75
AND 80 LBS.

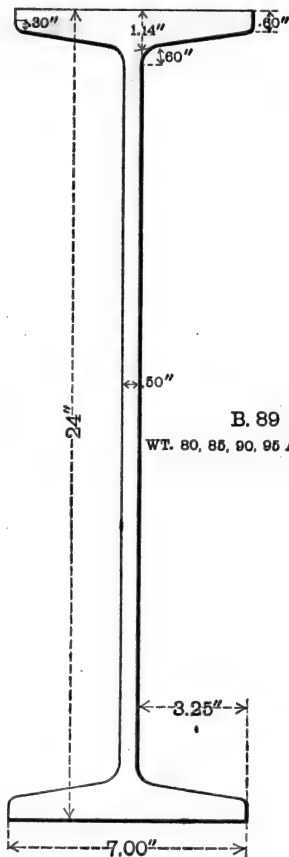
STANDARD BEAMS.



BEAMS.



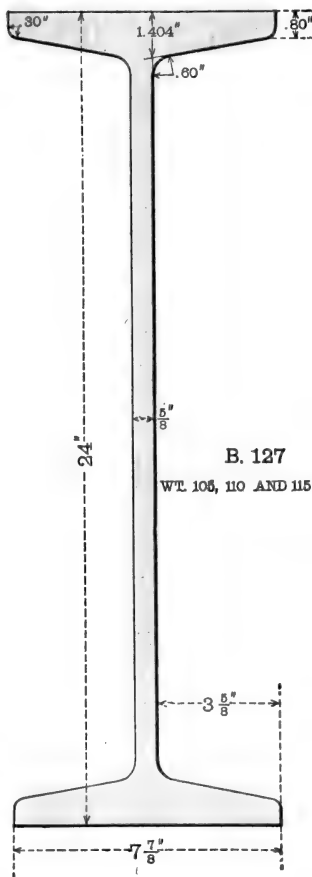
STANDARD BEAMS.



B. 89

WT. 80, 85, 90, 95 AND 100 LBS.

SPECIAL BEAMS.



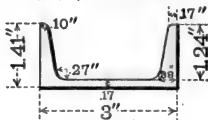
B. 127

WT. 106, 110 AND 115 LBS.

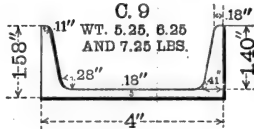
STANDARD CHANNELS.

C. 5

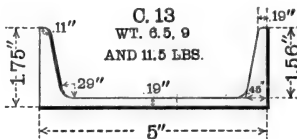
WT. 4, 5 AND 6 LBS.



C. 9

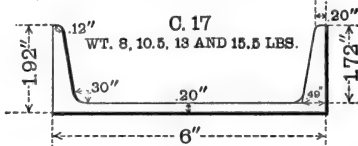
WT. 5.25, 6.25
AND 7.25 LBS.

C. 13

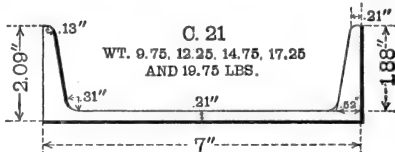
WT. 8.5, 9
AND 11.5 LBS.

C. 17

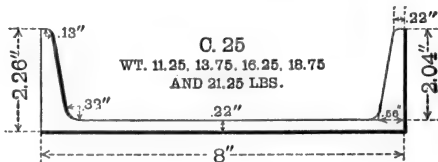
WT. 8, 10.5, 13 AND 15.5 LBS.



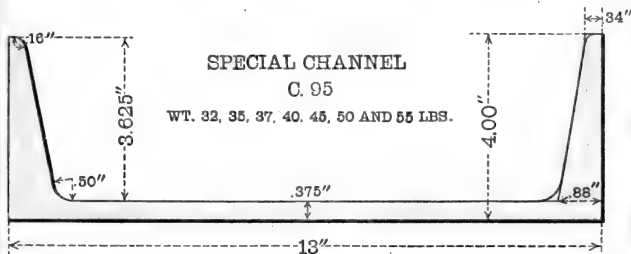
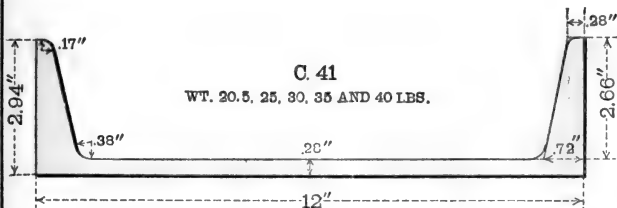
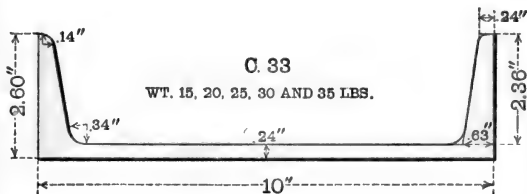
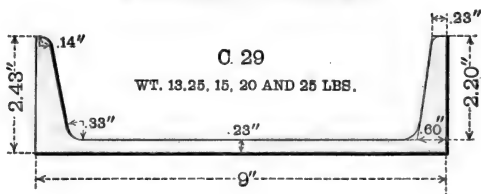
C. 21

WT. 9.75, 12.25, 14.75, 17.25
AND 19.75 LBS.

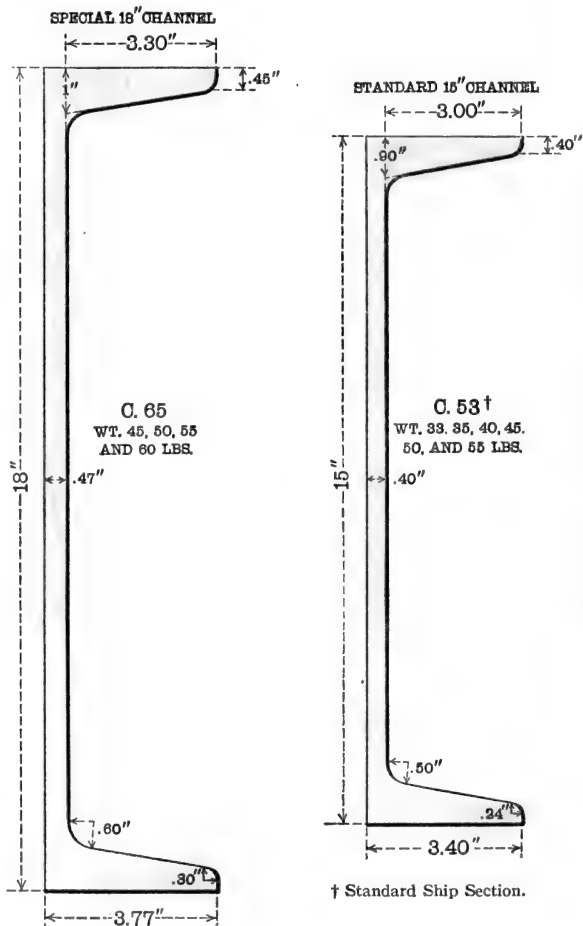
C. 25

WT. 11.25, 13.75, 16.25, 18.75
AND 21.25 LBS.

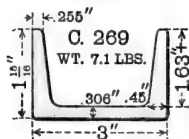
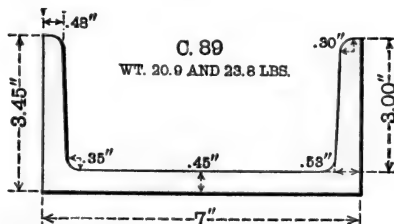
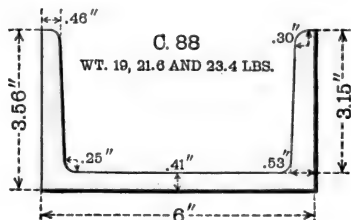
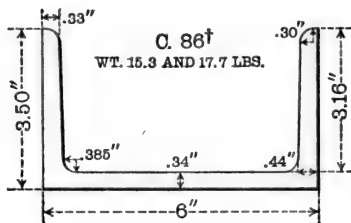
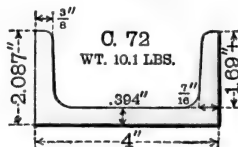
STANDARD CHANNELS.



CHANNELS.

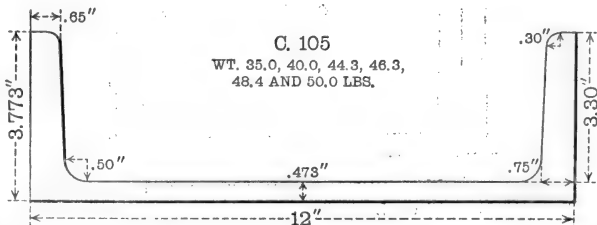
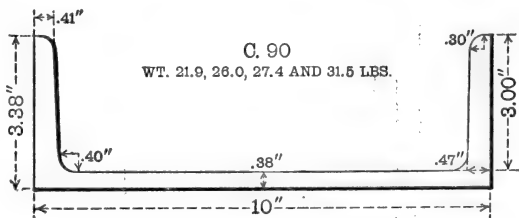
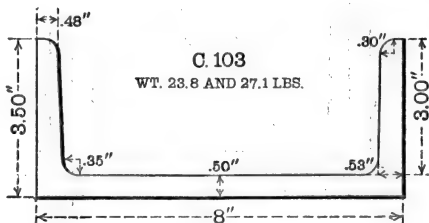
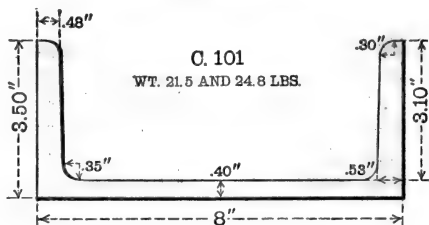


SPECIAL AND SHIP CHANNELS.

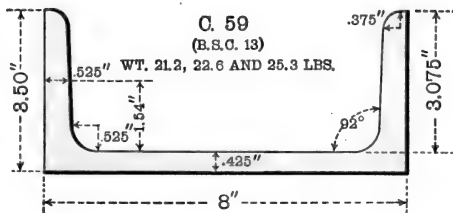
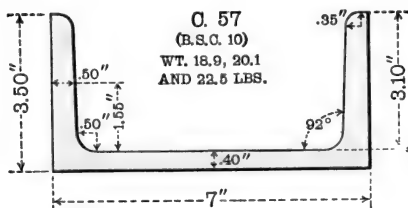
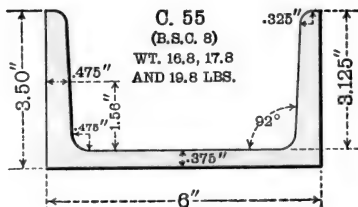
BRAKE BEAM
CHANNEL.CAR
CHANNEL.

† Standard Ship Channel.

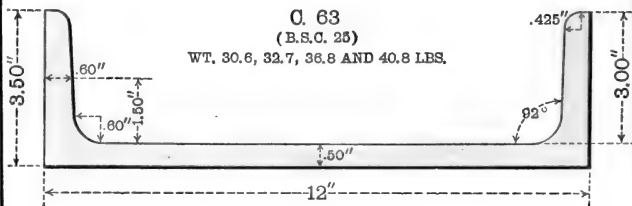
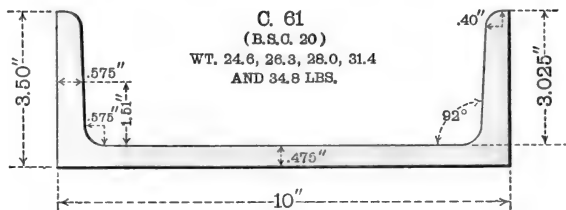
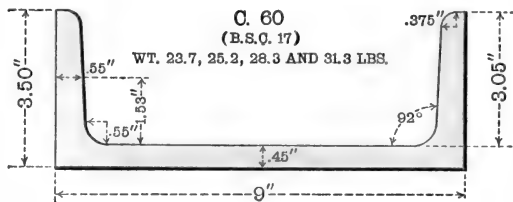
SHIP CHANNELS.



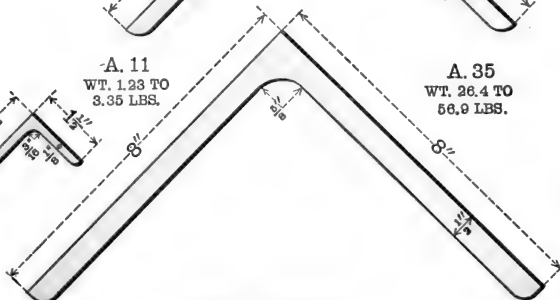
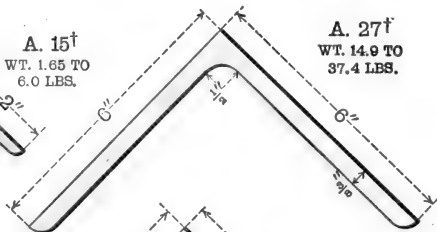
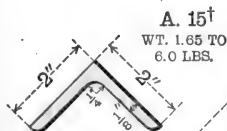
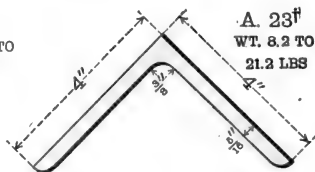
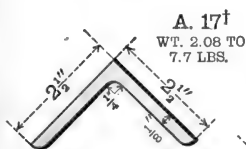
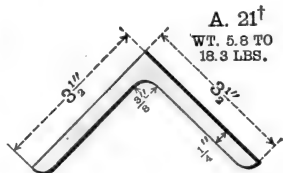
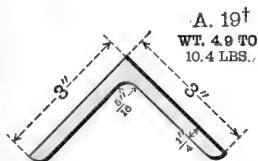
STANDARD SHIP CHANNELS.



STANDARD SHIP CHANNELS.

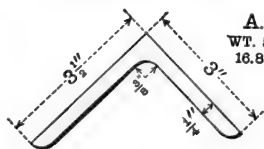


STANDARD ANGLES WITH EQUAL LEGS.

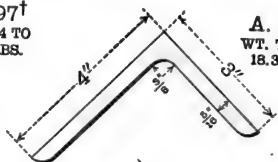


† Standard Ship Section.

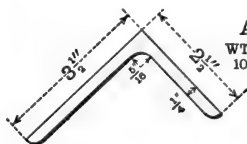
STANDARD ANGLES WITH UNEQUAL LEGS.



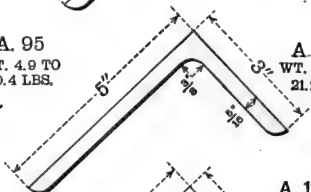
A. 97†
WT. 5.4 TO
16.8 LBS.



A. 99†
WT. 7.2 TO
18.3 LBS.



A. 95
WT. 4.9 TO
10.4 LBS.



A. 101†
WT. 8.2 TO
21.2 LBS.



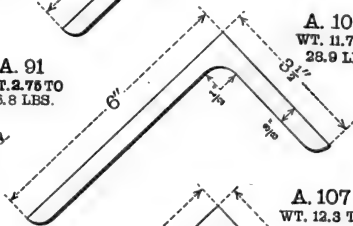
A. 93†
WT. 4.5 TO
9.5 LBS.



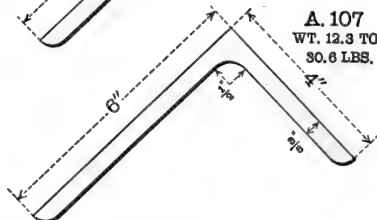
A. 103
WT. 8.7 TO
24.2 LBS.



A. 91
WT. 2.75 TO
6.8 LBS.



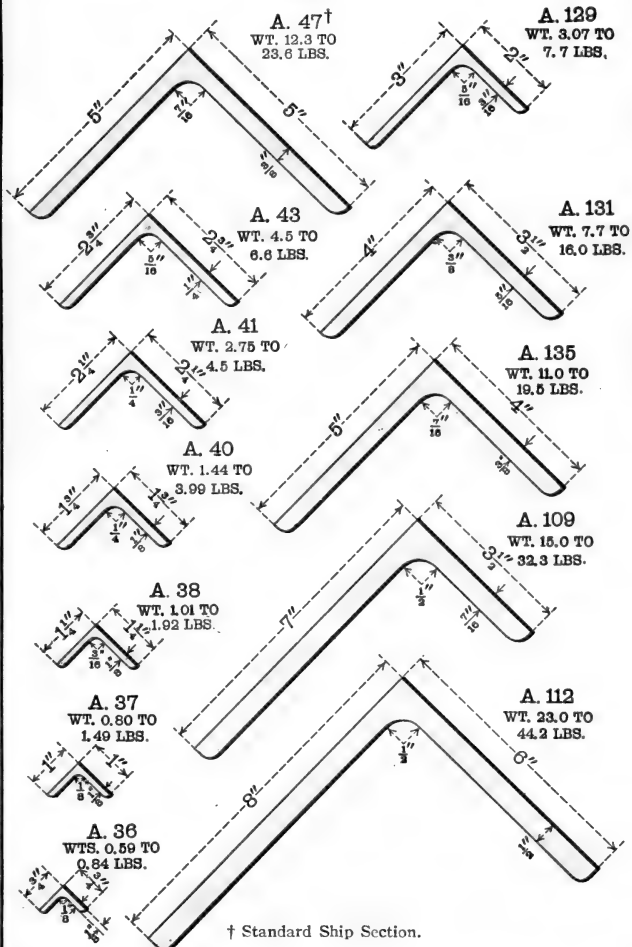
A. 105†
WT. 11.7 TO
28.9 LBS.



A. 107
WT. 12.3 TO
30.6 LBS.

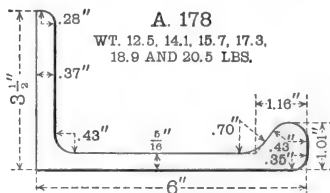
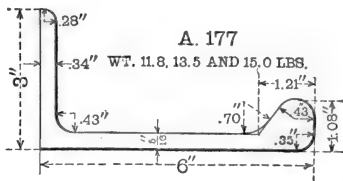
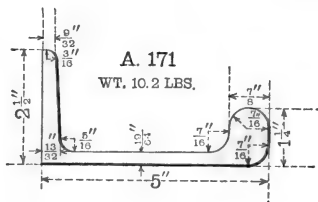
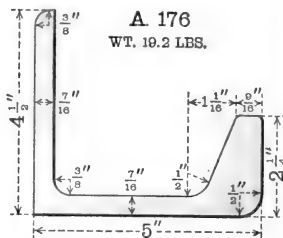
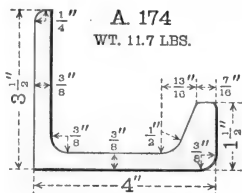
† Standard Ship Section.

SPECIAL ANGLES.

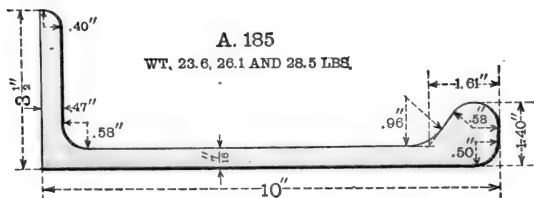
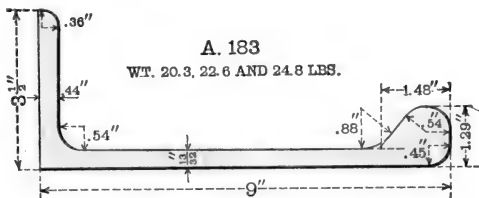
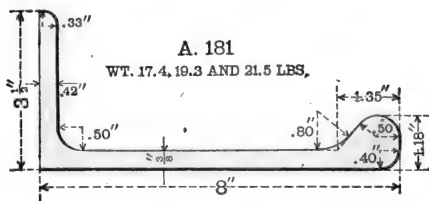
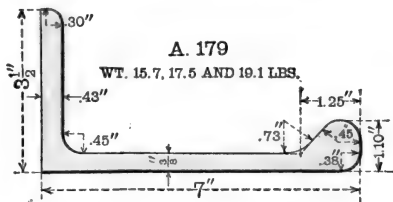


BULB ANGLES.

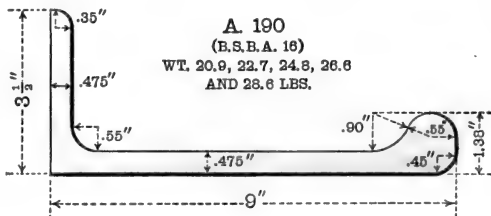
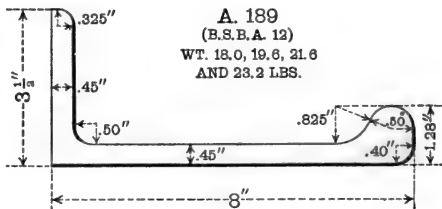
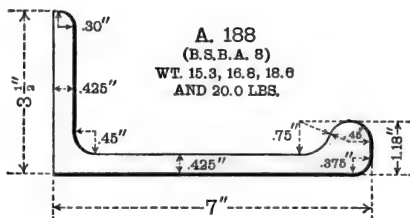
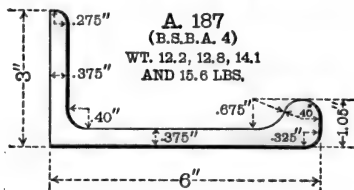
TOP GUARD ANGLES.



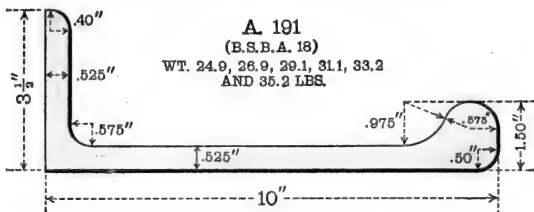
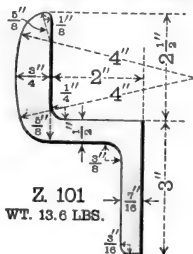
BULB ANGLES.



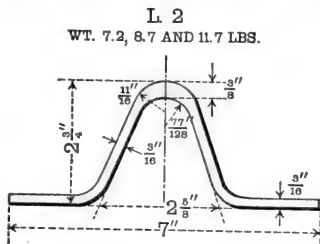
STANDARD BULB ANGLES.



STANDARD BULB ANGLES.

Z-BAR HATCH SECTION.
STANDARD SHIP SECTION.

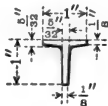
CAR SIDE STAKE SECTIONS.



T-BARS WITH EQUAL LEGS.

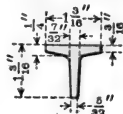
T. 5

WT. .89 LBS.



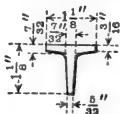
T. 183

WT. 1.51 LBS.



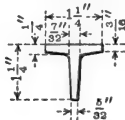
T. 181

WT. 1.37 LBS.



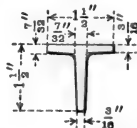
T. 187

WT. 1.60 LBS.



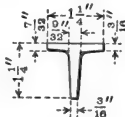
T. 191

WT. 1.94 LBS.



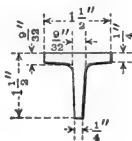
T. 188

WT. 1.70 LBS.



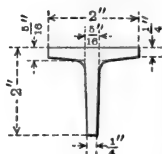
T. 193

WT. 2.47 LBS.



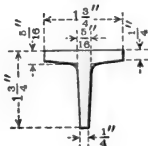
T. 37

WT. 3.56 LBS.



T. 194

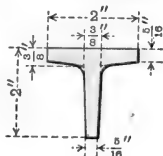
WT. 3.09 LBS.



T-BARS WITH EQUAL LEGS.

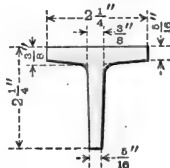
T. 39

WT. 4.3 LBS.



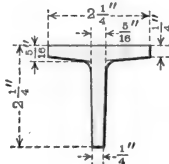
T. 42

WT. 4.9 LBS.



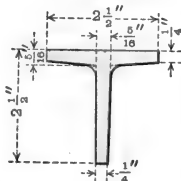
T. 41

WT. 4.1 LBS.



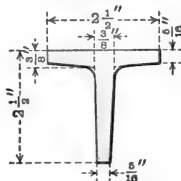
T. 47

WT. 4.6 LBS.



T. 49

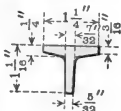
WT. 5.5 LBS.



T-BARS WITH UNEQUAL LEGS.

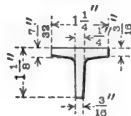
T. 16

WT. 1.48 LBS.



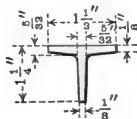
T. 18

WT. 1.56 LBS.



T. 20

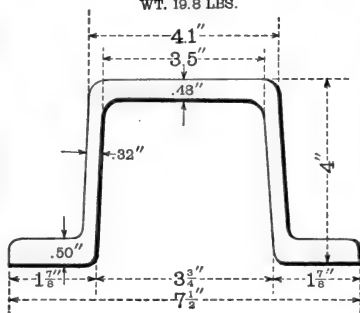
WT. 1.25 LBS.



DOOR-SPREADER.

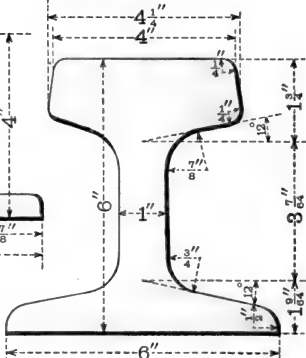
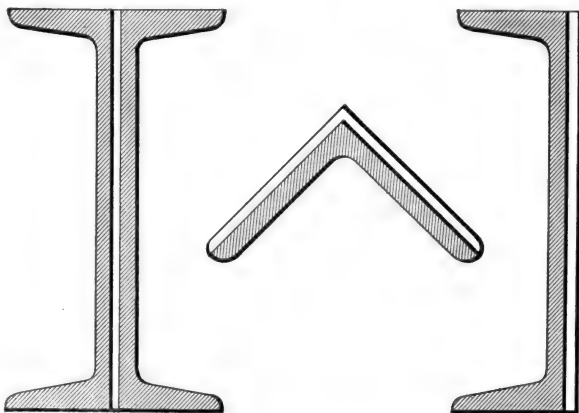
C. 250

WT. 19.8 LBS.

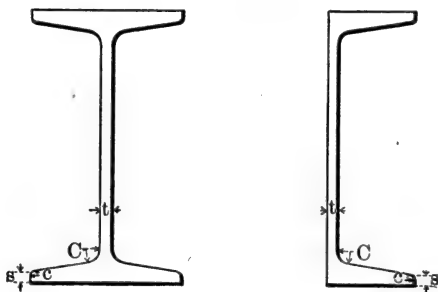
**CRANE RAIL.**

NQ. 539

WT. 50 LBS. (PER FOOT)

**METHOD OF INCREASING SECTIONAL AREA.**

STANDARD BEAMS AND CHANNELS.



The following data are common to all Standard I-Beams and Channels, with the exceptions stated:

$$c = \frac{6}{16} \text{ Minimum Web.}$$

$$C = \text{Minimum Web} + \frac{1}{16} \text{ inch.}$$

s = Minimum Thickness of Web = t Minimum for all Channels and Beams, except 20" I and 24" I.

For 20" Standard I, s = .55", t Minimum = .50".

For 24" Standard I, s = .60", t Minimum = .50".

The Slope of Flange of all Standard Beams and Channels is $16\frac{2}{3}\%$
 $= 9^\circ - 27' - 44'' = 2''$ per foot.

STANDARD BEAMS.

The following Formulas and Diagram relate to the Properties of I-Beams:

Weight per foot = $\text{Area} \times 3.4$.

Area = $td + 2s(b-t) + \frac{(b-t)^2}{12}$.

Section Modulus = $s = \frac{2I}{d}$.

Slope of Flange = $g = \frac{h-1}{b-t} = \frac{1}{6}$ for Standard Beams.

I = Moment of Inertia, Neutral Axis (1-1) parallel to flange.

$I = \frac{1}{12} [bd^3 - \frac{1}{8} (h^4 - 1^4)]$ or $\frac{1}{12} (h^4 - 1^4)$ for Standard Beams.

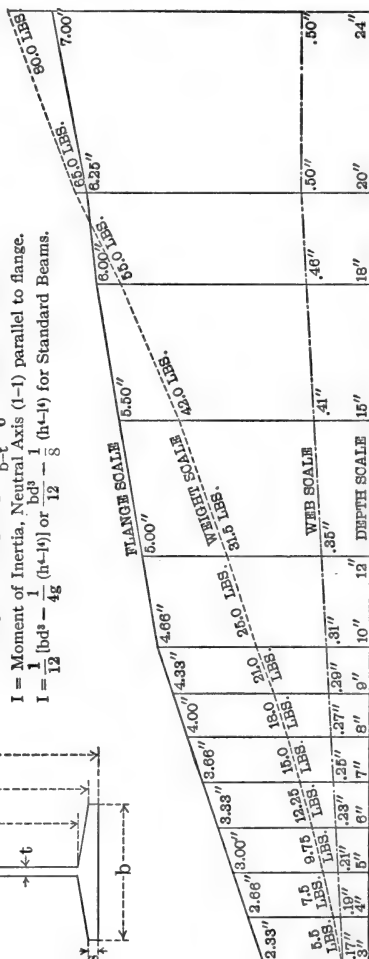
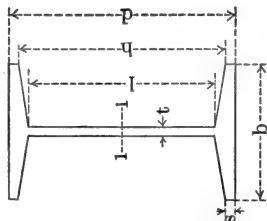


DIAGRAM FOR MINIMUM STANDARD BEAMS.

STANDARD CHANNELS

The following Formulas and Diagram relate to the Properties of Channels:

$$\text{Weight per foot} = \text{Area} \times 3.4.$$

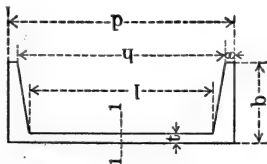
$$\text{Area} = td + 2s(b-t) + \frac{(b-t)^2}{6}.$$

$$\text{Section Modulus} = s = \frac{2I}{d}.$$

$$\text{Slope of Flange} = g = \frac{h-1}{2(b-t)}, \text{ or } \frac{1}{6} \text{ for Standard Channels.}$$

I = Moment of Inertia, Neutral Axis (1-1) parallel to flange.

$$I = \frac{1}{12} [bd^3 - \frac{1}{8g} (h^4 - 1^4)] \text{ or } \frac{bd^3}{12} - \frac{h^4 - 1^4}{16} \text{ for Standard Channels.}$$



| FLANGE SCALE | 1.41" | 1.68" | 1.75" | 1.92" | 2.09" | 2.26" | 2.43" | 2.60" | 2.84" | 3.40" |
|--------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| WEB SCALE | 17" | 18" | 6.5 | 8.0 | 9.75 | 11.25 | 12.25 | 15.0 | 20.5 | 34.0 |
| WEIGHT SCALE | 4.0 | 6.26 | 6.5 | 8.0 | 9.75 | 11.25 | 12.25 | 15.0 | 20.5 | 34.0 |
| DEPTH SCALE | 3" | 4" | 5" | 6" | 7" | 8" | 9" | 10" | 12" | 15" |

DIAGRAM FOR MINIMUM STANDARD CHANNELS.

PRESSED STEEL OR FLANGED CAR PARTS.

| | |
|----------------------------|--------------------------------|
| Truck Bolsters. | Drop Doors. |
| Side Sills. | Longitudinal Ridge Stiffeners. |
| Center Sills. | Cross Ridge Supports. |
| End Sills. | Cross Body Ties. |
| Draft Sills. | Diagonal Braces. |
| Draft Lugs. | Door Spreaders. |
| Sub-Side Sills. | Air Reservoir Supports. |
| Side Stakes. | Push Pole Pockets. |
| End Stakes. | Body Corner Caps. |
| Corner Stakes. | Door Hinge Butts. |
| Outside Hopper Plates. | Bolster Diaphragms. |
| Inside Hopper Plates. | Wheel Diaphragms. |
| Side Plates. | Cross Bearer Diaphragms. |
| End Plates. | Hopper Diaphragms. |
| Floor Plates. | Door Diaphragms. |
| Longitudinal Ridge Plates. | Center Diaphragms. |
| Cross-Ridge Plates. | Center Sill Diaphragms. |
| End-Plate Stiffeners. | Bolster Center Diaphragms. |
| Hopper Doors. | |

FORGINGS FOR CAR WORK.

| | |
|-------------------------------|--------------------------------|
| Air Cylinder Push Rod. | Chain Hook. |
| Air Reservoir Release Rod. | Chain Link. |
| Arch Bars. | Corner Bands |
| Bottom Follower Guide. | Column Bolt Nut Lock. |
| Bottom Side Bearing. | Coupler Yokes. |
| Bracket for Brake Shaft. | Coupling Links. |
| Brake Beam Hanger. | Coupling Pins. |
| Brake Beam Hanger Carrier. | Cylinder Lever Connecting Rod. |
| Brake Connection Rod Carrier. | Cylinder Lever Fulcrum. |
| Brake Levers. | Door Chain U-Bolt. |
| Brake Mast. | Door Hinge. |
| Brake Mast Yoke. | Door Hinge Pins. |
| Brake Pins. | Door Operating Lever. |
| Brake Rods with Clevises. | |
| Brake Step Bracket. | |

FORGINGS FOR CAR WORK (CONTINUED).

| | |
|------------------------------|-------------------------------|
| Door Safety Chain Support. | Lever Guides. |
| Door Shaft Pawl. | Live Truck Lever Guide. |
| Door Tumbling Link. | Main Follower Sprocket Wheel |
| Draft Cylinder Support. | Shaft. |
| Draw Bar Carrier. | Operating Shaft. |
| Draw Bar Liner. | Operating Shaft Cam. |
| Draw Bar Yoke. | Operating Shaft Cam Stops. |
| Door Clevises. | Operating Ratchet Pawl. |
| Door Tumbling Lever. | Operating Ratchet Pawl Guard. |
| End Sill Pipe Clamp. | Pipe Clamp. |
| Eye-Bolts. | Pipe Clamp and Support. |
| Floating Lever. | Pushrod Carrier. |
| Floating Lever Carrier. | Ratchet Wrench Dog. |
| Floating Lever Connecting | Roping Staple. |
| Rod. | Sheave and Link Pin. |
| Floating Lever Fulcrum. | Side Stake Pockets. |
| Grab Irons. | Sill Step Suspension Spring. |
| Hand Brake Lever Carrier. | Suspension Spring. |
| Hand Brake Lever Fulcrum. | Suspension Spring Hanger. |
| Hand Brake Lever Guide. | Tie Bars with Upset Ends or |
| Hand Brake Rod. | Plain. |
| Hand Brake Rod Guide. | Top Body Tie Angle. |
| Hand Brake Rod Stop. | Top Side Bearing. |
| Hand Brake Rod with Threaded | Truck and Body Center Plates. |
| Connection for Malleable | Truck Bolster Tie Bar. |
| Stop. | Truck Door Stop, Chain |
| Hook Bolts. | Clamp Hooks. |
| Inside Body Step. | Truck Levers. |
| Journal Bearing Wedges. | Truck Side Bearing. |
| King Bolt. | U-Bolt Clamp for Angle Valve. |
| King Pin Support. | Uncoupling Lever. |

A large variety of small forgings not listed above can be furnished to order.

STEEL INGOTS.

| Style of Mold (See Foot-note) | Mold Dimensions | | | Approximate Ingot Weight | Grade |
|-------------------------------------|-------------------------------------|-------------------------------------|-------------------|-----------------------------|----------------------------|
| | Bottom | Top | Height | | |
| | Inches | Inches | Ft.-Ins. | Pounds | |
| O,X. | 20 $\frac{1}{8}$ x 23 $\frac{3}{8}$ | 18 $\frac{1}{2}$ x 20 $\frac{1}{2}$ | 6-1 $\frac{1}{2}$ | 7300 | Open Hearth or Bessemer |
| O,F. | 21 x 21 | 19 x 19 | 6-3 | 7300 | |
| B,F. | 21 x 21 | 19 x 19 | 6-3 | 7100 | |
| I,F,S. | 21 x 21 | 25 x 25 | 6-0 | 8800 | |
| O,F. | 20 x 22 $\frac{1}{2}$ | 18 x 20 $\frac{1}{2}$ | 6-5 $\frac{1}{2}$ | 7300 | Open Hearth |
| I,F,S. | 16 $\frac{1}{2}$ x 20 $\frac{1}{4}$ | 20 $\frac{1}{2}$ x 23 $\frac{1}{2}$ | 6-2 | 7800 | " |
| *I,F,S. | 16 $\frac{1}{2}$ x 20 $\frac{1}{4}$ | 20 $\frac{1}{2}$ x 23 $\frac{1}{2}$ | 6-2 | 7900 | " |
| O,F. | 22 $\frac{3}{4}$ x 26 | 20 $\frac{3}{4}$ x 24 | 6-5 $\frac{1}{2}$ | 10400 | " |
| O,F. | 25 $\frac{1}{2}$ x 30 | 23 $\frac{1}{2}$ x 28 $\frac{1}{2}$ | 6-2 | 13500 | " |
| O,F. | 30 x 30 | 28 x 28 | 6-2 | 15500 | " |
| I,F,S. | 27 x 27 | 30 x 30 | 6-0 | 16300 | " |
| O,X. | 25 x 36 | 23 x 35 | 6-0 | 14000 | " |
| O,X. | 25 $\frac{1}{2}$ x 40 | 22 $\frac{1}{8}$ x 38 $\frac{1}{2}$ | 6-2 | 15500 | " |
| O,X. | 26 x 53 | 23 x 51 $\frac{1}{2}$ | 6-2 | 20500 | " |
| O,X. | 25 $\frac{1}{2}$ x 56 | 23 $\frac{3}{4}$ x 54 $\frac{1}{2}$ | 6-3 | 25500 | " |
| O,F. | 32 $\frac{1}{2}$ x 36 | 30 $\frac{1}{2}$ x 35 | 6-0 | 19500 | " |
| I,V. | 26 x 30 | 30 x 34 | 6-2 | 18600 | " |
| O,F. | 30 $\frac{1}{2}$ x 30 $\frac{1}{2}$ | 28 $\frac{1}{2}$ x 28 $\frac{1}{2}$ | 8-0 | 20400 | " |
| O,F. | 32 $\frac{1}{4}$ x 38 | 30 $\frac{1}{4}$ x 36 | 8-0 | 25000 | " |
| O,F,X. | 32 x 52 $\frac{1}{2}$ | 29 $\frac{1}{2}$ x 50 | 8-0 | 35000 | " |
| O,X. | 32 x 56 | 30 x 54 | 6-3 | 30000 | " |
| I,B,F,S. | 21 x 21 | 25 x 25 | 6-0 | 10200 | " |
| I,B,F,S. | 26 x 26 | 30 x 30 | 6-0 | 15700 | " |
| C,G. | 22 $\frac{1}{2}$ diam. | 20 diam. | 18-0 | 23800 | " |
| C,G. | 26 " | 23 $\frac{1}{2}$ " | 18-0 | 29100 | " |
| C,G. | 28 $\frac{1}{4}$ " | 26 " | 18-0 | 33800 | " |
| C,G. | 31 $\frac{1}{4}$ " | 29 " | 18-0 | 41800 | " |
| C,G. | 38 " | 34 " | 18-0 | 55000 | " |
| G,R. | 18 x 30 | 16 x 28 | 18-0 | 27500 | " |
| B,F. | 22 x 38 | 20 x 36 | 18-0 | 36500 | " |
| K,G,S. | 16 $\frac{3}{8}$ { short diam. | 19 { short diam. | 8-4 | 8300 | " |

B = Bottle-Necked; C = Circular; F = Ingot Sides Flat; G = Corrugated; I = Inverted; K = Octagonal; O = Open Top; R = Rectangular or Slab Style; V = Ingot Sides Concave; X = Ingot Sides Rounded or Convex; S = With Sinkhead; * = Irregular Taper.

Sizes of Hot and Cold Ingots will vary slightly from above dimensions.

STEEL SQUARES.All sizes from $\frac{3}{16}$ " to $2\frac{1}{8}$ " increasing by $\frac{1}{64}$ "All sizes from $2\frac{1}{8}$ " to $3\frac{3}{8}$ " increasing by $\frac{1}{32}$ "All sizes from $3\frac{1}{2}$ " to $5\frac{1}{2}$ " increasing by $\frac{1}{8}$ "Planished squares from $\frac{7}{32}$ " to $2\frac{1}{2}$ "**STEEL HAND ROUNDS.**All sizes from $1\frac{1}{8}$ " to $2\frac{7}{8}$ " increasing by $\frac{1}{64}$ "All sizes from $2\frac{7}{8}$ " to $3\frac{3}{16}$ " increasing by $\frac{1}{16}$ "All sizes from $3\frac{1}{4}$ " to $7\frac{1}{4}$ " increasing by $\frac{1}{8}$ "All sizes from $7\frac{1}{4}$ " to 8" increasing by $\frac{1}{4}$ "**STEEL GUIDE ROUNDS.**All sizes from $\frac{1}{4}$ " to $2\frac{5}{16}$ " increasing by $\frac{1}{64}$ "**LARGE STEEL ROUNDS.**

| DIAMETER Inches | MINIMUM LENGTHS Sheared with Rough Ends. Inches | MAXIMUM LENGTH Feet |
|--------------------|---|------------------------|
| 11 | 6 to 36 | 25 |
| 15 | 6 to 36 | $10\frac{1}{2}$ |
| 16 | 6 to 36 | $9\frac{1}{2}$ |

Other lengths shorter than maximum can only be furnished by special arrangement.

REGULAR FLATS.

| WIDTH Inches | THICKNESS. Inches | WIDTH Inches | THICKNESS Inches |
|----------------------------------|----------------------------------|---------------------|-----------------------------------|
| $\frac{1}{4}$ to 1 | $\frac{3}{16}$ to $\frac{9}{16}$ | $2\frac{1}{4}$ to 3 | $\frac{3}{16}$ to $2\frac{1}{4}$ |
| 1 to $1\frac{1}{8}$ | $\frac{3}{16}$ to $\frac{3}{4}$ | 3 to 4 | $\frac{3}{16}$ to $2\frac{3}{4}$ |
| $1\frac{1}{8}$ to $1\frac{1}{2}$ | $\frac{1}{8}$ to $\frac{7}{8}$ | 4 to $4\frac{1}{2}$ | $\frac{3}{16}$ to $1\frac{5}{16}$ |
| $1\frac{1}{2}$ to $2\frac{1}{4}$ | $\frac{3}{16}$ to $1\frac{1}{4}$ | $4\frac{1}{2}$ to 6 | $\frac{3}{16}$ to $2\frac{3}{16}$ |

Variation for intermediate widths less than 1" = $\frac{1}{64}$ ".

Variation for intermediate widths over 1" = $\frac{1}{16}$ ", or less by special arrangement.

THIN FLATS OR LIGHT BANDS.

| WIDTH | THICKNESS |
|---|--|
| $\frac{3}{8}$ " to $\frac{1}{2}$ " increasing by $\frac{1}{16}$ " | $\frac{1}{8}$ " (.125") to $\frac{5}{32}$ " (.156") |
| $\frac{1}{2}$ " to 12" increasing by $\frac{1}{16}$ " | $\frac{1}{16}$ " (.063") to $\frac{3}{32}$ " (.156") |

MAXIMUM LENGTHS OF

| Thickness in Inches. | WIDTH IN INCHES. | | | | | | | | | | | | | | | | | | | | | |
|----------------------------|------------------|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|
| | 4½ | 5 | 5½ | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | |
| LENGTH IN FEET. | | | | | | | | | | | | | | | | | | | | | | |
| 2 | | | | | 10 | 30 | 30 | 30 | 30 | 30 | | | | | | | | | | | | |
| 2½ | | | | 10 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | |
| 3 | | | | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | |
| 3½ | | | | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | |
| 4 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | |
| 4½ | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | |
| 5 | | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | |
| 5½ | | | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | |
| 6 | | | | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | |
| 7 | | | | | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 28 | |
| 8 | | | | | | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 28 | 27 | 26 | 25 |
| 9 | | | | | | | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 25 | 24 | 23 | 22 | |
| 10 | | | | | | | | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 23 | 21 | 20 | 20 | |
| 11 | | | | | | | | | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 29 | 28 | 20 | 19 | 19 | 18 |
| 12 | | | | | | | | | | 30 | 30 | 30 | 30 | 30 | 30 | 28 | 27 | 25 | 19 | 18 | 17 | 16 |
| 13 | | | | | | | | | | | 30 | 30 | 30 | 30 | 28 | 26 | 25 | 23 | 17 | 16 | 16 | 15 |
| 14 | | | | | | | | | | | | 30 | 28 | 26 | 24 | 23 | 22 | 16 | 15 | 14 | 14 | |
| 15 | | | | | | | | | | | | | 26 | 24 | 23 | 21 | 20 | 15 | 14 | 13 | 13 | |
| 16 | | | | | | | | | | | | | | 22 | 21 | 20 | 19 | 14 | 13 | 13 | 12 | |
| 17 | | | | | | | | | | | | | | | 20 | 19 | 18 | 15 | 13 | 12 | 12 | |
| 18 | | | | | | | | | | | | | | | | 18 | 17 | 12 | 12 | 11 | 11 | |
| 19 | | | | | | | | | | | | | | | | | 16 | 12 | 12 | 11 | 11 | |
| 20 | | | | | | | | | | | | | | | | | | 11 | 10 | 10 | 10 | |
| 21 | | | | | | | | | | | | | | | | | | | 10 | 10 | 9 | |
| 22 | | | | | | | | | | | | | | | | | | | | 9 | 9 | |

Minimum Length for sizes included by heavy lines = 1½ feet.

Minimum Length other sizes = 3 feet.

Under certain conditions other sizes than those listed

BILLETS, BLOOMS AND SLABS.

| WIDTH IN INCHES. | | | | | | | | | | | | | | | | | | | | | Thickness in Inches. |
|------------------|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----------------------------|
| 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 45 | 46 | 47 | 48 | 49 | 50 | 51 | |
| LENGTH IN FEET. | | | | | | | | | | | | | | | | | | | | | |
| 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 2 |
| 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 29 | 29 | 30 | 29 | 28 | 27 | 30 | 30 | 29 | 28 | 27 | 27 | 2½ |
| 30 | 30 | 30 | 30 | 30 | 28 | 27 | 27 | 26 | 25 | 30 | 25 | 24 | 24 | 30 | 30 | 25 | 25 | 24 | 24 | 28 | 3 |
| 30 | 30 | 30 | 30 | 30 | 25 | 24 | 24 | 23 | 22 | 30 | 22 | 22 | 21 | 30 | 30 | 22 | 22 | 21 | 21 | 25 | 3½ |
| 30 | 30 | 30 | 30 | 30 | 23 | 22 | 21 | 20 | 20 | 30 | 20 | 19 | 19 | 30 | 30 | 20 | 19 | 19 | 19 | 22 | 4 |
| 30 | 30 | 30 | 30 | 29 | 21 | 20 | 19 | 19 | 18 | 30 | 18 | 18 | 17 | 28 | 28 | 18 | 18 | 17 | 17 | 20 | 4½ |
| 30 | 30 | 29 | 28 | 27 | 19 | 18 | 18 | 17 | 16 | 27 | 17 | 16 | 16 | 26 | 25 | 16 | 16 | 16 | 16 | 18 | 5 |
| 27 | 26 | 25 | 24 | 23 | 16 | 15 | 15 | 14 | 14 | 23 | 14 | 14 | 13 | 22 | 21 | 14 | 14 | 13 | 13 | 16 | 5½ |
| 24 | 23 | 22 | 21 | 20 | 14 | 13 | 13 | 13 | 12 | 20 | 12 | 12 | 12 | 19 | 19 | 12 | 12 | 12 | 12 | 14 | 6 |
| 21 | 20 | 19 | 19 | 18 | 12 | 12 | 11 | 11 | 11 | 18 | 11 | 11 | 10 | 17 | 17 | 11 | 11 | 10 | 10 | 12 | 7 |
| 19 | 18 | 17 | 17 | 16 | 11 | 11 | 10 | 10 | 10 | 16 | 10 | 9 | 9 | 15 | 15 | 10 | 10 | 9 | 9 | 11 | 8 |
| 17 | 16 | 16 | 15 | 15 | 10 | 10 | 9 | 9 | 9 | 14 | 9 | 9 | 8 | 14 | 14 | 9 | 9 | 8 | 8 | 10 | 9 |
| 15 | 15 | 14 | 14 | 13 | 9 | 9 | 9 | 8 | 8 | 13 | 8 | 8 | 8 | 13 | 12 | 8 | 8 | 8 | 8 | 9 | 10 |
| 14 | 13 | 13 | 13 | 12 | 8 | 8 | 8 | 8 | 7 | 12 | 7 | 7 | 7 | 12 | 11 | 7 | 7 | 7 | 7 | 8 | 11 |
| 13 | 13 | 12 | 12 | 11 | 8 | 8 | 7 | 7 | 7 | 11 | 7 | 7 | 6 | 11 | 11 | 7 | 7 | 6 | 6 | 8 | 12 |
| 12 | 12 | 11 | 11 | 11 | 7 | 7 | 7 | 7 | 6 | 11 | 6 | 6 | 6 | 10 | 10 | 6 | 6 | 6 | 6 | 7 | 13 |
| 12 | 11 | 11 | 10 | 10 | 7 | 7 | 6 | 6 | 6 | 10 | 6 | 6 | 6 | 10 | 9 | 6 | 6 | 6 | 6 | 7 | 14 |
| 11 | 11 | 10 | 9 | 9 | 7 | 6 | 6 | 6 | 6 | 9 | 6 | 6 | 5 | 9 | 9 | 6 | 6 | 5 | 5 | 6 | 15 |
| 10 | 10 | 9 | 9 | 9 | 6 | 6 | 6 | 6 | 5 | 9 | 5 | 5 | 5 | 9 | 8 | 5 | 5 | 5 | 5 | 6 | 16 |
| 10 | 10 | 9 | 8 | 8 | | | | | | | | | | | | | | | | 19 | |
| 9 | 9 | 8 | 8 | 8 | | | | | | | | | | | | | | | | 20 | |
| 9 | 9 | 8 | 8 | 8 | | | | | | | | | | | | | | | | 21 | |
| 8 | 8 | 8 | 7 | 7 | | | | | | | | | | | | | | | | 22 | |

Minimum Length = 3 feet.

herein might be furnished by special arrangement.

SQUARE BILLETS. WITH ROUND CORNERS.

| Size. | Maximum Length. | Minimum Length. |
|------------------------------------|-----------------|-----------------|
| Inches. | Feet. | Feet. |
| $1\frac{3}{4} \times 1\frac{3}{4}$ | 30 | 24 |
| 2 x 2 | 30 | 24 |
| $2\frac{1}{4} \times 2\frac{1}{4}$ | 30 | 24 |
| 3 x 3 | 30 | 24 |
| 4 x 4 | 16 | $11\frac{1}{2}$ |
| $4\frac{1}{2} \times 4\frac{1}{2}$ | 16 | $11\frac{1}{2}$ |
| 5 x 5 | 16 | $11\frac{1}{2}$ |
| $5\frac{1}{2} \times 5\frac{1}{2}$ | 16 | $11\frac{1}{2}$ |
| 6 x 6 | 16 | $11\frac{1}{2}$ |

SHEET AND TIN BARS.

| Width. | Weight per Foot Length. | Maximum Length. | Minimum Length. |
|---------|----------------------------|--------------------|--------------------|
| Inches. | Pounds. | Feet. | Feet. |
| 8 | 8 | 30 | 25 |
| 8 | 9 | 30 | 25 |
| 8 | 10 | 30 | 25 |
| 8 | 11 | 30 | $20\frac{1}{2}$ |
| 8 | 12 | 30 | $20\frac{1}{2}$ |
| 8 | 13 | 30 | $20\frac{1}{2}$ |
| 8 | 14 | 30 | $16\frac{1}{2}$ |
| 8 | 15 | 30 | $16\frac{1}{2}$ |
| 8 | 16 | 30 | $16\frac{1}{2}$ |
| 8 | 17 | 30 | $16\frac{1}{2}$ |
| 8 | 18 | 30 | 13 |
| 8 | 19 | 30 | 13 |
| 8 | 20 | 30 | 13 |
| 8 | 21 | 30 | 13 |
| 8 | 22 | 30 | 13 |
| 8 | 23 | 30 | 13 |
| 8 | 24 | 30 | $9\frac{1}{2}$ |
| 8 | 25 | 30 | $9\frac{1}{2}$ |

EDGED PLATES.

| Width in Inches. | THICKNESS IN INCHES. | | | | | | | | | | | | | | |
|------------------------|-------------------------|---------------|----------------|---------------|----------------|---------------|----------------|---------------|---------------|---------------|----|----------------|----------------|----------------|----|
| | $\frac{3}{16}$ | $\frac{1}{4}$ | $\frac{5}{16}$ | $\frac{3}{8}$ | $\frac{7}{16}$ | $\frac{1}{2}$ | $\frac{9}{16}$ | $\frac{5}{8}$ | $\frac{3}{4}$ | $\frac{7}{8}$ | 1 | $1\frac{1}{4}$ | $1\frac{1}{2}$ | $1\frac{3}{4}$ | 2 |
| | MAXIMUM LENGTH IN FEET. | | | | | | | | | | | | | | |
| $6\frac{1}{8}$ -25 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 68 | 56 | 48 | 42 |
| 26-27 | 60 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 68 | 56 | 48 | 42 |
| 28 | 60 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 67 | 56 | 48 | 42 |
| 29 | 60 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 64 | 54 | 46 | 40 |
| 30 | 60 | 60 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 78 | 62 | 52 | 44 | 39 |
| 31 | ... | 60 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 75 | 60 | 50 | 43 | 37 |
| 32 | ... | 60 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 84 | 73 | 58 | 49 | 42 | 36 |
| 33 | ... | 60 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 81 | 71 | 57 | 47 | 40 | 35 |
| 34 | ... | 60 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 79 | 69 | 55 | 46 | 39 | 34 |
| 35 | ... | 60 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 76 | 67 | 53 | 44 | 38 | 33 |
| 36 | ... | 60 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 74 | 65 | 52 | 43 | 37 | 32 |

THIN SHEARED PLATES.

[illegible]

SHEARED PLATES.

| Width in Inches. | THICKNESS IN INCHES. | | | | | | | | |
|-------------------------------|--------------------------|---------------|----------------|---------------|----------------|---------------|----------------|---------------|-----------------|
| | $\frac{3}{16}$ | $\frac{1}{4}$ | $\frac{5}{16}$ | $\frac{3}{8}$ | $\frac{7}{16}$ | $\frac{1}{2}$ | $\frac{9}{16}$ | $\frac{5}{8}$ | $\frac{11}{16}$ |
| | MAXIMUM LENGTH IN INCHES | | | | | | | | |
| 24 | 400 | 525 | 575 | 600 | 600 | 600 | 600 | 600 | |
| 25-30 | 375 | 525 | 500 | 600 | 600 | 625 | 625 | 625 | |
| 31-36 | 375 | 475 | 525 | 550 | 550 | 575 | 575 | 575 | 575 |
| 37-42 | 450 | 525 | 550 | 575 | 610 | 600 | 600 | 600 | 575 |
| 43-48 | 450 | 525 | 575 | 600 | 600 | 600 | 600 | 600 | 600 |
| 49-54 | 450 | 525 | 550 | 600 | 600 | 625 | 625 | 625 | 600 |
| 55-60 | 400 | 525 | 550 | 600 | 600 | 625 | 625 | 625 | 600 |
| 61-66 | 350 | 475 | 500 | 575 | 575 | 600 | 600 | 600 | 600 |
| 67-72 | 325 | 450 | 500 | 540 | 550 | 575 | 575 | 575 | 575 |
| 73-78 | | 425 | 475 | 440 | 540 | 540 | 540 | 540 | 540 |
| 79-84 | | 400 | 475 | 440 | 540 | 540 | 540 | 540 | 540 |
| 85-90 | | 350 | 375 | 400 | 450 | 450 | 450 | 450 | 450 |
| 91-96 | | 300 | 325 | 350 | 400 | 400 | 400 | 400 | 400 |
| 97-102 | | 275 | 300 | 325 | 375 | 375 | 375 | 375 | 375 |
| 103-108 | | 250 | 275 | 300 | 350 | 350 | 350 | 350 | 350 |
| 109-114 | | 175 | 200 | 225 | 275 | 275 | 275 | 300 | 300 |
| 115-120 | | | 175 | 200 | 250 | 250 | 250 | 250 | 250 |
| 121-126 | | | | 180 | 180 | 180 | 180 | 180 | 180 |
| Maximum Diam. of Heads. | 72 | 115 | 124 | 127 | 127 | 127 | 127 | 127 | 127 |

Minimum Diameter of Heads (Circular Plates) = 30 inches.

SHEARED PLATES.

| THICKNESS IN INCHES. | | | | | | | | | | Width in Inches. |
|---------------------------|-----------------|---------------|-----------------|-----|----------------|----------------|----------------|----------------|-----|-------------------------------|
| $\frac{3}{4}$ | $\frac{13}{16}$ | $\frac{7}{8}$ | $\frac{15}{16}$ | 1 | $1\frac{1}{8}$ | $1\frac{1}{4}$ | $1\frac{1}{2}$ | $1\frac{3}{4}$ | 2 | |
| MAXIMUM LENGTH IN INCHES. | | | | | | | | | | |
| | | | | | | | | | | 24 |
| | | | | | | | | | | 25- 30 |
| 550 | 525 | 500 | 475 | 475 | 450 | 425 | 400 | 375 | 350 | 31- 36 |
| 575 | 525 | 500 | 500 | 500 | 475 | 425 | 400 | 375 | 350 | 37- 42 |
| 575 | 550 | 550 | 525 | 525 | 500 | 450 | 400 | 375 | 350 | 43- 48 |
| 575 | 550 | 550 | 525 | 525 | 500 | 450 | 400 | 375 | 350 | 49- 54 |
| 575 | 550 | 550 | 525 | 525 | 475 | 425 | 400 | 375 | 325 | 55- 60 |
| 575 | 550 | 550 | 525 | 525 | 475 | 425 | 375 | 350 | 325 | 61- 66 |
| 575 | 550 | 525 | 500 | 500 | 475 | 425 | 375 | 350 | 300 | 67- 72 |
| 525 | 500 | 475 | 450 | 450 | 425 | 375 | 325 | 300 | 280 | 73- 78 |
| 500 | 450 | 450 | 425 | 425 | 375 | 350 | 325 | 300 | 280 | 79- 84 |
| 425 | 400 | 400 | 375 | 375 | 350 | 325 | 280 | 270 | 260 | 85- 90 |
| 400 | 375 | 375 | 350 | 325 | 300 | 275 | 260 | 260 | 250 | 91- 96 |
| 375 | 350 | 350 | 325 | 300 | 275 | 250 | 250 | 240 | 240 | 97-102 |
| 350 | 325 | 325 | 300 | 275 | 250 | 250 | 180 | 175 | 160 | 103-108 |
| 300 | 275 | 275 | 250 | 250 | 225 | 200 | 175 | 160 | 150 | 109-114 |
| 275 | 250 | 250 | 225 | 225 | 200 | 200 | 175 | 160 | 150 | 115-120 |
| 180 | 200 | 200 | 175 | 175 | 160 | 160 | 150 | 144 | 144 | 121-126 |
| 127 | 126 | 126 | 126 | 126 | 126 | 125 | 125 | 125 | 125 | Maximum Diam. of Heads. |

Larger sizes up to 4 inch thickness, finished weight not exceeding 12,000 pounds, will be considered.

WEIGHTS AND DIMENSIONS OF STANDARD I-BEAMS.

| Section Number. | Depth of Beam. | Weight per Foot. | Area of Section. | Thickness of Web. | Width of Flange. | Page Number of Section. |
|--------------------|-------------------|---------------------|---------------------|----------------------|---------------------|-------------------------------|
| | Inches. | Pounds. | Sq. In. | Inch. | Inches. | |
| B 5 | 3 | 5.5 | 1.63 | .17 | 2.33 | 2 |
| " | " | 6.5 | 1.91 | .26 | 2.42 | " |
| " | " | 7.5 | 2.21 | .36 | 2.52 | " |
| B 9 | 4 | 7.5 | 2.21 | .19 | 2.66 | 2 |
| " | " | 8.5 | 2.50 | .26 | 2.73 | " |
| " | " | 9.5 | 2.79 | .34 | 2.81 | " |
| " | " | 10.5 | 3.09 | .41 | 2.88 | " |
| B 13 | 5 | 9.75 | 2.87 | .21 | 3.00 | 2 |
| " | " | 12.25 | 3.60 | .36 | 3.15 | " |
| " | " | 14.75 | 4.34 | .50 | 3.29 | " |
| B 17 | 6 | 12.25 | 3.61 | .23 | 3.33 | 2 |
| " | " | 14.75 | 4.34 | .35 | 3.45 | " |
| " | " | 17.25 | 5.07 | .47 | 3.57 | " |
| B 21 | 7 | 15.0 | 4.42 | .25 | 3.66 | 2 |
| " | " | 17.5 | 5.15 | .35 | 3.76 | " |
| " | " | 20.0 | 5.88 | .46 | 3.87 | " |
| B 25 | 8 | 18.0 | 5.33 | .27 | 4.00 | 3 |
| " | " | 20.25 | 5.96 | .35 | 4.08 | " |
| " | " | 22.75 | 6.69 | .44 | 4.17 | " |
| " | " | 25.25 | 7.43 | .53 | 4.26 | " |
| B 29 | 9 | 21.0 | 6.31 | .29 | 4.33 | 3 |
| " | " | 25.0 | 7.35 | .41 | 4.45 | " |
| " | " | 30.0 | 8.82 | .57 | 4.61 | " |
| " | " | 35.0 | 10.29 | .73 | 4.77 | " |
| B 33 | 10 | 25.0 | 7.37 | .31 | 4.66 | 3 |
| " | " | 30.0 | 8.82 | .45 | 4.80 | " |
| " | " | 35.0 | 10.29 | .60 | 4.95 | " |
| " | " | 40.0 | 11.76 | .75 | 5.10 | " |
| B 41 | 12 | 31.5 | 9.26 | .35 | 5.00 | 3 |
| " | " | 35.0 | 10.29 | .44 | 5.09 | " |
| " | " | 40.0 | 11.76 | .56 | 5.21 | " |
| B 53 | 15 | 42.0 | 12.48 | .41 | 5.50 | 4 |
| " | " | 45.0 | 13.24 | .46 | 5.55 | " |
| " | " | 50.0 | 14.71 | .56 | 5.65 | " |
| " | " | 55.0 | 16.18 | .66 | 5.75 | " |
| " | " | 60.0 | 17.65 | .75 | 5.84 | " |

Orders and inquiries concerning 12 in. 40 lb., 15 in. 60 lb., and 15 in. 80 lb. I-Beams should also specify by Section Number.

WEIGHTS AND DIMENSIONS OF STANDARD I-BEAMS.

| Section Number. | Depth of Beam. | Weight per Foot. | Area of Section. | Thickness of Web. | Width of Flange. | Page Number of Section. |
|-----------------|----------------|------------------|------------------|-------------------|------------------|-------------------------|
| | Inches. | Pounds. | Sq. In. | Inch. | Inches. | |
| B 65 | 18 | 55.0 | 15.93 | .46 | 6.00 | 6 |
| " | " | 60.0 | 17.65 | .56 | 6.10 | " |
| " | " | 65.0 | 19.12 | .64 | 6.18 | " |
| " | " | 70.0 | 20.59 | .72 | 6.26 | " |
| B 73 | 20 | 65.0 | 19.08 | .50 | 6.25 | 7 |
| " | " | 70.0 | 20.59 | .58 | 6.33 | " |
| " | " | 75.0 | 22.06 | .65 | 6.40 | " |
| B 89 | 24 | 80.0 | 23.32 | .50 | 7.00 | 8 |
| " | " | 85.0 | 25.00 | .57 | 7.07 | " |
| " | " | 90.0 | 26.47 | .63 | 7.13 | " |
| " | " | 95.0 | 27.94 | .69 | 7.19 | " |
| " | " | 100.0 | 29.41 | .75 | 7.25 | " |

WEIGHTS AND DIMENSIONS OF SPECIAL I-BEAMS.

| Section Number. | Depth of Beam. | Weight per Foot. | Area of Section. | Thickness of Web. | Width of Flange. | Page Number of Section. |
|-----------------|----------------|------------------|------------------|-------------------|------------------|-------------------------|
| | Inches. | Pounds. | Sq. In. | Inch. | Inches. | |
| B 105 | 12 | 40.0 | 11.84 | .46 | 5.25 | 4 |
| " | " | 45.0 | 13.24 | .58 | 5.37 | " |
| " | " | 50.0 | 14.71 | .70 | 5.49 | " |
| " | " | 55.0 | 16.18 | .82 | 5.61 | " |
| B 109 | 15 | 60.0 | 17.67 | .59 | 6.00 | 5 |
| " | " | 65.0 | 19.12 | .69 | 6.10 | " |
| " | " | 70.0 | 20.59 | .78 | 6.19 | " |
| " | " | 75.0 | 22.06 | .88 | 6.29 | " |
| " | " | 80.0 | 23.53 | .98 | 6.39 | " |
| B 113 | 15 | 80.0 | 23.57 | .80 | 6.40 | 5 |
| " | " | 85.0 | 25.00 | .90 | 6.50 | " |
| " | " | 90.0 | 26.47 | .99 | 6.59 | " |
| " | " | 95.0 | 27.94 | 1.09 | 6.69 | " |
| " | " | 100.0 | 29.41 | 1.19 | 6.79 | " |
| B 121 | 20 | 80.0 | 23.73 | .60 | 7.00 | 7 |
| " | " | 85.0 | 25.00 | .66 | 7.06 | " |
| " | " | 90.0 | 26.47 | .74 | 7.14 | " |
| " | " | 95.0 | 27.94 | .81 | 7.21 | " |
| " | " | 100.0 | 29.41 | .88 | 7.28 | " |
| B 127 | 24 | 105.0 | 30.98 | .63 | 7.88 | 9 |
| " | " | 110.0 | 32.48 | .69 | 7.94 | " |
| " | " | 115.0 | 33.98 | .75 | 8.00 | " |

Orders and inquiries concerning 12 in. 40 lb., 15 in. 60 lb., and 15 in. 80 lb. I-Beams should also specify by Section Number.

WEIGHTS AND DIMENSIONS OF STANDARD CHANNELS.

| Section Number. | Depth of Channel. | Weight per Foot. | Area of Section. | Thickness of Web. | Width of Flange. | Page Number of Section. |
|--------------------|-------------------------|------------------------|------------------------|-------------------------|------------------------|-------------------------------|
| | Inches. | Pounds. | Sq. In. | Inch. | Inches. | |
| C 5 | 3 | 4.0 | 1.19 | .17 | 1.41 | 10 |
| " | " | 5.0 | 1.47 | .26 | 1.50 | " |
| " | " | 6.0 | 1.76 | .36 | 1.60 | " |
| C 9 | 4 | 5.25 | 1.55 | .18 | 1.58 | 10 |
| " | " | 6.25 | 1.84 | .25 | 1.65 | " |
| " | " | 7.25 | 2.13 | .33 | 1.73 | " |
| C 13 | 5 | 6.50 | 1.95 | .19 | 1.75 | 10 |
| " | " | 9.00 | 2.65 | .33 | 1.89 | " |
| " | " | 11.50 | 3.38 | .48 | 2.04 | " |
| C 17 | 6 | 8.00 | 2.38 | .20 | 1.92 | 10 |
| " | " | 10.50 | 3.09 | .32 | 2.04 | " |
| " | " | 13.00 | 3.82 | .44 | 2.16 | " |
| " | " | 15.50 | 4.56 | .56 | 2.28 | " |
| C 21 | 7 | 9.75 | 2.85 | .21 | 2.09 | 10 |
| " | " | 12.25 | 3.60 | .32 | 2.20 | " |
| " | " | 14.75 | 4.34 | .42 | 2.30 | " |
| " | " | 17.25 | 5.07 | .53 | 2.41 | " |
| " | " | 19.75 | 5.81 | .63 | 2.51 | " |
| C 25 | 8 | 11.25 | 3.35 | .22 | 2.26 | 10 |
| " | " | 13.75 | 4.04 | .31 | 2.35 | " |
| " | " | 16.25 | 4.78 | .40 | 2.44 | " |
| " | " | 18.75 | 5.51 | .49 | 2.53 | " |
| " | " | 21.25 | 6.25 | .58 | 2.62 | " |
| C 29 | 9 | 13.25 | 3.89 | .23 | 2.43 | 11 |
| " | " | 15.00 | 4.41 | .29 | 2.49 | " |
| " | " | 20.00 | 5.88 | .45 | 2.65 | " |
| " | " | 25.00 | 7.35 | .61 | 2.81 | " |
| C 33 | 10 | 15.0 | 4.46 | .24 | 2.60 | 11 |
| " | " | 20.0 | 5.88 | .38 | 2.74 | " |
| " | " | 25.0 | 7.35 | .53 | 2.89 | " |
| " | " | 30.0 | 8.82 | .68 | 3.04 | " |
| " | " | 35.0 | 10.29 | .82 | 3.18 | " |
| C 41 | 12 | 20.5 | 6.03 | .28 | 2.94 | 11 |
| " | " | 25.0 | 7.35 | .39 | 3.05 | " |
| " | " | 30.0 | 8.82 | .51 | 3.17 | " |
| " | " | 35.0 | 10.29 | .64 | 3.30 | " |
| " | " | 40.0 | 11.76 | .76 | 3.42 | " |

WEIGHTS AND DIMENSIONS OF STANDARD CHANNELS.

| Section Number. | Depth of Channel. | Weight per Foot. | Area of Section. | Thickness of Web. | Width of Flange. | Page Number of Section. |
|-----------------|-------------------|------------------|------------------|-------------------|------------------|-------------------------|
| | Inches. | Pounds. | Sq. Ins. | Inch. | Inches. | |
| C 53 | 15 | 33 † | 9.90 | .40 | 3.40 | 12 |
| " | " | 35 † | 10.29 | .43 | 3.43 | " |
| " | " | 40 † | 11.76 | .52 | 3.52 | " |
| " | " | 45 † | 13.24 | .62 | 3.62 | " |
| " | " | 50 † | 14.71 | .72 | 3.72 | " |
| " | " | 55 † | 16.18 | .82 | 3.82 | " |

WEIGHTS AND DIMENSIONS OF SHIP AND SPECIAL CHANNELS.

| Section Number | Depth of Channel. | Weight per Foot. | Area of Section. | Thickness of Web. | Width of Flange. | Increase in Web and Flange for each Pound Increase of Weight. | Page Number of Section. |
|----------------|-------------------|------------------|------------------|-------------------|------------------|---|-------------------------|
| | Inches. | Pounds. | Sq. In. | Inch. | Inches. | Inch. | |
| C 269 | 3 | 7.1 | 2.07 | .306 | 1 1/8 | .098 | 13 |
| C 72 | 4 | 10.1 | 2.95 | .394 | 2.09 | .074 | 13 |
| C 86 | 6 | 15.3 † | 4.47 | .34 | 3.50 | .049 | 13 |
| " | " | 17.7 | 5.19 | .46 | 3.62 | " | " |
| C 88 | 6 | 19.0 | 5.58 | .41 | 3.56 | .049 | 13 |
| " | " | 21.6 | 6.36 | .54 | 3.69 | " | " |
| " | " | 23.4 | 6.87 | .63 | 3.78 | " | " |
| C 89 | 7 | 20.9 | 6.15 | .45 | 3.45 | .042 | 13 |
| " | " | 23.8 | 6.99 | .57 | 3.57 | " | " |
| C 101 | 8 | 21.5 | 6.30 | .40 | 3.50 | .037 | 14 |
| " | " | 24.8 | 7.26 | .52 | 3.62 | " | " |
| C 103 | 8 | 23.8 | 7.00 | .50 | 3.50 | .037 | 14 |
| " | " | 27.1 | 7.96 | .62 | 3.62 | " | " |
| C 90 | 10 | 21.9 | 6.44 | .38 | 3.38 | .029 | 14 |
| " | " | 26.0 | 7.64 | .50 | 3.50 | " | " |
| " | " | 27.4 | 8.04 | .54 | 3.54 | " | " |
| " | " | 31.5 | 9.24 | .66 | 3.66 | " | " |
| C 105 | 12 | 35.0 | 10.30 | .47 | 3.77 | .0245 | 14 |
| " | " | 40.0 | 11.76 | .60 | 3.90 | " | " |
| " | " | 44.3 | 13.02 | .70 | 4.00 | " | " |
| " | " | 46.3 | 13.62 | .75 | 4.05 | " | " |
| " | " | 48.4 | 14.22 | .80 | 4.10 | " | " |
| " | " | 50.0 | 14.70 | .84 | 4.14 | " | " |

† Standard Ship Section

WEIGHTS AND DIMENSIONS OF STANDARD SHIP CHANNELS.

Dimensions of standard 6-inch, 15.3 lb. ship channel on page 43.

| Section Number. | Depth of Channel. | Weight per Foot. | Area of Section. | Thickness of Web. | Width of Flange. | Increase in Web and Flange for each Pound increase of Weight. | Page Number of Section. |
|--------------------|-------------------------|------------------------|------------------------|-------------------------|------------------------|---|-------------------------------|
| | Inches. | Pounds. | Sq. Ins. | Inch. | Inches. | Inch. | |
| C 55 | 6 | 16.8 | 4.92 | .325 | 3.45 | .049 | 15 |
| " (BSC 8) | " | 17.8 | 5.22 | .375 | 3.50 | " | " |
| " | " | 19.8 | 5.82 | .475 | 3.60 | " | " |
| C 57 | 7 | 18.9 | 5.55 | .350 | 3.45 | .042 | 15 |
| " (BSC 10) | " | 20.1 | 5.90 | .400 | 3.50 | " | " |
| " | " | 22.5 | 6.60 | .500 | 3.60 | " | " |
| C 59 | 8 | 21.2 | 6.23 | .375 | 3.45 | .037 | 15 |
| " (BSC 13) | " | 22.6 | 6.63 | .425 | 3.50 | " | " |
| " | " | 25.3 | 7.43 | .525 | 3.60 | " | " |
| C 60 | 9 | 23.7 | 6.96 | .400 | 3.45 | .033 | 16 |
| " (BSC 17) | " | 25.2 | 7.41 | .450 | 3.50 | " | " |
| " | " | 28.3 | 8.31 | .550 | 3.60 | " | " |
| " | " | 31.3 | 9.21 | .650 | 3.70 | " | " |
| C 61 | 10 | 24.6 | 7.23 | .375 | 3.40 | .029 | 16 |
| " | " | 26.3 | 7.73 | .425 | 3.45 | " | " |
| " (BSC 20) | " | 28.0 | 8.23 | .475 | 3.50 | " | " |
| " | " | 31.4 | 9.23 | .575 | 3.60 | " | " |
| " | " | 34.8 | 10.23 | .675 | 3.70 | " | " |
| C 63 | 12 | 30.6 | 9.00 | .450 | 3.45 | .0245 | 16 |
| " (BSC 25) | " | 32.7 | 9.60 | .500 | 3.50 | " | " |
| " | " | 36.8 | 10.80 | .600 | 3.60 | " | " |
| " | " | 40.8 | 12.00 | .700 | 3.70 | " | " |

General slope of flange, $2^\circ = .035$.

WEIGHTS AND DIMENSIONS OF SHIP AND SPECIAL CHANNELS.—Continued.

| Section Number. | Depth of Channel. | Weight per Foot. | Area of Section. | Thickness of Web. | Width of Flange. | Increase in Web and Flange for each Pound increase of Weight. | Page Number of Section. |
|-----------------|-------------------|------------------|------------------|-------------------|------------------|---|-------------------------|
| | Inches. | Pounds. | Sq. Ins. | Inch. | Inches. | Inch. | |
| C 95 | 13 | 32 | 9.30 | .38 | 4.00 | .023 | 11 |
| " | " | 35 | 10.29 | .45 | 4.08 | " | " |
| " | " | 37 | 10.88 | .50 | 4.12 | " | " |
| " | " | 40 | 11.76 | .56 | 4.19 | " | " |
| " | " | 45 | 13.24 | .68 | 4.30 | " | " |
| " | " | 50 | 14.71 | .79 | 4.42 | " | " |
| " | " | 55 | 16.18 | .90 | 4.53 | " | " |
| C 65 | 18 | 45 | 13.25 | .47 | 3.77 | .016 | 12 |
| " | " | 50 | 14.71 | .55 | 3.85 | " | " |
| " | " | 55 | 16.18 | .63 | 3.93 | " | " |
| " | " | 60 | 17.65 | .72 | 4.02 | " | " |

WEIGHTS AND DIMENSIONS OF BULB ANGLES.

| Section Number | Size | Weight per Foot | Area of Section | Thickness Plain Leg | Thickness Bulb Leg | Length of Bulb | Width of Bulb | Page Number of Section |
|----------------|---------|-----------------|-----------------|----------------------------------|--------------------|-----------------|---------------|------------------------|
| | Inches | Pounds | Sq. Ins. | Inches | Inches | Inches | Inches | |
| A174 | 4 x 3½ | 11.7 | 3.42 | $\frac{3}{8}$ | $\frac{3}{8}$ | $\frac{57}{64}$ | 1½ | 20 |
| A176 | 5 x 4½ | 19.2 | 5.64 | $\frac{7}{16}$ | $\frac{7}{16}$ | 1¾ | 2¼ | " |
| A171 | 5 x 2½ | 10.2 | 3.00 | $\frac{9}{32}$ — $\frac{13}{32}$ | $\frac{19}{64}$ | $\frac{7}{8}$ | 1¼ | " |
| A177 | 6 x 3 | 11.8 | 3.47 | .34 | $\frac{5}{16}$ | 1.21 | 1.08 | " |
| " | " | 13.5 | 3.95 | .39 | $\frac{3}{8}$ | " | 1.14 | " |
| " | " | 15.0 | 4.41 | .43 | $\frac{7}{16}$ | " | 1.20 | " |
| A178 | 6 x 3½ | 12.5 | 3.66 | .37 | $\frac{5}{16}$ | 1.16 | 1.01 | " |
| " | " | 14.1 | 4.13 | .41 | $\frac{3}{8}$ | " | 1.08 | " |
| " | " | 15.7 | 4.60 | .45 | $\frac{7}{16}$ | " | 1.14 | " |
| " | " | 17.3 | 5.07 | .49 | $\frac{1}{2}$ | " | 1.20 | " |
| " | " | 18.9 | 5.53 | .53 | $\frac{9}{16}$ | " | 1.26 | " |
| " | " | 20.5 | 6.02 | .58 | $\frac{5}{8}$ | " | 1.33 | " |
| A179 | 7 x 3½ | 15.7 | 4.61 | .43 | $\frac{3}{8}$ | 1.25 | 1.10 | 21 |
| " | " | 17.5 | 5.13 | .46 | $\frac{7}{16}$ | " | 1.16 | " |
| " | " | 19.1 | 5.60 | .48 | $\frac{1}{2}$ | " | 1.23 | " |
| A181 | 8 x 3½ | 17.4 | 5.09 | .42 | $\frac{3}{8}$ | 1.35 | 1.18 | " |
| " | " | 19.3 | 5.64 | .44 | $\frac{7}{16}$ | " | 1.24 | " |
| " | " | 21.5 | 6.30 | .50 | $\frac{1}{2}$ | " | 1.30 | " |
| A183 | 9 x 3½ | 20.3 | 5.96 | .44 | $\frac{13}{32}$ | 1.48 | 1.29 | " |
| " | " | 22.6 | 6.62 | .48 | $\frac{3}{2}$ | " | 1.35 | " |
| " | " | 24.8 | 7.27 | .52 | $\frac{17}{32}$ | " | 1.41 | " |
| A185 | 10 x 3½ | 23.6 | 6.91 | .47 | $\frac{7}{16}$ | 1.61 | 1.40 | " |
| " | " | 26.1 | 7.64 | .51 | $\frac{1}{2}$ | " | 1.46 | " |
| " | " | 28.5 | 8.35 | .55 | $\frac{9}{16}$ | " | 1.53 | " |

WEIGHTS AND DIMENSIONS OF STANDARD BULB ANGLES.

| Section Number. | Size. | Weight per Foot. | Area of Section. | Thickness Plain Leg. | Thickness Bulb Leg. | Width of Bulb. | Page Number of Section. |
|--------------------|---------|---------------------|---------------------|-------------------------|------------------------|-------------------|-------------------------------|
| | Ins. | Lbs. | Sq. In. | Ins. | Ins. | Ins. | |
| A 187 | 6 x 3 | 12.2 | 3.58 | | .350 | 1.025 | 22 |
| " (BSBA 4) | " | 12.8 | 3.76 | .375 | .375 | 1.050 | " |
| " | " | 14.1 | 4.14 | | .425 | 1.100 | " |
| " | " | 15.6 | 4.58 | | .475 | 1.150 | " |
| A 188 | 7 x 3½ | 15.3 | 4.50 | | .375 | 1.125 | 22 |
| " (BSBA 8) | " | 16.8 | 4.94 | .425 | .425 | 1.175 | " |
| " | " | 18.6 | 5.46 | | .475 | 1.225 | " |
| " | " | 20.0 | 5.90 | | .525 | 1.275 | " |
| A 189 | 8 x 3½ | 18.0 | 5.29 | | .400 | 1.225 | 22 |
| " (BSBA 12) | " | 19.6 | 5.78 | .450 | .450 | 1.275 | " |
| " | " | 21.6 | 6.34 | | .500 | 1.325 | " |
| " | " | 23.2 | 6.83 | | .550 | 1.375 | " |
| A 190 | 9 x 3½ | 20.9 | 6.14 | | .425 | 1.325 | 22 |
| " (BSBA 16) | " | 22.7 | 6.68 | .475 | .475 | 1.375 | " |
| " | " | 24.8 | 7.29 | | .525 | 1.425 | " |
| " | " | 26.6 | 7.82 | | .575 | 1.475 | " |
| " | " | 28.6 | 8.41 | | .625 | 1.525 | " |
| A 191 | 10 x 3½ | 24.9 | 7.32 | | .475 | 1.450 | 23 |
| " (BSBA 18) | " | 26.9 | 7.90 | .525 | .525 | 1.500 | " |
| " | " | 29.1 | 8.55 | | .575 | 1.550 | " |
| " | " | 31.1 | 9.14 | | .625 | 1.600 | " |
| " | " | 33.2 | 9.77 | | .675 | 1.650 | " |
| " | " | 35.2 | 10.35 | | .725 | 1.700 | " |

WEIGHTS AND DIMENSIONS OF CAR SIDE STAKES.

| Section Number. | Extreme Width. | Depth. | Weight per Foot. | Area of Section. | Base Thickness. | Apex Thickness. | Groove Width. | Page Number of Section. |
|--------------------|-------------------|--------|---------------------|---------------------|--------------------|--------------------|------------------|-------------------------------|
| | Ins. | Ins. | Lbs. | Sq. In. | Ins. | Ins. | Ins. | |
| L 2 | 7 | 2½ | 7.2 | 2.10 | ¾ | ¾ | 2½ | 23 |
| " | " | 2⅜ | 8.7 | 2.54 | 1¼ | 1¼ | " | " |
| " | " | 2⅝ | 11.7 | 3.42 | 1½ | 1½ | " | " |

WEIGHTS AND DIMENSIONS OF REGULAR T-BARS. EQUAL LEGS.

| Section Number. | Width of Flange. | Depth of Bar. | Thickness of Flange. | Thickness of Stem. | Weight per Foot. | Area of Section. | Page Number of Section. |
|-----------------|------------------|-----------------|---------------------------------|---------------------------------|------------------|------------------|-------------------------|
| | Inches. | Inches. | Inch. | Inch. | Pounds. | Sq. Ins. | |
| T 5 | 1 | 1 | $\frac{1}{8}$ to $\frac{5}{32}$ | $\frac{1}{8}$ to $\frac{5}{32}$ | .89 | .26 | 24 |
| T 181 | $1\frac{1}{8}$ | $1\frac{1}{8}$ | $\frac{3}{16}$ " $\frac{7}{32}$ | $\frac{5}{32}$ " $\frac{7}{32}$ | 1.37 | .40 | " |
| T 183 | $1\frac{3}{16}$ | $1\frac{3}{16}$ | $\frac{3}{16}$ " $\frac{1}{4}$ | $\frac{5}{32}$ " $\frac{7}{32}$ | 1.51 | .44 | " |
| T 187 | $1\frac{1}{4}$ | $1\frac{1}{4}$ | $\frac{3}{16}$ " $\frac{1}{4}$ | $\frac{5}{32}$ " $\frac{7}{32}$ | 1.60 | .47 | " |
| T 188 | $1\frac{1}{4}$ | $1\frac{1}{4}$ | $\frac{3}{16}$ " $\frac{7}{32}$ | $\frac{3}{16}$ " $\frac{9}{32}$ | 1.70 | .50 | " |
| T 191 | $1\frac{1}{2}$ | $1\frac{1}{2}$ | $\frac{3}{16}$ " $\frac{7}{32}$ | $\frac{3}{16}$ " $\frac{7}{32}$ | 1.94 | .57 | " |
| T 193 | $1\frac{1}{2}$ | $1\frac{1}{2}$ | $\frac{1}{4}$ " $\frac{9}{32}$ | $\frac{1}{4}$ " $\frac{9}{32}$ | 2.47 | .73 | " |
| T 194 | $1\frac{3}{4}$ | $1\frac{3}{4}$ | $\frac{1}{4}$ " $\frac{5}{16}$ | $\frac{1}{4}$ " $\frac{5}{16}$ | 3.09 | .91 | " |
| T 37 | 2 | 2 | $\frac{1}{4}$ " $\frac{5}{16}$ | $\frac{1}{4}$ " $\frac{5}{16}$ | 3.56 | 1.05 | " |
| T 39 | 2 | 2 | $\frac{5}{16}$ " $\frac{3}{8}$ | $\frac{5}{16}$ " $\frac{3}{8}$ | 4.3 | 1.26 | 25 |
| T 41 | $2\frac{1}{4}$ | $2\frac{1}{4}$ | $\frac{1}{4}$ " $\frac{5}{16}$ | $\frac{1}{4}$ " $\frac{5}{16}$ | 4.1 | 1.19 | " |
| T 42 | $2\frac{1}{4}$ | $2\frac{1}{4}$ | $\frac{5}{16}$ " $\frac{3}{8}$ | $\frac{5}{16}$ " $\frac{3}{8}$ | 4.9 | 1.43 | " |
| T 47 | $2\frac{1}{2}$ | $2\frac{1}{2}$ | $\frac{1}{4}$ " $\frac{5}{16}$ | $\frac{1}{4}$ " $\frac{5}{16}$ | 4.6 | 1.33 | " |
| T 49 | $2\frac{1}{2}$ | $2\frac{1}{2}$ | $\frac{5}{16}$ " $\frac{3}{8}$ | $\frac{5}{16}$ " $\frac{3}{8}$ | 5.5 | 1.60 | " |

WEIGHTS AND DIMENSIONS OF REGULAR T-BARS. UNEQUAL LEGS.

| Section Number. | Width of Flange. | Depth of Bar. | Thickness of Flange. | Thickness of Stem. | Weight per Foot. | Area of Section. | Page Number of Section. |
|-----------------|------------------|-----------------|---------------------------------|----------------------------------|------------------|------------------|-------------------------|
| | Inches. | Inches. | Inch. | Inch. | Pounds. | Sq. Ins. | |
| T 16 | $1\frac{1}{4}$ | $1\frac{1}{16}$ | $\frac{3}{16}$ to $\frac{1}{4}$ | $\frac{5}{32}$ to $\frac{7}{32}$ | 1.48 | .43 | 25 |
| T 18 | $1\frac{1}{4}$ | $1\frac{1}{8}$ | $\frac{3}{16}$ " $\frac{7}{32}$ | $\frac{3}{16}$ " $\frac{1}{4}$ | 1.56 | .46 | " |
| T 20 | $1\frac{1}{2}$ | $1\frac{1}{4}$ | $\frac{1}{8}$ " $\frac{5}{32}$ | $\frac{1}{8}$ " $\frac{5}{32}$ | 1.25 | .37 | " |

WEIGHTS AND DIMENSIONS OF STANDARD ANGLES. EQUAL LEGS.

Sizes not specially marked were adopted as standard, May 21, 1910, by the Association of American Steel Manufacturers, for bridge, car, ship and general building construction. Sizes marked * are of special thickness and are not A. A. S. M. Standard.

| Section Num- ber. | Dimensions. | Thick- ness. | Weight per Foot. | Area of Section. | Section Num- ber. | Dimensions. | Thick- ness. | Weight per Foot. | Area of Section. |
|-------------------------|---------------|-----------------|------------------------|------------------------|-------------------------|-------------|-----------------|------------------------|------------------------|
| | Inches. | Inch. | Pounds. | Sq. Ins. | | Inches. | Inch. | Pounds. | Sq. Ins. |
| A 11 | 1 1/2 x 1 1/2 | 1/8 | 1.23 | .36 | A 23 | 4 x 4 | 5/16 | 8.2 | 2.40 |
| " | 1 1/2 x 1 1/2 | 3/16 | 1.80 | .53 | " | 4 x 4 | 3/8 | 9.8 | 2.86 |
| " | 1 1/2 x 1 1/2 | 1/4 | 2.34 | .69 | " | 4 x 4 | 7/16 | 11.3 | 3.31 |
| " | 1 1/2 x 1 1/2 | 5/16 | 2.86 | .84 | " | 4 x 4 | 1/2 | 12.8 | 3.75 |
| * " " | 1 1/2 x 1 1/2 | 3/8 | 3.35 | .98 | " | 4 x 4 | 9/16 | 14.3 | 4.18 |
| * A 15 | 2 x 2 | 1/8 | 1.65 | .48 | " | 4 x 4 | 5/8 | 15.7 | 4.61 |
| " | 2 x 2 | 3/16 | 2.44 | .72 | " | 4 x 4 | 3/4 | 17.1 | 5.03 |
| " | 2 x 2 | 1/4 | 3.19 | .94 | " | 4 x 4 | 7/8 | 18.5 | 5.44 |
| " | 2 x 2 | 5/16 | 3.92 | 1.15 | * " " | 4 x 4 | 13/16 | 19.9 | 5.84 |
| " | 2 x 2 | 3/8 | 4.7 | 1.36 | * " " | 4 x 4 | 7/8 | 21.2 | 6.23 |
| " | 2 x 2 | 7/16 | 5.3 | 1.56 | | | | | |
| * " " | 2 x 2 | 1/2 | 6.0 | 1.75 | | | | | |
| * A 17 | 2 1/2 x 2 1/2 | 1/8 | 2.08 | .61 | A 27 | 6 x 6 | 3/8 | 14.9 | 4.36 |
| " | 2 1/2 x 2 1/2 | 3/16 | 3.07 | .90 | " | 6 x 6 | 7/16 | 17.2 | 5.06 |
| " | 2 1/2 x 2 1/2 | 1/4 | 4.1 | 1.19 | " | 6 x 6 | 1/2 | 19.6 | 5.75 |
| " | 2 1/2 x 2 1/2 | 5/16 | 5.0 | 1.47 | " | 6 x 6 | 9/16 | 21.9 | 6.43 |
| " | 2 1/2 x 2 1/2 | 3/8 | 5.9 | 1.73 | " | 6 x 6 | 5/8 | 24.2 | 7.11 |
| " | 2 1/2 x 2 1/2 | 7/16 | 6.8 | 2.00 | " | 6 x 6 | 11/16 | 26.5 | 7.78 |
| * " " | 2 1/2 x 2 1/2 | 1/2 | 7.7 | 2.25 | " | 6 x 6 | 3/4 | 28.7 | 8.44 |
| A 19 | 3 x 3 | 1/4 | 4.9 | 1.44 | " | 6 x 6 | 13/16 | 31.0 | 9.09 |
| " | 3 x 3 | 5/16 | 6.1 | 1.78 | " | 6 x 6 | 7/8 | 33.1 | 9.73 |
| " | 3 x 3 | 3/8 | 7.2 | 2.11 | " | 6 x 6 | 15/16 | 35.3 | 10.37 |
| " | 3 x 3 | 7/16 | 8.3 | 2.43 | " | 6 x 6 | 1 | 37.4 | 11.00 |
| " | 3 x 3 | 1/2 | 9.4 | 2.75 | | | | | |
| * " " | 3 x 3 | 9/16 | 10.4 | 3.06 | A 35 | 8 x 8 | 1/2 | 26.4 | 7.75 |
| * A 21 | 3 1/2 x 3 1/2 | 1/4 | 5.8 | 1.69 | " | 8 x 8 | 9/16 | 29.6 | 8.68 |
| " | 3 1/2 x 3 1/2 | 5/16 | 7.2 | 2.09 | " | 8 x 8 | 5/8 | 32.7 | 9.61 |
| " | 3 1/2 x 3 1/2 | 3/8 | 8.5 | 2.48 | " | 8 x 8 | 11/16 | 35.8 | 10.53 |
| " | 3 1/2 x 3 1/2 | 7/16 | 9.8 | 2.87 | " | 8 x 8 | 3/4 | 38.9 | 11.44 |
| " | 3 1/2 x 3 1/2 | 1/2 | 11.1 | 3.25 | " | 8 x 8 | 13/16 | 42.0 | 12.34 |
| " | 3 1/2 x 3 1/2 | 5/8 | 12.4 | 3.62 | " | 8 x 8 | 7/8 | 45.0 | 13.23 |
| " | 3 1/2 x 3 1/2 | 3/4 | 13.6 | 3.98 | " | 8 x 8 | 15/16 | 48.1 | 14.12 |
| * " " | 3 1/2 x 3 1/2 | 11/16 | 14.8 | 4.34 | " | 8 x 8 | 1 | 51.0 | 15.00 |
| * " " | 3 1/2 x 3 1/2 | 3/4 | 16.0 | 4.69 | " | 8 x 8 | 1 1/16 | 54.0 | 15.87 |
| * " " | 3 1/2 x 3 1/2 | 13/16 | 17.1 | 5.03 | " | 8 x 8 | 1 1/8 | 56.9 | 16.73 |
| * " " | 3 1/2 x 3 1/2 | 7/8 | 18.3 | 5.36 | | | | | |

Standard Angles vary only by 1/16 inch. Sections shown on page 17.

† Standard Ship Section.

WEIGHTS AND DIMENSIONS OF STANDARD ANGLES. UNEQUAL LEGS.

Sizes not specially marked were adopted as standard, May 21, 1910, by the Association of American Steel Manufacturers, for bridge, car, ship and general building construction. Sizes marked * are of special thickness and are not A. A. S. M. standard.

| Section Num- ber. | Dimensions. Inches. | Thick- ness. Inch. | Weight per Foot. Pounds. | Area of Section. Sq. Ins. | Section Num- ber. | Dimensions. Inches. | Thick- ness. Inch. | Weight per Foot. Pounds. | Area of Section. Sq. Ins. |
|-------------------------|------------------------------------|------------------------------|---------------------------------------|--|-------------------------|----------------------------|------------------------------|---------------------------------------|--|
| A 91 | $2\frac{1}{2} \times 2$ | $\frac{3}{16}$ | 2.75 | .81 | A 99 | 4 x 3 | $\frac{5}{16} \dagger$ | 7.2 | 2.09 |
| " | $2\frac{1}{2} \times 2$ | $\frac{1}{4}$ | 3.62 | 1.06 | " | 4 x 3 | $\frac{3}{8} \dagger$ | 8.5 | 2.48 |
| " | $2\frac{1}{2} \times 2$ | $\frac{5}{16}$ | 4.5 | 1.31 | " | 4 x 3 | $\frac{7}{16} \dagger$ | 9.8 | 2.87 |
| " | $2\frac{1}{2} \times 2$ | $\frac{3}{8}$ | 5.3 | 1.55 | " | 4 x 3 | $\frac{1}{2} \dagger$ | 11.1 | 3.25 |
| * " | $2\frac{1}{2} \times 2$ | $\frac{7}{16}$ | 6.1 | 1.78 | " | 4 x 3 | $\frac{9}{16}$ | 12.4 | 3.62 |
| * " | $2\frac{1}{2} \times 2$ | $\frac{1}{2}$ | 6.8 | 2.00 | " | 4 x 3 | $\frac{5}{8}$ | 13.6 | 3.98 |
| A 93 | 3 x $2\frac{1}{2}$ | $\frac{1}{4} \dagger$ | 4.5 | 1.31 | * " | 4 x 3 | $\frac{11}{16}$ | 14.8 | 4.34 |
| " | 3 x $2\frac{1}{2}$ | $\frac{5}{16} \dagger$ | 5.6 | 1.62 | * " | 4 x 3 | $\frac{3}{4}$ | 16.0 | 4.69 |
| " | 3 x $2\frac{1}{2}$ | $\frac{3}{8} \dagger$ | 6.6 | 1.92 | * " | 4 x 3 | $\frac{13}{16}$ | 17.1 | 5.03 |
| " | 3 x $2\frac{1}{2}$ | $\frac{7}{16}$ | 7.6 | 2.22 | " | 4 x 3 | $\frac{7}{8}$ | 18.3 | 5.36 |
| * " | 3 x $2\frac{1}{2}$ | $\frac{1}{2}$ | 8.5 | 2.50 | A101 | 5 x 3 | $\frac{5}{16} \dagger$ | 8.2 | 2.40 |
| * " | 3 x $2\frac{1}{2}$ | $\frac{9}{16}$ | 9.5 | 2.78 | " | 5 x 3 | $\frac{3}{8} \dagger$ | 9.8 | 2.86 |
| A 95 | $3\frac{1}{2} \times 2\frac{1}{2}$ | $\frac{1}{4} \dagger$ | 4.9 | 1.44 | " | 5 x 3 | $\frac{7}{16} \dagger$ | 11.3 | 3.31 |
| " | $3\frac{1}{2} \times 2\frac{1}{2}$ | $\frac{5}{16}$ | 6.1 | 1.78 | " | 5 x 3 | $\frac{1}{2} \dagger$ | 12.3 | 3.75 |
| " | $3\frac{1}{2} \times 2\frac{1}{2}$ | $\frac{3}{8}$ | 7.2 | 2.11 | " | 5 x 3 | $\frac{9}{16}$ | 14.3 | 4.18 |
| " | $3\frac{1}{2} \times 2\frac{1}{2}$ | $\frac{7}{16}$ | 8.3 | 2.43 | " | 5 x 3 | $\frac{5}{8}$ | 15.7 | 4.61 |
| " | $3\frac{1}{2} \times 2\frac{1}{2}$ | $\frac{1}{2}$ | 9.4 | 2.75 | * " | 5 x 3 | $\frac{11}{16}$ | 17.1 | 5.03 |
| * " | $3\frac{1}{2} \times 2\frac{1}{2}$ | $\frac{9}{16}$ | 10.4 | 3.06 | * " | 5 x 3 | $\frac{3}{4}$ | 18.5 | 5.44 |
| *A 97 | $3\frac{1}{2} \times 3$ | $\frac{1}{4} \dagger$ | 5.4 | 1.56 | * " | 5 x 3 | $\frac{13}{16}$ | 19.9 | 5.84 |
| " | $3\frac{1}{2} \times 3$ | $\frac{5}{16} \dagger$ | 6.6 | 1.93 | * " | 5 x 3 | $\frac{7}{8}$ | 21.2 | 6.23 |
| " | $3\frac{1}{2} \times 3$ | $\frac{3}{8} \dagger$ | 7.9 | 2.30 | A103 | 5 x $3\frac{1}{2}$ | $\frac{5}{16}$ | 8.7 | 2.56 |
| " | $3\frac{1}{2} \times 3$ | $\frac{7}{16} \dagger$ | 9.1 | 2.65 | " | 5 x $3\frac{1}{2}$ | $\frac{3}{8}$ | 10.4 | 3.05 |
| " | $3\frac{1}{2} \times 3$ | $\frac{1}{2} \dagger$ | 10.2 | 3.00 | " | 5 x $3\frac{1}{2}$ | $\frac{7}{16}$ | 12.0 | 3.53 |
| " | $3\frac{1}{2} \times 3$ | $\frac{9}{16}$ | 11.4 | 3.34 | " | 5 x $3\frac{1}{2}$ | $\frac{1}{2}$ | 13.6 | 4.00 |
| * " | $3\frac{1}{2} \times 3$ | $\frac{5}{8}$ | 12.5 | 3.67 | " | 5 x $3\frac{1}{2}$ | $\frac{9}{16}$ | 15.2 | 4.47 |
| * " | $3\frac{1}{2} \times 3$ | $\frac{11}{16}$ | 13.6 | 4.00 | " | 5 x $3\frac{1}{2}$ | $\frac{5}{8}$ | 16.8 | 4.92 |
| * " | $3\frac{1}{2} \times 3$ | $\frac{3}{4}$ | 14.7 | 4.31 | " | 5 x $3\frac{1}{2}$ | $\frac{11}{16}$ | 18.3 | 5.37 |
| * " | $3\frac{1}{2} \times 3$ | $\frac{13}{16}$ | 15.8 | 4.62 | * " | 5 x $3\frac{1}{2}$ | $\frac{3}{4}$ | 19.8 | 5.81 |
| * " | $3\frac{1}{2} \times 3$ | $\frac{7}{8}$ | 16.8 | 4.92 | * " | 5 x $3\frac{1}{2}$ | $\frac{13}{16}$ | 21.3 | 6.25 |
| | | | | | * " | 5 x $3\frac{1}{2}$ | $\frac{7}{8}$ | 22.7 | 6.67 |
| | | | | | * " | 5 x $3\frac{1}{2}$ | $\frac{15}{16}$ | 24.2 | 7.09 |

Standard Angles vary only by $\frac{1}{16}$ inch. Sections shown on page 18.

† Standard Ship Section.

WEIGHTS AND DIMENSIONS OF STANDARD ANGLES. UNEQUAL LEGS.—CONTINUED.

Sizes not specially marked were adopted as standard, May 21, 1910, by the Association of American Steel Manufacturers, for bridge, car, ship and general building construction. Sizes marked * are of special thickness and are not A. A. S. M. standard.

| Section Number. | Dimensions. | Thick-ness. | Weight per Foot. | Area of Section. | Section Number. | Dimensions. | Thick-ness. | Weight per Foot. | Area of Section. |
|-----------------|---------------------|-------------------|------------------|------------------|-----------------|-------------|-----------------|------------------|------------------|
| | Inches. | Inch. | Pounds. | Sq. Ins. | | Inches. | Inch. | Pounds. | Sq. Ins. |
| A105 | 6 x 3 $\frac{1}{2}$ | $\frac{3}{8}$ † | 11.7 | 3.42 | A107 | 6 x 4 | $\frac{3}{8}$ | 12.3 | 3.61 |
| " | 6 x 3 $\frac{1}{2}$ | $\frac{7}{16}$ † | 13.5 | 3.97 | " | 6 x 4 | $\frac{7}{16}$ | 14.3 | 4.18 |
| " | 6 x 3 $\frac{1}{2}$ | $\frac{1}{2}$ † | 15.3 | 4.50 | " | 6 x 4 | $\frac{9}{16}$ | 16.2 | 4.75 |
| " | 6 x 3 $\frac{1}{2}$ | $\frac{9}{16}$ † | 17.1 | 5.03 | " | 6 x 4 | $\frac{3}{4}$ | 18.1 | 5.31 |
| " | 6 x 3 $\frac{1}{2}$ | $\frac{5}{8}$ † | 18.9 | 5.55 | " | 6 x 4 | $\frac{7}{8}$ | 20.0 | 5.86 |
| " | 6 x 3 $\frac{1}{2}$ | $\frac{11}{16}$ † | 20.6 | 6.06 | " | 6 x 4 | $\frac{11}{16}$ | 21.8 | 6.40 |
| " | 6 x 3 $\frac{1}{2}$ | $\frac{3}{4}$ † | 22.4 | 6.56 | " | 6 x 4 | $\frac{3}{4}$ | 23.6 | 6.94 |
| " | 6 x 3 $\frac{1}{2}$ | $\frac{13}{16}$ | 24.0 | 7.06 | " | 6 x 4 | $\frac{13}{16}$ | 25.4 | 7.47 |
| " | 6 x 3 $\frac{1}{2}$ | $\frac{7}{8}$ | 25.7 | 7.55 | " | 6 x 4 | $\frac{7}{8}$ | 27.2 | 7.98 |
| * " | 6 x 3 $\frac{1}{2}$ | $\frac{15}{16}$ | 27.3 | 8.03 | * " | 6 x 4 | $\frac{15}{16}$ | 28.9 | 8.50 |
| * " | 6 x 3 $\frac{1}{2}$ | 1 | 28.9 | 8.50 | * " | 6 x 4 | 1 | 30.6 | 9.00 |

WEIGHTS AND DIMENSIONS OF SPECIAL ANGLES. EQUAL LEGS.

| Section Number. | Dimensions. | Thick-ness. | Weight per Foot. | Area of Section. | Section Number. | Dimensions. | Thick-ness. | Weight per Foot. | Area of Section. |
|-----------------|-----------------------------------|----------------|------------------|------------------|-----------------|-----------------------------------|-------------------|------------------|------------------|
| | Inches. | Inch. | Pounds. | Sq. Ins. | | Inches. | Inch. | Pounds. | Sq. Ins. |
| A 36 | $\frac{3}{4}$ x $\frac{3}{4}$ | $\frac{1}{8}$ | .59 | .17 | A 41 | 2 $\frac{1}{4}$ x 2 $\frac{1}{4}$ | $\frac{3}{16}$ | 2.75 | .81 |
| " | $\frac{3}{4}$ x $\frac{3}{4}$ | $\frac{3}{16}$ | .84 | .25 | " | 2 $\frac{1}{4}$ x 2 $\frac{1}{4}$ | $\frac{1}{4}$ | 3.62 | 1.06 |
| | | | | | " | 2 $\frac{1}{4}$ x 2 $\frac{1}{4}$ | $\frac{5}{16}$ | 4.5 | 1.31 |
| A 37 | 1 x 1 | $\frac{1}{8}$ | .80 | .23 | | | | | |
| " | 1 x 1 | $\frac{3}{16}$ | 1.16 | .34 | A 43 | 2 $\frac{3}{4}$ x 2 $\frac{3}{4}$ | $\frac{1}{4}$ | 4.5 | 1.31 |
| " | 1 x 1 | $\frac{1}{4}$ | 1.49 | .44 | " | 2 $\frac{3}{4}$ x 2 $\frac{3}{4}$ | $\frac{5}{16}$ | 5.6 | 1.62 |
| | | | | | " | 2 $\frac{3}{4}$ x 2 $\frac{3}{4}$ | $\frac{3}{8}$ | 6.6 | 1.92 |
| A 38 | 1 $\frac{1}{4}$ x 1 $\frac{1}{4}$ | $\frac{1}{8}$ | 1.01 | .30 | | | | | |
| " | 1 $\frac{1}{4}$ x 1 $\frac{1}{4}$ | $\frac{3}{16}$ | 1.48 | .43 | A 47 | 5 x 5 | $\frac{3}{8}$ † | 12.3 | 3.61 |
| " | 1 $\frac{1}{4}$ x 1 $\frac{1}{4}$ | $\frac{1}{4}$ | 1.92 | .56 | " | 5 x 5 | $\frac{7}{16}$ † | 14.3 | 4.18 |
| A 40 | 1 $\frac{3}{4}$ x 1 $\frac{3}{4}$ | $\frac{1}{8}$ | 1.44 | .42 | " | 5 x 5 | $\frac{1}{2}$ † | 16.2 | 4.75 |
| " | 1 $\frac{3}{4}$ x 1 $\frac{3}{4}$ | $\frac{3}{16}$ | 2.12 | .62 | " | 5 x 5 | $\frac{9}{16}$ † | 18.1 | 5.31 |
| " | 1 $\frac{3}{4}$ x 1 $\frac{3}{4}$ | $\frac{1}{4}$ | 2.77 | .81 | " | 5 x 5 | $\frac{5}{8}$ † | 20.0 | 5.86 |
| " | 1 $\frac{3}{4}$ x 1 $\frac{3}{4}$ | $\frac{5}{16}$ | 3.39 | 1.00 | " | 5 x 5 | $\frac{11}{16}$ † | 21.8 | 6.40 |
| " | 1 $\frac{3}{4}$ x 1 $\frac{3}{4}$ | $\frac{3}{8}$ | 3.99 | 1.17 | " | 5 x 5 | $\frac{3}{4}$ † | 23.6 | 6.94 |

Standard Angles vary only by $\frac{1}{16}$ inch. Sections shown on pages 18 and 19.

† Standard Ship Section.

WEIGHTS AND DIMENSIONS OF SPECIAL ANGLES. UNEQUAL LEGS.

| Section Number | Dimensions | Thick-ness | Weight per Foot | Area of Section | Section Number | Dimensions | Thick-ness | Weight per Foot | Area of Section |
|----------------|---------------------|-----------------|-----------------|-----------------|----------------|---------------------|-----------------|-----------------|-----------------|
| | Inches | Inch | Pounds | Sq. Ins. | | Inches | Inch | Pounds | Sq. Ins. |
| A129 | 3 x 2 | $\frac{3}{16}$ | 3.07 | .90 | A109 | 7 x 3 $\frac{1}{2}$ | $\frac{7}{16}$ | 15.0 | 4.40 |
| " | 3 x 2 | $\frac{1}{4}$ | 4.1 | 1.19 | " | 7 x 3 $\frac{1}{2}$ | $\frac{1}{2}$ | 17.0 | 5.00 |
| " | 3 x 2 | $\frac{5}{16}$ | 5.0 | 1.47 | " | 7 x 3 $\frac{1}{2}$ | $\frac{9}{16}$ | 19.1 | 5.59 |
| " | 3 x 2 | $\frac{3}{8}$ | 5.9 | 1.73 | " | 7 x 3 $\frac{1}{2}$ | $\frac{5}{8}$ | 21.0 | 6.17 |
| " | 3 x 2 | $\frac{7}{16}$ | 6.8 | 2.00 | " | 7 x 3 $\frac{1}{2}$ | $\frac{11}{16}$ | 23.0 | 6.75 |
| " | 3 x 2 | $\frac{1}{2}$ | 7.7 | 2.25 | " | 7 x 3 $\frac{1}{2}$ | $\frac{3}{4}$ | 24.9 | 7.31 |
| | | | | | " | 7 x 3 $\frac{1}{2}$ | $\frac{13}{16}$ | 26.8 | 7.87 |
| A131 | 4 x 3 $\frac{1}{2}$ | $\frac{5}{16}$ | 7.7 | 2.25 | " | 7 x 3 $\frac{1}{2}$ | $\frac{7}{8}$ | 28.7 | 8.42 |
| " | 4 x 3 $\frac{1}{2}$ | $\frac{3}{8}$ | 9.1 | 2.67 | " | 7 x 3 $\frac{1}{2}$ | $\frac{15}{16}$ | 30.5 | 8.97 |
| " | 4 x 3 $\frac{1}{2}$ | $\frac{7}{16}$ | 10.6 | 3.09 | " | 7 x 3 $\frac{1}{2}$ | 1 | 32.3 | 9.50 |
| " | 4 x 3 $\frac{1}{2}$ | $\frac{1}{2}$ | 11.9 | 3.50 | | | | | |
| " | 4 x 3 $\frac{1}{2}$ | $\frac{9}{16}$ | 13.3 | 3.90 | A112 | 8 x 6 | $\frac{1}{2}$ | 23.0 | 6.75 |
| " | 4 x 3 $\frac{1}{2}$ | $\frac{5}{8}$ | 14.7 | 4.30 | " | 8 x 6 | $\frac{9}{16}$ | 25.7 | 7.56 |
| " | 4 x 3 $\frac{1}{2}$ | $\frac{11}{16}$ | 16.0 | 4.68 | " | 8 x 6 | $\frac{5}{8}$ | 28.5 | 8.36 |
| A135 | 5 x 4 | $\frac{3}{8}$ | 11.0 | 3.23 | " | 8 x 6 | $\frac{11}{16}$ | 31.2 | 9.15 |
| " | 5 x 4 | $\frac{7}{16}$ | 12.8 | 3.75 | " | 8 x 6 | $\frac{3}{4}$ | 33.8 | 9.94 |
| " | 5 x 4 | $\frac{1}{2}$ | 14.5 | 4.25 | " | 8 x 6 | $\frac{13}{16}$ | 36.5 | 10.72 |
| " | 5 x 4 | $\frac{9}{16}$ | 16.2 | 4.75 | " | 8 x 6 | $\frac{7}{8}$ | 39.1 | 11.48 |
| " | 5 x 4 | $\frac{5}{8}$ | 17.8 | 5.23 | " | 8 x 6 | $\frac{15}{16}$ | 41.7 | 12.25 |
| " | 5 x 4 | $\frac{11}{16}$ | 19.5 | 5.72 | " | 8 x 6 | 1 | 44.2 | 13.00 |

Sections shown on page 19.

BEAM TABLES.

Tables of safe loads for beams and channels and spacings of I-Beams for floors are given with explanatory notes on pages 100 to 135.

BEAMS AS GIRDERS.

In some cases two or more beams may be bolted together side by side to form a girder, in which case cast iron separators with bolts should be used to hold the various members together. Separators should be placed at each end of the girder, at points of concentrated loading, and for uniform loading should be located at distances apart not greater than twenty times the width of the smallest beam flange, in order to laterally support the upper flanges which are in compression and prevent their failure by buckling. The separators should preferably fit closely between the beam flanges so as to unite the beams forming the girder and thereby cause them to act together in resisting the load. Tables of Standard and Special Separators are given on pages 66 and 67.

CONNECTION ANGLES.

When beams are coped or fitted together at right angles, connection angles are generally used, standards for which, covering usual cases, are shown on pages 53, 54 and 55. Explanations and tables of limiting spans for which these standards may be used are given on pages 56 to 59. Beams may be fitted together thus with flush tops or bottoms or in intermediate positions, as required in cases where the girder or trimmer beam is the larger. In cases where the girder or trimmer beam is the smaller, special stirrups or other connections are required.

LIVE LOADS FOR FLOORS.

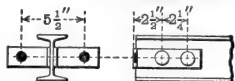
The following loads per square foot, exclusive of weight of floor materials, show the range assumed in usual practice:

| | |
|--------------------------------|---|
| Dwellings | 70 lbs. per sq. ft. |
| Offices | 70 to 100 lbs. per sq. ft. |
| Buildings for public assembly. | 120 to 150 lbs. per sq. ft. |
| Stores, warehouses, etc..... | 150 to 250 lbs. and upwards per sq. ft. |

On page 328 are given in detail the safe loads for which floors should be designed in accordance with the building laws of various cities.

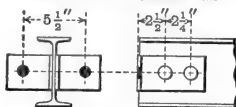
STANDARD CONNECTION ANGLES FOR I-BEAMS AND CHANNELS.

FOR 3" AND 4"
BEAMS AND CHANNELS



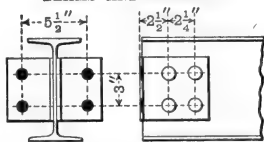
2- 6" x 4" x $\frac{3}{8}$ " ANGLES-2" LONG
WEIGHT 4.1 LBS.

FOR 5", 6" AND 7"
BEAMS AND CHANNELS



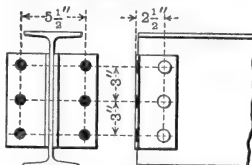
2- 6" x 4" x $\frac{3}{8}$ " ANGLES-3" LONG
WEIGHT 6.2 LBS.

FOR 8", 9" AND 10"
BEAMS AND CHANNELS



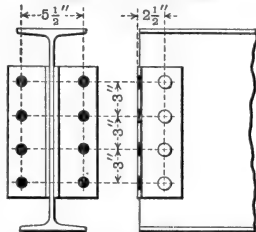
2- 6" x 4" x $\frac{3}{8}$ " ANGLES-5 $\frac{1}{2}$ " LONG
WEIGHT 11.3 LBS.

FOR 12"
BEAMS AND CHANNELS



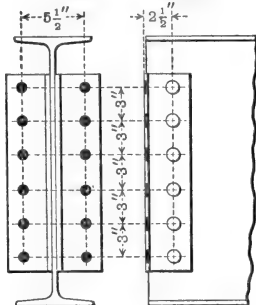
2- 4" x 4" x $\frac{7}{16}$ " ANGLES-8 $\frac{1}{2}$ " LONG
WEIGHT 16.1 LBS.

FOR 15", 18" AND 20"
BEAMS AND CHANNELS



2- 4" x 4" x $\frac{7}{16}$ " ANGLES-11 $\frac{1}{2}$ " LONG
WEIGHT 21.7 LBS.

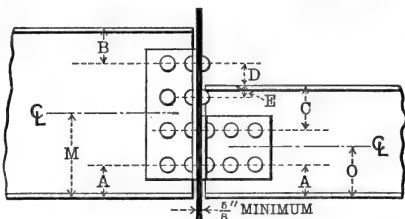
FOR 24" BEAMS



2- 4" x 4" x $\frac{1}{2}$ " ANGLES-17 $\frac{1}{2}$ " LONG
WEIGHT 37.4 LBS.

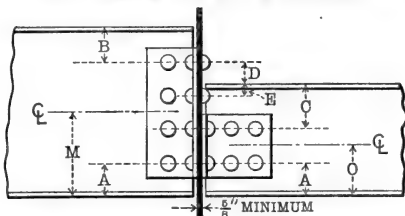
All rivets and bolts to be $\frac{3}{4}$ " diameter; all open holes $\frac{11}{16}$ " diameter.

**LOCATION OF CONNECTION ANGLES FOR
STANDARD BEAMS OF THE SAME OR DIFF-
ERENT SIZES FRAMING OPPOSITE,
BOTTOMS OR TOPS FLUSH.**



| Depth of Beams | | M | O | A | B | C | D | E |
|----------------|---------------|--------|--------|--------|--------|--------|--------|--------|
| Inches | | | | | | | | |
| Main Beam | Opposite Beam | Inches | Inches | Inches | Inches | Inches | Inches | Inches |
| 3 | 3 | 1½ | 1½ | 1½ | 1½ | 1½ | | |
| 4 | 3 | 1½ | 1½ | 1½ | 2½ | 1½ | | |
| 4 | 4 | 2 | 2 | 2 | 2 | 2 | | |
| 5 | 4 | 2⅛ | 2⅛ | 2⅛ | 2⅞ | 1⅞ | | |
| 5 | 5 | 2½ | 2½ | 2½ | 2½ | 2½ | | |
| 6 | 4 | 2⅜ | 2⅜ | 2⅜ | 3⅝ | 1⅝ | | |
| 6 | 5 | 2½ | 2½ | 2½ | 3½ | 2½ | | |
| 6 | 6 | 3 | 3 | 3 | 3 | 3 | | |
| 7 | 4 | 2⅜ | 2⅜ | 2⅜ | 4⅝ | 1⅝ | | |
| 7 | 5 | 2½ | 2½ | 2½ | 4½ | 2½ | | |
| 7 | 6 | 2½ | 2½ | 2½ | 4½ | 3½ | | |
| 7 | 7 | 3½ | 3½ | 3½ | 3½ | 3½ | | |
| 8 | 4 | 3⅝ | 2⅛ | 2⅛ | 2⅞ | 1⅞ | 1⅛ | |
| 8 | 5 | 4 | 2½ | 2½ | 2½ | 2½ | ½ | |
| 8 | 6 | 4 | 2½ | 2½ | 2½ | 3½ | | ½ |
| 8 | 7 | 4 | 2½ | 2½ | 2½ | 4½ | | ½ |
| 8 | 8 | 4 | 4 | 2½ | 2½ | 2½ | | |
| 9 | 5 | 4 | 2½ | 2½ | 3½ | 2½ | ½ | |
| 9 | 6 | 4 | 2½ | 2½ | 3½ | 3½ | | ½ |
| 9 | 7 | 4 | 2½ | 2½ | 3½ | 4½ | | 1½ |
| 9 | 8 | 4 | 4 | 2½ | 3½ | 2½ | | |
| 9 | 9 | 4½ | 4½ | 3 | 3 | 3 | | |
| 10 | 5 | 4 | 2½ | 2½ | 4½ | 2½ | ½ | |
| 10 | 6 | 4 | 2½ | 2½ | 4½ | 3½ | | ½ |
| 10 | 7 | 4 | 2½ | 2½ | 4½ | 4½ | | 1½ |
| 10 | 8 | 4 | 4 | 2½ | 4½ | 2½ | | |
| 10 | 9 | 4 | 4 | 2½ | 4½ | 3½ | | |
| 10 | 10 | 5 | 5 | 3½ | 3½ | 3½ | | |

**LOCATION OF CONNECTION ANGLES FOR
STANDARD BEAMS OF THE SAME OR DIFFERENT
SIZES FRAMING OPPOSITE,
BOTTOMS OR TOPS FLUSH.**



| Depth of Beams | | M | O | A | B | C | D | E |
|----------------|---------------|--------------------------------|--------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|
| Inches | | | | | | | | |
| Main Beam | Opposite Beam | Inches | Inches | Inches | Inches | Inches | Inches | Inches |
| 12 | 8* | 5 ³ / ₄ | 4 ¹ / ₄ | 2 ³ / ₄ | 3 ¹ / ₄ | 2 ¹ / ₄ | 3 ⁴ / ₄ | |
| 12 | 9* | 5 ³ / ₄ | 4 ¹ / ₄ | 2 ³ / ₄ | 3 ¹ / ₄ | 3 ¹ / ₄ | | 1 ¹ / ₄ |
| 12 | 10 | 5 ³ / ₄ | 4 ¹ / ₄ | 2 ³ / ₄ | 3 ¹ / ₄ | 4 ¹ / ₄ | | 1 ¹ / ₄ |
| 12 | 12 | 6 | 6 | 3 | 3 | 3 | | |
| 15 | 8* | 7 ¹ / ₄ | 4 ¹ / ₄ | 2 ³ / ₄ | 3 ¹ / ₄ | 2 ¹ / ₄ | 3 ⁴ / ₄ | |
| 15 | 9* | 7 ¹ / ₄ | 4 ¹ / ₄ | 2 ³ / ₄ | 3 ¹ / ₄ | 3 ¹ / ₄ | 2 ³ / ₄ | 1 ¹ / ₄ |
| 15 | 10 | 7 ¹ / ₄ | 4 ¹ / ₄ | 2 ³ / ₄ | 3 ¹ / ₄ | 4 ¹ / ₄ | 1 ³ / ₄ | 1 ¹ / ₄ |
| 15 | 12* | 7 ¹ / ₂ | 6 | 3 | 3 | 3 | 0 | 0 |
| 15 | 15 | 7 ¹ / ₂ | 7 ¹ / ₂ | 3 | 3 | 3 | | |
| 18 | 8* | 7 ¹ / ₄ | 4 ¹ / ₄ | 2 ³ / ₄ | 6 ¹ / ₄ | 2 ¹ / ₄ | 3 ⁴ / ₄ | |
| 18 | 9* | 7 ¹ / ₄ | 4 ¹ / ₄ | 2 ³ / ₄ | 6 ¹ / ₄ | 3 ¹ / ₄ | 2 ³ / ₄ | 1 ¹ / ₄ |
| 18 | 10 | 7 ¹ / ₄ | 4 ¹ / ₄ | 2 ³ / ₄ | 6 ¹ / ₄ | 3 ¹ / ₄ | 1 ³ / ₄ | 1 ¹ / ₄ |
| 18 | 12* | 7 ¹ / ₂ | 6 | 3 | 6 | 3 | 0 | 0 |
| 18 | 15 | 7 ¹ / ₂ | 7 ¹ / ₂ | 3 | 6 | 3 | | |
| 18 | 18 | 9 | 9 | 4 ¹ / ₂ | 4 ¹ / ₂ | 4 ¹ / ₂ | | |
| 20 | 8* | 7 ³ / ₈ | 4 ³ / ₈ | 2 ⁷ / ₈ | 8 ¹ / ₈ | 2 ¹ / ₈ | 7 ⁸ / ₈ | |
| 20 | 9* | 7 ¹ / ₂ | 4 ¹ / ₂ | 3 | 8 | 3 | 0 | 0 |
| 20 | 10* | 8 | 5 | 3 ¹ / ₂ | 7 ¹ / ₂ | 3 ¹ / ₂ | 2 ¹ / ₂ | 1 ¹ / ₂ |
| 20 | 12* | 7 ¹ / ₂ | 6 | 3 | 8 | 3 | 0 | 0 |
| 20 | 15 | 7 ¹ / ₂ | 7 ¹ / ₂ | 3 | 8 | 3 | | |
| 20 | 18 | 9 | 9 | 4 ¹ / ₂ | 6 ¹ / ₂ | 4 ¹ / ₂ | | |
| 20 | 20 | 10 | 10 | 5 ¹ / ₂ | 5 ¹ / ₂ | 5 ¹ / ₂ | | |
| 24 | 8* | 10 ³ / ₈ | 4 ³ / ₈ | 2 ⁷ / ₈ | 6 ¹ / ₈ | 2 ¹ / ₈ | 7 ⁸ / ₈ | |
| 24 | 9* | 10 ¹ / ₂ | 4 ¹ / ₂ | 3 | 6 | 3 | 0 | 0 |
| 24 | 10* | 11 | 5 | 3 ¹ / ₂ | 5 ¹ / ₂ | 3 ¹ / ₂ | 2 ¹ / ₂ | 1 ¹ / ₂ |
| 24 | 12* | 10 ¹ / ₂ | 6 | 3 | 6 | 3 | 0 | 0 |
| 24 | 15* | 10 ¹ / ₂ | 7 ¹ / ₂ | 3 | 6 | 3 | 0 | 0 |
| 24 | 18 | 12 | 9 | 4 ¹ / ₂ | 4 ¹ / ₂ | 4 ¹ / ₂ | 1 ¹ / ₂ | 1 ¹ / ₂ |
| 24 | 20 | 13 ¹ / ₂ | 10 ¹ / ₂ | 6 | 3 | 5 | 1 | 2 |
| 24 | 24 | 12 | 12 | 4 ¹ / ₂ | 4 ¹ / ₂ | 4 ¹ / ₂ | | |

*Opposite beam must be set back one inch to clear rivet heads.

STANDARD CONNECTION ANGLES FOR I-BEAMS AND CHANNELS.

Standard connection angles for all sizes of beams and channels are shown on page 53. These are of sufficient strength for all usual connections of the various sizes shown, figured on the basis of $\frac{3}{4}$ inch rivets or bolts and the following allowable unit stresses in pounds per square inch.

| Stress. | Shop Rivets. | Field Rivets or Turned Bolts. | Field Rough Bolts. |
|---------------------|--------------|----------------------------------|-----------------------|
| Single Shear..... | 12000 | 10000 | 8000 |
| Bearing—One Side... | 24000 | 20000 | 16000 |
| “ —Enclosed... | 30000 | 20000 | 16000 |

In cases where beams frame opposite, the web between outstanding legs of standard connection angles should not be less than $\frac{5}{8}$ inch thick.

When beams of very short spans are loaded to their full capacity, the end shear or reaction which has to be transmitted through the connections becomes so great that stronger connections than the standard should be used.

The following tables give the limits of length below which the standard connections do not apply and for which special designs should be made. For all lengths greater than those given in the tables the standard connections are sufficiently strong.

MINIMUM SPANS OF CHANNELS FOR LIMITING VALUES OF STANDARD CONNECTION ANGLES.

| Channel. | | | Web Con- nec- tion. | Outstanding Legs Connection. | | | |
|--------------------|---------|---------------------|--|---|---------------------------|---|---------------------------|
| Section Number. | Depth. | Weight per Foot. | | Field Rivets. | | Field Bolts. | |
| | Inches. | Pounds. | Enclosed Bearing Shop Rivets. Pounds. | Single Shear Rivets or Turned Bolts. Pounds. | Minimum Span. Feet. | Single Shear Rough Bolts. Pounds. | Minimum Span. Feet. |
| C 5 | 3 | 4.0 | 7650 | 8840 | .8 | 7070 | .9 |
| “ | “ | 5.0 | 11700 | “ | .8 | “ | 1.0 |
| “ | “ | 6.0 | 16200 | “ | .9 | “ | 1.1 |
| C 9 | 4 | 5.25 | 8100 | 8840 | 1.3 | 7070 | 1.5 |
| “ | “ | 6.25 | 11250 | “ | 1.3 | “ | 1.6 |
| “ | “ | 7.25 | 14850 | “ | 1.4 | “ | 1.8 |
| C 13 | 5 | 6.5 | 8550 | 8840 | 1.9 | 7070 | 2.3 |
| “ | “ | 9.0 | 14850 | “ | 2.2 | “ | 2.7 |
| “ | “ | 11.5 | 21600 | “ | 2.6 | “ | 3.2 |

MINIMUM SPANS OF CHANNELS FOR LIMITING VALUES OF STANDARD CONNECTION ANGLES.

| Channel. | | | Web Con- nection. | Outstanding Legs Connection. | | | |
|--------------------|---------|---------------------|-------------------------------------|--|------------------|------------------------------|------------------|
| Section Number. | Depth. | Weight per Foot. | Enclosed Bearing Shop Rivets. | Field Rivets. | | Field Bolts. | |
| | Inches. | Pounds. | | Single Shear Rivets or Turned Bolts. | Minimum Span. | Single Shear Rough Bolts. | Minimum Span. |
| | | | | Pounds. | Feet. | Pounds. | Feet. |
| C 17 | 6 | 8.0 | 9000 | 8840 | 2.7 | 7070 | 3.3 |
| " | " | 10.5 | 14400 | " | 3.1 | " | 3.8 |
| " | " | 13.0 | 19800 | " | 3.5 | " | 4.4 |
| " | " | 15.5 | 25200 | " | 4.0 | " | 5.0 |
| C 21 | 7 | 9.75 | 9450 | 8840 | 3.7 | 7070 | 4.6 |
| " | " | 12.25 | 14400 | " | 4.2 | " | 5.3 |
| " | " | 14.75 | 18900 | " | 4.7 | " | 5.9 |
| " | " | 17.25 | 23850 | " | 5.2 | " | 6.5 |
| " | " | 19.75 | 28350 | " | 5.8 | " | 7.2 |
| C 25 | 8 | 11.25 | 19800 | 17670 | 2.5 | 14140 | 3.1 |
| " | " | 13.75 | 27900 | " | 2.8 | " | 3.4 |
| " | " | 16.25 | 36000 | " | 3.1 | " | 3.8 |
| " | " | 18.75 | 44100 | " | 3.4 | " | 4.2 |
| " | " | 21.25 | 52200 | " | 3.6 | " | 4.5 |
| C 29 | 9 | 13.25 | 20700 | 17670 | 3.2 | 14140 | 4.0 |
| " | " | 15.00 | 26100 | " | 3.5 | " | 4.3 |
| " | " | 20.00 | 40500 | " | 4.1 | " | 5.1 |
| " | " | 25.00 | 54900 | " | 4.8 | " | 6.0 |
| C 33 | 10 | 15.0 | 21600 | 17670 | 4.1 | 14140 | 5.1 |
| " | " | 20.0 | 34200 | " | 4.8 | " | 6.0 |
| " | " | 25.0 | 47700 | " | 5.5 | " | 6.9 |
| " | " | 30.0 | 61200 | " | 6.3 | " | 7.8 |
| " | " | 35.0 | 73800 | " | 7.0 | " | 8.8 |
| C 41 | 12 | 20.5 | 18900 | 26510 | 6.1 | 21210 | 6.1 |
| " | " | 25.0 | 26320 | " | 4.9 | " | 6.1 |
| " | " | 30.0 | 34420 | " | 5.5 | " | 6.8 |
| " | " | 35.0 | 43200 | " | 6.0 | " | 7.6 |
| " | " | 40.0 | 51300 | " | 6.6 | " | 8.3 |
| C 53 | 15 | 33.0 | 36000 | 35340 | 6.3 | 28280 | 7.9 |
| " | " | 35.0 | 38700 | " | 6.5 | " | 8.1 |
| " | " | 40.0 | 46800 | " | 7.0 | " | 8.8 |
| " | " | 45.0 | 55800 | " | 7.6 | " | 9.5 |
| " | " | 50.0 | 64800 | " | 8.1 | " | 10.2 |
| " | " | 55.0 | 73800 | " | 8.7 | " | 10.9 |

MINIMUM SPANS OF I-BEAMS FOR LIMITING VALUES OF STANDARD CONNECTION ANGLES.

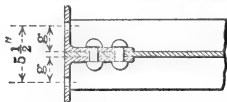
| I-Beam. | | | Web Con- nec- tion. | Outstanding Legs Connection. | | | |
|--------------------|---------|---------------------|--|---|---------------------------|---|---------------------------|
| Section Number. | Depth. | Weight per Foot. | | Field Rivets. | | Field Bolts. | |
| | Inches. | Pounds. | Enclosed Bearing Shop Rivets. Pounds. | Single Shear Rivets or Turned Bolts. Pounds. | Minimum Span. Feet. | Single Shear Rough Bolts. Pounds. | Minimum Span. Feet. |
| B 5 | 3 | 5.5 | 7650 | 8840 | 1.2 | 7070 | 1.3 |
| " | " | 6.5 | 11700 | " | 1.1 | " | 1.4 |
| " | " | 7.5 | 16200 | " | 1.2 | " | 1.5 |
| B 9 | 4 | 7.5 | 8550 | 8840 | 1.8 | 7070 | 2.3 |
| " | " | 8.5 | 11700 | " | 2.0 | " | 2.4 |
| " | " | 9.5 | 15300 | " | 2.1 | " | 2.6 |
| " | " | 10.5 | 18450 | " | 2.2 | " | 2.7 |
| B 13 | 5 | 9.75 | 9450 | 8840 | 3.0 | 7070 | 3.7 |
| " | " | 12.25 | 16200 | " | 3.3 | " | 4.2 |
| " | " | 14.75 | 22500 | " | 3.7 | " | 4.6 |
| B 17 | 6 | 12.25 | 10350 | 8840 | 4.4 | 7070 | 5.5 |
| " | " | 14.75 | 15750 | " | 4.9 | " | 6.1 |
| " | " | 17.25 | 21150 | " | 5.3 | " | 6.6 |
| B 21 | 7 | 15.00 | 11250 | 8840 | 6.3 | 7070 | 7.9 |
| " | " | 17.50 | 15750 | " | 6.8 | " | 8.5 |
| " | " | 20.00 | 20700 | " | 7.3 | " | 9.1 |
| B 25 | 8 | 18.00 | 24300 | 17670 | 4.3 | 14140 | 5.4 |
| " | " | 20.25 | 31500 | " | 4.6 | " | 5.7 |
| " | " | 22.75 | 39600 | " | 4.9 | " | 6.1 |
| " | " | 25.25 | 47700 | " | 5.2 | " | 6.5 |
| B 29 | 9 | 21.0 | 26100 | 17670 | 5.7 | 14140 | 7.2 |
| " | " | 25.0 | 36900 | " | 6.2 | " | 7.8 |
| " | " | 30.0 | 51300 | " | 6.9 | " | 8.6 |
| " | " | 35.0 | 65700 | " | 7.5 | " | 9.4 |
| B 33 | 10 | 25.0 | 27900 | 17670 | 7.4 | 14140 | 9.3 |
| " | " | 30.0 | 40500 | " | 8.1 | " | 10.2 |
| " | " | 35.0 | 54000 | " | 8.9 | " | 11.1 |
| " | " | 40.0 | 67500 | " | 9.6 | " | 12.0 |
| B 41 | 12 | 31.5 | 23625 | 26510 | 8.2 | 21210 | 9.1 |
| " | " | 35.0 | 29700 | " | 7.7 | " | 9.6 |
| " | " | 40.0 | 37800 | " | 8.3 | " | 10.4 |
| B 105 | 12 | 40.0 | 31050 | 26510 | 9.1 | 21210 | 11.3 |
| " | " | 45.0 | 39150 | " | 9.6 | " | 12.0 |
| " | " | 50.0 | 47250 | " | 10.2 | " | 12.8 |
| " | " | 55.0 | 48600 | " | 10.8 | " | 13.5 |

MINIMUM SPANS OF I-BEAMS FOR LIMITING VALUES OF STANDARD CONNECTION ANGLES.

| I-Beam. | | | Web Con- nection. | Outstanding Legs Connection. | | | |
|--------------------|---------|---------------------|-------------------------------------|--|------------------|------------------------------|------------------|
| Section Number. | Depth. | Weight per Foot. | Enclosed Bearing Shop Rivets. | Field Rivets. | | Field Bolts. | |
| | Inches. | Pounds. | Pounds. | Single Shear Rivets or Turned Bolts. | Minimum Span. | Single Shear Rough Bolts. | Minimum Span. |
| | | | | Pounds. | Feet. | Pounds. | Feet. |
| B 153 | 15 | 42.0 | 36900 | 35340 | 8.9 | 28280 | 11.2 |
| " | " | 45.0 | 41400 | " | 9.2 | " | 11.5 |
| " | " | 50.0 | 50400 | " | 9.8 | " | 12.2 |
| " | " | 55.0 | 59400 | " | 10.3 | " | 12.9 |
| " | " | 60.0 | 67500 | " | 10.9 | " | 13.6 |
| B 109 | 15 | 60.0 | 53100 | 35340 | 12.3 | 28280 | 15.4 |
| " | " | 65.0 | 62100 | " | 12.8 | " | 16.0 |
| " | " | 70.0 | 70200 | " | 13.4 | " | 16.7 |
| " | " | 75.0 | 79200 | " | 14.0 | " | 17.4 |
| " | " | 80.0 | 88200 | " | 14.5 | " | 18.1 |
| B 113 | *15 | 80.0 | 72000 | 35340 | 15.9 | 28280 | 19.9 |
| " | " | 85.0 | 81000 | " | 16.5 | " | 20.6 |
| " | " | 90.0 | 89100 | " | 17.0 | " | 21.3 |
| " | " | 95.0 | 98100 | " | 17.6 | " | 22.0 |
| " | " | 100.0 | 107100 | " | 18.1 | " | 22.6 |
| B 65 | 18 | 55.0 | 41400 | 35340 | 13.4 | 28280 | 16.7 |
| " | " | 60.0 | 50400 | " | 14.2 | " | 17.7 |
| " | " | 65.0 | 57600 | " | 14.8 | " | 18.5 |
| " | " | 70.0 | 64800 | " | 15.5 | " | 19.4 |
| B 73 | 20 | 65.0 | 45000 | 35340 | 17.7 | 28280 | 22.1 |
| " | " | 70.0 | 52200 | " | 18.5 | " | 23.0 |
| " | " | 75.0 | 58500 | " | 19.2 | " | 24.0 |
| B 121 | 20 | 80.0 | 54000 | 35340 | 22.2 | 28280 | 27.7 |
| " | " | 85.0 | 59400 | " | 22.8 | " | 28.5 |
| " | " | 90.0 | 66600 | " | 23.6 | " | 29.4 |
| " | " | 95.0 | 72900 | " | 24.3 | " | 30.3 |
| " | " | 100.0 | 79200 | " | 25.0 | " | 31.3 |
| B 89 | 24 | 80.0 | 67500 | 53020 | 17.6 | 42410 | 21.9 |
| " | " | 85.0 | 76950 | " | 18.2 | " | 22.8 |
| " | " | 90.0 | 85050 | " | 18.8 | " | 23.5 |
| " | " | 95.0 | 93150 | " | 19.4 | " | 24.2 |
| " | " | 100.0 | 101250 | " | 20.0 | " | 25.0 |
| B 127 | 24 | 105.0 | 85050 | 53020 | 23.6 | 42410 | 29.5 |
| " | " | 110.0 | 93150 | " | 24.2 | " | 30.3 |
| " | " | 115.0 | 101250 | " | 24.8 | " | 31.0 |

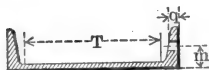
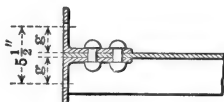
*Interior web edges of standard connection angles must be chamfered to avoid interference with beam web fillets.

STANDARD SPACING OF RIVET AND BOLT HOLES THROUGH FLANGES AND CONNECTION ANGLES OF I-BEAMS, AND TANGENT DISTANCES BETWEEN FILLETS MEASURED ALONG THE WEB.



| Depth of Beam | Wt. per Ft. | n | g | q | T | Depth of Beam | Wt. per Ft. | n | g | q | T |
|---------------|-------------|--------------------------------|--------------------------------|------|--------------------------------|---------------|-------------|-------------------------------|-------------------------------|-------------------------------|---------------------------------|
| Ins. | Lbs. | Ins. | Ins. | In. | Ins. | Ins. | Lbs. | Ins. | Ins. | In. | Ins. |
| 3 | 5.5 | 1 ⁷ / ₁₆ | 2 ³ / ₁₆ | 1/4 | 1 ¹ / ₁₆ | 15 | 42.0 | 3 | 2 ¹ / ₂ | 5/8 | 12 ¹ / ₁₆ |
| " | 6.5 | " | 2 ⁵ / ₈ | " | " | " | 45.0 | " | 2 ¹ / ₂ | " | " |
| " | 7.5 | " | 2 ¹ / ₂ | " | " | " | 50.0 | " | 2 ¹ / ₂ | " | " |
| " | " | " | " | " | " | " | 55.0 | " | 2 ¹ / ₂ | " | " |
| 4 | 7.5 | 1 ¹ / ₂ | 2 ³ / ₁₆ | 5/16 | 2 ¹ / ₁₆ | " | 60.0 | " | 2 ³ / ₈ | " | " |
| " | 8.5 | " | 2 ⁵ / ₈ | " | " | 15 | 60.0 | 3 ¹ / ₄ | 2 ¹ / ₂ | 7/8 | 11 ³ / ₄ |
| " | 9.5 | " | 2 ¹ / ₂ | " | " | " | 65.0 | " | 2 ¹ / ₂ | " | " |
| " | 10.5 | " | 2 ¹ / ₂ | " | " | " | 70.0 | " | 2 ³ / ₈ | " | " |
| 5 | 9.75 | 1 ³ / ₄ | 2 ⁵ / ₈ | 5/16 | 3 ⁹ / ₁₆ | " | 75.0 | " | 2 ¹ / ₂ | " | " |
| " | 12.25 | " | 2 ⁹ / ₁₆ | " | " | " | 80.0 | " | 2 ¹ / ₄ | " | " |
| " | 14.75 | " | 2 ¹ / ₂ | " | " | 15 | 80.0 | 3 ³ / ₄ | 2 ¹ / ₂ | 1 ¹ / ₂ | 10 ¹ / ₁₆ |
| 6 | 12.25 | 2 | 2 ⁵ / ₈ | 3/8 | 4 ⁷ / ₁₆ | " | 85.0 | " | 2 ¹ / ₂ | " | " |
| " | 14.75 | " | 2 ⁹ / ₁₆ | " | " | " | 90.0 | " | 2 ¹ / ₄ | " | " |
| " | 17.25 | " | 2 ¹ / ₂ | " | " | " | 95.0 | " | 2 ¹ / ₂ | " | " |
| " | " | " | " | " | " | " | 100.0 | " | 2 ³ / ₄ | 1 ¹ / ₈ | " |
| 7 | 15.00 | 2 ¹ / ₄ | 2 ⁵ / ₈ | 3/8 | 5 ⁵ / ₁₆ | " | 55.0 | 3 ¹ / ₄ | 2 ¹ / ₂ | 1 ¹ / ₂ | 15 ¹ / ₁₆ |
| " | 17.50 | " | 2 ⁹ / ₁₆ | " | " | 18 | 60.0 | " | 2 ¹ / ₂ | " | " |
| " | 20.00 | " | 2 ¹ / ₂ | " | " | " | 65.0 | " | 2 ¹ / ₂ | " | " |
| 8 | 18.00 | 2 ¹ / ₄ | 2 ⁵ / ₈ | 7/16 | 6 ³ / ₁₆ | " | 70.0 | " | 2 ³ / ₈ | " | " |
| " | 20.25 | " | 2 ⁹ / ₁₆ | " | " | 20 | 65.0 | 3 ¹ / ₂ | 2 ¹ / ₂ | 1 ¹ / ₂ | 16 ⁷ / ₈ |
| " | 22.75 | " | 2 ¹ / ₂ | " | " | " | 70.0 | " | 2 ¹ / ₂ | " | " |
| " | 25.25 | " | 2 ¹ / ₂ | " | " | " | 75.0 | " | 2 ¹ / ₂ | " | " |
| 9 | 21.0 | 2 ¹ / ₂ | 2 ¹ / ₂ | 1/2 | 7 ¹ / ₁₆ | " | 80.0 | 4 | 2 ¹ / ₂ | 1 ¹ / ₂ | 16 ¹ / ₁₆ |
| " | 25.0 | " | 2 ¹ / ₂ | " | " | 20 | 85.0 | " | 2 ¹ / ₂ | " | " |
| " | 30.0 | " | 2 ³ / ₈ | " | " | " | 90.0 | " | 2 ³ / ₈ | " | " |
| " | 35.0 | " | 2 ³ / ₈ | " | " | " | 95.0 | " | 2 ¹ / ₂ | " | " |
| 10 | 25.0 | 2 ⁵ / ₈ | 2 ¹ / ₂ | 1/2 | 7 ¹ / ₁₆ | " | 100.0 | " | 2 ¹ / ₂ | " | " |
| " | 30.0 | " | 2 ¹ / ₂ | " | " | 24 | 80.0 | 4 | 2 ¹ / ₂ | 7/8 | 20 ¹ / ₁₆ |
| " | 35.0 | " | 2 ¹ / ₂ | " | " | " | 85.0 | " | 2 ¹ / ₂ | " | " |
| " | 40.0 | " | 2 ¹ / ₂ | " | " | " | 90.0 | " | 2 ¹ / ₂ | " | " |
| 12 | 31.5 | 2 ³ / ₄ | 2 ¹ / ₂ | 1/2 | 9 ¹ / ₁₆ | " | 95.0 | " | 2 ¹ / ₂ | " | " |
| " | 35.0 | " | 2 ¹ / ₂ | " | " | " | 100.0 | " | 2 ³ / ₈ | " | " |
| " | 40.0 | " | 2 ¹ / ₂ | " | " | 24 | 105.0 | 4 | 2 ¹ / ₂ | 1 ¹ / ₈ | 20 ¹ / ₈ |
| 12 | 40.0 | 3 | 2 ¹ / ₂ | 1/2 | 9 ⁵ / ₁₆ | " | 110.0 | " | 2 ¹ / ₂ | " | " |
| " | 45.0 | " | 2 ¹ / ₂ | " | " | " | 115.0 | " | 2 ³ / ₈ | " | " |
| " | 50.0 | " | 2 ¹ / ₂ | " | " | " | " | " | " | " | " |
| " | 55.0 | " | 2 ¹ / ₂ | " | " | " | " | " | " | " | " |

STANDARD SPACING OF RIVET AND BOLT HOLES IN FLANGES AND CONNECTION ANGLES OF CHANNELS, AND TANGENT DISTANCES BE- TWEEN FILLETS MEASURED ALONG THE WEB.



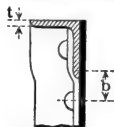
| Depth of Channel | Wt. per Ft. | m | g | q | T | Depth of Channel | Wt. per Ft. | m | g | q | T |
|------------------|-------------|----------------|----------------|----------------|-----------------|------------------|-------------|----------------|----------------|----------------|-----------------|
| Ins. | Lbs. | Ins. | Ins. | In. | Ins. | Ins. | Lbs. | Ins. | Ins. | In. | Ins. |
| 3 | 4.0 | $\frac{1}{8}$ | $2\frac{3}{4}$ | $\frac{1}{4}$ | $1\frac{1}{8}$ | 10 | 15.0 | $1\frac{1}{2}$ | $2\frac{5}{8}$ | $\frac{7}{16}$ | $8\frac{1}{8}$ |
| " | 5.0 | " | $2\frac{5}{8}$ | " | " | " | 20.0 | " | $2\frac{1}{8}$ | $2\frac{1}{2}$ | " |
| " | 6.0 | " | $2\frac{1}{8}$ | $\frac{3}{8}$ | " | " | 25.0 | 2 | $2\frac{1}{2}$ | " | " |
| 4 | 5.25 | 1 | $2\frac{3}{4}$ | $\frac{5}{16}$ | $2\frac{1}{8}$ | " | 30.0 | " | $2\frac{1}{2}$ | $2\frac{1}{2}$ | " |
| " | 6.25 | " | $2\frac{5}{8}$ | $2\frac{1}{8}$ | " | " | 35.0 | " | $2\frac{1}{2}$ | " | " |
| " | 7.25 | " | $2\frac{1}{2}$ | " | " | 12 | 20.5 | $1\frac{3}{4}$ | $2\frac{5}{8}$ | $\frac{1}{2}$ | $9\frac{1}{8}$ |
| 5 | 6.5 | 1 | $2\frac{3}{4}$ | $\frac{5}{16}$ | $3\frac{5}{8}$ | " | 25.0 | " | $2\frac{1}{8}$ | " | " |
| " | 9.0 | $1\frac{1}{4}$ | $2\frac{1}{2}$ | " | " | " | 30.0 | 2 | $2\frac{1}{2}$ | " | " |
| " | 11.5 | " | $2\frac{1}{2}$ | " | " | " | 35.0 | " | $2\frac{1}{8}$ | " | " |
| 6 | 8.0 | $1\frac{1}{8}$ | $2\frac{3}{4}$ | $\frac{3}{8}$ | $4\frac{1}{2}$ | " | 40.0 | " | $2\frac{3}{8}$ | " | " |
| " | 10.5 | " | $2\frac{1}{2}$ | " | " | 13 | 32.0 | $2\frac{3}{4}$ | $2\frac{1}{8}$ | $\frac{5}{16}$ | $10\frac{3}{8}$ |
| " | 13.0 | $1\frac{3}{8}$ | $2\frac{1}{2}$ | " | " | " | 35.0 | " | $2\frac{1}{2}$ | " | " |
| " | 15.5 | " | $2\frac{1}{2}$ | " | " | " | 37.0 | " | $2\frac{1}{2}$ | " | " |
| 7 | 9.75 | $1\frac{1}{4}$ | $2\frac{5}{8}$ | $\frac{3}{8}$ | $5\frac{7}{16}$ | " | 40.0 | 3 | $2\frac{1}{2}$ | " | " |
| " | 12.25 | " | $2\frac{1}{2}$ | " | " | " | 45.0 | " | $2\frac{1}{2}$ | " | " |
| " | 14.75 | " | $2\frac{1}{2}$ | " | " | " | 50.0 | " | $2\frac{1}{2}$ | " | " |
| " | 17.25 | $1\frac{1}{2}$ | $2\frac{1}{2}$ | " | " | " | 55.0 | " | $2\frac{1}{2}$ | " | " |
| " | 19.75 | " | $2\frac{1}{8}$ | " | " | 15 | 33.0 | $1\frac{7}{8}$ | $2\frac{1}{8}$ | $\frac{5}{8}$ | $12\frac{3}{8}$ |
| 8 | 11.25 | $1\frac{1}{4}$ | $2\frac{5}{8}$ | $\frac{3}{8}$ | $6\frac{5}{16}$ | " | 35.0 | " | $2\frac{1}{2}$ | " | " |
| " | 13.75 | " | $2\frac{1}{2}$ | " | " | " | 40.0 | " | $2\frac{1}{2}$ | " | " |
| " | 16.25 | $1\frac{1}{2}$ | $2\frac{1}{8}$ | " | " | " | 45.0 | $2\frac{1}{4}$ | $2\frac{1}{8}$ | " | " |
| " | 18.75 | " | $2\frac{1}{2}$ | " | " | " | 50.0 | " | $2\frac{3}{8}$ | " | " |
| " | 21.25 | " | $2\frac{1}{2}$ | " | " | " | 55.0 | " | $2\frac{1}{2}$ | " | " |
| 9 | 13.25 | $1\frac{3}{8}$ | $2\frac{5}{8}$ | $\frac{7}{16}$ | $7\frac{1}{4}$ | 18 | 45.0 | $2\frac{1}{4}$ | $2\frac{1}{2}$ | $\frac{7}{8}$ | 15 |
| " | 15.00 | " | $2\frac{1}{2}$ | " | " | " | 50.0 | " | $2\frac{1}{2}$ | " | " |
| " | 20.00 | $1\frac{3}{4}$ | $2\frac{1}{2}$ | " | " | " | 55.0 | " | $2\frac{1}{8}$ | " | " |
| " | 25.00 | " | $2\frac{1}{8}$ | " | " | " | 60.0 | " | $2\frac{3}{8}$ | " | " |

MAXIMUM SIZE OF RIVETS IN FLANGES OF BEAMS AND CHANNELS.

| I-BEAMS. | | | | | | CHANNELS. | | |
|----------------|--------------|---------------------|----------------|--------------|---------------------|-------------------|--------------|---------------------|
| Depth of Beam. | Weight. | Diameter of Rivets. | Depth of Beam. | Weight. | Diameter of Rivets. | Depth of Channel. | Weight. | Diameter of Rivets. |
| Inches. | Lbs. per Ft. | Inch. | Inches. | Lbs. per Ft. | Inch. | Inches. | Lbs. per Ft. | Inch. |
| 3 | 5.50 | $\frac{3}{8}$ | 15 | 42.0 | $\frac{3}{4}$ | 3 | 4.00 | $\frac{1}{4}$ |
| 4 | 7.50 | $\frac{1}{2}$ | 15 | 60.0 | $\frac{3}{4}$ | 4 | 5.25 | $\frac{1}{4}$ |
| 5 | 9.75 | " | 15 | 80.0 | $\frac{7}{8}$ | 5 | 6.50 | " |
| 6 | 12.25 | $\frac{5}{8}$ | 18 | 55.0 | " | 6 | 8.00 | $\frac{5}{8}$ |
| 7 | 15.00 | " | 20 | 65.0 | " | 7 | 9.75 | $\frac{5}{8}$ |
| 8 | 18.00 | $\frac{3}{4}$ | 20 | 80.0 | " | 8 | 11.25 | $\frac{3}{4}$ |
| 9 | 21.00 | " | 24 | 80.0 | " | 9 | 13.25 | " |
| 10 | 25.00 | " | 24 | 105.0 | " | 10 | 15.00 | " |
| 12 | 31.50 | " | | | | 12 | 20.50 | $\frac{1}{2}$ |
| 12 | 40.00 | " | | | | 15 | 33.00 | " |

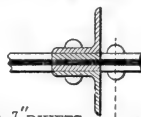
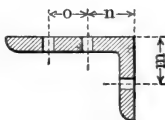
STANDARD SPACING OF RIVET AND BOLT HOLES IN ANGLES, WITH MAXIMUM

RIVETS IN SIZE OF RIVETS TO BE USED. CLEARANCE
CRIMPED ANGLES FOR RIVETING



$$b = 2t + 1\frac{1}{2}''$$

MINIMUM 2"



FOR $\frac{7}{8}$ " RIVETS
" $\frac{3}{4}$ " " " " " " " " " " "

ANGLES.

| Length of Leg. | m | Diam. of Rivet. | Length of Leg. | m | Diam. of Rivet. | Length of Leg. | m | n | o | Diam. of Rivet. |
|----------------|---------------|-----------------|----------------|----------------|-----------------|----------------|----------------|----------------|----------------|-----------------|
| Ins. | Ins. | Ins. | Ins. | Ins. | Ins. | Ins. | Ins. | Ins. | Ins. | Ins. |
| $\frac{3}{4}$ | $\frac{1}{2}$ | $\frac{1}{4}$ | 2 | $1\frac{1}{8}$ | $\frac{5}{8}$ | 4 | $2\frac{1}{2}$ | 2 | $1\frac{1}{4}$ | $\frac{7}{8}$ |
| 1 | $\frac{5}{8}$ | " | $2\frac{1}{4}$ | $1\frac{1}{4}$ | $\frac{3}{4}$ | $4\frac{1}{2}$ | " | " | $1\frac{3}{4}$ | " |
| $1\frac{1}{4}$ | $\frac{3}{4}$ | $\frac{3}{8}$ | $2\frac{1}{2}$ | $1\frac{3}{8}$ | " | 5 | 3 | " | $2\frac{1}{4}$ | " |
| $1\frac{3}{8}$ | $\frac{7}{8}$ | " | $2\frac{3}{4}$ | $1\frac{5}{8}$ | " | 6 | $3\frac{1}{2}$ | $2\frac{1}{2}$ | 3 | 1 |
| $1\frac{1}{2}$ | " | " | 3 | $1\frac{3}{4}$ | $\frac{7}{8}$ | 7 | 4 | " | " | $1\frac{1}{8}$ |
| $1\frac{3}{4}$ | 1 | $\frac{1}{2}$ | $3\frac{1}{2}$ | 2 | " | 8 | $4\frac{1}{2}$ | 3 | " | " |

BEARING PLATES FOR SHAPES USED AS BEAMS.

Shapes used as beams resting on masonry walls or piers will generally require bearing plates of steel or their equivalents, set in or upon the masonry to properly distribute the load thereon with due regard to the allowable safe pressures for the class of stonework or brickwork in question.

A table of bearing plates is given on page 65, which gives the bearing values in pounds for plates of various sizes based on the safe unit pressure allowable for different classes of masonry. As the strength of masonry varies largely according to the qualities of the material used, the workmanship and age, it is impossible to give absolute figures for safe unit pressures for all classes of work, but the values given on page 64 are believed to fairly represent these for the usual kinds of ordinary architectural masonry. The strength of ordinary masonry generally depends upon the crushing value of the mortar or cement used and does not bear any fixed relation to the ultimate strength of the brick or stone entering into the construction.

The table of bearing plates gives the bearing values of various sizes of plates when used with different classes of masonry, but the thickness of the plate should be computed for each case.

For a plate of given length and breadth the thickness depends upon the allowable load and unit stress, and the width of the flange of the beam or channel resting upon it.

The thickness may be determined by the following formula

$$t = .866 (l - b) \sqrt{\frac{R}{pb'l}}$$

t = thickness of plate in inches.

l = length of plate in inches, in a direction perpendicular to the axis of the beam or channel.

b = width of flange of beam or channel in inches.

R = reaction at point of support in pounds.

For uniformly distributed loads, R = one-half of the load given in Tables of Safe Loads, pages 106 to 123 inclusive.

p = allowable stress in pounds per square inch on extreme fibre of plate.

b' = width of plate in the direction of the axis of the beam or channel; *i. e.*, bearing on wall in inches.

If $p = 16\ 000$ lbs. for steel we have

$$t = .00685 (l - b) \sqrt{\frac{R}{b'l}}$$

EXAMPLE.

What is the proper size of steel bearing plate to be used in a wall of brick laid in cement mortar to support the end of a 10-inch standard I-Beam, weighing 40 pounds per foot, of 10 foot span, subjected to its safe load uniformly distributed?

On page 109 in the Table of Safe Loads Uniformly Distributed for Cambria I-Beams, the total load is found to be 33 850 pounds, and half of this, or 16 925 pounds, will be the reaction at each end.

On referring to the Table of Bearing Plates, on page 65, the proper size for this load on the class of masonry in question is found to be 6" x 10". The width of flange of a 10-inch 40 lb. standard beam is 5.10 inches.

Substituting these values in the formula for thickness gives

$$t = .00685 (10 - 5.10) \sqrt{\frac{16\ 925}{6 \times 10}} = .562$$

The nearest commercial size above this is $\frac{1}{2}$ inch, which is the thickness required.

If a shorter plate would suit the location better it may be seen from the table that a plate 8" x 8" will give the necessary bearing value and the thickness of this would be

$$t = .00685 (8 - 5.10) \sqrt{\frac{16\ 925}{8 \times 8}} = .323$$

and the nearest commercial size above this is $\frac{3}{8}$ ", which is the thickness required.

STANDARD BEARINGS AND BEARING PLATES.

| Size of Beams and Channels. | Bearing. | Bearing Plate. | | |
|-----------------------------------|----------|-------------------------|---------|-------------|
| | | Dimensions. | Weight. | Area. |
| Inches. | Inches. | Inches. | Pounds. | Sq. Inches. |
| 3 | 6 | 6 x 6 x $\frac{3}{8}$ | 3.9 | 36 |
| 4 | 6 | 6 x 6 x $\frac{3}{8}$ | " | 36 |
| 5 | 6 | 6 x 6 x $\frac{3}{8}$ | " | 36 |
| 6 | 6 | 6 x 6 x $\frac{3}{8}$ | " | 36 |
| 7 | 8 | 8 x 8 x $\frac{1}{2}$ | 9.1 | 64 |
| 8 | 8 | 8 x 8 x $\frac{1}{2}$ | " | 64 |
| 9 | 8 | 8 x 8 x $\frac{1}{2}$ | " | 64 |
| 10 | 12 | 12 x 12 x $\frac{3}{4}$ | 30.6 | 144 |
| 12 | 12 | 12 x 12 x $\frac{3}{4}$ | " | 144 |
| 15 | 12 | 12 x 15 x $\frac{3}{4}$ | 38.3 | 180 |
| 18 | 15 | 15 x 15 x $\frac{7}{8}$ | 55.8 | 225 |
| 20 | 15 | 15 x 18 x 1 | 76.5 | 270 |
| 24 | 15 | 15 x 18 x 1 | " | 270 |

SAFE BEARING VALUES OF WALL PLATES FOR VARIOUS STYLES OF MASONRY.

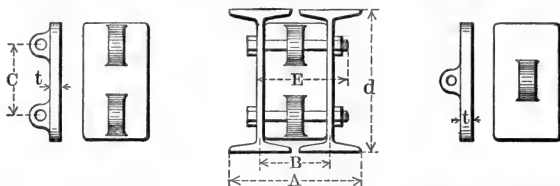
| Material. | Pounds per Sq. In. | Tons per Sq. Ft. |
|--|-----------------------|---------------------|
| Rubble Masonry in Cement Mortar..... | 250 | 18.0 |
| Brickwork " " " | 300 | 21.6 |
| First Class Sandstone (Dimension Stone) .. | 400 | 28.8 |
| " " Limestone | 500 | 36.0 |
| " " Granite | 600 | 43.2 |
| Portland Cement Concrete 1 : 2 : 4 | 600 | 43.2 |
| " " " 1 : 2 : 5 | 500 | 36.0 |

BEARING PLATES FOR I-BEAMS AND CHANNELS.

| Bearing on Wall. | Size of Plate. | Safe Bearing Value of Plate in 1000 Pounds. | | | | | | |
|------------------------|----------------------|---|-------------------------------|-------------------------|-------------------------|-------------------------|-------------------------|-------------------------|
| | | Rubble in Cement Mortar. | Brick in Cement Mortar. | Sand- stone. | Lime- stone. | Granite. | Concrete. 1:2:4. | Concrete. 1:2:5. |
| | | 250 lbs. per sq. in. | 300 lbs. per sq. in. | 400 lbs. per sq. in. | 500 lbs. per sq. in. | 600 lbs. per sq. in. | 600 lbs. per sq. in. | 500 lbs. per sq. in. |
| Ins. | Ins. | | | | | | | |
| 4 | 4 x 4 | 4.0 | 4.8 | 6.4 | 8.0 | 9.6 | 9.6 | 8.0 |
| 4 | 4 x 6 | 6.0 | 7.2 | 9.6 | 12.0 | 14.4 | 14.4 | 12.0 |
| 4 | 4 x 8 | 8.0 | 9.6 | 12.8 | 16.0 | 19.2 | 19.2 | 16.0 |
| 6 | 6 x 6 | 9.0 | 10.8 | 14.4 | 18.0 | 21.6 | 21.6 | 18.0 |
| 6 | 6 x 8 | 12.0 | 14.4 | 19.2 | 24.0 | 28.8 | 28.8 | 24.0 |
| 6 | 6 x 10 | 15.0 | 18.0 | 24.0 | 30.0 | 36.0 | 36.0 | 30.0 |
| 8 | 8 x 8 | 16.0 | 19.2 | 25.6 | 32.0 | 38.4 | 38.4 | 32.0 |
| 8 | 8 x 10 | 20.0 | 24.0 | 32.0 | 40.0 | 48.0 | 48.0 | 40.0 |
| 8 | 8 x 12 | 24.0 | 28.8 | 38.4 | 48.0 | 57.6 | 57.6 | 48.0 |
| 10 | 10 x 10 | 25.0 | 30.0 | 40.0 | 50.0 | 60.0 | 60.0 | 50.0 |
| 10 | 10 x 12 | 30.0 | 36.0 | 48.0 | 60.0 | 72.0 | 72.0 | 60.0 |
| 10 | 10 x 14 | 35.0 | 42.0 | 56.0 | 70.0 | 84.0 | 84.0 | 70.0 |
| 12 | 12 x 12 | 36.0 | 43.2 | 57.6 | 72.0 | 86.4 | 86.4 | 72.0 |
| 12 | 12 x 14 | 42.0 | 50.4 | 67.2 | 84.0 | 100.8 | 100.8 | 84.0 |
| 12 | 12 x 15 | 45.0 | 54.0 | 72.0 | 90.0 | 108.0 | 108.0 | 90.0 |
| 12 | 12 x 16 | 48.0 | 57.6 | 76.8 | 96.0 | 115.2 | 115.2 | 96.0 |
| 12 | 12 x 18 | 54.0 | 64.8 | 86.4 | 108.0 | 129.6 | 129.6 | 108.0 |
| 14 | 14 x 14 | 49.0 | 58.8 | 78.4 | 98.0 | 117.6 | 117.6 | 98.0 |
| 14 | 14 x 16 | 56.0 | 67.2 | 89.6 | 112.0 | 134.4 | 134.4 | 112.0 |
| 14 | 14 x 18 | 63.0 | 75.6 | 100.8 | 126.0 | 151.2 | 151.2 | 126.0 |
| 14 | 14 x 20 | 70.0 | 84.0 | 112.0 | 140.0 | 168.0 | 168.0 | 140.0 |
| 15 | 15 x 15 | 56.2 | 67.5 | 90.0 | 112.5 | 125.0 | 135.0 | 112.5 |
| 15 | 15 x 18 | 67.5 | 81.0 | 108.0 | 135.0 | 162.0 | 162.0 | 135.0 |
| 16 | 16 x 16 | 64.0 | 76.8 | 102.4 | 128.0 | 153.6 | 153.6 | 128.0 |
| 16 | 16 x 18 | 72.0 | 86.4 | 115.2 | 144.0 | 172.8 | 172.8 | 144.0 |
| 16 | 16 x 20 | 80.0 | 96.0 | 127.0 | 160.0 | 192.0 | 192.0 | 160.0 |
| 16 | 16 x 22 | 88.0 | 105.6 | 139.8 | 176.0 | 211.2 | 211.2 | 176.0 |
| 18 | 18 x 18 | 81.0 | 97.2 | 129.6 | 162.0 | 194.4 | 194.4 | 162.0 |
| 18 | 18 x 20 | 90.0 | 108.0 | 144.0 | 180.0 | 216.0 | 216.0 | 180.0 |
| 18 | 18 x 22 | 99.0 | 118.8 | 158.4 | 198.0 | 237.6 | 237.6 | 198.0 |
| 18 | 18 x 24 | 108.0 | 129.6 | 172.8 | 216.0 | 259.2 | 259.2 | 216.0 |
| 20 | 20 x 20 | 100.0 | 120.0 | 160.0 | 200.0 | 240.0 | 240.0 | 200.0 |
| 20 | 20 x 22 | 110.0 | 132.0 | 176.0 | 220.0 | 264.0 | 264.0 | 220.0 |
| 20 | 20 x 24 | 120.0 | 144.0 | 192.0 | 240.0 | 288.0 | 288.0 | 240.0 |
| 20 | 20 x 26 | 130.0 | 156.0 | 208.0 | 260.0 | 312.0 | 312.0 | 260.0 |

Safe Bearing Value of Plate = Area of Plate (in square inches) X Allowable Safe Bearing Value (per square inch) on the Masonry.

STANDARD CAST IRON SEPARATORS FOR I-BEAMS.



| Beams. | | | | Separators. | | | Bolts, Square Heads and Hex. Nuts. | | | | | |
|-------------------------|--------|------------------------|---------------------------------------|---------------------------------|------------|---------|--|-----------|---------------------------------|---------|------------------------------------|--|
| Section Num- ber. | Depth. | Weight per Foot. | Out to Out of Flanges of Beams. | Center to Cen- ter of Beams. | Thickness. | Weight. | Increase of Weight for each inch additional spread of beams. | Diameter. | Center to Cen- ter of Bolts. | Length. | Weight of Bolts and Nuts. | Increase of Weight of Bolts for each in. addi- tional spread of Beams. |
| | d | A | B | t | | C | | | E | | | |
| | In. | Pounds. | Inches. | Inches. | In. | Pounds. | | | Pounds. | In. | In. | |

SEPARATORS WITH ONE BOLT.

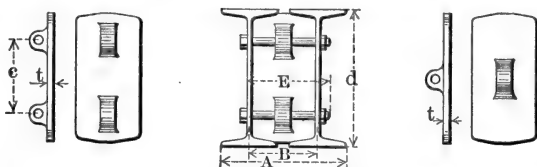
| | | | | | | | | | | | | |
|-------|----|-------|------------------|-----------------|---------------|-----|------|---------------|--|-----------------|------|------|
| B 5 | 3 | 5.5 | 5 $\frac{5}{16}$ | 3 | $\frac{3}{8}$ | 1.0 | .17 | $\frac{3}{8}$ | | 4 | .95 | .123 |
| B 9 | 4 | 7.5 | 5 $\frac{7}{8}$ | 3 $\frac{1}{4}$ | $\frac{1}{2}$ | 1.3 | .26 | $\frac{1}{2}$ | | 4 $\frac{1}{2}$ | 1.01 | " |
| B 13 | 5 | 9.75 | 6 $\frac{1}{2}$ | 3 $\frac{1}{2}$ | " | 1.8 | .36 | " | | 4 $\frac{3}{4}$ | 1.04 | " |
| B 17 | 6 | 12.25 | 7 $\frac{5}{8}$ | 4 | $\frac{1}{2}$ | 3.0 | .59 | " | | 5 $\frac{1}{4}$ | 1.11 | " |
| B 21 | 7 | 15.0 | 7 $\frac{7}{8}$ | 4 $\frac{1}{4}$ | " | 3.3 | .65 | " | | 5 $\frac{1}{2}$ | 1.14 | " |
| B 25 | 8 | 18.0 | 8 $\frac{1}{2}$ | 4 $\frac{1}{2}$ | " | 3.8 | .72 | " | | 5 $\frac{3}{4}$ | 1.17 | " |
| B 29 | 9 | 21.0 | 9 $\frac{5}{16}$ | 5 | " | 5.0 | .85 | " | | 6 $\frac{1}{4}$ | 1.23 | " |
| B 33 | 10 | 25.0 | 9 $\frac{7}{8}$ | 5 $\frac{1}{4}$ | " | 7.0 | .98 | " | | 6 $\frac{1}{2}$ | 1.26 | " |
| B 41 | 12 | 31.5 | 10 $\frac{3}{4}$ | 5 $\frac{3}{4}$ | " | 7.5 | 1.14 | " | | 7 | 1.32 | " |
| B 105 | 12 | 40.0 | 11 $\frac{1}{8}$ | 6 | " | 7.5 | 1.14 | " | | 7 $\frac{1}{2}$ | 1.38 | " |

SEPARATORS WITH TWO BOLTS.

| | | | | | | | | | | | | |
|-------|----|-------|------------------|-----------------|---------------|------|------|---------------|-----------------|-----------------|------|------|
| B 41 | 12 | 31.5 | 10 $\frac{3}{4}$ | 5 $\frac{3}{4}$ | $\frac{1}{2}$ | 7.8 | 1.20 | $\frac{3}{4}$ | 6 $\frac{1}{2}$ | 7 | 2.64 | .246 |
| B 105 | 12 | 40.0 | 11 $\frac{1}{8}$ | 6 | " | 7.8 | 1.20 | " | " | 7 $\frac{1}{2}$ | 2.76 | " |
| B 53 | 15 | 42.0 | 11 $\frac{3}{4}$ | 6 $\frac{1}{4}$ | " | 11.5 | 1.50 | " | 7 | 7 $\frac{3}{4}$ | 2.82 | " |
| B 109 | 15 | 60.0 | 12 $\frac{1}{2}$ | 6 $\frac{1}{2}$ | " | 11.5 | 1.50 | " | " | 8 $\frac{1}{4}$ | 2.95 | " |
| B 113 | 15 | 80.0 | 13 | 6 $\frac{3}{4}$ | " | 11.5 | 1.50 | " | " | 9 | 3.13 | " |
| B 65 | 18 | 55.0 | 12 $\frac{3}{4}$ | 6 $\frac{3}{4}$ | $\frac{5}{8}$ | 16.5 | 2.38 | " | 9 | 8 $\frac{1}{2}$ | 2.95 | " |
| B 73 | 20 | 65.0 | 13 $\frac{1}{4}$ | 7 | " | 17.5 | 2.60 | " | 10 | 8 $\frac{1}{2}$ | 3.01 | " |
| B 121 | 20 | 80.0 | 14 $\frac{1}{8}$ | 7 $\frac{1}{4}$ | " | 17.5 | 2.60 | " | " | 9 $\frac{1}{4}$ | 3.19 | " |
| B 89 | 24 | 80.0 | 14 $\frac{3}{4}$ | 7 $\frac{3}{4}$ | " | 25.5 | 3.25 | " | 12 | 9 $\frac{1}{4}$ | 3.19 | " |
| B 127 | 24 | 105.0 | 16 | 8 $\frac{1}{8}$ | " | 25.5 | 3.25 | " | " | 9 $\frac{1}{2}$ | 3.26 | " |

Lengths and weights of separator bolts in above table are for girders composed of two beams of minimum section as shown. Lengths of bolts for intermediate and maximum sizes of beams may be obtained by adding twice the increase of web thickness to the lengths given.

SPECIAL CAST IRON SEPARATORS FOR I-BEAMS.



| Beams. | | | | | Separators. | | | Bolts, Square Heads and Hex. Nuts. | | | | |
|-----------------|--------|------------|---------------------------------|----------------------------|-------------|---------|--|------------------------------------|----------------------------|---------|---------------------|--|
| Section Number. | Depth. | Weight per | Out to Out of Flanges of Beams. | Center to Center of Beams. | Thickness. | Weight. | Increase of Weight for each inch additional spread of Beams. | Diameter. | Center to Center of Bolts. | Length. | Weight of Bolts and | Increase of Weight of Bolts for each in. additional spread of Beams. |
| | Foot. | | | | | | | | | | | |
| | d | A | B | t | | | | | C | E | Nuts. | |
| | In. | Pounds. | Inches. | Inches. | In. | Pounds. | Pounds. | In. | Ins. | Ins. | Pounds. | Pound |

SEPARATORS WITH ONE BOLT.

| | | | | | | | | | | | | |
|-------|----|-------|-----------------|----------------|---------------|-----|------|---------------|--|----------------|------|------|
| B 5 | 3 | 5.5 | $5\frac{5}{16}$ | 3 | $\frac{3}{8}$ | 1.1 | .29 | $\frac{3}{4}$ | | 4 | .95 | .123 |
| B 9 | 4 | 7.5 | $5\frac{7}{8}$ | $3\frac{1}{4}$ | " | 1.6 | .38 | $\frac{3}{4}$ | | $4\frac{1}{2}$ | 1.01 | " |
| B 13 | 5 | 9.75 | $6\frac{1}{2}$ | $3\frac{1}{2}$ | " | 2.0 | .49 | " | | $4\frac{3}{4}$ | 1.04 | " |
| B 17 | 6 | 12.25 | $7\frac{5}{16}$ | 4 | $\frac{1}{2}$ | 3.3 | .78 | " | | $5\frac{1}{4}$ | 1.11 | " |
| B 21 | 7 | 15.0 | $7\frac{7}{8}$ | $4\frac{1}{4}$ | " | 3.9 | .92 | " | | $5\frac{1}{2}$ | 1.14 | " |
| B 25 | 8 | 18.0 | $8\frac{1}{2}$ | $4\frac{1}{2}$ | " | 4.7 | 1.06 | " | | $5\frac{3}{4}$ | 1.17 | " |
| B 29 | 9 | 21.0 | $9\frac{5}{16}$ | 5 | " | 5.9 | 1.20 | " | | $6\frac{1}{4}$ | 1.23 | " |
| B 33 | 10 | 25.0 | $9\frac{7}{8}$ | $5\frac{1}{4}$ | " | 6.8 | 1.33 | " | | $6\frac{1}{2}$ | 1.26 | " |
| B 41 | 12 | 31.5 | $10\frac{3}{4}$ | $5\frac{3}{4}$ | " | 8.8 | 1.61 | " | | 7 | 1.32 | " |
| B 105 | 12 | 40.0 | $11\frac{1}{4}$ | 6 | " | 8.9 | 1.58 | " | | $7\frac{1}{2}$ | 1.38 | " |

SEPARATORS WITH TWO BOLTS.

| | | | | | | | | | | | | |
|-------|----|-------|-----------------|----------------|---------------|------|------|---------------|----------------|----------------|------|------|
| B 41 | 12 | 31.5 | $10\frac{3}{4}$ | $5\frac{3}{4}$ | $\frac{1}{2}$ | 9.5 | 1.61 | $\frac{3}{4}$ | $6\frac{1}{2}$ | 7 | 2.64 | .246 |
| B 105 | 12 | 40.0 | $11\frac{1}{4}$ | 6 | " | 9.5 | 1.58 | " | " | $7\frac{1}{2}$ | 2.76 | " |
| B 53 | 15 | 42.0 | $11\frac{3}{4}$ | $6\frac{1}{4}$ | " | 12.5 | 2.02 | " | 7 | $7\frac{3}{4}$ | 2.82 | " |
| B 109 | 15 | 60.0 | $12\frac{3}{4}$ | $6\frac{3}{4}$ | " | 13.0 | 1.97 | " | " | $8\frac{1}{4}$ | 2.95 | " |
| B 113 | 15 | 80.0 | $13\frac{5}{8}$ | $7\frac{1}{4}$ | " | 13.2 | 1.91 | " | " | 9 | 3.13 | " |
| B 65 | 18 | 55.0 | $12\frac{3}{4}$ | $6\frac{3}{4}$ | $\frac{5}{8}$ | 19.8 | 2.41 | " | 9 | $8\frac{1}{4}$ | 2.95 | " |
| B 73 | 20 | 65.0 | $13\frac{1}{4}$ | 7 | " | 22.9 | 3.37 | " | 10 | $8\frac{1}{2}$ | 3.01 | " |
| B 121 | 20 | 80.0 | $14\frac{3}{4}$ | $7\frac{3}{4}$ | " | 24.6 | 3.34 | " | " | $9\frac{1}{4}$ | 3.19 | " |
| B 89 | 24 | 80.0 | $14\frac{3}{4}$ | $7\frac{3}{4}$ | " | 30.3 | 4.07 | " | 12 | $9\frac{1}{4}$ | 3.19 | " |
| B 127 | 24 | 105.0 | $16\frac{1}{2}$ | $8\frac{5}{8}$ | " | 32.5 | 4.07 | " | " | $9\frac{1}{2}$ | 3.26 | " |

Lengths and weights of separator bolts in above table are for girders composed of two beams of minimum section as shown. Lengths of bolts for intermediate and maximum sizes of beams may be obtained by adding twice the increase of web thickness to the lengths given.

FIREPROOF CONSTRUCTION.

Buildings of fireproof construction consist essentially of a steel frame or skeleton to support the floors, and in the case of high buildings, the outside walls also are carried by the steel framing. All parts of the steel work are enclosed and protected by some fire-resisting material, which should be of such quality and arrangement as not to disintegrate or fall away when heated to high temperatures and at the same time exposed to a stream of cold water. The fireproofing for the floors, in addition to its ability to afford a fireproof protection to the steel beams, must be capable of supporting the load and distributing it to the floor beams, which in turn transmit it to the columns and thence to the foundations.

One of the earlier forms of floors consists of brick arches built between and supported by the bottom flanges and lower portions of the web of iron or steel I-Beams, but this style has considerable dead weight and, as ordinarily constructed, does not provide fireproof protection for the bottom flanges of the beams. Another of the earlier forms of floor is composed of sheets of corrugated iron arched between the beams, on which a concrete filling is placed, and this also, as ordinarily constructed, does not provide protection for the bottom flanges of the beams, besides, it is quite heavy.

A later style of floor is the hollow tile system, which is composed of flat or segmental arches constructed of moulded blocks of hard burned clay, specially shaped, and of various depths to suit different loads and the sizes of the I-Beams supporting them. In the hollow tile system, the blocks may also be of porous terra-cotta which is lighter than hard clay.

Various other systems of fireproofing are now in use, the most usual forms of which consist of cement, concrete or other material used alone or deposited or arranged about a strengthening or supporting framework of steel shapes, bars, rods, wire, wire-cloth, etc.

Column or girder fireproofing may be accomplished by the use of hard clay or porous terra-cotta blocks shaped to fit and enclose the steel work, or the steel may be wrapped with wire, wire-cloth, metal lath, etc., and a concrete or plastered coating applied to it.

Fireproof partitions may be constructed of hollow tile composed of hard clay or porous terra-cotta to which the plaster finish may be directly applied, or they may be composed of suitable metal studding on which is secured the wire-cloth or metal lath that serves to support the concrete or other fireproofing, the surface then being plastered in the usual manner.

The dead weights of fireproof floors vary between wide limits dependent upon the system employed, the load to be carried and the distance between the supporting beams.

WEIGHTS OF HOLLOW TILE FLOOR ARCHES AND FIREPROOF MATERIALS.

END CONSTRUCTION, FLAT ARCH.

| Width of Span between Beams. | Depth of Arch. | Weight per Square Foot. |
|------------------------------|----------------|-------------------------|
| 5 feet to 6 feet. | 8 inches. | 27 pounds. |
| 6 " 7 " | 9 " | 29 " |
| 7 " 8 " | 10 " | 33 " |
| 8 " 9 " | 12 " | 38 " |

HOLLOW BRICK FOR FLAT ARCHES.

(SIDE CONSTRUCTION.)

| Width of Span between Beams. | Depth of Arch. | Weight per Square Foot. |
|-------------------------------------|----------------|-------------------------|
| 3 feet 6 inches to 4 feet 0 inches. | 6 inches. | 27 pounds. |
| 4 " 0 " 4 " 6 " | 7 " | 29 " |
| 4 " 6 " 5 " 0 " | 8 " | 32 " |
| 5 " 6 " 6 " 0 " | 9 " | 36 " |
| 6 " 0 " 6 " 6 " | 10 " | 39 " |
| 6 " 6 " 7 " 0 " | 12 " | 44 " |

PARTITIONS.

| | Thickness. | Weight per Square Foot. |
|---------------------------------|------------|-------------------------|
| Hollow Brick (Clay) Partitions. | 2 inches. | 11 pounds. |
| " " " " | 3 " | 14 " |
| " " " " | 4 " | 15 " |
| " " " " | 5 " | 19 " |
| " " " " | 6 " | 20 " |
| " " " " | 8 " | 27 " |
| Porous Terra-Cotta Partitions. | 3 " | 16 " |
| " " " " | 4 " | 19 " |
| " " " " | 5 " | 22 " |
| " " " " | 6 " | 23 " |
| " " " " | 8 " | 33 " |

FURRING, ROOFING AND CEILING.

| | Thickness. | Weight per Square Foot. |
|-----------------------------|------------|-------------------------|
| Porous Terra-Cotta Furring. | 2 inches. | 8 pounds. |
| " " " Roofing. | 2 " | 12 " |
| " " " " | 3 " | 14 " |
| " " " " | 4 " | 18 " |
| " " " Ceiling. | 2 " | 11 " |
| " " " " | 3 " | 14 " |
| " " " " | 4 " | 18 " |

6-inch Segmental Arches, $26\frac{1}{2}$ pounds per square foot.

8- " " " " 32 " " " "

2- " Porous Terra-Cotta Partition, 8 pounds per square foot.

8' x $3\frac{1}{4}$ ' x $2\frac{1}{4}$ ' Hollow Brick, 3000 lbs. per 1000.

TABLES OF SAFE LOADS—TERRA COTTA FLOOR ARCHES.

The Table of Safe Loads for Flat Arches, page 71, is applicable to all shapes of blocks. The areas given are obtained by passing a plane through the blocks at right angles to all the webs and are the areas for 1-foot width of arch. Generally speaking, end construction blocks of various shapes, but of the same depth and cross sectional area, have equal strength. The weight of the arch has not been deducted in Table of Safe Loads for Flat Arches. Therefore, this and other dead loads must be deducted to obtain the net safe live load for any arch and span.

EXAMPLE.—What load will an 8-inch arch carry (using a Factor of Safety of 5), for a span of 5 feet 6 inches, the blocks having a sectional area parallel to the beams, of 44.25 square inches?

Area of 8-inch block in Table = 37 sq. ins.

$44.25 \div 37 = 1.19$, Ratio of Actual Area to Tabular Area.

Safe Load in Table = 228, $\times 1.19 = 271$ pounds = Safe Load for Actual Area.

Weight of Arch = $44.25 \times 12 = 531$ cu. in. $\times .06 = 32$ lbs. per sq. ft.

$271 - 32 = 239$ lbs. = Safe Load in lbs. per sq. ft. for S. F. of 7.

$271 \times 7 \div 5 = 379$, $- 32 = 347$ lbs., Safe Load for S. F. of 5.

Tables of Safe Loads for Segmental Arches in spans up to 10 feet are given on pages 72 and 73. The areas of the blocks for which the safe loads are given are the areas per foot of arch parallel with beams. The weight of the arch blocks has been deducted in the Table, so that only the dead load of concrete fill, plastering, etc., must be deducted to obtain net live load.

Segmental arch construction is cheaper than flat arch construction, and is the stronger of the two. Where for any reason a flat arch is not deemed necessary, this is an admirable floor construction to use.

Even with this type of construction, the flat ceiling may be secured by suspending a metal lath ceiling below the arch from the bottom of the beams. To do this, however, adds so much to the cost that it is generally cheaper to use the Flat Arch.

Segmental Arches can also be built with a raised skew. This flattens the arch and reduces the amount and consequently the expense of the cinder concrete fill, but it also reduces the strength of the arch.

In Segmental Arches, the thrust on the beams (particularly at the bottom of beams) is very great, and where there is any doubt of the beams' sustaining the thrust, it is desirable to use steel tie rods. These tie rods may be fireproofed or left unprotected, the best practice being to protect them.

SAFE LOADS FOR FLAT FLOOR ARCHES OF SEMI-POROUS TERRA COTTA.

As given by manufacturers of this material.

Safety Factor 7.

| ARCHES. | 6 ins. | 7 ins. | 8 ins. | 9 ins. | 10 ins. | 12 ins. | 15 ins. |
|-------------|-------------------------|--------|--------|--------|---------|---------|---------|
| AREAS. | Square Inches. | | | | | | |
| | 31 | 34 | 37 | 40 | 43 | 49 | 58 |
| SPANS. | Pounds per Square Foot. | | | | | | |
| 1 Ft. 6 In. | 1928 | 2468 | 3069 | 3733 | 4459 | 6097 | 9022 |
| 2 " 0 " | 1085 | 1388 | 1726 | 2100 | 2508 | 3430 | 5075 |
| 2 " 6 " | 694 | 888 | 1104 | 1344 | 1605 | 2195 | 3248 |
| 3 " 0 " | 482 | 617 | 767 | 933 | 1114 | 1524 | 2255 |
| 3 " 3 " | 410 | 525 | 650 | 795 | 950 | 1299 | 1922 |
| 3 " 6 " | 354 | 453 | 563 | 685 | 819 | 1120 | 1657 |
| 3 " 9 " | 308 | 394 | 491 | 597 | 713 | 975 | 1443 |
| 4 " 0 " | 271 | 347 | 431 | 525 | 627 | 857 | 1268 |
| 4 " 3 " | 240 | 307 | 382 | 465 | 555 | 759 | 1124 |
| 4 " 6 " | 214 | 274 | 341 | 414 | 495 | 677 | 1002 |
| 4 " 9 " | 192 | 246 | 306 | 372 | 444 | 608 | 900 |
| 5 " 0 " | 173 | 222 | 276 | 336 | 401 | 548 | 812 |
| 5 " 3 " | 157 | 201 | 250 | 304 | 364 | 497 | 736 |
| 5 " 6 " | 143 | 183 | 228 | 277 | 331 | 453 | 671 |
| 5 " 9 " | 131 | 168 | 208 | 254 | 303 | 415 | 614 |
| 6 " 0 " | 120 | 154 | 191 | 233 | 278 | 381 | 563 |
| 6 " 3 " | 111 | 142 | 176 | 215 | 256 | 351 | 519 |
| 6 " 6 " | | 131 | 163 | 198 | 237 | 324 | 480 |
| 6 " 9 " | | 121 | 151 | 184 | 220 | 301 | 445 |
| 7 " 0 " | | 113 | 140 | 171 | 204 | 280 | 414 |
| 7 " 6 " | | | 122 | 149 | 178 | 243 | 360 |
| 8 " 0 " | | | 107 | 131 | 156 | 214 | 317 |
| 8 " 6 " | | | | 116 | 138 | 190 | 281 |
| 9 " 0 " | | | | 108 | 123 | 169 | 250 |
| 9 " 6 " | | | | | 111 | 152 | 225 |
| 10 " 0 " | | | | | 100 | 137 | 203 |
| 10 " 6 " | | | | | | 124 | 184 |
| 11 " 0 " | | | | | | 113 | 167 |
| 11 " 6 " | | | | | | 103 | 153 |
| 12 " 0 " | | | | | | 95 | 141 |

Above Safe Loads include weight of arch blocks and other dead load. Average weight of arch blocks (lbs. per sq. ft. of arch) = Sectional Area $\times 12 \times .06$. Below heavy lines, spans should be used for ceiling arches only.

SAFE LOADS FOR TERRA COTTA SEGMENTAL FLOOR ARCHES.

As given by manufacturers of this material.

Weight of Arch Blocks not included.

Factor of Safety 7.

| ARCHES. | | 4 ins. | 6 ins. | 8 ins. | 10 ins. |
|----------|----------------|-------------------------|--------|--------|---------|
| AREAS. | | Square Inches. | | | |
| | | 28 | 36 | 43 | 47 |
| SPANS. | RISE. | Pounds per Square Foot. | | | |
| Ft.-ins. | Inches. | | | | |
| 4-0 | $\frac{3}{4}$ | 702 | 902 | 1078 | 1178 |
| | 1 | 920 | 1148 | 1414 | 1545 |
| | $1\frac{1}{4}$ | 1155 | 1485 | 1774 | 1939 |
| | $1\frac{1}{2}$ | 1353 | 1740 | 2079 | 2272 |
| | $1\frac{3}{4}$ | 1545 | 1986 | 2373 | 2593 |
| | 2 | 1736 | 2233 | 2667 | 2915 |
| 4-6 | $\frac{3}{4}$ | 616 | 792 | 946 | 1034 |
| | 1 | 812 | 1044 | 1247 | 1363 |
| | $1\frac{1}{4}$ | 1020 | 1313 | 1568 | 1713 |
| | $1\frac{1}{2}$ | 1196 | 1539 | 1838 | 2009 |
| | $1\frac{3}{4}$ | 1381 | 1775 | 2121 | 2318 |
| | 2 | 1536 | 1975 | 2359 | 2578 |
| 5-0 | $\frac{3}{4}$ | 551 | 709 | 847 | 926 |
| | 1 | 744 | 951 | 1143 | 1249 |
| | $1\frac{1}{4}$ | 911 | 1172 | 1400 | 1530 |
| | $1\frac{1}{2}$ | 1072 | 1379 | 1647 | 1800 |
| | $1\frac{3}{4}$ | 1238 | 1592 | 1902 | 2078 |
| | 2 | 1379 | 1773 | 2118 | 2315 |
| 5-6 | $\frac{3}{4}$ | 499 | 641 | 766 | 837 |
| | 1 | 672 | 864 | 1032 | 1128 |
| | $1\frac{1}{4}$ | 826 | 1062 | 1269 | 1387 |
| | $1\frac{1}{2}$ | 984 | 1266 | 1512 | 1652 |
| | $1\frac{3}{4}$ | 1119 | 1439 | 1719 | 1879 |
| | 2 | 1258 | 1619 | 1933 | 2113 |
| 6-0 | $\frac{3}{4}$ | 455 | 585 | 699 | 764 |
| | 1 | 612 | 788 | 941 | 1028 |
| | $1\frac{1}{4}$ | 753 | 969 | 1157 | 1265 |
| | $1\frac{1}{2}$ | 898 | 1154 | 1379 | 1507 |
| | $1\frac{3}{4}$ | 1022 | 1315 | 1570 | 1716 |
| | 2 | 1148 | 1476 | 1763 | 1927 |
| 6-6 | $\frac{3}{4}$ | 428 | 551 | 658 | 719 |
| | 1 | 562 | 724 | 864 | 944 |
| | $1\frac{1}{4}$ | 701 | 902 | 1077 | 1177 |
| | $1\frac{1}{2}$ | 823 | 1058 | 1264 | 1382 |
| | $1\frac{3}{4}$ | 947 | 1218 | 1455 | 1590 |
| | 2 | 1055 | 1358 | 1622 | 1772 |
| 7-0 | $\frac{3}{4}$ | 394 | 508 | 606 | 662 |
| | 1 | 520 | 669 | 799 | 873 |
| | $1\frac{1}{4}$ | 648 | 834 | 996 | 1089 |

SAFE LOADS FOR TERRA COTTA SEGMENTAL FLOOR ARCHES.

As given by manufacturers of this material.

Weight of Arch Blocks not included.

Factor of Safety 7.

| ARCHES. | | 4 ins. | 6 ins. | 8 ins. | 10 ins. |
|----------|---------|-------------------------|--------|--------|---------|
| AREAS. | | Square Inches. | | | |
| | | 28 | 36 | 43 | 47 |
| SPANS. | RISE. | Pounds per Square Foot. | | | |
| Ft.-ins. | Inches. | | | | |
| 7-0 | 1½ | 762 | 981 | 1171 | 1280 |
| | 1¾ | 876 | 1127 | 1346 | 1471 |
| | 2 | 988 | 1264 | 1510 | 1650 |
| 7-6 | ¾ | 366 | 471 | 563 | 615 |
| | 1 | 482 | 621 | 741 | 810 |
| | 1¼ | 602 | 774 | 925 | 1011 |
| | 1½ | 715 | 920 | 1099 | 1201 |
| | 1¾ | 815 | 1049 | 1253 | 1369 |
| 8-0 | 2 | 915 | 1176 | 1405 | 1536 |
| | ¾ | 341 | 439 | 525 | 573 |
| | 1 | 457 | 588 | 703 | 768 |
| | 1¼ | 562 | 724 | 864 | 944 |
| | 1½ | 668 | 859 | 1026 | 1122 |
| 8-6 | 1¾ | 767 | 987 | 1179 | 1288 |
| | 2 | 854 | 1099 | 1312 | 1434 |
| | ¾ | 319 | 411 | 491 | 536 |
| | 1 | 428 | 551 | 658 | 719 |
| | 1¼ | 527 | 678 | 810 | 885 |
| 9-0 | 1½ | 626 | 806 | 963 | 1052 |
| | 1¾ | 719 | 926 | 1106 | 1203 |
| | 2 | 807 | 1037 | 1239 | 1354 |
| | ¾ | 300 | 386 | 461 | 504 |
| | 1 | 403 | 518 | 619 | 677 |
| 9-6 | 1¼ | 501 | 645 | 770 | 842 |
| | 1½ | 590 | 758 | 906 | 990 |
| | 1¾ | 677 | 871 | 1041 | 1137 |
| | 2 | 759 | 977 | 1167 | 1275 |
| | ¾ | 283 | 364 | 435 | 475 |
| 10-0 | 1 | 380 | 489 | 584 | 638 |
| | 1¼ | 472 | 608 | 726 | 793 |
| | 1½ | 561 | 721 | 862 | 942 |
| | 1¾ | 639 | 823 | 983 | 1074 |
| | 2 | 717 | 923 | 1102 | 1204 |
| 10-6 | ¾ | 267 | 344 | 411 | 449 |
| | 1 | 359 | 462 | 552 | 603 |
| | 1¼ | 447 | 576 | 688 | 751 |
| | 1½ | 531 | 683 | 816 | 892 |
| | 1¾ | 610 | 784 | 937 | 1024 |
| 10-0 | 2 | 683 | 879 | 1050 | 1147 |

TESTS OF FLOOR ARCHES.

A summary of the principal data and results of tests which were the subject of a paper entitled "Tests of Fire-proof Flooring Material," published in the *Transactions of the American Society of Civil Engineers*, Vols. xxxiv and xxxv, is given in the following table:

BREAKING LOAD OF HOLLOW TILE ARCHES.

| Depth of Arch. | Rise. | Span. | Length. | Total Load. | Load per Sq. Foot. | Total Horizontal Thrust. | Horizontal Thrust per Ft. of Arch. | BLOCKS. | | Character of Load. | Manner of Laying Joints. |
|----------------|-------|-------|---------|-------------|--------------------|--------------------------|------------------------------------|---------|-----------|--------------------|--------------------------|
| | | | | | | | | Style. | Material. | | |
| Ins. | Ins. | Ins. | Ins. | Lbs. | Lbs. | Lbs. | | | | | |
| 6. | 3.5 | 60 | 48. | 13750 | 688 | 29474 | 7369 | E | Hard | Dis. | Port. |
| 7.5 | 5. | 46 | 11.5 | 9000 | 2452 | 10367 | 10818 | " | " | " | N.M. |
| 7.5 | 5. | 60 | 35.2 | 11250 | | 33750 | 11505 | " | " | Cen. | Port. |
| 7.5 | 5. | 60 | 36.5 | 13000 | | 39000 | 12822 | " | Porous | " | " |
| 8. | 7. | 60 | 38.25 | 14500 | | 31071 | 9747 | " | " | " | " |
| 8. | 7. | 60 | 38.25 | 15750 | | 33750 | 10588 | " | Hard | " | " |
| 12. | 10. | 60 | 41. | 16400 | | 24600 | 7200 | " | " | " | " |
| 12. | 8.75 | 60 | 10. | 3100 | | 5314 | 6377 | " | " | " | N.M. |
| 12. | 9. | 60 | 10. | 5000 | | 8333 | 10000 | " | " | " | " |
| 12. | 9. | 60 | 10. | 15100 | 3630 | 12583 | 15100 | " | " | Dis. | " |
| 12. | 9.5 | 60 | 10. | 2500 | | 3947 | 4736 | " | " | Cen. | |
| 8. | 5.5 | 46 | 11.5 | 2500 | 681 | 2614 | 2727 | S | " | Dis. | N.M. |
| 8. | 5. | 45 | 11.5 | 1300 | 362 | 1463 | 1526 | " | " | " | " |
| 8. | 6. | 60 | 36. | 10000 | | 25000 | 8333 | " | " | Cen. | Port. |
| 8. | 5. | 60 | 36. | 5700 | 380 | 8550 | 2850 | " | " | Dis. | " |
| 8. | 5. | 60 | 12. | 3500 | 700 | 5250 | 5250 | " | " | " | N.M. |
| 8. | 5.5 | 60 | 12. | 10000 | 2000 | 13636 | 13636 | " | " | " | " |
| 8. | 5.5 | 60 | 12. | 2500 | | 6818 | 6818 | " | " | Cen. | " |
| 8. | 5.5 | 60 | 24. | 9950 | 995 | 13568 | 6784 | " | " | Dis. | " |
| 8. | 5.5 | 60 | 24. | 2500 | | 6818 | 3209 | " | " | Cen. | " |
| 10. | 7.5 | 60 | 36. | 13500 | 900 | 13500 | 4500 | " | " | Dis. | Port. |
| 10. | 8. | 60 | 37. | 14500 | 940 | 13594 | 4408 | " | " | " | |

NOTE.—In the above table the following abbreviations are used: "E," End Construction; "S," Side Construction; "Hard," Hard Clay; "Porous," Porous Terra-Cotta; "Dis.," Distributed Load; "Cen.," Concentrated Load at Center; "Port.," Portland Cement, and "N. M.," No Mortar.

The Loads per Sq. Foot in the above table were obtained in all cases by dividing the Total Load by the superficial area of the arch in square feet. The Horizontal Thrust for Distributed and Central Loads was obtained by formulæ similar to those given therefor on the following page, and for Central Loads this is double that for a Distributed Load of the same weight.

THRUST OF ARCHES.

The horizontal thrust of segmental floor arches, on the assumption of uniform loading, may be found by the following formula:

$$T = \frac{3WL^2}{2R}$$

in which

T = pressure or thrust in pounds per lineal foot of arch.

W = load on arch in pounds per square foot, uniformly distributed.

L = span of arch in feet.

R = rise of segmental arch in inches.

For a concentrated load at the center, of weight P, the thrust

$$T = \frac{3PL}{R}$$

For arches with flat tops and bottoms, such as are used in floors, the voussoir joints on each side of the central key are usually laid out on parallel lines, and in these cases the thrust may be determined approximately by using for R, in the above formula, the effective depth of the arch, which is somewhat less than the nominal depth, as indicated on page 77.

For segmental arches the rise R is the vertical distance from the highest part of the intrados to the plane of the springing line. If the radius of the intrados for segmental arches is r, the rise may be obtained from the following formula:

$$R = r - \sqrt{r^2 - \frac{L^2}{4}}$$

$$\text{conversely, } r = \frac{R}{2} + \frac{L^2}{8R}$$

TIE RODS.

Although in the completed structure the horizontal thrusts of adjoining arches may counterbalance each other, the tie rods should be so proportioned and spaced as to withstand the entire thrust of the arches, thus tying the structure together and facilitating the construction.

SPACING OF TIE RODS FOR TILE ARCHES.

The table on the next page was computed from the following formula, which was obtained from that giving the thrust of arches on page 75.

$$B = \frac{A \times R \times 10\,000}{WL^2}$$

in which

B = spacing of tie rods in feet.

A = net area of rod in square inches.

R = rise of arch in inches.

W = load in pounds per square foot of the arch.

L = span of arch in feet.

The above formula gives the spacing of tie rods corresponding to a tensile stress in the rods of 15 000 pounds per square inch, without considering the flexure of the beams.

In spacing tie rods, the lateral strength of beams, for flexure due to the thrust of the arches, should be taken into consideration, explanations for which are given on pages 78 to 81 inclusive.

Spacings for other loads than that of the table may be found by proportion, thus:

Required spacing =

$$\frac{100 + \text{weight of arch in pounds per square foot}}{\text{New load in lbs. per sq. ft.} + \text{weight of arch in lbs. per sq. ft.}} \times \text{spacing from table.}$$

Weights of tile arches per square foot are given on page 69.

As noted under the heading "Lateral Strength of Beams," on pages 82 and 83, care should be taken that the spacing of tie rods is not greater than twenty times the least flange width, otherwise the safe loads should be reduced to compensate for the strains produced by flexure of the upper flange considered as a column in compression.

SPACING OF TIE RODS FOR TILE ARCHES IN FEET.

For a uniform load of 100 lbs. per square foot in addition to the weight of the arch.

| Span of Arch. | Diameter of Tie Rods. | Nominal Depth of Arch. Inches. | | | | | |
|---------------|-----------------------|---|------|------|------|------|------|
| | | 6 | 7 | 8 | 9 | 10 | 12 |
| | | Effective Depth or Rise of Arch. Inches. | | | | | |
| Feet. | Inch. | 3.6 | 4.6 | 5.6 | 6.6 | 7.6 | 9.6 |
| 3 | $\frac{5}{8}$ | 6.4 | 8.0 | 9.5 | 10.9 | 12.3 | 15.0 |
| " | $\frac{3}{4}$ | 9.5 | 12.0 | 14.2 | 16.3 | 18.3 | 22.4 |
| " | $\frac{7}{8}$ | 13.2 | 16.6 | 19.8 | 22.6 | 25.5 | 31.1 |
| 4 | $\frac{5}{8}$ | 3.6 | 4.5 | 5.4 | 6.1 | 6.9 | 8.4 |
| " | $\frac{3}{4}$ | 5.4 | 6.7 | 8.0 | 9.2 | 10.3 | 12.6 |
| " | $\frac{7}{8}$ | 7.4 | 9.4 | 11.1 | 12.7 | 14.3 | 17.5 |
| 5 | $\frac{5}{8}$ | 2.3 | 2.9 | 3.4 | 3.9 | 4.4 | 5.4 |
| " | $\frac{3}{4}$ | 3.4 | 4.3 | 5.1 | 5.9 | 6.6 | 8.0 |
| " | $\frac{7}{8}$ | 4.8 | 6.0 | 7.1 | 8.1 | 9.2 | 11.2 |
| 6 | $\frac{5}{8}$ | .. | 2.0 | 2.4 | 2.7 | 3.1 | 3.7 |
| " | $\frac{3}{4}$ | .. | 3.0 | 3.6 | 4.1 | 4.6 | 5.6 |
| " | $\frac{7}{8}$ | .. | 4.2 | 4.9 | 5.7 | 6.4 | 7.8 |
| 7 | $\frac{5}{8}$ | .. | .. | .. | 2.0 | 2.3 | 2.8 |
| " | $\frac{3}{4}$ | .. | .. | .. | 3.0 | 3.4 | 4.1 |
| " | $\frac{7}{8}$ | .. | .. | .. | 4.2 | 4.7 | 5.7 |
| 8 | $\frac{5}{8}$ | .. | .. | .. | .. | 1.7 | 2.1 |
| " | $\frac{3}{4}$ | .. | .. | .. | .. | 2.6 | 3.1 |
| " | $\frac{7}{8}$ | .. | .. | .. | .. | 3.6 | 4.4 |

Spacings below heavy lines apply to greater spans than are recommended for that depth of arch.

LATERAL STRENGTH OF BEAMS TO RESIST FLEXURE DUE TO THRUST OF ARCHES, ETC.

In special cases where the thrust of a floor arch is exerted against a beam, channel, angle or other shape without other lateral support than the tie rods, or braces, this will produce lateral flexure and stresses in addition to those caused by the vertical loading. Throughout the body of the floor the thrusts of the adjoining arches, when completed, will usually counterbalance each other, but in the outer beams around shafts or elsewhere, if unsupported sideways, the stresses due to the lateral forces should be considered.

The total allowable stress per square inch for the extreme fibres of beams has been placed at 16 000 pounds per square inch, and in order that this may not be exceeded owing to lateral stresses, the stress due to vertical loading should be correspondingly reduced so that the resultant intensity shall not exceed the allowable limit. This may be calculated by considering the beam as continuous and laterally supported at intervals by the tie rods, the spans being equal to the spacing of the rods.

In this case the fibre stress due to the lateral forces is:

$$p' = \frac{wx_1B^2}{I'} \quad (1)$$

in which

p' = fibre stress in pounds per square inch due to lateral forces.

w = lateral load or thrust in pounds per lineal foot of section used as a beam.

x_1 = distance of the extreme fibre from the neutral axis in inches.

B = distance between tie rods or lateral supports in feet.

I' = moment of inertia about the vertical axis of the section or that one at right angles to the line of application of the lateral forces.

For I-Beams with the web placed vertically, as usual, x_1 becomes equal to $\frac{b}{2}$, where b is the width of the flange in inches.

In this case the above formula for intensity of unit stress due to lateral load becomes:

$$p' = \frac{wbB^2}{2 I'} \quad (2)$$

In order that the total resultant intensity of unit stress shall not exceed the allowable limit of 16 000 pounds per square inch, the stress due to vertical loading must be reduced by the amount of the intensity of stress due to the horizontal thrust of the arch, as determined by formula (2).

If p' represents the intensity of unit stress due to the horizontal thrust of the arch, and p the corresponding allowable intensity of unit stress due to the vertical loading, then

$$* p = 16\,000 - p'$$

Having thus obtained the reduced vertical stress p , the safe vertical load of the tables corresponding to this stress should accordingly be reduced by multiplying it by the ratio $\frac{p}{16\,000}$ and similarly for other stresses and corresponding loads, thus making proper allowance for the additional stresses produced by the lateral forces.

If the reduction of the safe loads on this account is a considerable proportion of the original amount due to vertical loading only, it would be more economical to provide lateral braces or tie rods at shorter intervals, thus avoiding the use of an excessive amount of material in the beam.

As the stresses due to vertical forces for usual cases of loading are a maximum at the center of the span it will ordinarily be sufficient to space the tie rods or braces at shorter intervals near the center in order to allow for the combined stresses due to vertical loading and horizontal thrusts.

The above method of calculation is not exact when considering the lateral thrust of arches, or loads from similar materials which do not exert a uniform pressure throughout their surfaces of contact with the sustaining beam on account of the friction and bond of their component parts, but this analysis of the stresses may serve as a guide in designing.

The above formulæ should be used in connection with the tables and formula given on pages 82 and 83 relating to the lateral strength of beams, due to compression of the upper flange figured as a column between points of lateral support.

* This method of treatment gives approximate results which are on the side of safety.

The correct determination can be secured by the use of the section modulus polygon. (See Transactions of the American Society of Civil Engineers, Vol. LVI, 1906, page 169, *et seq.*)

EXAMPLE.

What is the proper size of I-Beam without other lateral support than the usual tie rods, corresponding to a total fibre stress of 16 000 pounds per square inch under the following conditions? The beam is 18 feet between end supports and carries a tile arch on one side having a nominal depth of 9 inches, effective depth of 6.6 inches, a span of 5 feet, designed to carry a superimposed load of 75 pounds per square foot in addition to the weight of the arch and other floor materials. The hollow tile arch weighs 36 pounds per square foot and the other materials, including plastering, weigh 14 pounds, making a total load, exclusive of the weight of the beam, equal to 125 pounds per square foot.

For tie rods of $\frac{3}{4}$ " diameter the spacing between them would be 5.9 feet, as shown by the table of Spacing of Tie Rods on page 77 in which the safe stresses in the rods only are considered.

Substituting the proper values in the formula for lateral thrust of arches, given on page 75, this will be

$$T = \frac{3 \times 125 \times 5^2}{2 \times 6.6} = 710 \text{ lbs. per lineal foot.}$$

Substituting this value for w in formula (2) page 78 and assuming a 10" beam 25 lbs. per foot, the moment of inertia of which is 6.89, as given in the Tables of Properties of I-Beams, page 182, we have

$$p' = \frac{710 \times 4.66 \times 5.9^2}{2 \times 6.89} = 8\,358 \text{ lbs. per sq. in.}$$

Therefore $p = 16\,000 - 8\,358 = 7\,642 \text{ lbs. per sq. in.}$

Hence the safe load as determined by the consideration of vertical loads only, should be reduced to $\frac{7\,642}{16\,000}$, or approximately .48 of the amount given by the Tables of Safe Loads in case the spacing of the tie rods is not changed.

The safe vertical load for a 10" beam, weighing 25 lbs. per foot, 18 feet long between supports, for fibre stress of 16 000 lbs. per square inch, is 14 470 lbs. uniformly distributed, including the weight of the beam as given in the Tables of Safe Loads, on page 109, or 14 020 exclusive of the weight of the beam, and .48 of this is 6 730 lbs., which is the vertical load it can safely carry in order that the total stress due to it and the lateral thrust shall not exceed 16 000 lbs. per square inch.

The actual vertical load on the beam under consideration is as follows:

$$\frac{5}{2} \times 18 \times 125 = 5\,625 \text{ lbs.},$$

which is less than the allowable amount, 6 730 lbs., as figured above, so that a smaller beam may suffice.

Therefore, assume a 9-inch beam, weighing 21 lbs. per foot, the moment of inertia of which about an axis coincident with center line of web is found in the Table of Properties, on p. 182, to be 5.16.

In this case

$$p' = \frac{710 \times 4.33 \times 5.9^2}{2 \times 5.16} = 10\,370 \text{ lbs. per sq. in.}$$

Substituting this in the formula for p we have

$$p = 16\,000 - 10\,370 = 5\,630 \text{ lbs. per sq. in.}$$

Therefore the safe vertical load will be $\frac{5\,630}{16\,000}$, or approximately .35 of the tabular safe load.

The safe vertical load for a 9" 21 lb. beam, 18 feet long, for a fibre stress of 16 000 lbs. per square inch is 11 180 lbs., as given in the Table of Safe Loads, on page 109, and .35 of this, after deducting weight of the beam, is 3 781 lbs., which is less than the actual amount, 5 625 lbs., as calculated above, so that the 9" 21 lb. beam will not suffice.

If the spacing of the tie rods at the center be reduced from 5.9 feet to 3.25 feet, it may be found, in a manner similar to that used in the above calculations, that the safe vertical load for an 8" I-Beam, weighing 18.0 lbs. per foot, is reduced to .74 of its tabular value of 8 430 lbs., or 6 328 lbs., and as this amount is greater than the actual load as above, namely, 5 625 lbs., the 8" beam would answer the purpose, under the changed conditions as to spacing of tie rods. As this beam might deflect beyond the limit for plastered ceilings, it should be examined in accordance with the rule or formula given for obtaining safe deflections in the explanation of the Tables of Safe Loads, and elsewhere herein.

Calculating this by the rule given on page 102, the safe load for the allowable limit of deflection is

$$W = \frac{9\,480 \times 16^3}{18^2} = 7\,491 \text{ lbs.},$$

which is greater than the actual amount, 5 625 lbs., so that the 8" beam is sufficient and proper if the spacing of central tie rods be changed to 3.25 feet, as assumed in the last case.

LATERAL STRENGTH OF BEAMS, WITHOUT LATERAL SUPPORT.

The Tables of Safe Loads for Cambria I-Beams and Channels and Tables of Spacing of Cambria I-Beams, on pages 106 to 135, are calculated on the assumption that proper provision is made for preventing lateral deflection by means of tie rods or other braces. In order to prevent undue strains in the compression flange, considered as a column, the beams should be supported laterally at distances not exceeding twenty times the flange width, this ratio being determined by the following formula, which gives the safe load for solid columns of soft steel:

$$p = \frac{18000}{1 + \frac{l^2}{3000b^2}}$$

in which

p = allowable stress in pounds per square inch.

l = length between lateral supports in inches.

b = width of flange in inches.

Substituting 16 000 for p in the above formula, which is the allowable unit stress of the safe load tables, it is found that the ratio $\frac{l}{b} = 19.37$, from which it may be seen that the compression flange should be supported laterally at distances not exceeding twenty times the flange width as stated above.

Beams which are not thus supported laterally should not be loaded to their full transverse capacity. The allowable fibre stresses and proportions of their full loads which they can safely carry when laterally supported at various distances is given in the following table:

**REDUCTION IN VALUES OF ALLOWABLE FIBRE
STRESS AND SAFE LOADS FOR SHAPES
USED AS BEAMS DUE TO LATERAL
FLEXURE.**

| Ratio of Span or Distance between Lateral Supports to Flange Width. | Allowable Unit Stress for Direct Flexure in Extreme Fibre. | Proportion of Tabular Safe Load | Ratio of Span or Distance between Lateral Supports to Flange Width. | Allowable Unit Stress for Direct Flexure in Extreme Fibre. | Proportion of Tabular Safe Load |
|--|---|--|--|---|--|
| $\frac{l}{b}$ | P | to be Used. | $\frac{l}{b}$ | P | to be Used. |
| 19.37 | 16000 | 1.0 | 65 | 7474 | .47 |
| 20 | 15882 | .99 | 70 | 6835 | .43 |
| 25 | 14897 | .93 | 75 | 6261 | .39 |
| 30 | 13846 | .87 | 80 | 5745 | .36 |
| 35 | 12781 | .80 | 85 | 5281 | .33 |
| 40 | 11739 | .73 | 90 | 4865 | .30 |
| 45 | 10746 | .67 | 95 | 4491 | .28 |
| 50 | 9818 | .61 | 100 | 4154 | .26 |
| 55 | 8963 | .56 | 105 | 3850 | .24 |
| 60 | 8182 | .51 | 110 | 3576 | .22 |

The above table should be used in connection with the Tables of Safe Loads Uniformly Distributed for Cambria I-Beams and Channels, on pages 106 to 123 inclusive, and limits the values found therein under the conditions given above.

EXAMPLE.

Required the safe load for a 15-inch standard I-Beam weighing 42 pounds per foot for a span of 30 feet without lateral supports:

From the data the ratio $\frac{l}{b} = \frac{30 \times 12}{5.5} = 65$.

From the above table the proportion of the safe load which the beam can safely support under these conditions is .47. From the Table of Safe Loads for I-Beams, page 111, the safe load for this beam when properly supported laterally is 20 940 pounds, which multiplied by .47 gives 9 842 pounds as the safe load uniformly distributed under the conditions given, including the weight of the beam, or 8 582 pounds superimposed load.

APPROXIMATE WEIGHTS OF VARIOUS ROOF COVERINGS.

In Pounds per Square Foot.

| | |
|---|------|
| Copper Sheeting, B. W. G. No. 22..... | 1½ |
| Corrugated Iron, B. W. G. Nos. 26 to 16..... | 1-3½ |
| Felt, two Layers..... | ½ |
| Felt and Asphalt..... | 2 |
| Felt and Gravel, ⅝ inch thick..... | 6½ |
| Galvanized Iron, B. W. G. Nos. 26 to 16..... | 1-3 |
| Lath and Plaster Ceiling, Ordinary..... | 6-8 |
| Sheathing, 1 inch thick, Hemlock..... | 2 |
| " " " White Pine or Spruce..... | 2½ |
| " " " Yellow Pine..... | 4 |
| Shingles, 16 inch, laid 5½ inch to weather..... | 2 |
| Skylight Glass, ⅜ to ½ inch thick..... | 2½-7 |
| Slates, ⅝ to ⅞ inch thick, 3 inch double lap..... | 4-7 |
| Slag Roofing, 4-ply, with cement and sand..... | 4 |
| Steel Sheeting (See next page)..... | ¾-3 |
| Tiles (See Page 69)..... | 8-20 |
| Tin..... | ¾-1 |
| Zinc, B. W. G. No. 20..... | 1½ |

APPROXIMATE WEIGHT OF ROOFS INCLUDING FRAMING:

| | |
|---|-------|
| Corrugated Sheets..... | 8-10 |
| Shingle..... | 6-10 |
| Slate..... | 12-15 |
| Tar and Gravel..... | 10-12 |
| Tin..... | 6-8 |
| Tile..... | 20-30 |
| If roof is plastered underneath, add to values given above..... | 6 |

Weight of Roof Truss with span of 75 feet or less..... 5

Snow Load—25 lbs. per horizontal square foot of roof for all slopes up to 20°, reduced 1 lb. for each degree of slope in excess of 20°. No snow load to be considered for slope of 45° or more.

WIND PRESSURE ON ROOFS.

Based on 20 Lbs. per Sq. Ft. on a Vertical Plane.

$$1.84 \cos \alpha - 1.$$

FORMULA.—Normal Pressure per sq. ft. = $P \sin \alpha$

| Pitch of Roof. | Angle of Slope (α) with Horizontal. | Rise of Roof per Foot. | Normal Wind Pressure. |
|----------------------|---|------------------------|-----------------------|
| | Degrees. Minutes. | Inches. | Pounds per Sq. Ft. |
| 1/6 | 18 - 25 | 4 | 8.4 |
| 1/4 | 26 - 33 | 6 | 11.9 |
| 1/3 | 33 - 41 | 8 | 14.6 |
| 1/2 | 45 - 0 | 12 | 18.1 |
| 2/3 | 53 - 7 | 16 | 19.4 |
| 3/4 | 56 - 20 | 18 | 19.7 |
| 1 | 63 - 27 | 24 | 20.0 |

STEEL SHEETING.

Weights given (U. S. Standard) are based on 480 lbs. per cu. ft.

| Gauge Number U. S. Std. | Thickness | Weight—Lbs. per Sq. Ft. | | | | Spacing of Supports | |
|-------------------------------|-----------|-------------------------|------------|---------------|------------|----------------------|----------------------|
| | | Flat | | Corrugated | | Roof | Sides |
| | Inch | Black | Galvanized | Black Painted | Galvanized | Not Over Ft.—Ins. | Not Over Ft.—Ins. |
| 16 | .0625 | 2.50 | 2.66 | 2.75 | 2.81 | 5-9 | 7-8 |
| 28 | .05 | 2.00 | 2.16 | 2.20 | 2.36 | 5-9 | 7-8 |
| 20 | .0375 | 1.50 | 1.66 | 1.65 | 1.82 | 4-9 | 6-8 |
| 22 | .03125 | 1.25 | 1.41 | 1.38 | 1.54 | 3-9 | 5-8 |
| 24 | .025 | 1.00 | 1.16 | 1.11 | 1.27 | 2-9 | 3-10 |
| 26 | .01875 | .75 | .91 | .84 | .99 | | |
| 28 | .015625 | .63 | .79 | .69 | .86 | | |

Standard Flat and Corrugated Sheets furnished in lengths 48, 60, 72, 84, 96, 108 and 120 inches.

Standard Flat Sheets in widths 24, 26, 28, 30 and 32 inches.

Standard Corrugated Sheets in widths as follows:

| For | Width of Sheet Flat | Width of Sheet Corrugated | Width of Corrugation | Depth of Corrugation | Corrugation in Lap | Edges Laid | |
|------------|---------------------------|---------------------------------|----------------------------|----------------------------|--------------------------|------------|------|
| | Ins. | Ins. | Ins. | Ins. | | Up | Down |
| Roofing .. | 30 | 27½ | 2½ | ⅝ | 1½ | 1 | 1 |
| Roofing .. | 28 | 26 | " | " | 2 | | 2 |
| Siding ... | 28 | 26 | " | " | 1 | | 2 |

Sheets should preferably be ordered in even ft. lengths to span 2 purlin spaces.

End Lap:

6 inches for Roofing, roof pitch 6 inches.

8 inches for Roofing, roof pitch 4 inches.

8 inches for Roofing, roof pitch less than 4 inches, when laid with slater's cement.

4 inches for Roofs in snowless climates and for Siding.

Ridge Roll:—No. 24 Gauge; 96-inch lengths; 3-inch end lap, standard diameter 2½ inches; apron 6 inches.

Flashing:—No. 24 Gauge; 30-inch lengths; 3-inch end lap.

Corner Capping:—48-inch lengths; 4-inch end lap.

FASTENINGS.

Straps:—No. 18 U. S. Gauge Steel ¾-inch wide; 1 strap and 2 rivets or bolts for each lineal foot of purlin or girts; 1 bundle (400 lin. ft.) straps weighs 50 pounds; 1000 rivets weigh 6 pounds.

Clinch Rivets:—Should clinch at least 1 inch; 2 rivets to each lineal foot of purlin or girt.

Purlin leg 2 inches; 2½ to 3 inches: 3½ inches; 4 to 4½ inches.

Length 4 inches; 5 inches; 6 inches; 7 inches.

Number per pound 48 38 33 27

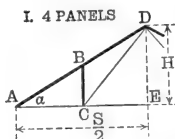
Clips and Bolts:—For fastening sheeting to purlins other than angle purlins when asbestos lining is used under sheeting. No. 16 steel slightly crimped. 2 clips and 2 bolts for each lineal foot of purlin or girt; 500 clips in one box. Hole for bolt ⅞" x 1".

Closing Rivets:—⅝-inch diameter; ⅜, ½, ⅝ and ¾-inch lengths; 1000=6 lbs. For side laps, 1 rivet for each lineal foot. For fastening flashing, etc., to sheeting, 2 for each lineal foot.

Nails:—For fastening sheeting to wooden purlins: 10d. clinch nails for roofing, one for each lineal foot (for both end and side laps), 50=1 pound. 8d. clinch nails for siding, one for each lineal foot (for both end and side laps), 70=1 pound. For sheeting on wooden sheathing in end laps and in the body of the sheets in rows about 3 or 4 feet apart, same as if purlins or girts occurred at these lines. For fastening flashing, etc., to wood use tinner's nails, 2 per foot. For fastening flashing, etc., to brick wall use 8d. nails, 2 per foot.

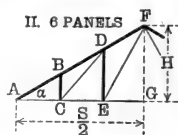
ROOF TRUSSES

(PRATT.)



$$n = S \div H = 2 \cot \alpha$$

P = Panel Load.



Heavy lines in diagrams indicate Compression Members.

I—4 Panels.

| Member | Length | Stress=P x | n = | | | | | | |
|--------|------------------------------|-------------------------------|------|----------------|-------------------|------|----------------|------|------|
| | | | 3 | $\frac{24}{7}$ | $2 \cot 30^\circ$ | 4 | $\frac{24}{5}$ | 5 | 6 |
| AB, BD | $S \sec \alpha \div 4$ | $\frac{3}{4} \sqrt{n^2 + 4}$ | 2.70 | 2.98 | 3.00 | 3.35 | 3.90 | 4.04 | 4.74 |
| AC | $S \div 4$ | $\frac{3}{4} n$ | 2.25 | 2.57 | 2.60 | 3.00 | 3.60 | 3.75 | 4.50 |
| CE | $S \div 2$ | $\frac{1}{2} n$ | 1.50 | 1.71 | 1.73 | 2.00 | 2.40 | 2.50 | 3.00 |
| BC | $H \div 2$ | 1 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| CD | $\sqrt{S^2 + 16 H^2} \div 4$ | $\frac{1}{4} \sqrt{n^2 + 16}$ | 1.25 | 1.32 | 1.32 | 1.41 | 1.56 | 1.60 | 1.80 |

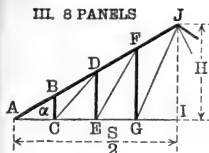
II—6 Panels.

| Member | Length | Stress = P x | n = | | | | | | |
|--------|------------------------------|-------------------------------|------|----------------|-------------------|------|----------------|------|------|
| | | | 3 | $\frac{24}{7}$ | $2 \cot 30^\circ$ | 4 | $\frac{24}{5}$ | 5 | 6 |
| AB, BD | $S \sec \alpha \div 6$ | $5/4 \sqrt{n^2 + 4}$ | 4.51 | 4.96 | 5.00 | 5.59 | 6.50 | 6.73 | 7.91 |
| DF | $S \sec \alpha \div 6$ | $\sqrt{n^2 + 4}$ | 3.61 | 3.97 | 4.00 | 4.47 | 5.20 | 5.39 | 6.32 |
| AC | $S \div 6$ | $5/4 n$ | 3.75 | 4.29 | 4.33 | 5.00 | 6.00 | 6.25 | 7.50 |
| CE | $S \div 6$ | n | 3.00 | 3.43 | 3.46 | 4.00 | 4.80 | 5.00 | 6.00 |
| EG | $S \div 3$ | $\frac{3}{4} n$ | 2.25 | 2.57 | 2.60 | 3.00 | 3.60 | 3.75 | 4.50 |
| BC | $H \div 3$ | 1 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| DE | $2H \div 3$ | $3/2$ | 1.50 | 1.50 | 1.50 | 1.50 | 1.50 | 1.50 | 1.50 |
| CD | $\sqrt{S^2 + 16 H^2} \div 6$ | $\frac{1}{4} \sqrt{n^2 + 16}$ | 1.25 | 1.32 | 1.32 | 1.41 | 1.56 | 1.60 | 1.80 |
| EF | $\sqrt{S^2 + 36 H^2} \div 6$ | $\frac{1}{4} \sqrt{n^2 + 36}$ | 1.68 | 1.73 | 1.73 | 1.80 | 1.92 | 1.95 | 2.12 |

COEFFICIENTS FOR CALCULATING TRUSS MEMBERS.

| n..... | 3 | $\frac{24}{7}$ | $2 \cot 30^\circ$ | 4 | $\frac{24}{5}$ | 5 | 6 |
|--|------------------|------------------|-------------------|------------------|------------------|------------------|------------------|
| α | $33^\circ 41.4'$ | $30^\circ 15.4'$ | 30° | $26^\circ 33.9'$ | $22^\circ 37.2'$ | $21^\circ 48.1'$ | $18^\circ 26.1'$ |
| $\sec \alpha$ | 1.2018 | 1.1577 | 1.1547 | 1.1180 | 1.0833 | 1.0770 | 1.0541 |
| $\sec^2 \alpha$ | 1.4444 | 1.3403 | 1.3333 | 1.2500 | 1.1736 | 1.1600 | 1.1111 |
| $\sec \alpha \tan \alpha$ | .8012 | .6753 | .6667 | .5590 | .4514 | .4308 | .3514 |
| $\sec \alpha \sqrt{9 \sec^2 \alpha - 8}$ | 2.6874 | 2.3334 | 2.3094 | 2.0156 | 1.7342 | 1.6824 | 1.4907 |

III. 8 PANELS



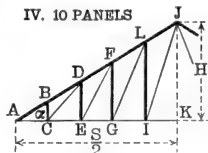
ROOF TRUSSES (PRATT).

$$n = S \div H = 2 \cot \alpha.$$

P = Panel Load.

Heavy lines in diagrams indicate compression members.

IV. 10 PANELS



III—8 Panels.

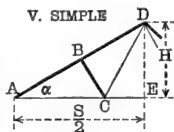
| Member | Length | Stress = P x | n = | | | | | | |
|--------|------------------------------|-----------------------|------|----------------|-------------------|------|----------------|------|-------|
| | | | 3 | $\frac{24}{7}$ | $2 \cot 30^\circ$ | 4 | $\frac{24}{5}$ | 5 | 6 |
| AB, BD | $S \sec \alpha \div 8$ | $7/4 \sqrt{n^2 + 4}$ | 6.31 | 6.95 | 7.00 | 7.83 | 9.10 | 9.45 | 11.07 |
| DF | $S \sec \alpha \div 8$ | $3/2 \sqrt{n^2 + 4}$ | 5.41 | 5.95 | 6.00 | 6.71 | 7.80 | 8.08 | 9.49 |
| FJ | $S \sec \alpha \div 8$ | $5/4 \sqrt{n^2 + 4}$ | 4.51 | 4.96 | 5.00 | 5.59 | 6.50 | 6.73 | 7.91 |
| AC | $S \div 8$ | $7/4 n$ | 5.25 | 6.00 | 6.06 | 7.00 | 8.40 | 8.75 | 10.50 |
| CE | $S \div 8$ | $3/2 n$ | 4.50 | 5.14 | 5.20 | 6.00 | 7.20 | 7.50 | 9.00 |
| EG | $S \div 8$ | $5/4 n$ | 3.75 | 4.29 | 4.33 | 5.00 | 6.00 | 6.25 | 7.50 |
| GI | $S \div 4$ | n | 3.00 | 3.43 | 3.46 | 4.00 | 4.80 | 5.00 | 6.00 |
| BC | $H \div 4$ | 1 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| DE | $H \div 2$ | $3/2$ | 1.50 | 1.50 | 1.50 | 1.50 | 1.50 | 1.50 | 1.50 |
| FG | $3H \div 4$ | 2 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| CD | $\sqrt{S^2 + 16 H^2} \div 8$ | $1/4 \sqrt{n^2 + 16}$ | 1.25 | 1.32 | 1.32 | 1.41 | 1.56 | 1.60 | 1.80 |
| EF | $\sqrt{S^2 + 36 H^2} \div 8$ | $1/4 \sqrt{n^2 + 36}$ | 1.68 | 1.73 | 1.73 | 1.80 | 1.92 | 1.95 | 2.12 |
| GJ | $\sqrt{S^2 + 64 H^2} \div 8$ | $1/4 \sqrt{n^2 + 64}$ | 2.14 | 2.18 | 2.18 | 2.24 | 2.33 | 2.36 | 2.50 |

IV—10 Panels.

| Member | Length | Stress = P x | n = | | | | | | |
|--------|--------------------------------|------------------------|------|----------------|-------------------|-------|----------------|-------|-------|
| | | | 3 | $\frac{24}{7}$ | $2 \cot 30^\circ$ | 4 | $\frac{24}{5}$ | 5 | 6 |
| AB, BD | $S \sec \alpha \div 10$ | $9/4 \sqrt{n^2 + 4}$ | 8.11 | 8.93 | 9.00 | 10.06 | 11.70 | 12.12 | 14.23 |
| DF | $S \sec \alpha \div 10$ | $2 \sqrt{n^2 + 4}$ | 7.21 | 7.94 | 8.00 | 8.94 | 10.40 | 10.77 | 12.65 |
| FL | $S \sec \alpha \div 10$ | $7/4 \sqrt{n^2 + 4}$ | 6.31 | 6.95 | 7.00 | 7.83 | 9.10 | 9.42 | 11.07 |
| LJ | $S \sec \alpha \div 10$ | $3/2 \sqrt{n^2 + 4}$ | 5.41 | 5.95 | 6.00 | 6.71 | 7.80 | 8.08 | 9.49 |
| AC | $S \div 10$ | $9/4 n$ | 6.75 | 7.71 | 7.79 | 9.00 | 10.80 | 11.25 | 13.50 |
| CE | $S \div 10$ | $2 n$ | 6.00 | 6.86 | 6.93 | 8.00 | 9.60 | 10.00 | 12.00 |
| EG | $S \div 10$ | $7/4 n$ | 5.25 | 6.00 | 6.06 | 7.00 | 8.40 | 8.75 | 10.50 |
| GI | $S \div 10$ | $3/2 n$ | 4.50 | 5.14 | 5.20 | 6.00 | 7.20 | 7.50 | 9.00 |
| IK | $S \div 5$ | $5/4 n$ | 3.75 | 4.29 | 4.33 | 5.00 | 6.00 | 6.25 | 7.50 |
| BC | $H \div 5$ | 1 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| DE | $2H \div 5$ | $3/2$ | 1.50 | 1.50 | 1.50 | 1.50 | 1.50 | 1.50 | 1.50 |
| FG | $3H \div 5$ | 2 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| LI | $4H \div 5$ | $5/2$ | 2.50 | 2.50 | 2.50 | 2.50 | 2.50 | 2.50 | 2.50 |
| CD | $\sqrt{S^2 + 16 H^2} \div 10$ | $1/4 \sqrt{n^2 + 16}$ | 1.25 | 1.32 | 1.32 | 1.41 | 1.56 | 1.60 | 1.80 |
| EF | $\sqrt{S^2 + 36 H^2} \div 10$ | $1/4 \sqrt{n^2 + 36}$ | 1.68 | 1.73 | 1.73 | 1.80 | 1.92 | 1.95 | 2.12 |
| GL | $\sqrt{S^2 + 64 H^2} \div 10$ | $1/4 \sqrt{n^2 + 64}$ | 2.14 | 2.18 | 2.18 | 2.24 | 2.33 | 2.36 | 2.50 |
| IJ | $\sqrt{S^2 + 100 H^2} \div 10$ | $1/4 \sqrt{n^2 + 100}$ | 2.61 | 2.64 | 2.65 | 2.69 | 2.77 | 2.80 | 2.92 |

ROOF TRUSSES (FINK).

VI. COMPOUND

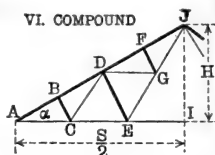


$$n = S + H = 2 \cot \alpha$$

$$P = \text{Panel Load.}$$

Heavy lines in diagrams indicate compression members.

V—Simple.



| Member | Length | Stress = P x | n= | | | | | | |
|--------|--|--------------------------------------|------|----------------|-------------|------|----------------|------|------|
| | | | 3 | $\frac{24}{7}$ | $2 \cot 30$ | 4 | $\frac{24}{5}$ | 5 | 6 |
| AB | S sec $\alpha \div 4$ | $\frac{3}{4} \sqrt{n^2+4}$ | 2.70 | 2.98 | 3.00 | 3.35 | 3.90 | 4.04 | 4.74 |
| BD | S sec $\alpha \div 4$ | $\frac{3 n^2 + 4}{4 \sqrt{n^2 + 4}}$ | 2.15 | 2.47 | 2.50 | 2.91 | 3.52 | 3.67 | 4.43 |
| AC | S sec ² $\alpha \div 4$ | $\frac{3}{4} n$ | 2.25 | 2.57 | 2.60 | 3.00 | 3.60 | 3.75 | 4.50 |
| CE | S (1 — $\frac{1}{2}$ sec ² α) | $\frac{1}{2} n$ | 1.50 | 1.71 | 1.73 | 2.00 | 2.40 | 2.50 | 3.00 |
| BC | S sec α tan $\alpha \div 4$ | $\frac{n}{\sqrt{n^2 + 4}}$ | 0.83 | 0.86 | 0.87 | 0.89 | 0.92 | 0.93 | 0.95 |
| CD | S sec ² $\alpha \div 4$ | $\frac{1}{4} n$ | 0.75 | 0.86 | 0.87 | 1.00 | 1.20 | 1.25 | 1.50 |

VI—Compound.

| Member | Length | Stress = $\frac{P}{x}$ | $n =$ | | | | | | |
|--------|-------------------------------------|---------------------------------------|-------|----------------|-------------------|------|----------------|------|-------|
| | | | 3 | $\frac{24}{7}$ | $2 \cot 30^\circ$ | 4 | $\frac{24}{5}$ | 5 | 6 |
| AB | $S \sec \alpha \div 8$ | $7/4 \sqrt{n^2 + 4}$ | 6.31 | 6.95 | 7.00 | 7.83 | 9.10 | 9.42 | 11.07 |
| BD | $S \sec \alpha \div 8$ | $\frac{7 n^2 + 20}{4 \sqrt{n^2 + 4}}$ | 5.76 | 6.44 | 6.50 | 7.38 | 8.72 | 9.05 | 10.75 |
| DF | $S \sec \alpha \div 8$ | $\frac{7 n^2 + 12}{4 \sqrt{n^2 + 4}}$ | 5.20 | 5.94 | 6.00 | 6.93 | 8.33 | 8.68 | 10.44 |
| FJ | $S \sec \alpha \div 8$ | $\frac{7 n^2 + 4}{4 \sqrt{n^2 + 4}}$ | 4.65 | 5.43 | 5.50 | 6.48 | 7.95 | 8.31 | 10.12 |
| AC | $S \sec^2 \alpha \div 8$ | $7/4 n$ | 5.25 | 6.00 | 6.06 | 7.00 | 8.40 | 8.75 | 10.50 |
| CE | $S \sec^2 \alpha \div 8$ | $3/2 n$ | 4.50 | 5.14 | 5.20 | 6.00 | 7.20 | 7.50 | 9.00 |
| EI | $S (1 - \frac{1}{2} \sec^2 \alpha)$ | n | 3.00 | 3.43 | 3.46 | 4.00 | 4.80 | 5.00 | 6.00 |
| BC, FG | $S \sec \alpha \tan \alpha \div 8$ | $\frac{n}{\sqrt{n^2 + 4}}$ | 0.83 | 0.86 | 0.87 | 0.89 | 0.92 | 0.93 | 0.95 |
| DE | $S \sec \alpha \tan \alpha \div 4$ | $\frac{2 n}{\sqrt{n^2 + 4}}$ | 1.66 | 1.73 | 1.73 | 1.79 | 1.85 | 1.86 | 1.90 |
| CD, DG | $S \sec^2 \alpha \div 8$ | $\frac{1}{4} n$ | 0.75 | 0.86 | 0.87 | 1.00 | 1.20 | 1.25 | 1.50 |
| EG | $S \sec^2 \alpha \div 8$ | $\frac{1}{2} n$ | 1.50 | 1.71 | 1.73 | 2.00 | 2.40 | 2.50 | 3.00 |
| GJ | $S \sec^2 \alpha \div 8$ | $\frac{3}{4} n$ | 2.25 | 2.57 | 2.60 | 3.00 | 3.60 | 3.75 | 4.50 |

ROOF TRUSSES

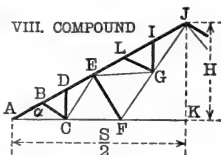
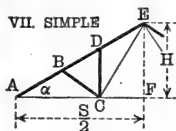
(FAN).

$$n = S + H = 2 \cot \alpha.$$

$$P = \text{Panel Load.}$$

Heavy lines in diagrams indicate compression members.

VII—Simple.

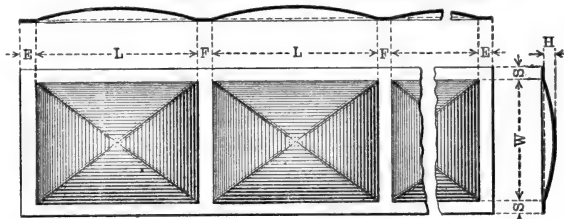


| Member | Length | Stress = P x | n = | | | | | | |
|--------|--|---|------|----------------|-------------------|------|----------------|------|------|
| | | | 3 | $\frac{24}{7}$ | $2 \cot 30^\circ$ | 4 | $\frac{24}{5}$ | 5 | 6 |
| AB | S sec α + 6 | $5/4 \sqrt{n^2 + 4}$ | 4.51 | 4.96 | 5.00 | 5.59 | 6.50 | 6.73 | 7.91 |
| BD | S sec α + 6 | $\frac{13 (n^2 + 36)}{12 \sqrt{n^2 + 4}}$ | 3.54 | 3.96 | 4.00 | 4.55 | 5.38 | 5.59 | 6.64 |
| DE | S sec α + 6 | $\frac{5 n^2 + 4}{4 \sqrt{n^2 + 4}}$ | 3.40 | 3.95 | 4.00 | 4.70 | 5.73 | 5.99 | 7.27 |
| AC | S sec ² α + 4 | $5/4$ n | 3.75 | 4.29 | 4.33 | 5.00 | 6.00 | 6.25 | 7.50 |
| CF | S (1 - $\frac{1}{2}$ sec ² α) | $\frac{3}{4}$ n | 2.25 | 2.57 | 2.60 | 3.00 | 3.60 | 3.75 | 4.50 |
| BC, CD | S sec $\alpha \sqrt{9 \sec^2 \alpha - 8}$ | $n \sqrt{n^2 + 36} \div 8$ | 0.93 | 1.00 | 1.00 | 1.08 | 1.18 | 1.21 | 1.34 |
| CE | S sec ² α + 4 [+ 12 | $\frac{1}{2}$ n [$6 \sqrt{n^2 + 4}$ | 1.50 | 1.71 | 1.73 | 2.00 | 2.40 | 2.50 | 3.00 |

VIII—Compound.

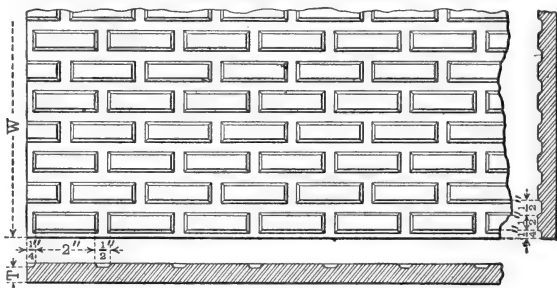
| Member | Length | Stress = P x | n = | | | | | | |
|--------------------|--|---|------|----------------|-------------------|-------|----------------|-------|-------|
| | | | 3 | $\frac{24}{7}$ | $2 \cot 30^\circ$ | 4 | $\frac{24}{5}$ | 5 | 6 |
| AB | S sec $\alpha \div 12$ | $\frac{11}{4} \sqrt{n^2 + 4}$ | 9.92 | 10.92 | 11.00 | 12.30 | 14.30 | 14.81 | 17.39 |
| BD | S sec $\alpha \div 12$ | $\frac{31 n^2 + 108}{12 \sqrt{n^2 + 4}}$ | 8.95 | 9.92 | 10.00 | 11.26 | 13.18 | 13.66 | 16.13 |
| DE | S sec $\alpha \div 12$ | $\frac{11 n^2 + 28}{4 \sqrt{n^2 + 4}}$ | 8.81 | 9.91 | 10.00 | 11.40 | 13.53 | 14.07 | 16.76 |
| EL | S sec $\alpha \div 12$ | $\frac{11 n^2 + 20}{4 \sqrt{n^2 + 4}}$ | 8.25 | 9.40 | 9.50 | 10.96 | 13.15 | 13.70 | 16.44 |
| LI | S sec $\alpha \div 12$ | $\frac{31 n^2 + 36}{12 \sqrt{n^2 + 4}}$ | 7.28 | 8.41 | 8.50 | 9.91 | 12.02 | 12.55 | 15.18 |
| IJ | S sec $\alpha \div 12$ | $\frac{11 n^2 + 4}{4 \sqrt{n^2 + 4}}$ | 7.14 | 8.40 | 8.50 | 10.06 | 12.38 | 12.95 | 15.81 |
| AC | S sec ² $\alpha \div 8$ | $\frac{11}{4} n$ | 8.25 | 9.43 | 9.53 | 11.00 | 13.20 | 13.75 | 16.50 |
| CF | S sec ² $\alpha \div 8$ | $\frac{9}{4} n$ | 6.75 | 7.71 | 7.79 | 9.00 | 10.80 | 11.25 | 13.50 |
| FK | S (1 — $\frac{1}{2}$ sec ² α) | $\frac{3}{2} n$ | 4.50 | 5.14 | 5.20 | 6.00 | 7.20 | 7.50 | 9.00 |
| BC, CD) GL, GI) | S sec $\alpha \sqrt{9 \sec^2 \alpha - 8}$ [$\div 24$] | $\frac{n \sqrt{n^2 + 36} \div}{6 \sqrt{n^2 + 4}}$ | 0.93 | 1.00 | 1.00 | 1.08 | 1.18 | 1.21 | 1.34 |
| EF | S sec $\alpha \tan \alpha \div 4$ | $\frac{3 n}{\sqrt{n^2 + 4}}$ | 2.50 | 2.59 | 2.60 | 2.68 | 2.77 | 2.79 | 2.85 |
| CE, EG | S sec ² $\alpha \div 8$ | $\frac{1}{2} n$ | 1.50 | 1.71 | 1.73 | 2.00 | 2.40 | 2.50 | 3.00 |
| FG | S sec ² $\alpha \div 8$ | $\frac{3}{4} n$ | 2.25 | 2.57 | 2.60 | 3.00 | 3.60 | 3.75 | 4.50 |
| GJ | S sec ² $\alpha \div 8$ | $\frac{5}{4} n$ | 3.75 | 4.29 | 4.33 | 5.00 | 6.00 | 6.25 | 7.50 |

CAMBRIA STANDARD BUCKLE PLATES.



| No. | SIZE OF BUCKLES. | | RISE OF BUCKLE (H). Ins. | PLATE THICKNESS. Ins. | NUMBER OF BUCKLES PER PLATE. | WIDTH OF FLANGES AND FILLETS. |
|-----|------------------|-----------|-----------------------------|---|------------------------------|--|
| | Side (L). | Side (W). | | | | |
| | Ft. Ins. | Ft. Ins. | | | | |
| 1 | 2-8 | 2-8 | 2 | $\frac{1}{4}$, $\frac{5}{16}$ or $\frac{3}{8}$ | 1 to 10 | END FLANGES (E) Preferably made alike, from 2 to 18 ins. wide. If wider than 18 ins., use angles riveted across the plates for stiffeners. |
| 2 | 2-8 | 3-8 | 2 | " | 1 " 10 | |
| 3 | 3-8 | 2-8 | 2 | " | 1 " 8 | |
| 4 | 3-1 | 3-2 | 3 | " | 1 " 9 | SIDE FLANGES (S) Preferably made alike, from 2 to 6 ins. wide. Best not to exceed 4 ins. |
| 5 | 3-2 | 3-1 | 3 | " | 1 " 9 | |
| 6 | 3-1 | 3-9 | 3 | " | 1 " 9 | |
| 7 | 3-9 | 3-1 | 3 | " | 1 " 8 | FILLETS (F) From 2 to 6 ins. wide. Best not to exceed 4 ins. |
| 8 | 4-0 | 4-0 | 3 | " | 1 " 7 | |
| 9 | 4-6 | 3-11 | $3\frac{1}{2}$ | " | 1 " 6 | |
| 10 | 3-11 | 4-6 | $3\frac{1}{2}$ | " | 1 " 7 | |
| 11 | 3-6 | 5-6 | $3\frac{1}{2}$ | " | 1 " 2 | |
| 12 | 5-6 | 3-6 | $3\frac{1}{2}$ | " | 1 " 2 | |

ROLLED STEEL SAFETY FLOOR PLATES.



| WIDTH (W). | THICKNESS (T). | MAXIMUM LENGTH. |
|------------|---------------------------------|-----------------|
| Inches. | Inches. | Feet. |
| 18 to 25 | $\frac{5}{16}$ to $\frac{3}{4}$ | 50 |
| 25 " 36 | $\frac{5}{16}$ " $\frac{1}{2}$ | 50 |

FIREPROOFING—REINFORCED CONCRETE.

The actual fire tests of reinforced concrete have been limited, but experience, together with the results of tests so far made, indicates that concrete may be safely used for fireproofing purposes. It is in itself incombustible and proof against ordinary fire when composed of the best materials properly mixed, applied and anchored in place. For a fireproof filling or deadening layer in floors, these same materials without reinforcement may be used or clean hard burned cinders may be substituted for this purpose. The low rate of heat conductivity is one reason of its value for fireproofing and the concrete actually affected by fire, remains in position and affords protection to the concrete beneath it. The thickness of protective coating required, depends upon the probable duration of a fire, which is likely to occur in the structure. However, for ordinary conditions, it is recommended, as a general rule, that the metal in girders and columns be protected by a minimum of 2 inches, beams $1\frac{1}{2}$ inches, and floor slabs, the different minimum values, as indicated in the accompanying table.

A properly designed combination of protected steel framework with reinforced concrete floor slabs, if well executed is particularly safe and effective in fireproof building construction, and the use of concrete and steel in the floor slab is especially advantageous, affording both strength and rigidity.

In reinforced concrete design, the following assumptions are recommended and considered by almost all authorities, and are, therefore, used as the basis for the formulæ and tables of pages 92 and 93, but it must be noted that all these ideal conditions cannot be had in practice and if possible allowance should be made accordingly.

(1) Calculations should be made with reference to working stresses and safe loads, rather than to ultimate strengths and ultimate loads.

(2) A section, plane before bending remains plane after bending.

(3) The modulus of concrete in compression within the usual limits of working stresses is constant. The distribution of compressive forces in slabs is therefore rectilinear.

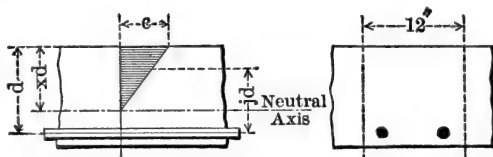
(4) The tensile stresses in the concrete shall be neglected in calculating the reinforced slab resistance.

(5) Perfect adhesion between concrete and reinforcement is assumed.

(6) Initial stresses in the reinforcement due to contraction or expansion in the concrete may be neglected.

These above assumptions, while not entirely borne out by experimental data, are recommended and used by various authorities on this subject in the interest of simplicity and uniformity.

REINFORCED CONCRETE FLOOR SLABS.



NOTATION.

- w** = Total weight in lbs. per sq. ft. including slab weight.
L = Span in feet c. to c. of beam supports.
M = Bending Moment for 12" width of slab (inch pounds).
E_c = Modulus of Elasticity for concrete.
E_s = " " " " steel.
r = Ratio. $E_s \div E_c$.
C = Extreme fibre stress of concrete in compression.
S = " " " " steel in tension.
K = Constant for a given steel and concrete.
d = Effective depth of slab in inches.
p = Ratio of steel area to effective slab area.
x = Distance, Top of slab to Neutral Axis $\div d$.
j = " between centers of stress $\div d$.
V = Maximum Shear, 12" width of slab.
v = Unit shear.
u = Unit bond stress.
Σo = Sum of perimeters of bars (in 12" width of slab).

FORMULÆ.

M = $1.5 wL^2$ —for slabs freely supported.

= $1.2 wL^2$ — " " continuous over supports.

$$p = \frac{C^2 r}{2 S (Cr + S)} \quad x = rp \left(\sqrt{1 + \frac{2}{rp}} - 1 \right)$$

$$K = \frac{Sp}{3} \left(\frac{2Cr + 3S}{Cr + S} \right) \quad j = 1 - \frac{x}{3}$$

$$d = \sqrt{\frac{M}{12 K}} \quad \text{Steel Area (12" width of slab)} = 12 dp$$

$$v = \frac{V}{12 jd} \quad (\text{not to exceed 60 lbs. for stone or 25 lbs. for cinder concrete}).$$

$$u = \frac{V}{jd \Sigma o} \quad (\text{not to exceed 60 lbs. for stone or 30 lbs. for cinder concrete}).$$

For Square and Round Bars, refer to pages 451-457.

NOTE.—Best practice indicates that Spans of Floor Slabs should not exceed seven feet between steel beams or steel girders. Generally speaking, the span should in no case exceed 10 feet for ordinary work.

REINFORCED CONCRETE FLOOR SLABS.

Values deduced from formulæ, page 92, using unit stresses based on modern safe practice.

| Concrete. | Weight per cu. ft. Pounds. | C | S | $r = \frac{E_s}{E_c + E_s}$ | P | K | I | J |
|-------------------|----------------------------------|-----|-------|-----------------------------|-------|------|------|------|
| Stone. 1:2:4. | 150 | 500 | 16000 | 15 | .0050 | 71.5 | .320 | .893 |
| Cinder. 1:2:4. | 110 | 185 | 16000 | 30 | .0015 | 21.8 | .258 | .914 |

THICKNESS OF CONCRETE BELOW STEEL.

| Depth of Slab "d" (inches). | $2\frac{1}{2}$ to 4 | $4\frac{1}{2}$ to $8\frac{1}{2}$ | 9 to 12 | 13 to 18 | 19 to 20 | Above 20 |
|---|---------------------------|--|----------------|----------------|----------------|-------------|
| Thickness of Concrete below Lower Surface of Steel Rods (inches). | $\frac{3}{4}$ | 1 | $1\frac{1}{4}$ | $1\frac{1}{2}$ | $1\frac{3}{4}$ | 2 |

SPACING OF REINFORCING BARS.

The lateral spacing of parallel bars should not be less than two and one-half diameters, center to center, nor greater than $2\frac{1}{2} \times$ thickness of slab; nor should the distance from edge of slab to center of nearest bar be less than one and one-half diameters. The clear spacing between two layers of bars should not be less than one-half inch.

Cross reinforcement of steel rods of small diameter ($\frac{1}{4}$ ") laid parallel to the principal beams upon which the slab rests, should be used to prevent shrinkage and temperature cracks and to give added strength. They should be spaced about two feet, center to center.

DISTRIBUTION OF LOAD FOR SLABS OF FOUR SIDES SUPPORT.

Where length of slab exceeds 1.5 width, the entire load should be carried by transverse reinforcement. Slabs of smaller ratio of dimension may well be reinforced in both directions. Distribution of the load may be determined by use of the formula

$$r = \frac{l^4}{l^4 + b^4}$$

in which r = proportion of load carried by transverse reinforcement, l = length and b = breadth of slab.

Using values thus determined, each set of reinforcement is to be calculated as in slabs having two supports only.

NOTE.—In all cases of two-way reinforcement, intersections of rods should be securely tied with heavy wire.

LIMITING SPANS AND MAXIMUM LOADS OF I-BEAMS AND CHANNELS DUE TO CRIPPLING OF THE WEB.

I-Beams and Channels, when used as beams for very short spans in which the ratio of length of span to depth of beam is small, should be examined for safe strength of the web considered as a column, subjected to crippling due to the shearing strains.

The Tables of Safe Loads of Beams and Channels are computed with regard to the safe unit stresses due to flexure, and, with one or two exceptions, as indicated by dotted lines and accompanying foot-notes, the lengths of spans tabulated are such that the limitation due to web crippling does not appear. The shearing stresses acting in the web of a beam may be considered to consist of two stresses of equal intensity acting at right angles to each other, and at angles of 45 degrees with the neutral axis. The intensity of each of these stresses is equal to the intensity of the vertical shear, which is a maximum at the points of support for uniform loading, and uniform throughout from the point of loading to the supports for a superimposed concentrated load at the center.

The vertical shears for different systems of loading may be obtained by the use of moments in the usual way, and these are given for various cases on pages 162 to 165 inclusive.

The shearing stresses which act at angles of 45 degrees with the neutral axis are equivalent to compressive and tensile forces, and the former will tend to buckle the web, which should therefore be figured as composed of a series of columns of a length equal to its diagonal depth.

If c is the vertical depth of the web in the clear between the fillets which connect it with the flanges, the square of the length of the column to be considered will be $2c^2$.

Substituting this value for l^2 in the formula for long columns

$$p = \frac{12000}{1 + \frac{l^2}{3000 t^2}}$$

we have

$$p = \frac{12000}{1 + \frac{c^2}{1500 t^2}}$$

in which

p = intensity of vertical shear, in pounds per square inch =

$$\frac{\text{Total shear in pounds}}{dt}.$$

c = depth of web in clear between fillets in inches.

t = thickness of web in inches.

d = depth of beam in inches.

This formula is also applicable for computing the safe shearing stress in the webs of plate girders, in which case the length, l , is the vertical distance between centers of upper and lower rows of rivet holes connecting the webs and flanges.

The webs of plate girders should be reinforced by stiffening angles at points of support and concentrated loading, and in cases where the intensity of shear exceeds that given by the above formula the web should be provided with stiffeners.

The following tables have been prepared based upon the above formula for safe unit shearing stress in the webs of beams and channels.

**MAXIMUM SAFE LOADS FOR I-BEAMS OF ANY
LENGTH AND CORRESPONDING MINIMUM
SAFE SPANS BASED UPON CRIPPLING
OF THE WEB.**

For loads in pounds uniformly distributed including weight of beam.

| Section Num- ber. | Depth of Beam. | Weight per Foot. | Maximum Safe Load. | Mini- mum Span. | Section Num- ber. | Depth of Beam. | Weight per Foot. | Maximum Safe Load. | Mini- mum Span. |
|-------------------------|----------------------|------------------------|--------------------------|-----------------------|-------------------------|----------------------|------------------------|--------------------------|-----------------------|
| | Inches. | Pounds. | Pounds. | Feet. | | Inches. | Pounds. | Pounds. | Feet. |
| B 5 | 3 | 5.5 | 10900 | 1.7 | B 53 | 15 | 42 | 86530 | 7.3 |
| | | 6.5 | 17790 | 1.1 | | | 45 | 106100 | 6.2 |
| | | 7.5 | 25230 | .9 | | | 50 | 146260 | 4.8 |
| B 9 | 4 | 7.5 | 15330 | 2.1 | B 109 | 15 | 55 | 186740 | 4.0 |
| | | 8.5 | 22670 | 1.6 | | | 60 | 222970 | 3.6 |
| | | 9.5 | 30820 | 1.2 | | | 60 | 160940 | 5.5 |
| B 13 | 5 | 10.5 | 37820 | 1.1 | B 113 | 15 | 65 | 201330 | 4.6 |
| | | 9.75 | 20050 | 2.6 | | | 70 | 237380 | 4.1 |
| | | 12.25 | 39730 | 1.5 | | | 75 | 276990 | 3.7 |
| B 17 | 6 | 14.75 | 57400 | 1.2 | B 65 | 18 | 80 | 316160 | 3.4 |
| | | 12.25 | 25130 | 3.1 | | | 80 | 247900 | 4.6 |
| | | 14.75 | 44320 | 2.0 | | | 85 | 287290 | 4.2 |
| B 21 | 7 | 17.25 | 62890 | 1.6 | B 73 | 20 | 90 | 322350 | 3.9 |
| | | 15 | 30510 | 3.7 | | | 95 | 361780 | 3.6 |
| | | 17.5 | 49320 | 2.5 | | | 100 | 399220 | 3.4 |
| B 25 | 8 | 20 | 69540 | 1.9 | B 89 | 24 | 55 | 109040 | 8.8 |
| | | 18 | 36310 | 4.2 | | | 60 | 155580 | 6.6 |
| | | 20.25 | 53560 | 3.1 | | | 65 | 194040 | 5.5 |
| B 29 | 9 | 22.75 | 72760 | 2.4 | B 121 | 20 | 70 | 232870 | 4.9 |
| | | 25.25 | 91590 | 2.1 | | | 65 | 129150 | 9.6 |
| | | 21 | 42450 | 4.8 | | | 70 | 169980 | 7.3 |
| B 33 | 10 | 25 | 71530 | 3.1 | B 89 | 24 | 75 | 206910 | 6.7 |
| | | 30 | 109620 | 2.3 | | | 80 | 182710 | 8.7 |
| | | 35 | 146670 | 1.9 | | | 85 | 214600 | 7.7 |
| B 41 | 12 | 25 | 48960 | 5.4 | B 127 | 24 | 90 | 257610 | 6.6 |
| | | 30 | 86630 | 3.4 | | | 95 | 295400 | 6.0 |
| | | 35 | 126460 | 2.6 | | | 100 | 333150 | 5.5 |
| B 105 | 12 | 40 | 165320 | 2.2 | B 127 | 24 | 80 | 127540 | 14.7 |
| | | 31.5 | 62890 | 6.2 | | | 85 | 166820 | 11.8 |
| | | 35 | 91730 | 4.5 | | | 90 | 202450 | 10.1 |
| B 105 | 12 | 40 | 130540 | 3.5 | | | 95 | 239330 | 8.8 |
| | | 40 | 99380 | 4.9 | | | 100 | 277070 | 7.9 |
| | | 45 | 138110 | 3.8 | | | 105 | 203800 | 12.3 |
| B 105 | 12 | 50 | 176250 | 3.2 | | | 110 | 243290 | 10.6 |
| | | 55 | 213760 | 2.8 | | | 115 | 281900 | 9.4 |

MAXIMUM SAFE LOADS FOR STANDARD CHANNELS OF ANY LENGTH AND CORRESPONDING MINIMUM SAFE SPANS BASED UPON CRIPPLING OF THE WEB.

For loads in pounds uniformly distributed including weight of channel.

| Section Number. | Depth of Channel. Inches. | Weight per Foot. Pounds. | Maximum Safe Load. Pounds. | Minimum Span. Feet. | Section Number. | Depth of Channel. Inches. | Weight per Foot. Pounds. | Maximum Safe Load. Pounds. | Minimum Span. Feet. |
|-----------------|------------------------------|-----------------------------|-------------------------------|------------------------|-----------------|------------------------------|-----------------------------|-------------------------------|------------------------|
| C 5 | 3 | 4 | 10970 | 1.1 | C 25 | 8 | 18.75 | 83150 | 1.5 |
| | | 5 | 17830 | 0.8 | | | 21.25 | 101800 | 1.3 |
| | | 6 | 25260 | .6 | | | | | |
| C 9 | 4 | 5.25 | 14300 | 1.4 | C 29 | 9 | 13.25 | 28120 | 4.0 |
| | | 6.25 | 21660 | 1.1 | | | 15 | 42250 | 2.9 |
| | | 7.25 | 29830 | .9 | | | 20 | 80980 | 1.8 |
| | | | | | | | 25 | 118810 | 1.4 |
| C 13 | 5 | 6.5 | 17390 | 1.6 | C 33 | 10 | 15 | 30570 | 4.7 |
| | | 9 | 35900 | 1.1 | | | 20 | 67420 | 2.6 |
| | | 11.5 | 54920 | .9 | | | 25 | 107670 | 1.9 |
| | | | | | | | 30 | 147010 | 1.6 |
| C 17 | 6 | 8 | 20280 | 2.3 | | | 35 | 182940 | 1.4 |
| | | 10.5 | 39580 | 1.4 | C 41 | 12 | 20.5 | 41390 | 5.5 |
| | | 13 | 58300 | 1.1 | | | 25 | 75440 | 3.5 |
| | | 15.5 | 76540 | 1.0 | | | 30 | 114230 | 2.6 |
| C 21 | 7 | 9.75 | 22950 | 2.8 | | | 35 | 156000 | 2.1 |
| | | 12.25 | 43660 | 1.7 | | | 40 | 193920 | 1.9 |
| | | 14.75 | 62200 | 1.4 | C 53 | 15 | 33 | 83430 | 5.4 |
| | | 17.25 | 82110 | 1.2 | | | 35 | 95070 | 4.9 |
| | | 19.75 | 99880 | 1.1 | | | 40 | 130940 | 4.3 |
| C 25 | 8 | 11.25 | 25560 | 3.4 | | | 45 | 171400 | 3.2 |
| | | 13.75 | 44800 | 2.2 | | | 50 | 211750 | 2.8 |
| | | 16.25 | 64140 | 1.7 | | | 55 | 251710 | 2.5 |
| | | | | | | | | | |

**COEFFICIENTS FOR DEFLECTION IN INCHES FOR
CAMBRIA SHAPES, USED AS BEAMS SUBJECTED
TO SAFE LOADS UNIFORMLY DISTRIBUTED.**

| Distance between Supports in Feet. | Coefficient for Fibre Stress of 16 000 lbs. per Square Inch. | Coefficient for Fibre Stress of 12 500 lbs. per Square Inch. | Distance between Supports in Feet. | Coefficient for Fibre Stress of 16 000 lbs. per Square Inch. | Coefficient for Fibre Stress of 12 500 lbs. per Square Inch. |
|---|---|---|---|---|---|
| L | H | H' | L | H | H' |
| 4 | .265 | .207 | 23 | 8.756 | 6.841 |
| 5 | .414 | .323 | 24 | 9.534 | 7.448 |
| 6 | .596 | .466 | 25 | 10.345 | 8.082 |
| 7 | .811 | .634 | 26 | 11.189 | 8.741 |
| 8 | 1.059 | .828 | 27 | 12.066 | 9.427 |
| 9 | 1.341 | 1.047 | 28 | 12.977 | 10.138 |
| 10 | 1.655 | 1.293 | 29 | 13.920 | 10.875 |
| 11 | 2.003 | 1.565 | 30 | 14.897 | 11.638 |
| 12 | 2.383 | 1.862 | 31 | 15.906 | 12.427 |
| 13 | 2.797 | 2.185 | 32 | 16.949 | 13.241 |
| 14 | 3.244 | 2.534 | 33 | 18.025 | 14.082 |
| 15 | 3.724 | 2.909 | 34 | 19.134 | 14.948 |
| 16 | 4.237 | 3.310 | 35 | 20.276 | 15.841 |
| 17 | 4.783 | 3.737 | 36 | 21.451 | 16.759 |
| 18 | 5.363 | 4.190 | 37 | 22.659 | 17.703 |
| 19 | 5.975 | 4.668 | 38 | 23.901 | 18.672 |
| 20 | 6.621 | 5.172 | 39 | 25.175 | 19.668 |
| 21 | 7.299 | 5.703 | 40 | 26.483 | 20.690 |
| 22 | 8.011 | 6.259 | | | |

The above coefficients are for use in obtaining the deflection of steel shapes subjected to transverse strain, under their uniformly distributed safe loads for extreme fibre stresses of 16 000 pounds and 12 500 pounds per square inch; the modulus of elasticity being 29 000 000.

To find the deflection of any shape that is symmetrical about its neutral axis under the above conditions of loading when used as a beam, such as I-Beams, Channels, etc., divide the coefficient in the table corresponding to the given span and fibre stress, by the depth of the beam in inches. The result will be the deflection in inches.

To find the deflection of any shape that is unsymmetrical about its neutral axis when used as a beam, under the above conditions of loading, such as Angles, etc., divide the coefficient in the table corresponding to the given span and fibre stress by twice the distance of the most remote fibre from the neutral axis, expressed in inches.

If, in construction, the beam is placed in position in the usual manner upon its end supports without special scaffolding or falsework between them, it will deflect somewhat by reason of its own weight, and upon the addition of external loading a further deflection will occur.

The deflections obtained as above described are the total deflections due to the weight of the beam itself and the superimposed safe load uniformly distributed.

Thus, to find, from the preceding table, the deflection in inches for Cambria shapes used as Beams under their safe loads uniformly distributed including the weight of the beam :

Let D = deflection in inches,

L = length between supports in feet.

H = coefficient for deflection from table for fibre stress of 16 000 pounds per square inch.

H' = coefficient for deflection from table for fibre stress of 12 500 pounds per square inch.

d = depth of beam in inches for symmetrical sections.

x_1 = distances in inches from neutral axis to most remote fibre for unsymmetrical sections.

FOR SYMMETRICAL SECTIONS.

For fibre stress of 16 000 pounds per square inch $D = \frac{H}{d}$

For fibre stress of 12 500 pounds per square inch $D = \frac{H'}{d}$

FOR UNSYMMETRICAL SECTIONS.

For fibre stress of 16 000 pounds per square inch $D = \frac{H}{2x_1}$

For fibre stress of 12 500 pounds per square inch $D = \frac{H'}{2x_1}$

EXAMPLES.

Case I.—To find the deflection of a 9" I-Beam weighing 30 pounds per foot, for a span of 15 feet and a maximum fibre stress of 16 000 pounds per square inch, under its safe load uniformly distributed.

From the above table the deflection coefficient for this case is found to be 3.724 which divided by 9, the depth of the beam in inches, gives .414, which is the required deflection in inches.

The safe load for this beam under the conditions named is 16 100 pounds including the weight of the beam itself as stated in the Tables of Safe Loads for Cambria I-Beams on page 109.

Case II.—To find the deflection of a 6" \times 4" \times $\frac{1}{2}$ " angle, supported at the ends on its short leg as a horizontal base, for a span of 9 feet and a maximum fibre stress of 16 000 pounds per square inch under its safe load uniformly distributed including its own weight.

From the table of "Properties of Angles" on page 207 the distance x' from the neutral axis to the back of the shorter leg is found to be 1.99 inches, which subtracted from the length of long leg, 6 inches, gives 4.01 as the distance x_1 from the neutral axis to the most remote fibre. From the above table the deflection coefficient for this case is found to be 1.341, which divided by 8.02, twice x_1 , gives .167, which is the required deflection in inches.

NOTE.—For deflections of Beams and Channels due to any central or uniform load see coefficients of deflection N and N' in the Tables of Properties relating to these sections and the accompanying explanations.

For deflections of any symmetrical beams due to various systems of loading, see general formulæ and diagrams on pages 160 to 165 inclusive.

TABLES OF SAFE LOADS FOR CAMBRIA SECTIONS USED AS BEAMS, AND SPACING FOR CAMBRIA I-BEAMS.

Pages 106 to 159 inclusive.

TABLES OF SAFE LOADS AND SPACINGS.

The Tables of Safe Loads for Cambria I-Beams, Channels, and Angles, give the safe loads in pounds uniformly distributed for all usual spans based upon extreme fibre stresses of 16 000 pounds per square inch.

These loads include the weight of the steel shape itself, which should be deducted in order to obtain the external load that it will safely carry. In case the shape is used to support a floor, the weight of the steel, together with that of the other portions of the floor construction, must be deducted in order to obtain the net live load which can be safely sustained. Weights of hollow tile floor arches and fireproofing material are given on page 69. to which should be added the weight of plastering, filling on top of arches and the weight of the material forming the surface of the floor, in order to obtain the dead load of materials in figuring fireproof floors, in addition to the weight of the steel.

A table of superimposed loads per square foot, exclusive of the weights of materials, in accordance with the usual practice for different classes of buildings, is given on p. 52.

The Tables of Safe Loads for Cambria sections used as beams and the Tables for Spacing of Cambria I-Beams are calculated on the assumption that proper provision has been made for preventing lateral deflection by means of tie-rods or other braces spaced at suitable distances apart; which for beams and channels should not exceed twenty times the flange width. In cases where intermediate lateral support is not provided, the safe loads shown in the tables must be reduced, and for beams and channels the

amount of this reduction can be determined by reference to the explanations and tables therefor on pages 82 and 83.

The thrust of floor arches, which is considerable, particularly in the case of long spans or distances between tie-rods, should be taken into account where it tends to produce lateral flexure of the floor beams.

Explanations of this and a formula for reducing the unit stresses from vertical loading, on account of the additional stresses caused by horizontal forces, are given on pages 78 to 81 inclusive.

In some instances the allowable deflection will govern the design rather than the transverse strength, as in the case of beams carrying plastered ceilings, in which the deflection should be limited to $\frac{1}{360}$ inch per foot of span, or $\frac{1}{360}$ of the distance between supports in order to avoid cracking the plaster.

This limit of deflection is indicated in the tables by full horizontal lines, the figures below which correspond to loads or spacings for the given spans that will produce greater deflections than the allowable limit for plastered ceilings.

The deflection limits of the Tables of Safe Loads have been calculated for the total loads, including the weight of the section used as a beam. The superimposed live load will not produce all of this deflection, and therefore the deflection limit of the tables includes an element of safety for the reason that the beams will be deflected, after being put in place, by their own weight and that of the floor materials before the plastering is applied.

In cases where the deflection limits the use of the beam for the safe loads corresponding to the fibre stresses of the tables, the beam may be used with a less load such as to produce only the allowable deflection. The lesser load corresponding to the limit of deflection may be obtained for any span from the Table of Safe Loads as follows:

$$W = \frac{W_s \times L^2}{L_1^2}$$

in which

W = safe load in pounds for the limit of deflection for plastered ceilings = $\frac{1}{860}$ of the span.

W_s = safe load of tables next above the line giving the limit of deflection.

L = length of span in feet corresponding to W_s from the table

L_1 = length of span for the case under consideration.

This may also be expressed by the following—

RULE.

Multiply the safe load next above the heavy line of the tables by the square of the corresponding span in feet and divide the product by the square of the required span. The result will be the required load corresponding to the limit of allowable deflection for plastered ceilings.

A Table of Deflections for Cambria shapes used as beams, subjected to their safe loads uniformly distributed, and accompanying explanations with examples, are given on pages 98 and 99.

TABLES OF SAFE LOADS FOR I-BEAMS AND CHANNELS.

Tables of Safe Loads for all sizes and weights of Cambria I-Beams and channels for the usual spans, expressed in feet, are given on pages 106 to 123 inclusive.

TABLES FOR SPACING OF CAMBRIA I-BEAMS.

Tables for Spacing of Cambria I-Beams for a total load of 100 pounds per square foot including the weight of the beam, corresponding to spans from 4 to 48 feet, are given on pages 124 to 135 inclusive.

For any given size of beam the spacing or distances from centers to centers for different intensities of loading varies inversely as the load, so that the spacing for any intensity of loading may be found from the tabular spacing by proportion as stated in the notes at the foot of the tables.

TABLES OF SAFE LOADS FOR ANGLES.

Tables of uniformly distributed safe loads for the usual sizes of angles, are given on pages 138 to 159. In these tables the safe loads for equal leg angles are given on the assumption that one of the legs of the angle is horizontal and the other leg vertical. In the case of angles with unequal legs the safe loads are given for both positions, that is, with the long leg vertical and with the short leg vertical.

EXAMPLES OF APPLICATION OF TABLES OF SAFE LOADS AND TABLES OF SPACING.

EXAMPLE I.

What is the proper size of beam with a clear span of 24 feet to carry a superimposed load of 30 000 pounds uniformly distributed, the deflection to be such as not to crack a plastered ceiling?

From the Tables of Safe Loads for Cambria I-Beams, page 111, it is found that a 15-inch standard beam of this length, weighing 60 pounds per foot, will carry a gross load of 31 910 pounds, and the weight of the beam itself is $60 \times 24 = 1440$ pounds. Thus the net load may be 30 470 pounds, so that this is the proper size for the conditions named, as its deflection is within the allowable limit, which is shown to be at a span of 30 feet as indicated by the horizontal line on the table.

Similarly it may be found from page 112, that a 15-inch special beam, of 60 pounds per foot, will more than suffice, but as this section is not regularly kept in stock the standard 15-inch 60-pound beam should be ordered if prompt delivery is wanted.

It may also be found from page 114, that an 18-inch 55-pound beam will amply suffice, and as this is both stiffer and lighter than the 15-inch 60-pound beams, it could be used with economy if otherwise suitable for the location.

EXAMPLE II.

What is the safe load for an 8-inch standard I-Beam weighing 18.0 pounds per foot for a span of 20 feet, the deflection to be such as not to crack a plastered ceiling?

From the Tables of Safe Loads, page 108, it is found that the safe load for the beam in question is 7 580 pounds, but this value is below the line which indicates the span corresponding to the allowable limit of deflection.

Substituting the proper values in the formula for obtaining the reduced load corresponding to the allowable deflection, as given on page 101, we have

$$W = \frac{W_s \times L^2}{L_1^2} = \frac{9\,480 \times 16^2}{20^2} = 6\,067 \text{ pounds.}$$

which is the safe load required.

EXAMPLE III.

Required the best arrangement of beams for the floor system of a building 40 feet wide x 88 feet deep to safely support a live load of 100 pounds per square foot, using 10-inch tile arches resting on 12-inch I-Beams.

The weight of the floor materials will be about 50 pounds per square foot, allowing 39 pounds for the arch and 11 pounds for the other materials, or a total load of 150 pounds per square foot to be carried by the beams.

From the Table of Spacing for I-Beams for a uniform load of 100 pounds per square foot, page 128, it is seen that 12" standard I-Beams weighing $31\frac{1}{2}$ pounds per foot and spaced 9.6 feet apart from center to center can be used with a span of 20 feet, and for a load of 150 pounds per square foot the spacing will be

$$\frac{9.6 \times 100}{150} = 6.4 \text{ feet.}$$

This will require one row of interior columns lengthwise of building.

To support the beams at the center of the building will require a line of girder beams resting on the columns. Assume the columns 22 feet apart, thus dividing the building into 8 bays, four on each side of the center.

The load on each girder will be

$$\frac{40}{2} \times 22 \times 150 = 66\,000 \text{ pounds.}$$

From the Table of Safe Loads, page 111, it is found that this will require two 15-inch standard I-Beams, each weighing 60 pounds per foot.

On account of the advisability of spacing the floor beams equally, the arrangement outlined above would reduce their distances to $\frac{22}{4} = 5.5$ feet center to center, so that 10-inch I-Beams, weighing 40 pounds per foot, might be used for the body of the floor, as may be determined by referring to the Table of Spacings of Cambria I-Beams, page 127, and calculating as before, with the result that the allowable spacing for these conditions is found to be 5.7 feet. The 10-inch 40-pound beam under these conditions, will, however, deflect almost to the allowable limit for plastered ceilings, besides, they are heavier than the 12-inch 31.5-pound beams first considered, so that the latter will be the stiffer and more economical.

Although the load on the girder is not uniformly distributed, but concentrated at three points between the supports, the bending moment in this case will be the same as if the load were figured to be distributed uniformly, and for similar cases with different spacings the moments would be very nearly identical.

TABLES OF MAXIMUM BENDING MOMENTS.

The Tables of Maximum Bending Moments for beams and channels given on pages 136 and 137 are useful in determining the proper section required to support one or more irregularly located concentrated loads or various arrangements of loads to which the tables of safe loads uniformly distributed will not apply.

The method used consists in computing the maximum bending moment in foot pounds resulting from the specified loading, the proper section corresponding to a fibre stress of 16 000 or 12 500 lbs. per square inch, being taken directly from the tables without further computation.

SAFE LOADS IN POUNDS UNIFORMLY DISTRIBUTED FOR CAMBRIA I-BEAMS.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of beam.

| Distance between supports in feet. | STANDARD I-BEAMS. | | | | | | |
|---|-------------------|-------------|-------------|-----------------|-------------|-------------|--------------|
| | 3 Inch No. B 5. | | | 4 Inch No. B 9. | | | |
| | 5.5 lbs. | 6.5 lbs. | 7.5 lbs. | 7.5 lbs. | 8.5 lbs. | 9.5 lbs. | 10.5 lbs. |
| 4 | 4410 | 4780 | 5180 | 7950 | 8470 | 9000 | 9520 |
| 5 | 3530 | 3830 | 4140 | 6360 | 6780 | 7200 | 7610 |
| 6 | 2940 | 3190 | 3450 | 5300 | 5650 | 6000 | 6350 |
| 7 | 2520 | 2730 | 2960 | 4540 | 4840 | 5140 | 5440 |
| 8 | 2210 | 2390 | 2590 | 3980 | 4240 | 4500 | 4760 |
| 9 | 1960 | 2130 | 2300 | 3530 | 3770 | 4000 | 4230 |
| 10 | 1770 | 1910 | 2070 | 3180 | 3390 | 3600 | 3810 |
| 11 | 1600 | 1740 | 1880 | 2890 | 3080 | 3270 | 3460 |
| 12 | 1470 | 1590 | 1730 | 2650 | 2820 | 3000 | 3170 |
| 13 | 1360 | 1470 | 1590 | 2450 | 2610 | 2770 | 2930 |
| 14 | 1260 | 1370 | 1480 | 2270 | 2420 | 2570 | 2720 |
| 15 | 1180 | 1280 | 1380 | 2120 | 2260 | 2400 | 2540 |
| 16 | 1100 | 1200 | 1290 | 1990 | 2120 | 2250 | 2380 |
| 17 | 1040 | 1130 | 1220 | 1870 | 1990 | 2120 | 2240 |
| 18 | 980 | 1060 | 1150 | 1770 | 1880 | 2000 | 2120 |
| 19 | 930 | 1010 | 1090 | 1670 | 1780 | 1890 | 2000 |
| 20 | 880 | 960 | 1040 | 1590 | 1690 | 1800 | 1900 |
| 21 | 840 | 910 | 990 | 1510 | 1610 | 1710 | 1810 |

For safe loads below the heavy lines, the deflections will be greater than the allowable limit for plastered ceilings = $\frac{1}{360}$ span.

SAFE LOADS IN POUNDS UNIFORMLY DISTRIBUTED FOR CAMBRIA I-BEAMS.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of beam.

| Distance between supports in feet. | STANDARD I-BEAMS. | | | | | |
|---|-------------------|---------------|---------------|------------------|---------------|---------------|
| | 5 Inch No. B 13. | | | 6 Inch No. B 17. | | |
| | 9.75 lbs. | 12.25 lbs. | 14.75 lbs. | 12.25 lbs. | 14.75 lbs. | 17.25 lbs. |
| 4 | 12900 | 14520 | 16160 | 19370 | 21320 | 23280 |
| 5 | 10320 | 11620 | 12930 | •15490 | •17050 | 18620 |
| 6 | 8600 | 9680 | 10770 | 12910 | 14210 | •15520 |
| 7 | 7370 | 8300 | 9230 | 11070 | 12180 | 13300 |
| 8 | 6450 | 7260 | 8080 | 9680 | 10660 | 11640 |
| 9 | 5730 | 6460 | 7180 | 8610 | 9470 | 10350 |
| 10 | 5160 | 5810 | 6460 | 7750 | 8530 | 9310 |
| 11 | 4690 | 5280 | 5880 | 7040 | 7750 | 8460 |
| 12 | 4300 | 4840 | 5390 | 6460 | 7110 | 7760 |
| 13 | 3970 | 4470 | 4970 | 5960 | 6560 | 7160 |
| 14 | 3680 | 4150 | 4620 | 5530 | 6090 | 6650 |
| 15 | 3440 | 3870 | 4310 | 5160 | 5680 | 6210 |
| 16 | 3220 | 3630 | 4040 | 4840 | 5330 | 5820 |
| 17 | 3030 | 3420 | 3800 | 4560 | 5020 | 5480 |
| 18 | 2870 | 3230 | 3590 | 4300 | 4740 | 5170 |
| 19 | 2720 | 3060 | 3400 | 4080 | 4490 | 4900 |
| 20 | 2580 | 2900 | 3230 | 3870 | 4260 | 4660 |
| 21 | 2460 | 2770 | 3080 | 3690 | 4060 | 4430 |
| 22 | 2340 | 2640 | 2940 | 3520 | 3880 | 4230 |
| 23 | 2240 | 2530 | 2810 | 3370 | 3710 | 4050 |
| 24 | 2150 | 2420 | 2690 | 3230 | 3550 | 3880 |
| 25 | 2060 | 2320 | 2590 | 3100 | 3410 | 3720 |
| 26 | 1980 | 2230 | 2490 | 2980 | 3280 | 3580 |
| 27 | 1910 | 2150 | 2390 | 2870 | 3160 | 3450 |
| 28 | | | | 2770 | 3050 | 3330 |

For safe loads below the heavy lines, the deflections will be greater than the allowable limit for plastered ceilings = $\frac{1}{360}$ span.

Above single dot, safe loads are too great for standard connections.

SAFE LOADS IN POUNDS UNIFORMLY DISTRIBUTED FOR CAMBRIA I-BEAMS.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of beam.

| Distance between supports in feet. | STANDARD I-BEAMS. | | | | | | |
|---|-------------------|--------------|------------|------------------|---------------|---------------|---------------|
| | 7 Inch No. B 21. | | | 8 Inch No. B 25. | | | |
| | 15 lbs. | 17.5 lbs. | 20 lbs. | 18.00 lbs. | 20.25 lbs. | 22.75 lbs. | 25.25 lbs. |
| 4 | 27600 | 29850 | 32140 | | | | |
| 5 | 22080 | 23880 | 25710 | 30330 | 32100 | 34190 | 36290 |
| 6 | 18400 | 19900 | 21430 | 25280 | 26750 | 28500 | •30240 |
| 7 | •15770 | •17060 | 18370 | 21670 | 22930 | 24420 | 25920 |
| 8 | 13800 | 14930 | •16070 | 18960 | 20060 | 21370 | 22680 |
| 9 | 12270 | 13270 | 14280 | 16850 | 17830 | 19000 | 20160 |
| 10 | 11040 | 11940 | 12860 | 15170 | 16050 | 17100 | 18140 |
| 11 | 10040 | 10860 | 11690 | 13790 | 14590 | 15540 | 16490 |
| 12 | 9200 | 9950 | 10710 | 12640 | 13380 | 14250 | 15120 |
| 13 | 8490 | 9190 | 9890 | 11670 | 12350 | 13150 | 13960 |
| 14 | 7890 | 8530 | 9180 | 10830 | 11470 | 12210 | 12960 |
| 15 | 7360 | 7960 | 8570 | 10110 | 10700 | 11400 | 12100 |
| 16 | 6900 | 7460 | 8030 | 9480 | 10030 | 10690 | 11340 |
| 17 | 6490 | 7020 | 7560 | 8920 | 9440 | 10060 | 10670 |
| 18 | 6130 | 6630 | 7140 | 8430 | 8920 | 9500 | 10080 |
| 19 | 5810 | 6280 | 6770 | 7980 | 8450 | 9000 | 9550 |
| 20 | 5520 | 5970 | 6430 | 7580 | 8030 | 8550 | 9070 |
| 21 | 5260 | 5690 | 6120 | 7220 | 7640 | 8140 | 8640 |
| 22 | 5020 | 5430 | 5840 | 6890 | 7300 | 7770 | 8250 |
| 23 | 4800 | 5190 | 5590 | 6590 | 6980 | 7430 | 7890 |
| 24 | 4600 | 4980 | 5360 | 6320 | 6690 | 7120 | 7560 |
| 25 | 4420 | 4780 | 5140 | 6070 | 6420 | 6840 | 7260 |
| 26 | 4250 | 4590 | 4940 | 5830 | 6170 | 6580 | 6980 |
| 27 | 4090 | 4420 | 4760 | 5620 | 5940 | 6330 | 6720 |
| 28 | 3940 | 4260 | 4590 | 5420 | 5730 | 6110 | 6480 |
| 29 | 3810 | 4120 | 4430 | 5230 | 5530 | 5900 | 6260 |

For safe loads below the heavy lines, the deflections will be greater than the allowable limit for plastered ceilings = $\frac{1}{360}$ span.

Above single dot, safe loads are too great for standard connections.

SAFE LOADS IN POUNDS UNIFORMLY DISTRIBUTED FOR CAMBRIA I-BEAMS.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of beam.

| Distance between supports in feet. | STANDARD I-BEAMS. | | | | | | | |
|---|-------------------|------------|------------|------------|-------------------|------------|------------|------------|
| | 9 Inch No. B 29. | | | | 10 Inch No. B 33. | | | |
| | 21 lbs. | 25 lbs. | 30 lbs. | 35 lbs. | 25 lbs. | 30 lbs. | 35 lbs. | 40 lbs. |
| 8 | 25160 | 27240 | 30180 | 33120 | | | | |
| 9 | 22370 | 24210 | 26830 | 29440 | | | | |
| 10 | 20130 | 21790 | 24150 | 26500 | 26050 | 28620 | 31240 | 33850 |
| 11 | 18300 | 19810 | 21950 | 24090 | 23680 | 26020 | 28400 | 30780 |
| 12 | 16770 | 18160 | 20120 | 22080 | 21710 | 23850 | 26030 | 28210 |
| 13 | 15480 | 16760 | 18570 | 20380 | 20040 | 22020 | 24030 | 26040 |
| 14 | 14380 | 15570 | 17250 | 18930 | 18610 | 20450 | 22310 | 24180 |
| 15 | 13420 | 14530 | 16100 | 17670 | 17360 | 19080 | 20830 | 22570 |
| 16 | 12580 | 13620 | 15090 | 16560 | 16280 | 17890 | 19520 | 21160 |
| 17 | 11840 | 12820 | 14200 | 15590 | 15320 | 16840 | 18380 | 19910 |
| 18 | 11180 | 12110 | 13410 | 14720 | 14470 | 15900 | 17350 | 18810 |
| 19 | 10590 | 11470 | 12710 | 13950 | 13710 | 15070 | 16440 | 17820 |
| 20 | 10064 | 10900 | 12070 | 13250 | 13020 | 14310 | 15620 | 16930 |
| 21 | 9590 | 10380 | 11500 | 12620 | 12400 | 13630 | 14880 | 16120 |
| 22 | 9150 | 9910 | 10980 | 12050 | 11840 | 13010 | 14200 | 15390 |
| 23 | 8750 | 9480 | 10500 | 11520 | 11320 | 12450 | 13580 | 14720 |
| 24 | 8390 | 9080 | 10060 | 11040 | 10850 | 11930 | 13020 | 14110 |
| 25 | 8050 | 8720 | 9660 | 10600 | 10420 | 11450 | 12500 | 13540 |
| 26 | 7740 | 8380 | 9290 | 10190 | 10020 | 11010 | 12020 | 13020 |
| 27 | 7460 | 8070 | 8940 | 9810 | 9650 | 10600 | 11570 | 12540 |
| 28 | 7190 | 7780 | 8620 | 9460 | 9300 | 10220 | 11160 | 12090 |
| 29 | 6940 | 7510 | 8330 | 9140 | 8980 | 9870 | 10770 | 11670 |
| 30 | 6710 | 7260 | 8050 | 8830 | 8680 | 9540 | 10410 | 11280 |
| 31 | 6490 | 7030 | 7790 | 8550 | 8400 | 9230 | 10080 | 10920 |
| 32 | | | | | 8140 | 8950 | 9760 | 10580 |
| 33 | | | | | 7890 | 8670 | 9470 | 10260 |

For safe loads below the heavy lines, the deflections will be greater than the allowable limit for plastered ceilings = $\frac{1}{360}$ span.

SAFE LOADS IN POUNDS UNIFORMLY DISTRIBUTED FOR CAMBRIA I-BEAMS.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of beam.

| Distance between supports in feet. | STANDARD I-BEAMS. | | | SPECIAL I-BEAMS. | | | |
|---|----------------------|------------|------------|---------------------|------------|------------|------------|
| | 12 Inch No. B 41. | | | 12 Inch No. B 105. | | | |
| | 31.5 lbs. | 35 lbs. | 40 lbs. | 40 lbs. | 45 lbs. | 50 lbs. | 55 lbs. |
| 10 | 38370 | 40580 | 43720 | 47810 | 50790 | 53930 | 57070 |
| 11 | 34880 | 36890 | 39740 | 43470 | 46180 | •49030 | •51880 |
| 12 | 31970 | 33820 | 36430 | 39840 | 42330 | 44940 | 47560 |
| 13 | 29510 | 31220 | 33630 | 36780 | 39070 | 41480 | 43900 |
| 14 | 27400 | 28990 | 31230 | 34150 | 36280 | 38520 | 40760 |
| 15 | 25580 | 27050 | 29140 | 31880 | 33860 | 35950 | 38040 |
| 16 | 23980 | 25360 | 27320 | 29880 | 31750 | 33710 | 35670 |
| 17 | 22570 | 23870 | 25720 | 28130 | 29880 | 31720 | 33570 |
| 18 | 21310 | 22540 | 24290 | 26560 | 28220 | 29960 | 31700 |
| 19 | 20190 | 21360 | 23010 | 25160 | 26730 | 28380 | 30040 |
| 20 | 19180 | 20290 | 21860 | 23910 | 25400 | 26960 | 28530 |
| 21 | 18270 | 19320 | 20820 | 22770 | 24190 | 25680 | 27170 |
| 22 | 17440 | 18450 | 19870 | 21730 | 23090 | 24510 | 25940 |
| 23 | 16680 | 17640 | 19010 | 20790 | 22080 | 23450 | 24810 |
| 24 | 15990 | 16910 | 18220 | 19920 | 21160 | 22470 | 23780 |
| 25 | 15350 | 16230 | 17490 | 19130 | 20320 | 21570 | 22830 |
| 26 | 14760 | 15610 | 16810 | 18390 | 19540 | 20740 | 21950 |
| 27 | 14210 | 15030 | 16190 | 17710 | 18810 | 19970 | 21140 |
| 28 | 13700 | 14490 | 15610 | 17080 | 18140 | 19260 | 20380 |
| 29 | 13230 | 13990 | 15070 | 16490 | 17510 | 18600 | 19680 |
| 30 | 12790 | 13530 | 14570 | 15940 | 16930 | 17980 | 19020 |
| 31 | 12380 | 13090 | 14100 | 15420 | 16380 | 17400 | 18410 |
| 32 | 11990 | 12680 | 13660 | 14940 | 15870 | 16850 | 17830 |
| 33 | 11630 | 12300 | 13250 | 14490 | 15390 | 16340 | 17290 |
| 34 | 11280 | 11940 | 12860 | 14060 | 14940 | 15860 | 16780 |
| 35 | 10960 | 11590 | 12490 | 13660 | 14510 | 15410 | 16300 |

For safe loads below the heavy lines, the deflections will be greater than the allowable limit for plastered ceilings = $\frac{1}{360}$ span.

Above single dot, safe loads are too great for standard connections.

SAFE LOADS IN POUNDS UNIFORMLY DISTRIBUTED FOR CAMBRIA I-BEAMS.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of beam.

| Distance between supports in feet. | STANDARD I-BEAM. | | | | |
|--|-------------------|------------|------------|------------|------------|
| | 15 Inch No. B 53. | | | | |
| | 42 lbs. | 45 lbs. | 50 lbs. | 55 lbs. | 60 lbs. |
| 10 | 62830 | 64830 | 68750 | 72670 | 76600 |
| 11 | 57120 | 58940 | 62500 | •66070 | •69630 |
| 12 | 52360 | 54030 | 57290 | 60560 | 63830 |
| 13 | 48330 | 49870 | 52890 | 55900 | 58920 |
| 14 | 44880 | 46310 | 49110 | 51910 | 54710 |
| 15 | 41880 | 43220 | 45840 | 48450 | 51060 |
| 16 | 39270 | 40520 | 42970 | 45420 | 47870 |
| 17 | 36960 | 38140 | 40440 | 42750 | 45060 |
| 18 | 34900 | 36020 | 38200 | 40370 | 42550 |
| 19 | 33070 | 34120 | 36190 | 38250 | 40310 |
| 20 | 31410 | 32420 | 34380 | 36340 | 38300 |
| 21 | 29920 | 30870 | 32740 | 34610 | 36470 |
| 22 | 28560 | 29470 | 31250 | 33030 | 34820 |
| 23 | 27320 | 28190 | 29890 | 31600 | 33300 |
| 24 | 26130 | 27010 | 28650 | 30280 | 31910 |
| 25 | 25130 | 25930 | 27500 | 29070 | 30640 |
| 26 | 24160 | 24940 | 26440 | 27950 | 29460 |
| 27 | 23270 | 24010 | 25460 | 26920 | 28370 |
| 28 | 22440 | 23150 | 24550 | 25960 | 27360 |
| 29 | 21660 | 22360 | 23710 | 25060 | 26410 |
| 30 | 20940 | 21610 | 22920 | 24220 | 25530 |
| 31 | 20270 | 20910 | 22180 | 23440 | 24710 |
| 32 | 19630 | 20260 | 21490 | 22710 | 23940 |
| 33 | 19040 | 19650 | 20830 | 22020 | 23210 |
| 34 | 18480 | 19070 | 20220 | 21370 | 22530 |
| 35 | 17950 | 18520 | 19640 | 20760 | 21880 |

For safe loads below the heavy lines, the deflections will be greater than the allowable limit for plastered ceilings = $\frac{1}{360}$ span.

Above single dot, safe loads are too great for standard connections.

SAFE LOADS IN POUNDS UNIFORMLY DISTRIBUTED FOR CAMBRIA I-BEAMS.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of beam.

| Distance between supports in feet. | SPECIAL I-BEAM. | | | | |
|--|--------------------|------------|------------|------------|------------|
| | 15 Inch No. B 109. | | | | |
| | 60 lbs. | 65 lbs. | 70 lbs. | 75 lbs. | 80 lbs. |
| 10 | 86610 | 90470 | 94390 | 98310 | 102230 |
| 11 | 78740 | 82240 | 85810 | 89370 | 92940 |
| 12 | 72180 | 75390 | 78660 | 81920 | 85190 |
| 13 | • 66630 | • 69590 | 72610 | 75620 | 78640 |
| 14 | 61870 | 64620 | • 67420 | • 70220 | 73020 |
| 15 | 57740 | 60310 | 62920 | 65540 | • 68150 |
| 16 | 54130 | 56540 | 58990 | 61440 | 63890 |
| 17 | 50950 | 53220 | 55520 | 57830 | 60140 |
| 18 | 48120 | 50260 | 52440 | 54620 | 56790 |
| 19 | 45590 | 47610 | 49680 | 51740 | 53810 |
| 20 | 43310 | 45230 | 47190 | 49150 | 51120 |
| 21 | 41240 | 43080 | 44950 | 46810 | 48680 |
| 22 | 39370 | 41120 | 42900 | 44690 | 46470 |
| 23 | 37660 | 39330 | 41040 | 42740 | 44450 |
| 24 | 36090 | • 37690 | 39330 | 40960 | 42600 |
| 25 | 34650 | 36190 | 37750 | 39320 | 40890 |
| 26 | 33310 | 34790 | 36300 | 37810 | 39320 |
| 27 | 32080 | 33510 | 34960 | 36410 | 37860 |
| 28 | 30930 | 32310 | 33710 | 35110 | 36510 |
| 29 | 29870 | 31200 | 32550 | 33900 | 35250 |
| 30 | 28870 | 30160 | 31460 | 32770 | 34080 |
| 31 | 27940 | 29180 | 30450 | 31710 | 32980 |
| 32 | 27070 | 28270 | 29500 | 30720 | 31950 |
| 33 | 26250 | 27410 | 28600 | 29790 | 30980 |
| 34 | 25470 | 26610 | 27760 | 28910 | 30070 |
| 35 | 24750 | 25850 | 26970 | 28090 | 29210 |

For safe loads below the heavy lines, the deflections will be greater than the allowable limit for plastered ceilings = $\frac{1}{360}$ span.

Above single dot, safe loads are too great for standard connections.

SAFE LOADS IN POUNDS UNIFORMLY DISTRIBUTED FOR CAMBRIA I-BEAMS.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of beam.

| Distance between supports in feet. | SPECIAL I-BEAM. | | | | |
|--|--------------------|------------|------------|------------|-------------|
| | 15 Inch No. B 113. | | | | |
| | 80 lbs. | 85 lbs. | 90 lbs. | 95 lbs. | 100 lbs. |
| 10 | 112230 | 116030 | 119960 | 123880 | 127800 |
| 11 | 102030 | 105490 | 109050 | 112620 | 116180 |
| 12 | 93520 | 96700 | 99960 | 103230 | 106500 |
| 13 | 86330 | 89260 | 92270 | 95290 | 98310 |
| 14 | 80160 | 82880 | 85680 | 88480 | 91280 |
| 15 | 74820 | 77360 | 79970 | 82580 | 85200 |
| 16 | •70140 | 72520 | 74970 | 77420 | 79870 |
| 17 | 66020 | •68260 | •70560 | 72870 | 75180 |
| 18 | 62350 | 64460 | 66640 | •68820 | 71000 |
| 19 | 59070 | 61070 | 63130 | 65200 | •67260 |
| 20 | 56110 | 58020 | 59980 | 61940 | 63900 |
| 21 | 53440 | 55250 | 57120 | 58990 | 60860 |
| 22 | 51010 | 52740 | 54530 | 56310 | 58090 |
| 23 | 48800 | 50450 | 52150 | 53860 | 55560 |
| 24 | 46760 | 48350 | 49980 | 51620 | 53250 |
| 25 | 44890 | 46410 | 47980 | 49550 | 51120 |
| 26 | 43170 | 44630 | 46140 | 47650 | 49150 |
| 27 | 41570 | 42980 | 44430 | 45880 | 47330 |
| 28 | 40080 | 41440 | 42840 | 44240 | 45640 |
| 29 | 38700 | 40010 | 41360 | 42720 | 44070 |
| 30 | 37410 | 38680 | 39990 | 41290 | 42600 |
| 31 | 36200 | 37430 | 38700 | 39960 | 41230 |
| 32 | 35070 | 36260 | 37490 | 38710 | 39940 |
| 33 | 34010 | 35160 | 36350 | 37540 | 38730 |
| 34 | 33010 | 34130 | 35280 | 36430 | 37590 |
| 35 | 32070 | 33150 | 34270 | 35390 | 36510 |

For safe loads below the heavy lines, the deflections will be greater than the allowable limit for plastered ceilings = $\frac{1}{360}$ span.

Above single dot, safe loads are too great for standard connections.

SAFE LOADS IN POUNDS UNIFORMLY DISTRIBUTED FOR CAMBRIA I-BEAMS.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of beam.

| Distance between supports in feet. | STANDARD I-BEAMS. | | | | | | |
|---|-------------------|------------|------------|------------|-------------------|------------|------------|
| | 18 Inch No. B 65. | | | | 20 Inch No. B 73. | | |
| | 55 lbs. | 60 lbs. | 65 lbs. | 70 lbs. | 65 lbs. | 70 lbs. | 75 lbs. |
| 14 | 67350 | 71260 | 74620 | 77990 | 89110 | 92940 | 96670 |
| 15 | 62860 | •66510 | •69650 | 72790 | 83170 | 86740 | 90230 |
| 16 | 58930 | 62360 | 65300 | •68240 | 77970 | 81320 | 84590 |
| 17 | 55460 | 58650 | 61460 | 64220 | 73380 | 76540 | 79610 |
| 18 | 52380 | 55430 | 58040 | 60660 | •69310 | 72280 | 75190 |
| 19 | 49630 | 52510 | 54990 | 57460 | 65660 | •68480 | 71230 |
| 20 | 47140 | 49880 | 52240 | 54590 | 62370 | 65060 | •67670 |
| 21 | 44900 | 47510 | 49750 | 51990 | 59400 | 61960 | 64450 |
| 22 | 42860 | 45350 | 47490 | 49360 | 56700 | 59140 | 61520 |
| 23 | 40990 | 43380 | 45420 | 47470 | 54240 | 56570 | 58840 |
| 24 | 39290 | 41570 | 43530 | 45490 | 51980 | 54210 | 56390 |
| 25 | 37720 | 39910 | 41790 | 43670 | 49900 | 52040 | 54140 |
| 26 | 36260 | 38370 | 40180 | 41990 | 47980 | 50040 | 52050 |
| 27 | 34920 | 36950 | 38690 | 40440 | 46200 | 48190 | 50130 |
| 28 | 33670 | 35630 | 37310 | 38990 | 44550 | 46470 | 48340 |
| 29 | 32510 | 34400 | 36030 | 37650 | 43020 | 44870 | 46670 |
| 30 | 31430 | 33260 | 34820 | 36390 | 41580 | 43370 | 45110 |
| 31 | 30420 | 32180 | 33700 | 35220 | 40240 | 41970 | 43660 |
| 32 | 29460 | 31200 | 32650 | 34120 | 38980 | 40660 | 42290 |
| 33 | 28570 | 30230 | 31660 | 33080 | 37800 | 39430 | 41010 |
| 34 | 27730 | 29340 | 30730 | 32110 | 36690 | 38270 | 39810 |
| 35 | 26940 | 28510 | 29850 | 31190 | 35640 | 37170 | 38670 |
| 36 | 26190 | 27710 | 29020 | 30330 | 34650 | 36140 | 37590 |
| 37 | 25480 | 26960 | 28240 | 29510 | 33720 | 35160 | 36580 |
| 38 | 24810 | 26250 | 27490 | 28730 | 32830 | 34240 | 35620 |
| 39 | 24180 | 25580 | 26790 | 27990 | 31990 | 33360 | 34700 |
| 40 | 23570 | 24940 | 26120 | 27290 | 31190 | 32530 | 33830 |

For safe loads below the heavy lines, the deflections will be greater than the allowable limit for plastered ceilings = $\frac{1}{360}$ span.

Above single dot, safe loads are too great for standard connections.

SAFE LOADS IN POUNDS UNIFORMLY DISTRIBUTED FOR CAMBRIA I-BEAMS.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of beam.

| Distance between supports in feet. | SPECIAL I-BEAM. | | | | |
|--|--------------------|------------|------------|------------|-------------|
| | 20 Inch No. B 121. | | | | |
| | 80 lbs. | 85 lbs. | 90 lbs. | 95 lbs. | 100 lbs. |
| 16 | 97750 | 100570 | 103840 | 107100 | 110370 |
| 17 | 92000 | 94650 | 97730 | 100800 | 103880 |
| 18 | 86890 | 89390 | 92300 | 95200 | 98110 |
| 19 | 82320 | 84690 | 87440 | 90190 | 92950 |
| 20 | 78200 | 80460 | 83070 | 85680 | 88300 |
| 21 | 74480 | 76620 | 79110 | 81600 | 84090 |
| 22 | 71090 | 73140 | 75520 | 77890 | 80270 |
| 23 | • 68000 | • 69960 | 72230 | 74510 | 76780 |
| 24 | 65170 | 67050 | • 69220 | 71400 | 73580 |
| 25 | 62560 | 64360 | 66460 | • 68550 | • 70640 |
| 26 | 60160 | 61890 | 63900 | 65910 | 67920 |
| 27 | 57930 | 59600 | 61530 | 63470 | 65410 |
| 28 | 55860 | 57470 | 59340 | 61200 | 63070 |
| 29 | 53930 | 55490 | 57290 | 59090 | 60900 |
| 30 | 52140 | 53640 | 55380 | 57120 | 58870 |
| 31 | 50450 | 51910 | 53590 | 55280 | 56970 |
| 32 | 48880 | 50280 | 51920 | 53550 | 55190 |
| 33 | 47400 | 48760 | 50350 | 51930 | 53510 |
| 34 | 46000 | 47330 | 48860 | 50400 | 51940 |
| 35 | 44690 | 45970 | 47470 | 48960 | 50460 |
| 36 | 43450 | 44700 | 46150 | 47600 | 49050 |
| 37 | 42270 | 43490 | 44900 | 46320 | 47730 |
| 38 | 41160 | 42340 | 43720 | 45100 | 46470 |
| 39 | 40100 | 41260 | 42600 | 43940 | 45280 |
| 40 | 39100 | 40230 | 41530 | 42840 | 44150 |

Above single dot, safe loads are too great for standard connections.

SAFE LOADS IN POUNDS UNIFORMLY DISTRIBUTED FOR CAMBRIA I-BEAMS.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of beam.

| Distance between supports in feet. | STANDARD I-BEAM. | | | | |
|--|-------------------|------------|------------|------------|-------------|
| | 24 Inch No. B 89. | | | | |
| | 80 lbs. | 85 lbs. | 90 lbs. | 95 lbs. | 100 lbs. |
| 18 | 103070 | 107050 | 110540 | 114020 | 117510 |
| 19 | 97650 | •101420 | •104720 | 108020 | 111330 |
| 20 | 92770 | 96350 | 99480 | •102620 | •105760 |
| 21 | 88350 | 91760 | 94750 | 97740 | 100720 |
| 22 | 84330 | 87590 | 90440 | 93290 | 96140 |
| 23 | 80670 | 83780 | 86510 | 89240 | 91960 |
| 24 | 77300 | 80290 | 82900 | 85520 | 88130 |
| 25 | 74210 | 77080 | 79590 | 82100 | 86410 |
| 26 | 71360 | 74110 | 76530 | 78940 | 81350 |
| 27 | 68720 | 71370 | 73690 | 76020 | 78340 |
| 28 | 66260 | 68820 | 71060 | 73300 | 75540 |
| 29 | 63980 | 66450 | 68610 | 70770 | 72940 |
| 30 | 61840 | 64230 | 66320 | 68410 | 70510 |
| 31 | 59850 | 62160 | 64180 | 66210 | 68230 |
| 32 | 57980 | 60220 | 62180 | 64140 | 66100 |
| 33 | 56220 | 58390 | 60290 | 62200 | 64100 |
| 34 | 54570 | 56680 | 58520 | 60370 | 62210 |
| 35 | 53010 | 55060 | 56850 | 58640 | 60430 |
| 36 | 51540 | 53530 | 55270 | 57010 | 58760 |
| 37 | 50140 | 52080 | 53780 | 55470 | 57170 |
| 38 | 48820 | 50710 | 52360 | 54010 | 55660 |
| 39 | 47570 | 49410 | 51020 | 52630 | 54240 |
| 40 | 46380 | 48170 | 49740 | 51310 | 52880 |
| 41 | 45280 | 47000 | 48530 | 50060 | 51590 |
| 42 | 44170 | 45880 | 47370 | 48870 | 50360 |
| 43 | 43150 | 44810 | 46270 | 47730 | 49190 |
| 44 | 42170 | 43790 | 45220 | 46650 | 48070 |
| 45 | 41230 | 42820 | 44220 | 45610 | 47000 |
| 46 | 40330 | 41890 | 43250 | 44620 | 45980 |
| 47 | 39470 | 41000 | 42330 | 43670 | 45000 |
| 48 | 38650 | 40140 | 41450 | 42760 | 44070 |

Above single dot, safe loads are too great for standard connections.

SAFE LOADS IN POUNDS UNIFORMLY DISTRIBUTED FOR CAMBRIA I-BEAMS.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of beam.

| Distance between supports in feet. | SPECIAL I-BEAM. | | |
|---|--------------------|-------------|-------------|
| | 24 Inch No. B 127. | | |
| | 105 lbs. | 110 lbs. | 115 lbs. |
| 18 | 138840 | 142390 | 145950 |
| 19 | 131530 | 134890 | 138270 |
| 20 | 124950 | 128150 | 131350 |
| 21 | 119000 | 122050 | 125100 |
| 22 | 113590 | 116500 | 119410 |
| 23 | 108660 | 111440 | 114220 |
| 24 | • 104130 | 106790 | 109460 |
| 25 | 99960 | • 102530 | • 105080 |
| 26 | 96120 | 98580 | 101040 |
| 27 | 92560 | 94930 | 97300 |
| 28 | 89250 | 91540 | 93830 |
| 29 | 86170 | 88380 | 90590 |
| 30 | 83300 | 85440 | 87570 |
| 31 | 80620 | 82680 | 84740 |
| 32 | 78100 | 80100 | 82100 |
| 33 | 75730 | 77670 | 79610 |
| 34 | 73500 | 75380 | 77270 |
| 35 | 71400 | 73230 | 75060 |
| 36 | 69420 | 71200 | 72970 |
| 37 | 67540 | 69270 | 71000 |
| 38 | 65770 | 67450 | 69130 |
| 39 | 64080 | 65720 | 67360 |
| 40 | 62480 | 64080 | 65680 |
| 41 | 60950 | 62510 | 64080 |
| 42 | 59500 | 61030 | 62550 |
| 43 | 58120 | 59610 | 61090 |
| 44 | 56800 | 58250 | 59710 |
| 45 | 55530 | 56960 | 58380 |
| 46 | 54330 | 55720 | 57110 |
| 47 | 53170 | 54530 | 55890 |
| 48 | 52060 | 53400 | 54730 |

Above single dot, safe loads are too great for standard connections.

SAFE LOADS IN POUNDS UNIFORMLY DISTRIBUTED FOR CAMBRIA CHANNELS.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of channel.

| Distance between supports in feet. | STANDARD CHANNELS. | | | | | | | | |
|---|--------------------|------|------|-----------------|------|------|------------------|------|-------|
| | 3 Inch No. C 5. | | | 4 Inch No. C 9. | | | 5 Inch No. C 13. | | |
| | 4 | 5 | 6 | 5.25 | 6.25 | 7.25 | 6.5 | 9 | 11.5 |
| | lbs. | lbs. | lbs. | lbs. | lbs. | lbs. | lbs. | lbs. | lbs. |
| 4 | 2910 | 3290 | 3680 | 5060 | 5570 | 6090 | 7910 | 9460 | 11100 |
| 5 | 2330 | 2630 | 2940 | 4050 | 4450 | 4870 | 6330 | 7570 | 8880 |
| 6 | 1940 | 2190 | 2450 | 3370 | 3710 | 4060 | 5270 | 6310 | 7400 |
| 7 | 1660 | 1880 | 2100 | 2890 | 3180 | 3480 | 4520 | 5410 | 6340 |
| 8 | 1450 | 1640 | 1840 | 2530 | 2780 | 3050 | 3960 | 4730 | 5550 |
| 9 | 1290 | 1460 | 1630 | 2250 | 2470 | 2710 | 3520 | 4210 | 4930 |
| 10 | 1160 | 1310 | 1470 | 2020 | 2230 | 2440 | 3160 | 3790 | 4440 |
| 11 | 1060 | 1190 | 1340 | 1840 | 2020 | 2210 | 2880 | 3440 | 4040 |
| 12 | 970 | 1100 | 1230 | 1690 | 1860 | 2030 | 2640 | 3150 | 3700 |
| 13 | 890 | 1010 | 1130 | 1560 | 1710 | 1870 | 2430 | 2910 | 3410 |
| 14 | 830 | 940 | 1050 | 1440 | 1590 | 1740 | 2260 | 2700 | 3170 |
| 15 | 780 | 880 | 980 | 1350 | 1480 | 1620 | 2110 | 2520 | 2960 |
| 16 | 730 | 820 | 920 | 1260 | 1390 | 1520 | 1980 | 2370 | 2770 |
| 17 | 680 | 770 | 870 | 1190 | 1310 | 1430 | 1860 | 2230 | 2610 |
| 18 | 650 | 730 | 820 | 1120 | 1240 | 1350 | 1760 | 2100 | 2470 |
| 19 | 610 | 690 | 770 | 1060 | 1170 | 1280 | 1670 | 1990 | 2340 |
| 20 | 580 | 660 | 740 | 1010 | 1110 | 1220 | 1580 | 1890 | 2220 |
| 21 | 550 | 630 | 700 | 960 | 1060 | 1160 | 1510 | 1800 | 2110 |
| 22 | 530 | 600 | 670 | 920 | 1010 | 1110 | 1440 | 1720 | 2020 |
| 23 | 510 | 570 | 640 | 880 | 970 | 1060 | 1380 | 1650 | 1930 |
| 24 | 480 | 550 | 610 | 840 | 930 | 1020 | 1320 | 1580 | 1850 |
| 25 | 470 | 530 | 590 | 810 | 890 | 970 | 1270 | 1510 | 1780 |

For safe loads below the heavy lines, the deflections will be greater than the allowable limit for plastered ceilings = $\frac{1}{100}$ span.

SAFE LOADS IN POUNDS UNIFORMLY DISTRIBUTED FOR CAMBRIA CHANNELS.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of channel.

| Distance between supports in feet. | STANDARD CHANNELS. | | | | | | | | | |
|---|--------------------|-------|-------|-------|-------|------------------|--------|--------|--------|--|
| | 6 Inch No. C 17. | | | | | 7 Inch No. C 21. | | | | |
| | 8 | 10.5 | 13 | 15.5 | 9.75 | 12.25 | 14.75 | 17.25 | 19.75 | |
| | lbs. | lbs. | lbs. | lbs. | lbs. | lbs. | lbs. | lbs. | lbs. | |
| 4 | 11550 | 13440 | 15400 | 17360 | 16070 | 18410 | 20700 | 22990 | 25280 | |
| 5 | 9240 | 10750 | 12320 | 13890 | 12850 | •14730 | •16560 | 18390 | 20220 | |
| 6 | 7700 | 8960 | 10270 | 11570 | 10710 | 12280 | 13800 | •15330 | •16850 | |
| 7 | 6600 | 7680 | 8800 | 9920 | 9180 | 10520 | 11830 | 13140 | 14440 | |
| 8 | 5780 | 6720 | 7700 | 8680 | 8030 | 9210 | 10350 | 11490 | 12640 | |
| 9 | 5130 | 5970 | 6840 | 7720 | 7140 | 8180 | 9200 | 10220 | 11230 | |
| 10 | 4620 | 5380 | 6160 | 6940 | 6430 | 7370 | 8280 | 9200 | 10110 | |
| 11 | 4200 | 4890 | 5600 | 6310 | 5840 | 6700 | 7530 | 8360 | 9190 | |
| 12 | 3850 | 4480 | 5130 | 5790 | 5360 | 6140 | 6900 | 7660 | 8430 | |
| 13 | 3550 | 4130 | 4740 | 5340 | 4940 | 5670 | 6370 | 7070 | 7780 | |
| 14 | 3300 | 3840 | 4400 | 4960 | 4590 | 5260 | 5910 | 6570 | 7220 | |
| 15 | 3080 | 3580 | 4110 | 4630 | 4280 | 4910 | 5520 | 6130 | 6740 | |
| 16 | 2890 | 3360 | 3850 | 4340 | 4020 | 4600 | 5180 | 5750 | 6320 | |
| 17 | 2720 | 3160 | 3620 | 4080 | 3780 | 4330 | 4870 | 5410 | 5950 | |
| 18 | 2570 | 2990 | 3420 | 3860 | 3570 | 4090 | 4600 | 5110 | 5620 | |
| 19 | 2430 | 2830 | 3240 | 3650 | 3380 | 3880 | 4360 | 4840 | 5320 | |
| 20 | 2310 | 2690 | 3080 | 3470 | 3210 | 3680 | 4140 | 4600 | 5060 | |
| 21 | 2200 | 2560 | 2930 | 3310 | 3060 | 3510 | 3940 | 4380 | 4810 | |
| 22 | 2100 | 2440 | 2800 | 3160 | 2920 | 3350 | 3760 | 4180 | 4600 | |
| 23 | 2010 | 2340 | 2680 | 3020 | 2790 | 3200 | 3600 | 4000 | 4400 | |
| 24 | 1930 | 2240 | 2570 | 2890 | 2680 | 3070 | 3450 | 3830 | 4210 | |
| 25 | 1850 | 2150 | 2460 | 2780 | 2570 | 2950 | 3310 | 3680 | 4040 | |

For safe loads below the heavy lines, the deflections will be greater than the allowable limit for plastered ceilings = $\frac{1}{360}$ span.

Above single dot, safe loads are too great for standard connections.

SAFE LOADS IN POUNDS UNIFORMLY DISTRIBUTED FOR CAMBRIA CHANNELS.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of channel.

| Distance between supports in feet. | STANDARD CHANNELS. | | | | | | | | |
|---|--------------------|-------|-------|-------|-------|------------------|-------|-------|-------|
| | 8 Inch No. C 25. | | | | | 9 Inch No. C 29. | | | |
| | 11.25 | 13.75 | 16.25 | 18.75 | 21.25 | 13.25 | 15 | 20 | 25 |
| | lbs. | lbs. | lbs. | lbs. | lbs. | lbs. | lbs. | lbs. | lbs. |
| 4 | 21530 | 24000 | 26610 | 29230 | 31840 | 28040 | 30130 | 36020 | 41900 |
| 5 | 17230 | 19200 | 21290 | 23380 | 25470 | 22430 | 24110 | 28810 | 33520 |
| 6 | 14360 | 16000 | 17740 | 19480 | 21230 | 18690 | 20090 | 24010 | 27930 |
| 7 | 12310 | 13710 | 15210 | 16700 | 18200 | 16020 | 17220 | 20580 | 23940 |
| 8 | 10770 | 12000 | 13310 | 14610 | 15920 | 14020 | 15070 | 18010 | 20950 |
| 9 | 9570 | 10670 | 11830 | 12990 | 14150 | 12460 | 13390 | 16010 | 18620 |
| 10 | 8610 | 9600 | 10650 | 11690 | 12740 | 11220 | 12050 | 14410 | 16760 |
| 11 | 7830 | 8730 | 9680 | 10630 | 11580 | 10200 | 10960 | 13100 | 15240 |
| 12 | 7180 | 8000 | 8870 | 9740 | 10610 | 9350 | 10040 | 12010 | 13970 |
| 13 | 6630 | 7380 | 8190 | 8990 | 9800 | 8630 | 9270 | 11080 | 12890 |
| 14 | 6150 | 6860 | 7600 | 8350 | 9100 | 8010 | 8610 | 10290 | 11970 |
| 15 | 5740 | 6400 | 7100 | 7790 | 8490 | 7480 | 8040 | 9600 | 11170 |
| 16 | 5380 | 6000 | 6650 | 7310 | 7960 | 7010 | 7530 | 9000 | 10470 |
| 17 | 5070 | 5650 | 6260 | 6880 | 7490 | 6600 | 7090 | 8470 | 9860 |
| 18 | 4790 | 5330 | 5910 | 6490 | 7080 | 6230 | 6700 | 8000 | 9310 |
| 19 | 4530 | 5050 | 5600 | 6150 | 6700 | 5900 | 6340 | 7580 | 8820 |
| 20 | 4310 | 4800 | 5320 | 5850 | 6370 | 5610 | 6030 | 7200 | 8380 |
| 21 | 4100 | 4570 | 5070 | 5570 | 6070 | 5340 | 5740 | 6860 | 7980 |
| 22 | 3920 | 4360 | 4840 | 5310 | 5790 | 5100 | 5480 | 6550 | 7620 |
| 23 | 3750 | 4170 | 4630 | 5080 | 5540 | 4880 | 5240 | 6260 | 7290 |
| 24 | 3590 | 4000 | 4440 | 4870 | 5310 | 4670 | 5020 | 6000 | 6980 |
| 25 | 3450 | 3840 | 4260 | 4680 | 5090 | 4490 | 4820 | 5760 | 6700 |

For safe loads below the heavy lines, the deflections will be greater than the allowable limit for plastered ceilings = $\frac{1}{360}$ span.

Above single dot, safe loads are too great for standard connections.

SAFE LOADS IN POUNDS UNIFORMLY DISTRIBUTED FOR CAMBRIA CHANNELS.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of channel.

| Distance between supports in feet. | STANDARD CHANNEL. | | | | |
|--|-------------------|------------|------------|------------|------------|
| | 10 Inch No. C 33. | | | | |
| | 15 lbs. | 20 lbs. | 25 lbs. | 30 lbs. | 35 lbs. |
| 10 | 14270 | 16790 | 19410 | 22020 | 24640 |
| 11 | 12970 | 15270 | 17640 | 20020 | 22400 |
| 12 | 11890 | 14000 | 16170 | 18350 | 20530 |
| 13 | 10980 | 12920 | 14930 | 16940 | 18950 |
| 14 | 10190 | 12000 | 13860 | 15730 | 17600 |
| 15 | 9510 | 11200 | 12940 | 14680 | 16430 |
| 16 | 8920 | 10500 | 12130 | 13760 | 15400 |
| 17 | 8390 | 9880 | 11420 | 12950 | 14490 |
| 18 | 7930 | 9330 | 10780 | 12240 | 13690 |
| 19 | 7510 | 8840 | 10220 | 11590 | 12970 |
| 20 | 7130 | 8400 | 9700 | 11010 | 12320 |
| 21 | 6790 | 8000 | 9240 | 10490 | 11730 |
| 22 | 6490 | 7630 | 8820 | 10010 | 11200 |
| 23 | 6200 | 7300 | 8440 | 9580 | 10710 |
| 24 | 5940 | 7000 | 8090 | 9180 | 10270 |
| 25 | 5710 | 6720 | 7760 | 8810 | 9860 |
| 26 | 5490 | 6460 | 7460 | 8470 | 9480 |
| 27 | 5280 | 6220 | 7190 | 8160 | 9130 |
| 28 | 5100 | 6000 | 6930 | 7870 | 8800 |
| 29 | 4920 | 5790 | 6690 | 7590 | 8500 |
| 30 | 4760 | 5600 | 6470 | 7340 | 8210 |

For safe loads below the heavy lines, the deflections will be greater than the allowable limit for plastered ceilings = $\frac{1}{360}$ span.

SAFE LOADS IN POUNDS UNIFORMLY DISTRIBUTED FOR CAMBRIA CHANNELS.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of channel.

| Distance between supports in feet. | STANDARD CHANNEL. | | | | |
|--|-------------------|------------|------------|------------|------------|
| | 12 Inch No. C 41. | | | | |
| | 20.5 lbs. | 25 lbs. | 30 lbs. | 35 lbs. | 40 lbs. |
| 10 | 22780 | 25600 | 28740 | 31870 | 35010 |
| 11 | 20700 | 23270 | 26120 | 28980 | 31830 |
| 12 | 18980 | 21330 | 23950 | 26560 | 29180 |
| 13 | 17520 | 19690 | 22110 | 24520 | 26930 |
| 14 | 16270 | 18290 | 20530 | 22770 | 25010 |
| 15 | 15180 | 17070 | 19160 | 21250 | 23340 |
| 16 | 14230 | 16000 | 17960 | 19920 | 21880 |
| 17 | 13400 | 15060 | 16900 | 18750 | 20600 |
| 18 | 12650 | 14220 | 15970 | 17710 | 19450 |
| 19 | 11990 | 13470 | 15120 | 16780 | 18430 |
| 20 | 11390 | 12800 | 14370 | 15940 | 17510 |
| 21 | 10850 | 12190 | 13680 | 15180 | 16670 |
| 22 | 10350 | 11640 | 13060 | 14490 | 15910 |
| 23 | 9900 | 11130 | 12490 | 13860 | 15220 |
| 24 | 9490 | 10670 | 11970 | 13280 | 14590 |
| 25 | 9110 | 10240 | 11490 | 12750 | 14000 |
| 26 | 8760 | 9850 | 11050 | 12260 | 13470 |
| 27 | 8440 | 9480 | 10640 | 11810 | 12970 |
| 28 | 8130 | 9140 | 10260 | 11380 | 12500 |
| 29 | 7850 | 8830 | 9910 | 10990 | 12070 |
| 30 | 7590 | 8530 | 9580 | 10620 | 11670 |

For safe loads below the heavy lines, the deflections will be greater than the allowable limit for plastered ceilings = $\frac{1}{360}$ span.

SAFE LOADS IN POUNDS UNIFORMLY DISTRIBUTED FOR CAMBRIA CHANNELS.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of channel.

| Distance between supports in feet. | STANDARD CHANNEL. | | | | | |
|---|--------------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| | 15 Inch No. C 53. | | | | | |
| | 33 lbs. | 35 lbs. | 40 lbs. | 45 lbs. | 50 lbs. | 55 lbs. |
| 10 | 44450 | 45500 | 49420 | 53350 | 57270 | 61190 |
| 11 | 40410 | 41370 | 44930 | 48500 | 52060 | 55630 |
| 12 | 37040 | 37920 | 41190 | 44460 | 47720 | 50990 |
| 13 | 34190 | 35000 | 38020 | 41040 | 44050 | 47070 |
| 14 | 31750 | 32500 | 35300 | 38100 | 40910 | 43710 |
| 15 | 29630 | 30340 | 32950 | 35560 | 38180 | 40790 |
| 16 | 27780 | 28440 | 30890 | 33340 | 35790 | 38240 |
| 17 | 26150 | 26770 | 29070 | 31380 | 33690 | 35990 |
| 18 | 24700 | 25280 | 27460 | 29640 | 31820 | 33990 |
| 19 | 23400 | 23950 | 26010 | 28080 | 30140 | 32210 |
| 20 | 22230 | 22750 | 24710 | 26670 | 28630 | 30590 |
| 21 | 21170 | 21670 | 23540 | 25400 | 27270 | 29140 |
| 22 | 20210 | 20680 | 22470 | 24250 | 26030 | 27810 |
| 23 | 19330 | 19780 | 21490 | 23190 | 24900 | 26600 |
| 24 | 18520 | 18960 | 20590 | 22230 | 23860 | 25500 |
| 25 | 17780 | 18200 | 19770 | 21340 | 22910 | 24480 |
| 26 | 17100 | 17500 | 19010 | 20520 | 22030 | 23530 |
| 27 | 16460 | 16850 | 18310 | 19760 | 21210 | 22660 |
| 28 | 15880 | 16250 | 17650 | 19050 | 20450 | 21850 |
| 29 | 15330 | 15690 | 17040 | 18400 | 19750 | 21100 |
| 30 | 14820 | 15170 | 16470 | 17780 | 19090 | 20400 |

SPACING OF CAMBRIA I-BEAMS FOR UNI- FORM LOAD OF 100 LBS. PER SQUARE FOOT.

Proper distance in feet, center to center of Beams.

Maximum fibre stress 16 000 pounds per square inch.

| Distance between supports in feet. | STANDARD I-BEAMS. | | | | | | |
|---|-------------------|-------------|-------------|-----------------|-------------|-------------|--------------|
| | 3 Inch No. B 5. | | | 4 Inch No. B 9. | | | |
| | 5.5 lbs. | 6.5 lbs. | 7.5 lbs. | 7.5 lbs. | 8.5 lbs. | 9.5 lbs. | 10.5 lbs. |
| 4 | 11.0 | 12.0 | 12.9 | 19.9 | 21.2 | 22.5 | 23.8 |
| 5 | 7.1 | 7.7 | 8.3 | 12.7 | 13.6 | 14.4 | 15.2 |
| 6 | 4.9 | 5.3 | 5.8 | 8.8 | 9.4 | 10.0 | 10.6 |
| 7 | 3.6 | 3.9 | 4.2 | 6.5 | 6.9 | 7.3 | 7.8 |
| 8 | 2.8 | 3.0 | 3.2 | 5.0 | 5.3 | 5.6 | 5.9 |
| 9 | 2.2 | 2.4 | 2.6 | 3.9 | 4.2 | 4.4 | 4.7 |
| 10 | 1.8 | 1.9 | 2.1 | 3.2 | 3.4 | 3.6 | 3.8 |
| 11 | 1.5 | 1.6 | 1.7 | 2.6 | 2.8 | 3.0 | 3.1 |
| 12 | 1.2 | 1.3 | 1.4 | 2.2 | 2.4 | 2.5 | 2.6 |
| 13 | 1.0 | 1.1 | 1.2 | 1.9 | 2.0 | 2.1 | 2.3 |
| 14 | | 1.0 | 1.1 | 1.6 | 1.7 | 1.8 | 1.9 |
| 15 | | | | 1.4 | 1.5 | 1.6 | 1.7 |
| 16 | | | | 1.2 | 1.3 | 1.4 | 1.5 |
| 17 | | | | 1.1 | 1.2 | 1.2 | 1.3 |
| 18 | | | | 1.0 | 1.0 | 1.1 | 1.2 |
| 19 | | | | | | 1.0 | 1.1 |
| 20 | | | | | | | 1.0 |

For spacings below the heavy lines the deflections will be greater than the allowable limit for plastered ceilings = $\frac{1}{360}$ span.

Spacings for other intensities of loading may be obtained from those in tables as follows:

$$\text{Required spacing} = \frac{\text{Intensity of loading from table}}{\text{New intensity of loading}} \times \text{Computed spacing from table.}$$

SPACING OF CAMBRIA I-BEAMS FOR UNIFORM LOAD OF 100 LBS. PER SQUARE FOOT.

Proper distance in feet, center to center of Beams.
Maximum fibre stress 16 000 pounds per square inch.

| Distance between supports in feet. | STANDARD I-BEAMS. | | | | | |
|---|-------------------|---------------|---------------|------------------|---------------|---------------|
| | 5 Inch No. B 13. | | | 6 Inch No. B 17. | | |
| | 9.75 lbs. | 12.25 lbs. | 14.75 lbs. | 12.25 lbs. | 14.75 lbs. | 17.25 lbs. |
| 4 | 32.2 | 36.3 | 40.4 | 48.4 | 53.3 | 58.2 |
| 5 | 20.6 | 23.2 | 25.9 | •31.0 | •34.1 | 37.2 |
| 6 | 14.3 | 16.1 | 18.0 | 21.5 | 23.7 | •25.9 |
| 7 | 10.5 | 11.9 | 13.2 | 15.8 | 17.4 | 19.0 |
| 8 | 8.1 | 9.1 | 10.1 | 12.1 | 13.3 | 14.5 |
| 9 | 6.4 | 7.2 | 8.0 | 9.6 | 10.5 | 11.5 |
| 10 | 5.2 | 5.8 | 6.5 | 7.7 | 8.5 | 9.3 |
| 11 | 4.3 | 4.8 | 5.3 | 6.4 | 7.0 | 7.7 |
| 12 | 3.6 | 4.0 | 4.5 | 5.4 | 5.9 | 6.5 |
| 13 | 3.1 | 3.4 | 3.8 | 4.6 | 5.0 | 5.5 |
| 14 | 2.6 | 3.0 | 3.3 | 4.0 | 4.4 | 4.8 |
| 15 | 2.3 | 2.6 | 2.9 | 3.4 | 3.8 | 4.1 |
| 16 | 2.0 | 2.3 | 2.5 | 3.0 | 3.3 | 3.6 |
| 17 | 1.8 | 2.0 | 2.2 | 2.7 | 3.0 | 3.2 |
| 18 | 1.6 | 1.8 | 2.0 | 2.4 | 2.6 | 2.9 |
| 19 | 1.4 | 1.6 | 1.8 | 2.1 | 2.4 | 2.6 |
| 20 | 1.3 | 1.5 | 1.6 | 1.9 | 2.1 | 2.3 |
| 21 | 1.2 | 1.3 | 1.5 | 1.8 | 1.9 | 2.1 |
| 22 | 1.1 | 1.2 | 1.3 | 1.6 | 1.8 | 1.9 |
| 23 | 1.0 | 1.1 | 1.2 | 1.5 | 1.6 | 1.8 |
| 24 | | 1.0 | 1.1 | 1.3 | 1.5 | 1.6 |
| 25 | | | 1.0 | 1.2 | 1.4 | 1.5 |
| 26 | | | 1.0 | 1.1 | 1.3 | 1.4 |
| 27 | | | | 1.1 | 1.2 | 1.3 |
| 28 | | | | 1.0 | 1.1 | 1.2 |

For spacings above single dot the safe loads are too great for standard connections.

For spacings below the heavy lines the deflections will be greater than the allowable limit for plastered ceilings = $\frac{1}{385}$ span.

Spacings for other intensities of loading may be obtained from those in tables as follows:

$$\text{Required spacing} = \frac{\text{Intensity of loading from table}}{\text{New intensity of loading}} \times \text{Computed spacing from table.}$$

SPACING OF CAMBRIA I-BEAMS FOR UNIFORM LOAD OF 100 LBS. PER SQUARE FOOT.

Proper distance in feet, center to center of Beams.
Maximum fibre stress 16 000 pounds per square inch.

| Distance between supports in feet. | STANDARD I-BEAMS. | | | | | | |
|------------------------------------|--------------------------|-----------|---------|-------------------------|------------|------------|------------|
| | 7 Inch No. B 21. | | | 8 Inch No. B 25. | | | |
| | 15 lbs. | 17.5 lbs. | 20 lbs. | 18.00 lbs. | 20.25 lbs. | 22.75 lbs. | 25.25 lbs. |
| 4 | 69.0 | 74.6 | 80.3 | | | | |
| 5 | 44.2 | 47.8 | 51.4 | 60.7 | 64.2 | 68.4 | 72.6 |
| 6 | 30.7 | 33.2 | 35.7 | 42.1 | 44.6 | 47.5 | •50.4 |
| 7 | •22.5 | •24.4 | 26.2 | 31.0 | 32.8 | 34.9 | 37.0 |
| 8 | 17.3 | 18.7 | •20.1 | 23.7 | 25.1 | 26.7 | 28.3 |
| 9 | 13.6 | 14.7 | 15.9 | 18.7 | 19.8 | 21.1 | 22.4 |
| 10 | 11.0 | 11.9 | 12.9 | 15.2 | 16.1 | 17.1 | 18.1 |
| 11 | 9.1 | 9.9 | 10.6 | 12.5 | 13.3 | 14.1 | 15.0 |
| 12 | 7.7 | 8.3 | 8.9 | 10.5 | 11.1 | 11.9 | 12.6 |
| 13 | 6.5 | 7.1 | 7.6 | 9.0 | 9.5 | 10.1 | 10.7 |
| 14 | 5.6 | 6.1 | 6.6 | 7.7 | 8.2 | 8.7 | 9.3 |
| 15 | 4.9 | 5.3 | 5.7 | 6.7 | 7.1 | 7.6 | 8.1 |
| 16 | 4.3 | 4.7 | 5.0 | 5.9 | 6.3 | 6.7 | 7.1 |
| 17 | 3.8 | 4.1 | 4.4 | 5.2 | 5.6 | 5.9 | 6.3 |
| 18 | 3.4 | 3.7 | 4.0 | 4.7 | 5.0 | 5.3 | 5.6 |
| 19 | 3.1 | 3.3 | 3.6 | 4.2 | 4.4 | 4.7 | 5.0 |
| 20 | 2.8 | 3.0 | 3.2 | 3.8 | 4.0 | 4.3 | 4.5 |
| 21 | 2.5 | 2.7 | 2.9 | 3.4 | 3.6 | 3.9 | 4.1 |
| 22 | 2.3 | 2.5 | 2.7 | 3.1 | 3.3 | 3.5 | 3.7 |
| 23 | 2.1 | 2.3 | 2.4 | 2.9 | 3.0 | 3.2 | 3.4 |
| 24 | 1.9 | 2.1 | 2.2 | 2.6 | 2.8 | 3.0 | 3.1 |
| 25 | 1.8 | 1.9 | 2.1 | 2.4 | 2.6 | 2.7 | 2.9 |
| 26 | 1.6 | 1.8 | 1.9 | 2.2 | 2.4 | 2.5 | 2.7 |
| 27 | 1.5 | 1.6 | 1.8 | 2.1 | 2.2 | 2.3 | 2.5 |
| 28 | 1.4 | 1.5 | 1.6 | 1.9 | 2.0 | 2.2 | 2.3 |

For spacings above single dot the safe loads are too great for standard connections.

For spacing above the dotted line the safe load for bending is greater than the safe load for web crippling, as explained and shown on pages 82 to 84 inclusive.

For spacings below the heavy lines the deflections will be greater than the allowable limit for plastered ceilings = $\frac{1}{180}$ span.

Spacings for other intensities of loading may be obtained from those in tables as follows:

$$\text{Required spacing} = \frac{\text{Intensity of loading from table}}{\text{New intensity of loading}} \times \text{Computed spacing from table.}$$

SPACING OF CAMBRIA I-BEAMS FOR UNIFORM LOAD OF 100 LBS. PER SQUARE FOOT.

Proper distance in feet, center to center of Beams.
Maximum fibre stress 16 000 pounds per square inch.

| Distance between supports in feet. | STANDARD I-BEAMS. | | | | | | | |
|---|-------------------|------------|------------|------------|-------------------|------------|------------|------------|
| | 9 Inch No. B 29. | | | | 10 Inch No. B 33. | | | |
| | 21 lbs. | 25 lbs. | 30 lbs. | 35 lbs. | 25 lbs. | 30 lbs. | 35 lbs. | 40 lbs. |
| 8 | 31.5 | 34.1 | 37.7 | 41.4 | | | | |
| 9 | 24.9 | 26.9 | 29.8 | 32.7 | | | | |
| 10 | 20.1 | 21.8 | 24.1 | 26.5 | 26.0 | 28.6 | 31.2 | 33.9 |
| 11 | 16.6 | 18.0 | 20.0 | 21.9 | 21.5 | 23.7 | 25.8 | 28.0 |
| 12 | 14.0 | 15.1 | 16.8 | 18.4 | 18.1 | 19.9 | 21.7 | 23.5 |
| 13 | 11.9 | 12.9 | 14.3 | 15.7 | 15.4 | 16.9 | 18.5 | 20.0 |
| 14 | 10.3 | 11.1 | 12.3 | 13.5 | 13.3 | 14.6 | 15.9 | 17.3 |
| 15 | 8.9 | 9.7 | 10.7 | 11.8 | 11.6 | 12.7 | 13.9 | 15.0 |
| 16 | 7.9 | 8.5 | 9.4 | 10.4 | 10.2 | 11.2 | 12.2 | 13.2 |
| 17 | 7.0 | 7.5 | 8.4 | 9.2 | 9.0 | 9.9 | 10.8 | 11.7 |
| 18 | 6.2 | 6.7 | 7.5 | 8.2 | 8.0 | 8.8 | 9.6 | 10.4 |
| 19 | 5.6 | 6.0 | 6.7 | 7.3 | 7.2 | 7.9 | 8.7 | 9.4 |
| 20 | 5.0 | 5.4 | 6.0 | 6.6 | 6.5 | 7.2 | 7.8 | 8.5 |
| 21 | 4.6 | 4.9 | 5.5 | 6.0 | 5.9 | 6.5 | 7.1 | 7.7 |
| 22 | 4.2 | 4.5 | 5.0 | 5.5 | 5.4 | 5.9 | 6.5 | 7.0 |
| 23 | 3.8 | 4.1 | 4.6 | 5.0 | 4.9 | 5.4 | 5.9 | 6.4 |
| 24 | 3.5 | 3.8 | 4.2 | 4.6 | 4.5 | 5.0 | 5.4 | 5.9 |
| 25 | 3.2 | 3.5 | 3.9 | 4.2 | 4.2 | 4.6 | 5.0 | 5.4 |
| 26 | 3.0 | 3.2 | 3.6 | 3.9 | 3.9 | 4.2 | 4.6 | 5.0 |
| 27 | 2.8 | 3.0 | 3.3 | 3.6 | 3.6 | 3.9 | 4.3 | 4.6 |
| 28 | 2.6 | 2.8 | 3.1 | 3.4 | 3.3 | 3.7 | 4.0 | 4.3 |
| 29 | 2.4 | 2.6 | 2.9 | 3.2 | 3.1 | 3.4 | 3.7 | 4.0 |
| 30 | 2.2 | 2.4 | 2.7 | 2.9 | 2.9 | 3.2 | 3.5 | 3.8 |
| 31 | 2.1 | 2.3 | 2.5 | 2.8 | 2.7 | 3.0 | 3.3 | 3.5 |
| 32 | | | | | 2.5 | 2.8 | 3.1 | 3.3 |
| 33 | | | | | 2.4 | 2.6 | 2.9 | 3.1 |

For spacings below the heavy lines the deflections will be greater than the allowable limit for plastered ceilings = $\frac{1}{160}$ span.

Spacings for other intensities of loading may be obtained from those in tables as follows:

$$\text{Required spacing} = \frac{\text{Intensity of loading from table}}{\text{New intensity of loading}} \times \text{Computed spacing from table.}$$

SPACING OF CAMBRIA I-BEAMS FOR UNIFORM LOAD OF 100 LBS. PER SQUARE FOOT.

Proper distance in feet, center to center of Beams.
Maximum fibre stress 16 000 pounds per square inch.

| Distance between supports in feet. | STANDARD I-BEAM. | | | SPECIAL I-BEAM. | | | |
|------------------------------------|-------------------|---------|---------|--------------------|---------|---------|---------|
| | 12 Inch No. B 41. | | | 12 Inch No. B 105. | | | |
| | 31.5 lbs. | 35 lbs. | 40 lbs. | 40 lbs. | 45 lbs. | 50 lbs. | 55 lbs. |
| 10 | 38.4 | 40.6 | 43.7 | 47.8 | 50.8 | 53.9 | 57.1 |
| 11 | 31.7 | 33.5 | 36.1 | 39.5 | 42.0 | 44.6 | 47.2 |
| 12 | 26.6 | 28.2 | 30.4 | 33.2 | 35.3 | 37.5 | 39.6 |
| 13 | 22.7 | 24.0 | 25.9 | 28.3 | 30.1 | 31.9 | 33.8 |
| 14 | 19.6 | 20.7 | 22.3 | 24.4 | 25.9 | 27.5 | 29.1 |
| 15 | 17.1 | 18.0 | 19.4 | 21.3 | 22.6 | 24.0 | 25.4 |
| 16 | 15.0 | 15.9 | 17.1 | 18.7 | 19.8 | 21.1 | 22.3 |
| 17 | 13.3 | 14.0 | 15.1 | 16.5 | 17.6 | 18.7 | 19.7 |
| 18 | 11.8 | 12.5 | 13.5 | 14.8 | 15.7 | 16.6 | 17.6 |
| 19 | 10.6 | 11.2 | 12.1 | 13.2 | 14.1 | 14.9 | 15.8 |
| 20 | 9.6 | 10.1 | 10.9 | 12.0 | 12.7 | 13.5 | 14.3 |
| 21 | 8.7 | 9.2 | 9.9 | 10.8 | 11.5 | 12.2 | 12.9 |
| 22 | 7.9 | 8.4 | 9.0 | 9.9 | 10.5 | 11.1 | 11.8 |
| 23 | 7.3 | 7.7 | 8.3 | 9.0 | 9.6 | 10.2 | 10.8 |
| 24 | 6.7 | 7.0 | 7.6 | 8.3 | 8.8 | 9.4 | 9.9 |
| 25 | 6.1 | 6.5 | 7.0 | 7.7 | 8.1 | 8.6 | 9.1 |
| 26 | 5.7 | 6.0 | 6.5 | 7.1 | 7.5 | 8.0 | 8.4 |
| 27 | 5.3 | 5.6 | 6.0 | 6.6 | 7.0 | 7.4 | 7.8 |
| 28 | 4.9 | 5.2 | 5.6 | 6.1 | 6.5 | 6.9 | 7.3 |
| 29 | 4.6 | 4.8 | 5.2 | 5.7 | 6.0 | 6.4 | 6.8 |
| 30 | 4.3 | 4.5 | 4.9 | 5.3 | 5.6 | 6.0 | 6.3 |
| 31 | 4.0 | 4.2 | 4.5 | 5.0 | 5.3 | 5.6 | 5.9 |
| 32 | 3.7 | 4.0 | 4.3 | 4.7 | 5.0 | 5.3 | 5.6 |
| 33 | 3.5 | 3.7 | 4.0 | 4.4 | 4.7 | 5.0 | 5.2 |
| 34 | 3.3 | 3.5 | 3.8 | 4.1 | 4.4 | 4.7 | 4.9 |
| 35 | 3.1 | 3.3 | 3.6 | 3.9 | 4.1 | 4.4 | 4.7 |

For spacings above single dot the safe loads are too great for standard connections.

For spacings below the heavy lines the deflections will be greater than the allowable limit for plastered ceilings = $\frac{1}{320}$ span.

Spacings for other intensities of loading may be obtained from those in tables as follows:

$$\text{Required spacing} = \frac{\text{Intensity of loading from table}}{\text{New intensity of loading}} \times \text{Computed spacing from table.}$$

SPACING OF CAMBRIA I-BEAMS FOR UNIFORM LOAD OF 100 LBS. PER SQUARE FOOT.

Proper distance in feet, center to center of Beams.
Maximum fibre stress 16 000 pounds per square inch.

| Distance between supports in feet. | STANDARD I-BEAM. | | | | |
|------------------------------------|-------------------|---------|---------|---------|---------|
| | 15 Inch No. B 53. | | | | |
| | 42 lbs. | 45 lbs. | 50 lbs. | 55 lbs. | 60 lbs. |
| 10 | 62.8 | 64.8 | 68.8 | 72.7 | 76.6 |
| 11 | 51.9 | 53.6 | 56.8 | •60.1 | •63.3 |
| 12 | 43.6 | 45.0 | 47.7 | 50.5 | 53.2 |
| 13 | 37.2 | 38.4 | 40.7 | 43.0 | 45.3 |
| 14 | 32.0 | 33.1 | 35.1 | 37.1 | 39.1 |
| 15 | 27.9 | 28.8 | 30.6 | 32.3 | 34.0 |
| 16 | 24.5 | 25.3 | 26.9 | 28.4 | 29.9 |
| 17 | 21.7 | 22.4 | 23.8 | 25.1 | 26.5 |
| 18 | 19.4 | 20.0 | 21.2 | 22.4 | 23.6 |
| 19 | 17.4 | 18.0 | 19.0 | 20.1 | 21.2 |
| 20 | 15.7 | 16.2 | 17.2 | 18.2 | 19.1 |
| 21 | 14.2 | 14.7 | 15.6 | 16.5 | 17.4 |
| 22 | 13.0 | 13.4 | 14.2 | 15.0 | 15.8 |
| 23 | 11.9 | 12.3 | 13.0 | 13.7 | 14.5 |
| 24 | 10.9 | 11.3 | 11.9 | 12.6 | 13.3 |
| 25 | 10.1 | 10.4 | 11.0 | 11.6 | 12.3 |
| 26 | 9.3 | 9.6 | 10.2 | 10.8 | 11.3 |
| 27 | 8.6 | 8.9 | 9.4 | 10.0 | 10.5 |
| 28 | 8.0 | 8.3 | 8.8 | 9.3 | 9.8 |
| 29 | 7.5 | 7.7 | 8.2 | 8.6 | 9.1 |
| 30 | 7.0 | 7.2 | 7.6 | 8.1 | 8.5 |
| 31 | 6.5 | 6.7 | 7.2 | 7.6 | 8.0 |
| 32 | 6.1 | 6.3 | 6.7 | 7.1 | 7.5 |
| 33 | 5.8 | 6.0 | 6.3 | 6.7 | 7.0 |
| 34 | 5.4 | 5.6 | 5.9 | 6.3 | 6.6 |
| 35 | 5.1 | 5.3 | 5.6 | 5.9 | 6.3 |

For spacings above single dot the safe loads are too great for standard connections.

For spacings below the heavy lines the deflections will be greater than the allowable limit for plastered ceilings = $\frac{1}{360}$ span.

Spacings for other intensities of loading may be obtained from those in tables as follows:

$$\text{Required spacing} = \frac{\text{Intensity of loading from table}}{\text{New intensity of loading}} \times \text{Computed spacing from table.}$$

SPACING OF CAMBRIA I-BEAMS FOR UNIFORM LOAD OF 100 LBS. PER SQUARE FOOT.

Proper distance in feet, center to center of Beams.
Maximum fibre stress 16 000 pounds per square inch.

| Distance between supports in feet. | SPECIAL I-BEAM. | | | | |
|---|---------------------------|------------|------------|------------|------------|
| | 15 Inch No. B 109. | | | | |
| | 60 lbs. | 65 lbs. | 70 lbs. | 75 lbs. | 80 lbs. |
| 10 | 86.6 | 90.5 | 94.4 | 98.3 | 102.2 |
| 11 | 71.6 | 74.8 | 78.0 | 81.2 | 84.5 |
| 12 | 60.1 | 62.8 | 65.5 | 68.3 | 71.0 |
| 13 | •51.3 | •53.5 | 55.9 | 58.2 | 60.5 |
| 14 | 44.2 | 46.2 | •48.2 | •50.2 | 52.2 |
| 15 | 38.5 | 40.2 | 41.9 | 43.7 | •45.4 |
| 16 | 33.8 | 35.3 | 36.9 | 38.4 | 39.9 |
| 17 | 30.0 | 31.3 | 32.7 | 34.0 | 35.4 |
| 18 | 26.7 | 27.9 | 29.1 | 30.3 | 31.6 |
| 19 | 24.0 | 25.1 | 26.1 | 27.2 | 28.3 |
| 20 | 21.7 | 22.6 | 23.6 | 24.6 | 25.6 |
| 21 | 19.6 | 20.5 | 21.4 | 22.3 | 23.2 |
| 22 | 17.9 | 18.7 | 19.5 | 20.3 | 21.1 |
| 23 | 16.4 | 17.1 | 17.8 | 18.6 | 19.3 |
| 24 | 15.0 | 15.7 | 16.4 | 17.1 | 17.7 |
| 25 | 13.9 | 14.5 | 15.1 | 15.7 | 16.4 |
| 26 | 12.8 | 13.4 | 14.0 | 14.5 | 15.1 |
| 27 | 11.9 | 12.4 | 12.9 | 13.5 | 14.0 |
| 28 | 11.0 | 11.5 | 12.0 | 12.5 | 13.0 |
| 29 | 10.3 | 10.8 | 11.2 | 11.7 | 12.2 |
| 30 | 9.6 | 10.1 | 10.5 | 10.9 | 11.4 |
| 31 | 9.0 | 9.4 | 9.8 | 10.2 | 10.6 |
| 32 | 8.5 | 8.8 | 9.2 | 9.6 | 10.0 |
| 33 | 8.0 | 8.3 | 8.7 | 9.0 | 9.4 |
| 34 | 7.5 | 7.8 | 8.2 | 8.5 | 8.8 |
| 35 | 7.1 | 7.4 | 7.7 | 8.0 | 8.3 |

For spacings above single dot the safe loads are too great for standard connections.

For spacings below the heavy lines the deflections will be greater than the allowable limit for plastered ceilings = $\frac{1}{320}$ span.

Spacings for other intensities of loading may be obtained from those in tables as follows:

$$\text{Required spacing} = \frac{\text{Intensity of loading from table}}{\text{New intensity of loading}} \times \text{Computed spacing from table.}$$

SPACING OF CAMBRIA I-BEAMS FOR UNIFORM LOAD OF 100 LBS. PER SQUARE FOOT.

Proper distance in feet, center to center of Beams.
Maximum fibre stress 16 000 pounds per square inch.

| Distance between supports in feet. | SPECIAL I-BEAM. | | | | |
|---|--------------------|------------|------------|------------|-------------|
| | 15 Inch No. B 113. | | | | |
| | 80 lbs. | 85 lbs. | 90 lbs. | 95 lbs. | 100 lbs. |
| 10 | 112.2 | 116.0 | 120.0 | 123.9 | 127.8 |
| 11 | 92.8 | 95.9 | 99.1 | 102.4 | 105.6 |
| 12 | 77.9 | 80.6 | 83.3 | 86.0 | 88.7 |
| 13 | 66.4 | 68.7 | 71.0 | 73.3 | 75.6 |
| 14 | 57.3 | 59.2 | 61.2 | 63.2 | 65.2 |
| 15 | 49.9 | 51.6 | 53.3 | 55.1 | 56.8 |
| 16 | •43.8 | 45.3 | 46.9 | 48.4 | 49.9 |
| 17 | 38.8 | •40.2 | •41.5 | 42.9 | 44.2 |
| 18 | 34.6 | 35.8 | 37.0 | •38.2 | 39.4 |
| 19 | 31.1 | 32.1 | 33.2 | 34.3 | •35.4 |
| 20 | 28.1 | 29.0 | 30.0 | 31.0 | 31.9 |
| 21 | 25.4 | 26.3 | 27.2 | 28.1 | 29.0 |
| 22 | 23.2 | 24.0 | 24.8 | 25.6 | 26.4 |
| 23 | 21.2 | 21.9 | 22.7 | 23.4 | 24.2 |
| 24 | 19.5 | 20.1 | 20.8 | 21.5 | 22.2 |
| 25 | 18.0 | 18.6 | 19.2 | 19.8 | 20.4 |
| 26 | 16.6 | 17.2 | 17.7 | 18.3 | 18.9 |
| 27 | 15.4 | 15.9 | 16.5 | 17.0 | 17.5 |
| 28 | 14.3 | 14.8 | 15.3 | 15.8 | 16.3 |
| 29 | 13.3 | 13.8 | 14.3 | 14.7 | 15.2 |
| 30 | 12.5 | 12.9 | 13.3 | 13.8 | 14.2 |
| 31 | 11.7 | 12.1 | 12.5 | 12.9 | 13.3 |
| 32 | 11.0 | 11.3 | 11.7 | 12.1 | 12.5 |
| 33 | 10.3 | 10.7 | 11.0 | 11.4 | 11.7 |
| 34 | 9.7 | 10.0 | 10.4 | 10.7 | 11.1 |
| 35 | 9.2 | 9.5 | 9.8 | 10.1 | 10.4 |

For spacings above single dot the safe loads are too great for standard connections.

For spacings below the heavy lines the deflections will be greater than the allowable limit for plastered ceilings = $\frac{1}{360}$ span.

Spacings for other intensities of loading may be obtained from those in tables as follows:

$$\text{Required spacing} = \frac{\text{Intensity of loading from table}}{\text{New intensity of loading}} \times \text{Computed spacing from table.}$$

SPACING OF CAMBRIA I-BEAMS FOR UNIFORM LOAD OF 100 LBS. PER SQUARE FOOT.

Proper distance in feet, center to center of Beams.
Maximum fibre stress 16 000 pounds per square inch.

| Distance between supports in feet. | STANDARD I-BEAMS. | | | | | | |
|------------------------------------|-------------------|---------|---------|---------|-------------------|---------|---------|
| | 18 Inch No. B 65. | | | | 20 Inch No. B 73. | | |
| | 55 lbs. | 60 lbs. | 65 lbs. | 70 lbs. | 65 lbs. | 70 lbs. | 75 lbs. |
| 14 | 48.1 | 50.9 | 53.3 | 55.7 | 63.6 | 66.4 | 69.1 |
| 15 | 41.9 | •44.3 | •46.4 | 48.5 | 55.4 | 57.8 | 60.2 |
| 16 | 36.8 | 39.0 | 40.8 | •42.6 | 48.7 | 50.8 | 52.9 |
| 17 | 32.6 | 34.5 | 36.2 | 37.8 | 43.2 | 45.0 | 46.8 |
| 18 | 29.1 | 30.8 | 32.2 | 33.7 | •38.5 | 40.2 | 41.8 |
| 19 | 26.1 | 27.6 | 28.9 | 30.2 | 34.6 | •36.0 | 37.5 |
| 20 | 23.6 | 24.9 | 26.1 | 27.3 | 31.2 | 32.5 | •33.8 |
| 21 | 21.4 | 22.6 | 23.7 | 24.8 | 28.3 | 29.5 | 30.7 |
| 22 | 19.5 | 20.6 | 21.6 | 22.6 | 25.8 | 26.9 | 28.0 |
| 23 | 17.8 | 18.9 | 19.7 | 20.6 | 23.6 | 24.6 | 25.6 |
| 24 | 16.5 | 17.3 | 18.1 | 19.0 | 21.7 | 22.6 | 23.5 |
| 25 | 15.1 | 16.0 | 16.7 | 17.5 | 20.0 | 20.8 | 21.7 |
| 26 | 13.9 | 14.8 | 15.5 | 16.2 | 18.5 | 19.2 | 20.0 |
| 27 | 12.9 | 13.7 | 14.3 | 15.0 | 17.1 | 17.8 | 18.6 |
| 28 | 12.0 | 12.7 | 13.3 | 13.9 | 15.9 | 16.6 | 17.3 |
| 29 | 11.2 | 11.9 | 12.4 | 13.0 | 14.8 | 15.5 | 16.1 |
| 30 | 10.5 | 11.1 | 11.6 | 12.1 | 13.9 | 14.5 | 15.0 |
| 31 | 9.8 | 10.4 | 10.9 | 11.4 | 13.0 | 13.5 | 14.1 |
| 32 | 9.2 | 9.7 | 10.2 | 10.7 | 12.2 | 12.7 | 13.2 |
| 33 | 8.7 | 9.2 | 9.6 | 10.0 | 11.5 | 11.9 | 12.4 |
| 34 | 8.2 | 8.6 | 9.0 | 9.4 | 10.8 | 11.3 | 11.7 |
| 35 | 7.7 | 8.1 | 8.5 | 8.9 | 10.2 | 10.6 | 11.0 |
| 36 | 7.3 | 7.7 | 8.1 | 8.4 | 9.6 | 10.0 | 10.4 |
| 37 | 6.9 | 7.3 | 7.6 | 8.0 | 9.1 | 9.5 | 9.9 |
| 38 | 6.5 | 6.9 | 7.2 | 7.6 | 8.6 | 9.0 | 9.4 |
| 39 | 6.2 | 6.5 | 6.8 | 7.2 | 8.2 | 8.5 | 8.9 |
| 40 | 5.9 | 6.2 | 6.5 | 6.8 | 7.8 | 8.1 | 8.4 |

For spacings above single dot the safe loads are too great for standard connections.

For spacings below the heavy lines the deflections will be greater than the allowable limit for plastered ceilings = $\frac{1}{360}$ span.

Spacings for other intensities of loading may be obtained from those in tables as follows:

$$\text{Required spacing} = \frac{\text{Intensity of loading from table}}{\text{New intensity of loading.}} \times \text{Computed spacing from table.}$$

SPACING OF CAMBRIA I-BEAMS FOR UNIFORM LOAD OF 100 LBS. PER SQUARE FOOT.

Proper distance in feet, center to center of Beams.
Maximum fibre stress 16 000 pounds per square inch.

| Distance between supports in feet. | SPECIAL I-BEAM. | | | | |
|---|--------------------|------------|------------|------------|-------------|
| | 20 Inch No. B 121. | | | | |
| | 80 lbs. | 85 lbs. | 90 lbs. | 95 lbs. | 100 lbs. |
| 16 | 61.1 | 62.9 | 64.9 | 66.9 | 69.0 |
| 17 | 54.1 | 55.7 | 57.5 | 59.3 | 61.1 |
| 18 | 48.3 | 49.7 | 51.3 | 52.9 | 54.5 |
| 19 | 43.3 | 44.6 | 46.0 | 47.5 | 48.9 |
| 20 | 39.1 | 40.2 | 41.5 | 42.8 | 44.1 |
| 21 | 35.5 | 36.5 | 37.7 | 38.9 | 40.0 |
| 22 | 32.3 | 33.2 | 34.3 | 35.4 | 36.5 |
| 23 | •29.6 | •30.4 | 31.4 | 32.4 | 33.4 |
| 24 | 27.2 | 27.9 | •28.8 | 29.8 | 30.7 |
| 25 | 25.0 | 25.7 | 26.6 | •27.4 | 28.3 |
| 26 | 23.1 | 23.8 | 24.6 | 25.4 | •26.1 |
| 27 | 21.5 | 22.1 | 22.8 | 23.5 | 24.2 |
| 28 | 19.9 | 20.5 | 21.2 | 21.9 | 22.5 |
| 29 | 18.6 | 19.1 | 19.8 | 20.4 | 21.0 |
| 30 | 17.4 | 17.9 | 18.5 | 19.0 | 19.6 |
| 31 | 16.3 | 16.7 | 17.3 | 17.8 | 18.4 |
| 32 | 15.3 | 15.7 | 16.2 | 16.7 | 17.2 |
| 33 | 14.4 | 14.8 | 15.3 | 15.7 | 16.2 |
| 34 | 13.5 | 13.9 | 14.4 | 14.8 | 15.3 |
| 35 | 12.8 | 13.1 | 13.6 | 14.0 | 14.4 |
| 36 | 12.1 | 12.4 | 12.8 | 13.2 | 13.6 |
| 37 | 11.4 | 11.8 | 12.1 | 12.5 | 12.9 |
| 38 | 10.8 | 11.1 | 11.5 | 11.9 | 12.1 |
| 39 | 10.3 | 10.6 | 10.9 | 11.2 | 11.6 |
| 40 | 9.8 | 10.0 | 10.4 | 10.7 | 11.0 |

For spacings above single dot the safe loads are too great for standard connections.

Spacings for other intensities of loading may be obtained from those in tables as follows:

$$\text{Required spacing} = \frac{\text{Intensity of loading from table}}{\text{New intensity of loading}} \times \text{Computed spacing from table.}$$

SPACING OF CAMBRIA I-BEAMS FOR UNIFORM LOAD OF 100 LBS. PER SQUARE FOOT.

Proper distance in feet, center to center of Beams.
Maximum fibre stress 16 000 pounds per square inch.

| Distance between supports in feet. | STANDARD I-BEAM. | | | | |
|---|-------------------|------------|------------|------------|-------------|
| | 24 Inch No. B 89. | | | | |
| | 80 lbs. | 85 lbs. | 90 lbs. | 95 lbs. | 100 lbs. |
| 18 | 57.3 | 59.5 | 61.4 | 63.3 | 65.3 |
| 19 | 51.4 | •53.4 | •55.1 | 56.9 | 58.6 |
| 20 | 46.4 | 48.2 | 49.7 | •51.3 | •52.9 |
| 21 | 42.1 | 43.7 | 45.1 | 46.5 | 48.0 |
| 22 | 38.3 | 39.8 | 41.1 | 42.4 | 43.7 |
| 23 | 35.1 | 36.4 | 37.6 | 38.8 | 40.0 |
| 24 | 32.2 | 33.5 | 34.5 | 35.6 | 36.7 |
| 25 | 29.7 | 30.8 | 31.8 | 32.8 | 33.8 |
| 26 | 27.4 | 28.5 | 29.4 | 30.4 | 31.3 |
| 27 | 25.5 | 26.4 | 27.3 | 28.2 | 29.0 |
| 28 | 23.7 | 24.6 | 25.4 | 26.2 | 27.0 |
| 29 | 22.1 | 22.9 | 23.7 | 24.4 | 25.2 |
| 30 | 20.6 | 21.4 | 22.1 | 22.8 | 23.5 |
| 31 | 19.3 | 20.1 | 20.7 | 21.4 | 22.0 |
| 32 | 18.1 | 18.8 | 19.4 | 20.0 | 20.7 |
| 33 | 17.0 | 17.7 | 18.3 | 18.8 | 19.4 |
| 34 | 16.0 | 16.7 | 17.2 | 17.8 | 18.3 |
| 35 | 15.1 | 15.7 | 16.2 | 16.8 | 17.3 |
| 36 | 14.3 | 14.9 | 15.4 | 15.8 | 16.3 |
| 37 | 13.5 | 14.1 | 14.5 | 15.0 | 15.4 |
| 38 | 12.8 | 13.3 | 13.7 | 14.2 | 14.6 |
| 39 | 12.2 | 12.6 | 13.1 | 13.5 | 13.9 |
| 40 | 11.6 | 12.0 | 12.4 | 12.8 | 13.2 |
| 41 | 11.0 | 11.5 | 11.8 | 12.2 | 12.6 |
| 42 | 10.5 | 10.9 | 11.3 | 11.6 | 12.0 |
| 43 | 10.0 | 10.4 | 10.8 | 11.1 | 11.4 |
| 44 | 9.6 | 9.9 | 10.3 | 10.6 | 10.9 |
| 45 | 9.2 | 9.5 | 9.8 | 10.1 | 10.4 |
| 46 | 8.7 | 9.1 | 9.4 | 9.7 | 10.0 |
| 47 | 8.4 | 8.7 | 9.0 | 9.3 | 9.6 |
| 48 | 8.0 | 8.3 | 8.6 | 8.9 | 9.2 |

For spacings above single dot, the safe loads are too great for standard connections.

Spacings for other intensities of loading may be obtained from those in tables as follows:

$$\text{Required spacing} = \frac{\text{Intensity of loading from table}}{\text{New intensity of loading}} \times \text{Computed spacing from table.}$$

SPACING OF CAMBRIA I-BEAMS FOR UNIFORM LOAD OF 100 LBS. PER SQUARE FOOT.

Proper distance in feet, center to center of Beams.
Maximum fibre stress 16 000 pounds per square inch.

| Distance between supports in feet. | SPECIAL I-BEAM. | | |
|---|--------------------|-------------|-------------|
| | 24 Inch No. B 127. | | |
| | 105 lbs. | 110 lbs. | 115 lbs. |
| 18 | 77.1 | 79.1 | 81.1 |
| 19 | 69.2 | 71.0 | 72.8 |
| 20 | 62.5 | 64.1 | 65.7 |
| 21 | 56.7 | 58.1 | 59.6 |
| 22 | 51.6 | 53.0 | 54.3 |
| 23 | 47.2 | 48.4 | 49.6 |
| 24 | • 43.4 | • 44.5 | • 45.6 |
| 25 | 40.0 | • 41.0 | • 42.0 |
| 26 | 37.0 | 37.9 | 38.8 |
| 27 | 34.3 | 35.1 | 36.0 |
| 28 | 31.9 | 32.7 | 33.5 |
| 29 | 29.7 | 30.5 | 31.2 |
| 30 | 27.8 | 28.5 | 29.2 |
| 31 | 26.0 | 26.7 | 27.3 |
| 32 | 24.4 | 25.0 | 25.6 |
| 33 | 22.9 | 23.5 | 24.1 |
| 34 | 21.6 | 22.2 | 22.7 |
| 35 | 20.4 | 20.9 | 21.4 |
| 36 | 19.3 | 19.8 | 20.3 |
| 37 | 18.3 | 18.7 | 19.2 |
| 38 | 17.3 | 17.7 | 18.2 |
| 39 | 16.4 | 16.8 | 17.2 |
| 40 | 15.6 | 16.0 | 16.4 |
| 41 | 14.9 | 15.2 | 15.6 |
| 42 | 14.2 | 14.5 | 14.9 |
| 43 | 13.5 | 13.8 | 14.2 |
| 44 | 12.9 | 13.2 | 13.6 |
| 45 | 12.3 | 12.6 | 13.0 |
| 46 | 11.8 | 12.1 | 12.4 |
| 47 | 11.3 | 11.6 | 11.9 |
| 48 | 10.8 | 11.1 | 11.4 |

For spacings above single dot the safe loads are too great for standard connections.

Spacings for other intensities of loading may be obtained from those in tables as follows:

$$\text{Required spacing} = \frac{\text{Intensity of loading from table}}{\text{New intensity of loading}} \times \text{Computed spacing from table.}$$

MAXIMUM BENDING MOMENTS IN FOOT POUNDS FOR CAMBRIA I-BEAMS.

| Section Num- ber. | Depth of Beam. | Weight per Foot. | Maximum Bending Moment. | | Section Num- ber. | Depth of Beam. | Weight per Foot. | Maximum Bending Moment. | | | |
|-------------------------|----------------------|------------------------|----------------------------|----------------------------|-------------------------|----------------------------|----------------------------|----------------------------|--------|--------|--------|
| | | | Foot Pounds. | | | | | Foot Pounds. | | | |
| | Inches. | Pounds. | Fibre Stress | Fibre Stress | | Fibre Stress | Fibre Stress | | | | |
| | | | 16 000 lbs. per Sq. In. | 12 500 lbs. per Sq. In. | | 16 000 lbs. per Sq. In. | 12 500 lbs. per Sq. In. | | | | |
| B 5 | 3 | 5.5 | 2270 | 1770 | B 53 | 15 | 42 | 78530 | 61350 | | |
| " | " | 6.5 | 2400 | 1880 | " | " | 45 | 81070 | 63330 | | |
| " | " | 7.5 | 2530 | 1980 | " | " | 50 | 86000 | 67190 | | |
| B 9 | 4 | 7.5 | 4000 | 3130 | " | " | 55 | 90800 | 70940 | | |
| " | " | 8.5 | 4270 | 3330 | " | " | 60 | 95730 | 74790 | | |
| " | " | 9.5 | 4530 | 3540 | B109 | 15 | 60 | 108270 | 84580 | | |
| " | " | 10.5 | 4800 | 3750 | | | " | " | 65 | 113070 | 88330 |
| B 13 | 5 | 9.75 | 6400 | 5000 | " | " | 70 | 118000 | 92190 | | |
| " | " | 12.25 | 7200 | 5630 | " | " | 75 | 122930 | 96040 | | |
| " | " | 14.75 | 8130 | 6350 | " | " | 80 | 127730 | 99790 | | |
| B 17 | 6 | 12.25 | 9730 | 7600 | B113 | 15 | 80 | 140270 | 109580 | | |
| " | " | 14.75 | 10670 | 8330 | " | " | 85 | 145070 | 113330 | | |
| " | " | 17.25 | 11600 | 9060 | " | " | 90 | 150000 | 117190 | | |
| B 21 | 7 | 15 | 13870 | 10830 | " | " | 95 | 154800 | 120940 | | |
| | | 17.5 | 14930 | 11670 | 100 | | 159730 | 124790 | | | |
| | | 20 | 16130 | 12600 | B 65 | | 18 | 55 | 117870 | 92080 | |
| B 25 | 8 | 18 | 18930 | 14790 | | " | | " | 60 | 124670 | 97400 |
| | | 20.25 | 20000 | 15630 | | " | | " | 65 | 130530 | 101980 |
| | | 22.75 | 21330 | 16670 | " | " | 70 | 136530 | 106670 | | |
| " | " | 25.25 | 22670 | 17710 | B 73 | 20 | 65 | 156000 | 121880 | | |
| B 29 | 9 | 21 | 25200 | 19690 | " | " | 70 | 162670 | 127080 | | |
| | | 25 | 27200 | 21250 | " | " | 75 | 169200 | 132190 | | |
| | | 30 | 30130 | 23540 | B121 | 20 | 80 | 195470 | 152710 | | |
| 35 | 33070 | 25830 | " | " | | | 85 | 201200 | 157190 | | |
| B 33 | 10 | 25 | 32530 | 25420 | | | " | " | 90 | 207730 | 162290 |
| | | 30 | 35730 | 27920 | " | " | 95 | 214270 | 167400 | | |
| | | 35 | 39070 | 30520 | " | " | 100 | 220800 | 172500 | | |
| " | " | 40 | 42270 | 33020 | B 89 | 24 | 80 | 231870 | 181150 | | |
| B 41 | 12 | 31.5 | 48000 | 37500 | " | " | 85 | 240930 | 188230 | | |
| | | 35 | 50670 | 39580 | " | " | 90 | 248670 | 194270 | | |
| | | 40 | 54670 | 42710 | " | " | 95 | 256530 | 200420 | | |
| B105 | 12 | 40 | 59730 | 46670 | " | " | 100 | 264400 | 206560 | | |
| | | 45 | 63470 | 49580 | B127 | 24 | 105 | 312380 | 244050 | | |
| | | 50 | 67470 | 52710 | | | " | " | 110 | 320380 | 250300 |
| | | 55 | 71330 | 55730 | | | " | " | 115 | 328380 | 256550 |

MAXIMUM BENDING MOMENTS IN FOOT POUNDS FOR CAMBRIA CHANNELS.

| Section Num- ber. | Depth of Chan- nel. | Weight per Foot. | Maximum Bending Moment. | | Section Num- ber. | Depth of Chan- nel. | Weight per Foot. | Maximum Bending Moment. | |
|-------------------------|------------------------------|------------------------|---|---|-------------------------|------------------------------|---|---|-------|
| | | | Foot Pounds. | | | | | Foot Pounds. | |
| | Inches. | Pounds. | Fibre Stress 16 000 lbs. per Sq. In. | Fibre Stress 12 500 lbs. per Sq. In. | Inches. | Pounds. | Fibre Stress 16 000 lbs. per Sq. In. | Fibre Stress 12 500 lbs. per Sq. In. | |
| C 5 | 3 | 4 | 1470 | 1150 | C29 | 9 | 13.25 | 14000 | 10940 |
| " | " | 5 | 1600 | 1250 | " | " | 15 | 15070 | 11770 |
| " | " | 6 | 1870 | 1460 | " | " | 20 | 18000 | 14060 |
| | | | | | " | " | 25 | 20930 | 16350 |
| C 9 | 4 | 5.25 | 2530 | 1980 | C33 | 10 | 15 | 17870 | 13960 |
| " | " | 6.25 | 2800 | 2190 | " | " | 20 | 20930 | 16350 |
| " | " | 7.25 | 3070 | 2400 | " | " | 25 | 24270 | 18960 |
| C13 | 5 | 6.5 | 4000 | 3130 | " | " | 30 | 27470 | 21460 |
| " | " | 9 | 4670 | 3650 | " | " | 35 | 30800 | 24060 |
| " | " | 11.5 | 5600 | 4380 | | | | | |
| C17 | 6 | 8 | 5730 | 4480 | C41 | 12 | 20.5 | 28530 | 22290 |
| " | " | 10.5 | 6670 | 5210 | " | " | 25 | 32000 | 25000 |
| " | " | 13 | 7730 | 6040 | " | " | 30 | 35870 | 28020 |
| " | " | 15.5 | 8670 | 6770 | " | " | 35 | 39870 | 31150 |
| | | | | | " | " | 40 | 43730 | 34170 |
| C21 | 7 | 9.75 | 8000 | 6250 | C53 | 15 | 33 | 55600 | 43440 |
| " | " | 12.25 | 9200 | 7190 | " | " | 35 | 56930 | 44480 |
| " | " | 14.75 | 10400 | 8130 | " | " | 40 | 61730 | 48230 |
| " | " | 17.25 | 11470 | 8960 | " | " | 45 | 66670 | 52080 |
| " | " | 19.75 | 12670 | 9900 | " | " | 50 | 71600 | 55940 |
| | | | | | " | " | 55 | 76530 | 59790 |
| C25 | 8 | 11.25 | 10800 | 8440 | C65 | 18 | 45 | 86530 | 67600 |
| " | " | 13.75 | 12000 | 9380 | " | " | 50 | 92310 | 72130 |
| " | " | 16.25 | 13330 | 10420 | " | " | 55 | 98070 | 76620 |
| " | " | 18.75 | 14670 | 11460 | " | " | 60 | 104190 | 81410 |
| " | " | 21.25 | 15870 | 12400 | | | | | |

SAFE LOADS IN POUNDS UNIFORMLY DISTRIBUTED FOR CAMBRIA ANGLES.

EQUAL LEGS.

NEUTRAL AXIS PARALLEL TO EITHER LEG.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.



| Distance between supports in feet. | Section No. A 11. | | | | |
|---|--|----------------------|----------------------|----------------------|----------------------|
| | $1\frac{1}{2}'' \times 1\frac{1}{2}''$ | | | | |
| | $\frac{1}{8}''$ | $\frac{3}{16}''$ | $\frac{1}{4}''$ | $\frac{5}{16}''$ | $\frac{3}{8}''$ |
| | 1.23 lbs. per ft. | 1.80 lbs. per ft. | 2.34 lbs. per ft. | 2.86 lbs. per ft. | 3.35 lbs. per ft. |
| 2 | 390 | 560 | 720 | 860 | 1010 |
| 3 | 260 | 370 | 480 | 580 | 670 |
| 4 | 190 | 280 | 360 | 430 | 500 |
| 5 | 150 | 220 | 290 | 350 | 400 |
| 6 | 130 | 190 | 240 | 290 | 340 |
| 7 | 110 | 160 | 200 | 250 | 290 |
| 8 | 100 | 140 | 180 | 220 | 250 |
| 9 | 90 | 120 | 160 | 190 | 220 |

| Distance between supports in feet. | Section No. A 40. | | | | |
|---|--|----------------------|----------------------|----------------------|----------------------|
| | $1\frac{3}{4}'' \times 1\frac{3}{4}''$ | | | | |
| | $\frac{1}{8}''$ | $\frac{3}{16}''$ | $\frac{1}{4}''$ | $\frac{5}{16}''$ | $\frac{3}{8}''$ |
| | 1.44 lbs. per ft. | 2.12 lbs. per ft. | 2.77 lbs. per ft. | 3.39 lbs. per ft. | 3.99 lbs. per ft. |
| 2 | 530 | 770 | 990 | 1200 | 1400 |
| 3 | 350 | 510 | 660 | 800 | 940 |
| 4 | 260 | 380 | 500 | 600 | 700 |
| 5 | 210 | 310 | 400 | 480 | 560 |
| 6 | 170 | 250 | 330 | 400 | 470 |
| 7 | 150 | 220 | 280 | 340 | 400 |
| 8 | 130 | 190 | 250 | 300 | 350 |
| 9 | 110 | 170 | 220 | 270 | 310 |
| 10 | 100 | 150 | 200 | 240 | 280 |

| Distance between supports in feet. | Section No. A 15. | | | | | | |
|---|----------------------|----------------------|----------------------|----------------------|---------------------|---------------------|---------------------|
| | $2'' \times 2''$ | | | | | | |
| | $\frac{1}{8}''$ | $\frac{3}{16}''$ | $\frac{1}{4}''$ | $\frac{5}{16}''$ | $\frac{3}{8}''$ | $\frac{7}{16}''$ | $\frac{1}{2}''$ |
| | 1.65 lbs. per ft. | 2.44 lbs. per ft. | 3.19 lbs. per ft. | 3.92 lbs. per ft. | 4.7 lbs. per ft. | 5.3 lbs. per ft. | 6.0 lbs. per ft. |
| 2 | 690 | 1020 | 1320 | 1600 | 1870 | 2130 | 2380 |
| 3 | 460 | 680 | 880 | 1070 | 1250 | 1420 | 1590 |
| 4 | 340 | 510 | 660 | 800 | 940 | 1070 | 1190 |
| 5 | 270 | 410 | 530 | 640 | 750 | 850 | 950 |
| 6 | 230 | 340 | 440 | 530 | 620 | 710 | 790 |
| 7 | 190 | 290 | 380 | 460 | 540 | 610 | 680 |
| 8 | 170 | 250 | 330 | 400 | 470 | 530 | 600 |
| 9 | 150 | 230 | 290 | 360 | 420 | 470 | 530 |
| 10 | 130 | 200 | 260 | 320 | 370 | 430 | 480 |

For safe loads below heavy lines the deflections will be greater than the allowable limit for plastered ceilings = $\frac{1}{325}$ span.

SAFE LOADS IN POUNDS UNIFORMLY DISTRIBUTED FOR CAMBRIA ANGLES.

EQUAL LEGS.

NEUTRAL AXIS PARALLEL TO EITHER LEG.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.



| Distance between supports in feet. | Section No. A 41 | | |
|---|--|----------------------|---------------------|
| | $2\frac{1}{4}'' \times 2\frac{1}{4}''$ | | |
| | $\frac{3}{16}''$ | $\frac{1}{4}''$ | $\frac{5}{16}''$ |
| | 2.75 lbs. per ft. | 3.62 lbs. per ft. | 4.5 lbs. per ft. |
| 2 | 1300 | 1690 | 2060 |
| 3 | 870 | 1120 | 1370 |
| 4 | 650 | 840 | 1030 |
| 5 | 520 | 670 | 820 |
| 6 | 430 | 560 | 690 |
| 7 | 370 | 480 | 590 |
| 8 | 320 | 420 | 510 |
| 9 | 290 | 380 | 460 |
| 10 | 260 | 340 | 410 |
| 11 | 240 | 310 | 370 |
| 12 | 220 | 280 | 340 |

| Distance between supports in feet. | Section No. A 17. | | | | | | |
|---|--|----------------------|---------------------|---------------------|---------------------|---------------------|---------------------|
| | $2\frac{1}{2}'' \times 2\frac{1}{2}''$ | | | | | | |
| | $\frac{1}{8}''$ | $\frac{3}{16}''$ | $\frac{1}{4}''$ | $\frac{5}{16}''$ | $\frac{3}{8}''$ | $\frac{7}{16}''$ | $\frac{1}{2}''$ |
| | 2.08 lbs. per ft. | 3.07 lbs. per ft. | 4.1 lbs. per ft. | 5.0 lbs. per ft. | 5.9 lbs. per ft. | 6.8 lbs. per ft. | 7.7 lbs. per ft. |
| 2 | 1060 | 1610 | 2100 | 2570 | 3020 | 3450 | 3860 |
| 3 | 710 | 1080 | 1400 | 1710 | 2010 | 2300 | 2580 |
| 4 | 530 | 810 | 1050 | 1290 | 1510 | 1720 | 1930 |
| 5 | 420 | 650 | 840 | 1030 | 1210 | 1380 | 1550 |
| 6 | 350 | 540 | 700 | 860 | 1010 | 1150 | 1290 |
| 7 | 300 | 460 | 600 | 730 | 860 | 990 | 1100 |
| 8 | 260 | 400 | 530 | 640 | 760 | 860 | 970 |
| 9 | 230 | 360 | 470 | 570 | 670 | 770 | 860 |
| 10 | 210 | 320 | 420 | 510 | 600 | 690 | 770 |
| 11 | 190 | 290 | 380 | 470 | 550 | 630 | 700 |
| 12 | 170 | 270 | 350 | 430 | 500 | 580 | 640 |

For safe loads below heavy lines the deflections will be greater than the allowable limit for plastered ceilings = $\frac{1}{360}$ span.

SAFE LOADS IN POUNDS UNIFORMLY DISTRIBUTED FOR CAMBRIA ANGLES.

EQUAL LEGS.

NEUTRAL AXIS PARALLEL TO EITHER LEG.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.



| Distance between supports in feet. | Section No. A 43. | | |
|------------------------------------|--|------------------|------------------|
| | $2\frac{3}{4}'' \times 2\frac{3}{4}''$ | | |
| | $\frac{1}{4}''$ | $\frac{5}{16}''$ | $\frac{3}{8}''$ |
| | 4.5 lbs. per ft. | 5.6 lbs. per ft. | 6.6 lbs. per ft. |
| 2 | 2570 | 3140 | 3700 |
| 3 | 1710 | 2090 | 2460 |
| 4 | 1280 | 1570 | 1850 |
| 5 | 1030 | 1260 | 1480 |
| 6 | 860 | 1050 | 1230 |
| 7 | 730 | 900 | 1060 |
| 8 | 640 | 790 | 920 |
| 9 | 570 | 700 | 820 |
| 10 | 510 | 630 | 740 |
| 11 | 470 | 570 | 670 |
| 12 | 430 | 520 | 620 |

| Distance between supports in feet. | Section No. A 19. | | | | | |
|------------------------------------|-------------------|------------------|------------------|------------------|------------------|-------------------|
| | $3'' \times 3''$ | | | | | |
| | $\frac{1}{4}''$ | $\frac{5}{16}''$ | $\frac{3}{8}''$ | $\frac{7}{16}''$ | $\frac{1}{2}''$ | $\frac{9}{16}''$ |
| | 4.9 lbs. per ft. | 6.1 lbs. per ft. | 7.2 lbs. per ft. | 8.3 lbs. per ft. | 9.4 lbs. per ft. | 10.4 lbs. per ft. |
| 2 | 3080 | 3770 | 4440 | 5090 | 5720 | 6320 |
| 3 | 2050 | 2510 | 2960 | 3390 | 3810 | 4210 |
| 4 | 1540 | 1890 | 2220 | 2540 | 2860 | 3160 |
| 5 | 1230 | 1510 | 1780 | 2040 | 2290 | 2530 |
| 6 | 1030 | 1260 | 1480 | 1700 | 1910 | 2110 |
| 7 | 880 | 1080 | 1270 | 1450 | 1630 | 1810 |
| 8 | 770 | 940 | 1110 | 1270 | 1430 | 1580 |
| 9 | 680 | 840 | 990 | 1130 | 1270 | 1410 |
| 10 | 620 | 750 | 890 | 1020 | 1140 | 1260 |
| 11 | 560 | 690 | 810 | 930 | 1040 | 1150 |
| 12 | 510 | 630 | 740 | 850 | 950 | 1050 |

For safe loads below heavy lines the deflections will be greater than the allowable limit for plastered ceilings = $\frac{1}{360}$ span.

SAFE LOADS IN POUNDS UNIFORMLY DISTRIBUTED FOR CAMBRIA ANGLES.

EQUAL LEGS.

NEUTRAL AXIS PARALLEL TO EITHER LEG.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.



Section No. A 21.

| Distance between supports in feet. | $3\frac{1}{2}'' \times 3\frac{1}{2}''$ | | | | | | | | | | |
|---|---|--|---|--|--|---|--|--|--|--|--|
| | $\frac{1}{4}''$ 5.8 lbs. per ft. | $\frac{5}{16}''$ 7.2 lbs. per ft. | $\frac{3}{8}''$ 8.5 lbs. per ft. | $\frac{7}{16}''$ 9.8 lbs. per ft. | $\frac{1}{2}''$ 11.1 lbs. per ft. | $\frac{9}{16}''$ 12.4 lbs. per ft. | $\frac{5}{8}''$ 13.6 lbs. per ft. | $\frac{11}{16}''$ 14.8 lbs. per ft. | $\frac{3}{4}''$ 16.0 lbs. per ft. | $\frac{13}{16}''$ 17.1 lbs. per ft. | $\frac{7}{8}''$ 18.3 lbs. per ft. |
| 2 | 4210 | 5200 | 6140 | 7050 | 7940 | 8800 | 9630 | 10440 | 11230 | 12010 | 12760 |
| 3 | 2810 | 3470 | 4100 | 4700 | 5290 | 5860 | 6420 | 6960 | 7490 | 8000 | 8510 |
| 4 | 2110 | 2600 | 3070 | 3530 | 3970 | 4400 | 4810 | 5220 | 5620 | 6000 | 6380 |
| 5 | 1680 | 2080 | 2460 | 2820 | 3180 | 3520 | 3850 | 4180 | 4490 | 4800 | 5110 |
| 6 | 1400 | 1730 | 2050 | 2350 | 2650 | 2930 | 3210 | 3480 | 3740 | 4000 | 4250 |
| 7 | 1200 | 1490 | 1760 | 2020 | 2270 | 2510 | 2750 | 2980 | 3210 | 3430 | 3650 |
| 8 | 1050 | 1300 | 1540 | 1760 | 1980 | 2200 | 2410 | 2610 | 2810 | 3000 | 3190 |
| 9 | 940 | 1160 | 1370 | 1570 | 1760 | 1950 | 2140 | 2320 | 2500 | 2670 | 2840 |
| 10 | 840 | 1040 | 1230 | 1410 | 1590 | 1760 | 1930 | 2090 | 2250 | 2400 | 2550 |
| 11 | 770 | 950 | 1120 | 1280 | 1440 | 1600 | 1750 | 1900 | 2040 | 2180 | 2320 |
| 12 | 700 | 870 | 1020 | 1180 | 1320 | 1470 | 1600 | 1740 | 1870 | 2000 | 2130 |
| 13 | 650 | 800 | 950 | 1090 | 1220 | 1350 | 1480 | 1610 | 1730 | 1850 | 1960 |
| 14 | 600 | 740 | 880 | 1010 | 1130 | 1260 | 1380 | 1490 | 1610 | 1720 | 1820 |
| 15 | 560 | 690 | 820 | 940 | 1060 | 1170 | 1280 | 1390 | 1500 | 1600 | 1700 |
| 16 | 530 | 650 | 770 | 880 | 990 | 1100 | 1200 | 1310 | 1400 | 1500 | 1600 |

Section No. A 23.

| Distance between supports in feet. | 4" x 4" | | | | | | | | | |
|---|------------------|-----------------|------------------|-----------------|------------------|-----------------|-------------------|-----------------|-------------------|-----------------|
| | $\frac{5}{16}$ " | $\frac{3}{8}$ " | $\frac{7}{16}$ " | $\frac{1}{2}$ " | $\frac{9}{16}$ " | $\frac{5}{8}$ " | $\frac{11}{16}$ " | $\frac{3}{4}$ " | $\frac{13}{16}$ " | $\frac{7}{8}$ " |
| | 8.2 | 9.8 | 11.3 | 12.8 | 14.3 | 15.7 | 17.1 | 18.5 | 19.9 | 21.2 |
| | lbs. per ft. | lbs. per ft. | lbs. per ft. | lbs. per ft. | lbs. per ft. | lbs. per ft. | lbs. per ft. | lbs. per ft. | lbs. per ft. | lbs. per ft. |
| 2 | 6870 | 8120 | 9340 | 10530 | 11690 | 12810 | 13910 | 14980 | 16030 | 17060 |
| 3 | 4580 | 5420 | 6230 | 7020 | 7790 | 8540 | 9270 | 9990 | 10690 | 11370 |
| 4 | 3430 | 4060 | 4670 | 5270 | 5840 | 6410 | 6960 | 7490 | 8020 | 8530 |
| 5 | 2750 | 3250 | 3740 | 4210 | 4670 | 5130 | 5560 | 5990 | 6410 | 6820 |
| 6 | 2290 | 2710 | 3120 | 3510 | 3900 | 4270 | 4640 | 4990 | 5340 | 5690 |
| 7 | 1960 | 2320 | 2670 | 3010 | 3340 | 3660 | 3970 | 4280 | 4580 | 4870 |
| 8 | 1720 | 2030 | 2340 | 2630 | 2920 | 3200 | 3480 | 3740 | 4010 | 4260 |
| 9 | 1530 | 1810 | 2080 | 2340 | 2600 | 2850 | 3090 | 3330 | 3560 | 3790 |
| 10 | 1370 | 1620 | 1870 | 2110 | 2340 | 2560 | 2780 | 3000 | 3210 | 3410 |
| 11 | 1250 | 1480 | 1700 | 1910 | 2130 | 2330 | 2530 | 2720 | 2910 | 3100 |
| 12 | 1140 | 1350 | 1560 | 1760 | 1950 | 2140 | 2320 | 2500 | 2670 | 2840 |
| 13 | 1060 | 1250 | 1440 | 1620 | 1800 | 1970 | 2140 | 2300 | 2470 | 2620 |
| 14 | 980 | 1160 | 1340 | 1500 | 1670 | 1830 | 1990 | 2140 | 2290 | 2440 |
| 15 | 920 | 1080 | 1250 | 1400 | 1560 | 1710 | 1860 | 2000 | 2140 | 2270 |
| 16 | 860 | 1020 | 1170 | 1320 | 1460 | 1600 | 1740 | 1870 | 2000 | 2130 |

For safe loads below heavy lines the deflections will be greater than the allowable limit for plastered ceilings = $\frac{1}{160}$ span.

SAFE LOADS IN POUNDS UNIFORMLY DISTRIBUTED FOR CAMBRIA ANGLES.

EQUAL LEGS.

NEUTRAL AXIS PARALLEL TO EITHER LEG.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.



| Distance between supports in feet. | Section No. A 47. | | | | | | |
|------------------------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| | 5" x 5" | | | | | | |
| | $\frac{3}{8}$ " | $\frac{7}{16}$ " | $\frac{1}{2}$ " | $\frac{9}{16}$ " | $\frac{5}{8}$ " | $\frac{11}{16}$ " | $\frac{3}{4}$ " |
| | 12.3 lbs. per ft. | 14.3 lbs. per ft. | 16.2 lbs. per ft. | 18.1 lbs. per ft. | 20.0 lbs. per ft. | 21.8 lbs. per ft. | 23.6 lbs. per ft. |
| 2 | 12910 | 14900 | 16830 | 18720 | 20570 | 22380 | 24160 |
| 3 | 8610 | 9930 | 11220 | 12480 | 13710 | 14920 | 16110 |
| 4 | 6460 | 7450 | 8410 | 9360 | 10280 | 11190 | 12080 |
| 5 | 5170 | 5960 | 6730 | 7490 | 8230 | 8950 | 9660 |
| 6 | 4310 | 4960 | 5610 | 6240 | 6860 | 7460 | 8050 |
| 7 | 3690 | 4260 | 4810 | 5350 | 5880 | 6390 | 6900 |
| 8 | 3230 | 3720 | 4210 | 4680 | 5140 | 5600 | 6040 |
| 9 | 2870 | 3310 | 3740 | 4160 | 4570 | 4970 | 5370 |
| 10 | 2580 | 2980 | 3370 | 3740 | 4110 | 4480 | 4830 |
| 11 | 2350 | 2710 | 3060 | 3400 | 3740 | 4070 | 4390 |
| 12 | 2150 | 2480 | 2800 | 3120 | 3430 | 3730 | 4030 |
| 13 | 1990 | 2290 | 2590 | 2880 | 3160 | 3440 | 3720 |
| 14 | 1850 | 2130 | 2400 | 2670 | 2940 | 3200 | 3450 |
| 15 | 1720 | 1990 | 2240 | 2500 | 2740 | 2980 | 3220 |
| 16 | 1610 | 1860 | 2100 | 2340 | 2570 | 2800 | 3020 |
| 17 | 1520 | 1750 | 1980 | 2200 | 2420 | 2630 | 2840 |
| 18 | 1440 | 1660 | 1870 | 2080 | 2290 | 2490 | 2680 |

| Distance between supports in feet. | Section No. A 27. | | | | | | | | | | |
|------------------------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| | 6" x 6" | | | | | | | | | | |
| | $\frac{3}{8}$ " | $\frac{7}{16}$ " | $\frac{1}{2}$ " | $\frac{9}{16}$ " | $\frac{5}{8}$ " | $\frac{11}{16}$ " | $\frac{3}{4}$ " | $\frac{13}{16}$ " | $\frac{7}{8}$ " | $\frac{15}{16}$ " | 1" |
| | 14.9 lbs. per ft. | 17.2 lbs. per ft. | 19.6 lbs. per ft. | 21.9 lbs. per ft. | 24.2 lbs. per ft. | 26.5 lbs. per ft. | 28.7 lbs. per ft. | 31.0 lbs. per ft. | 33.1 lbs. per ft. | 35.3 lbs. per ft. | 37.4 lbs. per ft. |
| 2 | 18820 | 21720 | 24610 | 27420 | 30170 | 32880 | 35540 | 38150 | 40720 | 43240 | 45720 |
| 3 | 12550 | 14480 | 16400 | 18280 | 20120 | 21920 | 23690 | 25430 | 27150 | 28830 | 30480 |
| 4 | 9410 | 10860 | 12300 | 13710 | 15090 | 16440 | 17770 | 19080 | 20360 | 21620 | 22860 |
| 5 | 7530 | 8690 | 9840 | 10970 | 12070 | 13150 | 14220 | 15260 | 16290 | 17300 | 18290 |
| 6 | 6270 | 7240 | 8200 | 9140 | 10060 | 10960 | 11850 | 12720 | 13570 | 14410 | 15240 |
| 7 | 5380 | 6210 | 7030 | 7830 | 8620 | 9390 | 10150 | 10900 | 11630 | 12360 | 13080 |
| 8 | 4700 | 5430 | 6150 | 6850 | 7540 | 8220 | 8890 | 9540 | 10180 | 10810 | 11430 |
| 9 | 4180 | 4830 | 5470 | 6090 | 6710 | 7310 | 7900 | 8480 | 9050 | 9610 | 10160 |
| 10 | 3760 | 4340 | 4920 | 5480 | 6030 | 6580 | 7110 | 7630 | 8140 | 8650 | 9140 |
| 11 | 3420 | 3950 | 4470 | 4990 | 5490 | 5980 | 6460 | 6940 | 7400 | 7860 | 8310 |
| 12 | 3140 | 3620 | 4100 | 4570 | 5030 | 5480 | 5920 | 6360 | 6790 | 7210 | 7620 |
| 13 | 2900 | 3340 | 3790 | 4220 | 4640 | 5060 | 5470 | 5870 | 6260 | 6650 | 7030 |
| 14 | 2690 | 3100 | 3520 | 3920 | 4310 | 4700 | 5080 | 5450 | 5820 | 6180 | 6530 |
| 15 | 2510 | 2900 | 3280 | 3660 | 4020 | 4380 | 4740 | 5090 | 5430 | 5770 | 6100 |
| 16 | 2350 | 2720 | 3080 | 3430 | 3770 | 4110 | 4440 | 4770 | 5090 | 5410 | 5720 |
| 17 | 2210 | 2560 | 2900 | 3230 | 3550 | 3870 | 4180 | 4490 | 4790 | 5090 | 5380 |
| 18 | 2090 | 2410 | 2730 | 3050 | 3350 | 3650 | 3950 | 4240 | 4520 | 4810 | 5080 |
| 19 | 1980 | 2290 | 2590 | 2890 | 3180 | 3460 | 3740 | 4020 | 4290 | 4550 | 4810 |
| 20 | 1880 | 2170 | 2460 | 2740 | 3020 | 3290 | 3550 | 3820 | 4070 | 4320 | 4570 |
| 21 | 1790 | 2070 | 2340 | 2610 | 2870 | 3130 | 3390 | 3630 | 3880 | 4120 | 4350 |
| 22 | 1710 | 1970 | 2240 | 2490 | 2740 | 2990 | 3230 | 3470 | 3700 | 3930 | 4160 |

For safe loads below heavy lines the deflections will be greater than the allowable limit for plastered ceilings = $\frac{1}{160}$ span.

SAFE LOADS IN POUNDS UNIFORMLY DISTRIBUTED FOR CAMBRIA ANGLES.

EQUAL LEGS.

NEUTRAL AXIS PARALLEL TO EITHER LEG.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.



Section No. A 35.

Distance

between

sup-
parts

in feet.

8" x 8"

 $\frac{1}{2}$ " $\frac{9}{16}$ " $\frac{5}{8}$ " $\frac{11}{16}$ " $\frac{3}{4}$ " $\frac{13}{16}$ " $\frac{7}{8}$ " $\frac{15}{16}$ "

1"

 $1\frac{1}{16}$ " $1\frac{1}{8}$ "26.4
lbs.
per ft.29.6
lbs.
per ft.32.7
lbs.
per ft.35.8
lbs.
per ft.38.9
lbs.
per ft.42.0
lbs.
per ft.45.0
lbs.
per ft.48.1
lbs.
per ft.51.0
lbs.
per ft.54.0
lbs.
per ft.56.9
lbs.
per ft.4
522310
1785024910
1992027470
2198030000
2400032490
2599034950
2796037370
2990039760
3181042120
3370044450
3556046750
374006
7
8
9
1014880
12750
11160
9920
893016600
14230
12450
11070
998018310
15700
13740
12210
1099020000
17140
15000
13330
1200021660
18570
16250
14440
1300023300
19970
17480
15530
1398024920
21360
18690
16610
1495026510
22720
19880
17670
1591028080
24070
21060
18720
1685029630
25400
22220
19760
1778031160
26710
23370
20780
1870011
12
13
14
158110
7440
6870
6380
59509060
8300
7660
7120
66409990
9160
8450
7850
733010910
10000
9230
8570
800011820
10830
10070
9280
866012710
11650
10750
9990
932013590
12460
11500
10680
997014460
13250
12240
11360
1060015320
14040
12960
12030
1123016160
14820
13680
12700
1185017000
15580
14380
13360
1247016
17
18
19
205580
5250
4960
4700
44606230
5860
5530
5240
49806870
6460
6100
5780
54907500
7060
6670
6320
60008120
7650
7220
6840
65008740
8220
7770
7360
69909340
8790
8310
7870
74709940
9360
8840
8370
795010530
9910
9360
8870
842011110
10460
9880
9360
889011690
11000
10390
9840
935021
22
23
24
254250
4060
3880
3720
35704740
4530
4330
4150
39805230
4990
4780
4580
44005710
5450
5220
5000
48006190
5910
5650
5420
52006660
6350
6080
5830
55907120
6800
6500
6230
59807570
7230
6920
6630
63608020
7660
7330
7020
67408470
8080
7730
7410
71108900
8500
8130
7790
748026
27
28
29
303430
3310
3190
3080
29803830
3690
3560
3440
33204230
4070
3920
3790
36604620
4440
4290
4140
40005000
4810
4640
4480
43305380
5180
4990
4820
46605750
5540
5340
5160
49806120
5890
5680
5480
53006480
6240
6020
5810
56206840
6590
6350
6130
59307190
6930
6680
6450
6230

For safe loads below heavy lines the deflections will be greater than the allowable limit for plastered ceilings = $\frac{1}{320}$ span.

SAFE LOADS IN POUNDS UNIFORMLY DISTRIBUTED FOR CAMBRIA ANGLES.

UNEQUAL LEGS.

NEUTRAL AXIS PARALLEL TO LONG LEG.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.



| Distance between supports in feet. | Section No. A 91. | | | | | | Section No. A 129. | | | | | |
|---|------------------------------|------------------------------|-----------------------------|-----------------------------|-----------------------------|-----------------------------|------------------------------|-----------------------------|-----------------------------|-----------------------------|-----------------------------|-----------------------------|
| | 2½" x 2" | | | | | | 3" x 2" | | | | | |
| | 3" 16 | 1" 4 | 5" 16 | 3" 8 | 7" 16 | 1" 2 | 3" 16 | 1" 4 | 5" 16 | 3" 8 | 7" 16 | 1" 2 |
| | 2.75 lbs. per foot. | 3.62 lbs. per foot. | 4.5 lbs. per foot. | 5.3 lbs. per foot. | 6.1 lbs. per foot. | 6.8 lbs. per foot. | 3.07 lbs. per foot. | 4.1 lbs. per foot. | 5.0 lbs. per foot. | 5.9 lbs. per foot. | 6.8 lbs. per foot. | 7.7 lbs. per foot. |
| 2 | 1050 | 1360 | 1650 | 1930 | 2200 | 2460 | 1070 | 1390 | 1690 | 1980 | 2260 | 2530 |
| 3 | 700 | 900 | 1100 | 1290 | 1470 | 1640 | 710 | 920 | 1120 | 1320 | 1510 | 1690 |
| 4 | 520 | 680 | 830 | 970 | 1100 | 1230 | 530 | 690 | 840 | 990 | 1130 | 1260 |
| 5 | 420 | 540 | 660 | 770 | 880 | 990 | 430 | 550 | 670 | 790 | 900 | 1010 |
| 6 | 350 | 450 | 550 | 640 | 730 | 820 | 360 | 460 | 560 | 660 | 750 | 840 |
| 7 | 300 | 390 | 470 | 550 | 630 | 700 | 310 | 400 | 480 | 570 | 650 | 720 |
| 8 | 260 | 340 | 410 | 480 | 550 | 620 | 270 | 350 | 420 | 500 | 560 | 630 |
| 9 | 230 | 290 | 360 | 420 | 480 | 540 | 240 | 310 | 370 | 440 | 500 | 560 |
| 10 | 210 | 260 | 330 | 380 | 430 | 490 | 210 | 280 | 340 | 400 | 450 | 510 |
| 11 | 190 | 240 | 300 | 340 | 390 | 440 | 190 | 250 | 310 | 360 | 410 | 460 |
| 12 | 170 | 220 | 270 | 320 | 360 | 400 | 180 | 230 | 280 | 330 | 380 | 420 |

| Distance between supports in feet. | Section No. A 93. | | | | | |
|---|---------------------|---------------------|---------------------|---------------------|---------------------|---------------------|
| | 3" x 2½" | | | | | |
| | 1" 4 | 5" 16 | 3" 8 | 7" 16 | 1" 2 | 9" 16 |
| | 4.5 lbs. per ft. | 5.6 lbs. per ft. | 6.6 lbs. per ft. | 7.6 lbs. per ft. | 8.5 lbs. per ft. | 9.5 lbs. per ft. |
| 2 | 2160 | 2640 | 3100 | 3540 | 3970 | 4380 |
| 3 | 1440 | 1760 | 2060 | 2360 | 2650 | 2920 |
| 4 | 1080 | 1320 | 1550 | 1770 | 1980 | 2190 |
| 5 | 860 | 1050 | 1240 | 1420 | 1590 | 1750 |
| 6 | 720 | 880 | 1030 | 1180 | 1320 | 1460 |
| 7 | 620 | 750 | 880 | 1010 | 1130 | 1250 |
| 8 | 540 | 660 | 770 | 890 | 990 | 1100 |
| 9 | 480 | 590 | 690 | 790 | 880 | 970 |
| 10 | 430 | 530 | 620 | 710 | 790 | 880 |
| 11 | 390 | 480 | 560 | 640 | 720 | 800 |
| 12 | 360 | 440 | 520 | 590 | 660 | 730 |

For safe loads below heavy lines the deflections will be greater than the allowable limit for plastered ceilings = $\frac{1}{360}$ span.

SAFE LOADS IN POUNDS UNIFORMLY DISTRIBUTED FOR CAMBRIA ANGLES.

UNEQUAL LEGS.

NEUTRAL AXIS PARALLEL TO LONG LEG.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.



| Distance between supports in feet. | Section No. A 95. | | | | | |
|---|--|------------------------|------------------------|------------------------|------------------------|-------------------------|
| | $3\frac{1}{2}'' \times 2\frac{1}{2}''$ | | | | | |
| | $\frac{1}{4}''$ | $\frac{5}{16}''$ | $\frac{3}{8}''$ | $\frac{7}{16}''$ | $\frac{1}{2}''$ | $\frac{9}{16}''$ |
| | 4.9 lbs. per ft. | 6.1 lbs. per ft. | 7.2 lbs. per ft. | 8.3 lbs. per ft. | 9.4 lbs. per ft. | 10.4 lbs. per ft. |
| 2 | 2200 | 2690 | 3160 | 3610 | 4050 | 4480 |
| 3 | 1460 | 1790 | 2110 | 2410 | 2700 | 2990 |
| 4 | 1100 | 1340 | 1580 | 1810 | 2030 | 2240 |
| 5 | 880 | 1080 | 1260 | 1450 | 1620 | 1790 |
| 6 | 730 | 900 | 1050 | 1200 | 1350 | 1490 |
| 7 | 630 | 770 | 900 | 1030 | 1160 | 1280 |
| 8 | 550 | 670 | 790 | 900 | 1010 | 1120 |
| 9 | 490 | 600 | 700 | 800 | 900 | 1000 |
| 10 | 440 | 540 | 630 | 720 | 810 | 900 |
| 11 | 400 | 490 | 570 | 660 | 740 | 810 |
| 12 | 370 | 450 | 530 | 600 | 680 | 750 |

| Distance between supports in feet. | Section No. A 97. | | | | | | | | | | |
|---|-----------------------------|------------------------|------------------------|------------------------|-------------------------|-------------------------|-------------------------|-------------------------|-------------------------|-------------------------|-------------------------|
| | $3\frac{1}{2}'' \times 3''$ | | | | | | | | | | |
| | $\frac{1}{4}''$ | $\frac{5}{16}''$ | $\frac{3}{8}''$ | $\frac{7}{16}''$ | $\frac{1}{2}''$ | $\frac{9}{16}''$ | $\frac{5}{8}''$ | $\frac{11}{16}''$ | $\frac{3}{4}''$ | $\frac{13}{16}''$ | $\frac{7}{8}''$ |
| | 5.4 lbs. per ft. | 6.6 lbs. per ft. | 7.9 lbs. per ft. | 9.1 lbs. per ft. | 10.2 lbs. per ft. | 11.4 lbs. per ft. | 12.5 lbs. per ft. | 13.6 lbs. per ft. | 14.7 lbs. per ft. | 15.8 lbs. per ft. | 16.8 lbs. per ft. |
| 2 | 4160 | 3850 | 4540 | 5200 | 5840 | 6460 | 7070 | 7660 | 8230 | 8790 | 9350 |
| 3 | 2770 | 2570 | 3030 | 3470 | 3900 | 4310 | 4710 | 5110 | 5490 | 5860 | 6230 |
| 4 | 2080 | 1930 | 2270 | 2600 | 2920 | 3230 | 3530 | 3830 | 4120 | 4400 | 4670 |
| 5 | 1660 | 1540 | 1820 | 2090 | 2340 | 2590 | 2830 | 3060 | 3290 | 3520 | 3740 |
| 6 | 1390 | 1280 | 1510 | 1730 | 1950 | 2150 | 2360 | 2550 | 2740 | 2930 | 3120 |
| 7 | 1190 | 1100 | 1300 | 1490 | 1670 | 1850 | 2020 | 2190 | 2350 | 2510 | 2670 |
| 8 | 1040 | 960 | 1130 | 1300 | 1460 | 1620 | 1770 | 1910 | 2060 | 2200 | 2340 |
| 9 | 920 | 860 | 1010 | 1160 | 1300 | 1440 | 1570 | 1700 | 1830 | 1950 | 2080 |
| 10 | 830 | 770 | 910 | 1040 | 1170 | 1290 | 1410 | 1530 | 1650 | 1760 | 1870 |
| 11 | 750 | 700 | 830 | 950 | 1060 | 1180 | 1290 | 1390 | 1500 | 1600 | 1700 |
| 12 | 690 | 640 | 760 | 870 | 970 | 1080 | 1180 | 1280 | 1370 | 1470 | 1560 |
| 13 | 640 | 590 | 700 | 800 | 900 | 990 | 1090 | 1180 | 1270 | 1350 | 1440 |
| 14 | 590 | 550 | 650 | 740 | 830 | 920 | 1010 | 1090 | 1180 | 1260 | 1340 |

For safe loads below heavy lines the deflections will be greater than the allowable limit for plastered ceilings = $\frac{1}{360}$ span.

SAFE LOADS IN POUNDS UNIFORMLY DISTRIBUTED FOR CAMBRIA ANGLES.

UNEQUAL LEGS.

NEUTRAL AXIS PARALLEL TO LONG LEG.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.



| Distance between supports in feet. | Section No. A 99. | | | | | | | | | |
|---|------------------------|------------------------|------------------------|-------------------------|-------------------------|-------------------------|-------------------------|-------------------------|-------------------------|-------------------------|
| | 4" x 3" | | | | | | | | | |
| | $\frac{5}{16}$ " | $\frac{3}{8}$ " | $\frac{7}{16}$ " | $\frac{1}{2}$ " | $\frac{9}{16}$ " | $\frac{5}{8}$ " | $\frac{11}{16}$ " | $\frac{3}{4}$ " | $\frac{13}{16}$ " | $\frac{7}{8}$ " |
| | 7.2 lbs. per ft. | 8.5 lbs. per ft. | 9.8 lbs. per ft. | 11.1 lbs. per ft. | 12.4 lbs. per ft. | 13.6 lbs. per ft. | 14.8 lbs. per ft. | 16.0 lbs. per ft. | 17.1 lbs. per ft. | 18.3 lbs. per ft. |
| 2 | 3920 | 4620 | 5290 | 5950 | 6580 | 7200 | 7810 | 8400 | 8980 | 9550 |
| 3 | 2610 | 3080 | 3530 | 3960 | 4390 | 4800 | 5200 | 5600 | 5980 | 6360 |
| 4 | 1960 | 2310 | 2650 | 2970 | 3290 | 3600 | 3900 | 4200 | 4490 | 4770 |
| 5 | 1570 | 1850 | 2120 | 2380 | 2630 | 2880 | 3120 | 3360 | 3590 | 3820 |
| 6 | 1310 | 1540 | 1760 | 1980 | 2190 | 2400 | 2600 | 2800 | 2990 | 3180 |
| 7 | 1120 | 1320 | 1510 | 1700 | 1880 | 2060 | 2230 | 2400 | 2560 | 2730 |
| 8 | 980 | 1150 | 1320 | 1490 | 1650 | 1800 | 1950 | 2100 | 2240 | 2390 |
| 9 | 870 | 1030 | 1180 | 1320 | 1460 | 1600 | 1730 | 1870 | 1990 | 2120 |
| 10 | 780 | 920 | 1060 | 1190 | 1320 | 1440 | 1560 | 1680 | 1800 | 1910 |
| 11 | 710 | 840 | 960 | 1080 | 1200 | 1310 | 1420 | 1530 | 1630 | 1740 |
| 12 | 650 | 770 | 880 | 990 | 1100 | 1200 | 1300 | 1400 | 1500 | 1590 |
| 13 | 600 | 710 | 810 | 910 | 1010 | 1110 | 1200 | 1290 | 1380 | 1470 |
| 14 | 560 | 660 | 760 | 850 | 940 | 1030 | 1120 | 1200 | 1280 | 1360 |

| Distance between supports in feet. | Section No. A 131. | | | | | | |
|---|---------------------|---------------------|----------------------|----------------------|----------------------|----------------------|----------------------|
| | 4" x 3½" | | | | | | |
| | $\frac{5}{16}$ " | $\frac{3}{8}$ " | $\frac{7}{16}$ " | $\frac{1}{2}$ " | $\frac{9}{16}$ " | $\frac{5}{8}$ " | $\frac{11}{16}$ " |
| | 7.7 lbs. per ft. | 9.1 lbs. per ft. | 10.6 lbs. per ft. | 11.9 lbs. per ft. | 13.3 lbs. per ft. | 14.7 lbs. per ft. | 16.0 lbs. per ft. |
| 2 | 5300 | 6260 | 7190 | 8090 | 8970 | 9760 | 10650 |
| 3 | 3530 | 4170 | 4790 | 5390 | 5980 | 6510 | 7100 |
| 4 | 2650 | 3130 | 3590 | 4040 | 4480 | 4880 | 5320 |
| 5 | 2120 | 2500 | 2870 | 3240 | 3590 | 3900 | 4260 |
| 6 | 1770 | 2090 | 2400 | 2700 | 2990 | 3250 | 3550 |
| 7 | 1510 | 1790 | 2050 | 2310 | 2560 | 2790 | 3040 |
| 8 | 1320 | 1560 | 1800 | 2020 | 2240 | 2440 | 2660 |
| 9 | 1180 | 1390 | 1600 | 1800 | 1990 | 2170 | 2370 |
| 10 | 1060 | 1250 | 1440 | 1620 | 1790 | 1950 | 2130 |
| 11 | 960 | 1140 | 1310 | 1470 | 1630 | 1770 | 1940 |
| 12 | 880 | 1040 | 1200 | 1350 | 1490 | 1630 | 1770 |
| 13 | 820 | 960 | 1110 | 1240 | 1380 | 1500 | 1640 |
| 14 | 760 | 890 | 1030 | 1160 | 1280 | 1390 | 1520 |

For safe loads below heavy lines the deflections will be greater than the allowable limit for plastered ceilings = $\frac{1}{360}$ span.

SAFE LOADS IN POUNDS UNIFORMLY DISTRIBUTED FOR CAMBRIA ANGLES.

UNEQUAL LEGS.

NEUTRAL AXIS PARALLEL TO LONG LEG.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.



Section No. A 101.

5" x 3"

Distance
between
supports
in feet.

| | $\frac{5}{16}$ " | $\frac{3}{8}$ " | $\frac{7}{16}$ " | $\frac{1}{2}$ " | $\frac{9}{16}$ " | $\frac{5}{8}$ " | $\frac{11}{16}$ " | $\frac{3}{4}$ " | $\frac{13}{16}$ " | $\frac{7}{8}$ " |
|----|------------------------|------------------------|-------------------------|-------------------------|-------------------------|-------------------------|-------------------------|-------------------------|-------------------------|-------------------------|
| | 8.2 lbs. per ft. | 9.8 lbs. per ft. | 11.3 lbs. per ft. | 12.8 lbs. per ft. | 14.3 lbs. per ft. | 15.7 lbs. per ft. | 17.1 lbs. per ft. | 18.5 lbs. per ft. | 19.9 lbs. per ft. | 21.2 lbs. per ft. |
| 2 | 4020 | 4740 | 5430 | 6110 | 6770 | 7410 | 8040 | 8660 | 9270 | 9870 |
| 3 | 2680 | 3160 | 3620 | 4070 | 4510 | 4940 | 5360 | 5770 | 6180 | 6580 |
| 4 | 2010 | 2370 | 2720 | 3060 | 3380 | 3710 | 4020 | 4330 | 4630 | 4940 |
| 5 | 1610 | 1900 | 2170 | 2440 | 2710 | 2960 | 3220 | 3460 | 3710 | 3950 |
| 6 | 1340 | 1580 | 1810 | 2040 | 2260 | 2470 | 2680 | 2890 | 3090 | 3290 |
| 7 | 1150 | 1350 | 1550 | 1750 | 1930 | 2120 | 2300 | 2470 | 2650 | 2820 |
| 8 | 1000 | 1180 | 1360 | 1530 | 1690 | 1850 | 2010 | 2160 | 2320 | 2470 |
| 9 | 890 | 1050 | 1210 | 1360 | 1500 | 1650 | 1790 | 1920 | 2060 | 2190 |
| 10 | 800 | 950 | 1090 | 1220 | 1350 | 1480 | 1610 | 1730 | 1850 | 1970 |
| 11 | 730 | 860 | 990 | 1110 | 1230 | 1350 | 1460 | 1570 | 1690 | 1790 |
| 12 | 670 | 790 | 910 | 1020 | 1130 | 1240 | 1340 | 1440 | 1540 | 1650 |
| 13 | 620 | 730 | 840 | 940 | 1040 | 1140 | 1240 | 1330 | 1430 | 1520 |
| 14 | 570 | 680 | 780 | 870 | 970 | 1060 | 1150 | 1240 | 1320 | 1410 |

Section No. A 103.

5" x 3½"

Distance
between
sup-
ports
in feet.

| | $\frac{5}{16}$ " | $\frac{3}{8}$ " | $\frac{7}{16}$ " | $\frac{1}{2}$ " | $\frac{9}{16}$ " | $\frac{5}{8}$ " | $\frac{11}{16}$ " | $\frac{3}{4}$ " | $\frac{13}{16}$ " | $\frac{7}{8}$ " | $\frac{15}{16}$ " |
|----|------------------------|-------------------------|-------------------------|-------------------------|-------------------------|-------------------------|-------------------------|-------------------------|-------------------------|-------------------------|-------------------------|
| | 8.7 lbs. per ft. | 10.4 lbs. per ft. | 12.0 lbs. per ft. | 13.6 lbs. per ft. | 15.2 lbs. per ft. | 16.8 lbs. per ft. | 18.3 lbs. per ft. | 19.8 lbs. per ft. | 21.3 lbs. per ft. | 22.7 lbs. per ft. | 24.2 lbs. per ft. |
| 2 | 5450 | 6430 | 7400 | 8320 | 9230 | 10110 | 10980 | 11820 | 12650 | 13450 | 14270 |
| 3 | 3630 | 4290 | 4930 | 5550 | 6150 | 6740 | 7320 | 7880 | 8430 | 8970 | 9510 |
| 4 | 2720 | 3220 | 3700 | 4160 | 4610 | 5060 | 5490 | 5910 | 6330 | 6730 | 7130 |
| 5 | 2180 | 2570 | 2960 | 3330 | 3690 | 4050 | 4390 | 4730 | 5060 | 5380 | 5710 |
| 6 | 1820 | 2140 | 2470 | 2770 | 3080 | 3370 | 3660 | 3940 | 4220 | 4490 | 4760 |
| 7 | 1560 | 1840 | 2110 | 2380 | 2640 | 2890 | 3140 | 3380 | 3610 | 3850 | 4080 |
| 8 | 1360 | 1610 | 1850 | 2080 | 2310 | 2530 | 2740 | 2960 | 3160 | 3370 | 3570 |
| 9 | 1210 | 1430 | 1640 | 1850 | 2050 | 2250 | 2440 | 2630 | 2810 | 2990 | 3170 |
| 10 | 1090 | 1290 | 1480 | 1660 | 1850 | 2020 | 2200 | 2360 | 2530 | 2690 | 2850 |
| 11 | 990 | 1170 | 1340 | 1510 | 1680 | 1840 | 2000 | 2150 | 2300 | 2450 | 2590 |
| 12 | 910 | 1070 | 1230 | 1390 | 1540 | 1690 | 1830 | 1970 | 2110 | 2240 | 2380 |
| 13 | 840 | 990 | 1140 | 1280 | 1420 | 1560 | 1690 | 1820 | 1950 | 2070 | 2190 |
| 14 | 780 | 920 | 1060 | 1190 | 1320 | 1440 | 1570 | 1690 | 1810 | 1920 | 2040 |

For safe loads below heavy lines the deflections will be greater than the allowable limit for plastered ceilings = $\frac{1}{360}$ span.

SAFE LOADS IN POUNDS UNIFORMLY DISTRIBUTED FOR CAMBRIA ANGLES.

UNEQUAL LEGS.

NEUTRAL AXIS PARALLEL TO LONG LEG.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.



| Distance between supports in feet. | Section No. A 135. | | | | | |
|------------------------------------|--------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| | 5" x 4" | | | | | |
| | $\frac{3}{8}$ " | $\frac{7}{16}$ " | $\frac{1}{2}$ " | $\frac{9}{16}$ " | $\frac{5}{8}$ " | $\frac{11}{16}$ " |
| | 11.0 lbs. per ft. | 12.8 lbs. per ft. | 14.5 lbs. per ft. | 16.2 lbs. per ft. | 17.8 lbs. per ft. | 19.5 lbs. per ft. |
| 2 | 8370 | 9630 | 10860 | 12050 | 13220 | 14360 |
| 3 | 5580 | 6420 | 7240 | 8030 | 8810 | 9570 |
| 4 | 4180 | 4810 | 5430 | 6030 | 6610 | 7180 |
| 5 | 3350 | 3850 | 4340 | 4820 | 5290 | 5740 |
| 6 | 2790 | 3210 | 3620 | 4020 | 4410 | 4790 |
| 7 | 2390 | 2750 | 3100 | 3440 | 3780 | 4100 |
| 8 | 2090 | 2410 | 2710 | 3010 | 3300 | 3590 |
| 9 | 1860 | 2140 | 2410 | 2680 | 2940 | 3190 |
| 10 | 1670 | 1930 | 2170 | 2410 | 2640 | 2870 |
| 11 | 1520 | 1750 | 1970 | 2190 | 2400 | 2610 |
| 12 | 1390 | 1600 | 1810 | 2010 | 2200 | 2390 |
| 13 | 1290 | 1480 | 1670 | 1850 | 2030 | 2210 |
| 14 | 1200 | 1380 | 1550 | 1720 | 1890 | 2050 |
| 15 | 1120 | 1280 | 1450 | 1610 | 1760 | 1910 |
| 16 | 1050 | 1200 | 1360 | 1510 | 1650 | 1790 |

| Distance between supports in feet. | Section No. A 105. | | | | | | | | | | |
|------------------------------------|--------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| | 6" x 3½" | | | | | | | | | | |
| | $\frac{3}{8}$ " | $\frac{7}{16}$ " | $\frac{1}{2}$ " | $\frac{9}{16}$ " | $\frac{5}{8}$ " | $\frac{11}{16}$ " | $\frac{3}{4}$ " | $\frac{13}{16}$ " | $\frac{7}{8}$ " | $\frac{15}{16}$ " | 1" |
| | 11.7 lbs. per ft. | 13.5 lbs. per ft. | 15.3 lbs. per ft. | 17.1 lbs. per ft. | 18.9 lbs. per ft. | 20.6 lbs. per ft. | 22.4 lbs. per ft. | 24.0 lbs. per ft. | 25.7 lbs. per ft. | 27.3 lbs. per ft. | 28.9 lbs. per ft. |
| 2 | 6570 | 7550 | 8500 | 9430 | 10340 | 11230 | 12100 | 12960 | 13800 | 14640 | 15470 |
| 3 | 4380 | 5030 | 5670 | 6290 | 6890 | 7480 | 8070 | 8640 | 9200 | 9760 | 10310 |
| 4 | 3280 | 3770 | 4250 | 4720 | 5170 | 5610 | 6050 | 6480 | 6900 | 7320 | 7730 |
| 5 | 2630 | 3020 | 3400 | 3770 | 4140 | 4490 | 4840 | 5180 | 5520 | 5850 | 6190 |
| 6 | 2190 | 2520 | 2830 | 3140 | 3450 | 3740 | 4030 | 4320 | 4600 | 4880 | 5160 |
| 7 | 1880 | 2160 | 2430 | 2690 | 2950 | 3210 | 3460 | 3700 | 3940 | 4180 | 4420 |
| 8 | 1640 | 1890 | 2120 | 2360 | 2580 | 2810 | 3020 | 3240 | 3450 | 3660 | 3870 |
| 9 | 1460 | 1680 | 1890 | 2100 | 2300 | 2490 | 2690 | 2880 | 3070 | 3250 | 3440 |
| 10 | 1310 | 1510 | 1700 | 1890 | 2070 | 2250 | 2420 | 2590 | 2760 | 2930 | 3090 |
| 11 | 1190 | 1370 | 1550 | 1710 | 1880 | 2040 | 2200 | 2360 | 2510 | 2660 | 2810 |
| 12 | 1090 | 1260 | 1420 | 1570 | 1720 | 1870 | 2020 | 2160 | 2300 | 2440 | 2580 |
| 13 | 1010 | 1160 | 1310 | 1450 | 1590 | 1730 | 1860 | 1990 | 2120 | 2250 | 2380 |
| 14 | 940 | 1080 | 1210 | 1350 | 1480 | 1600 | 1730 | 1850 | 1970 | 2090 | 2210 |

For safe loads below heavy lines the deflections will be greater than the allowable limit for plastered ceilings = $\frac{1}{360}$ span.

SAFE LOADS IN POUNDS UNIFORMLY DISTRIBUTED FOR CAMBRIA ANGLES.

UNEQUAL LEGS.

NEUTRAL AXIS PARALLEL TO LONG LEG.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.



Section No. A 107.

| Distance between supports in feet. | 6" x 4" | | | | | | | | | | |
|------------------------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| | 3" | 7" | 1" | 9" | 5" | 11" | 3" | 13" | 7" | 15" | 1" |
| | 12.3 lbs. per ft. | 14.3 lbs. per ft. | 16.2 lbs. per ft. | 18.1 lbs. per ft. | 20.0 lbs. per ft. | 21.8 lbs. per ft. | 23.6 lbs. per ft. | 25.4 lbs. per ft. | 27.2 lbs. per ft. | 28.9 lbs. per ft. | 30.6 lbs. per ft. |
| 2 | 8550 | 9840 | 11100 | 12320 | 13520 | 14690 | 15840 | 16970 | 18070 | 19160 | 20230 |
| 3 | 5700 | 6560 | 7400 | 8220 | 9020 | 9800 | 10560 | 11310 | 12050 | 12770 | 13490 |
| 4 | 4280 | 4920 | 5550 | 6160 | 6760 | 7350 | 7920 | 8480 | 9040 | 9580 | 10120 |
| 5 | 3420 | 3940 | 4440 | 4930 | 5410 | 5880 | 6340 | 6790 | 7230 | 7660 | 8090 |
| 6 | 2850 | 3280 | 3700 | 4110 | 4510 | 4900 | 5280 | 5660 | 6020 | 6390 | 6740 |
| 7 | 2440 | 2810 | 3170 | 3520 | 3860 | 4200 | 4530 | 4850 | 5160 | 5470 | 5780 |
| 8 | 2140 | 2460 | 2770 | 3080 | 3380 | 3670 | 3960 | 4240 | 4520 | 4790 | 5060 |
| 9 | 1900 | 2190 | 2470 | 2740 | 3010 | 3270 | 3520 | 3770 | 4020 | 4260 | 4500 |
| 10 | 1710 | 1970 | 2220 | 2460 | 2700 | 2940 | 3170 | 3390 | 3610 | 3830 | 4050 |
| 11 | 1550 | 1790 | 2020 | 2240 | 2460 | 2670 | 2880 | 3080 | 3290 | 3480 | 3680 |
| 12 | 1430 | 1640 | 1850 | 2050 | 2250 | 2450 | 2640 | 2830 | 3010 | 3190 | 3370 |
| 13 | 1320 | 1510 | 1710 | 1900 | 2080 | 2260 | 2440 | 2610 | 2780 | 2950 | 3110 |
| 14 | 1220 | 1410 | 1590 | 1760 | 1930 | 2100 | 2260 | 2420 | 2580 | 2740 | 2890 |
| 15 | 1140 | 1310 | 1480 | 1640 | 1800 | 1960 | 2110 | 2260 | 2410 | 2550 | 2700 |
| 16 | 1070 | 1230 | 1390 | 1540 | 1690 | 1840 | 1980 | 2120 | 2260 | 2400 | 2530 |

Section No. A 109.

| Distance between supports in feet. | 7" x 3½" | | | | | | | | | |
|---|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|
| | 7" | 1' | 9" | 5" | 11" | 3' | 13" | 7' | 15" | 1' |
| | 15.0 | 17.0 | 19.1 | 21.0 | 23.0 | 24.9 | 26.8 | 28.7 | 30.5 | 32.3 |
| | lbs. per ft. | lbs. per ft. | lbs. per ft. | lbs. per ft. | lbs. per ft. | lbs. per ft. | lbs. per ft. | lbs. per ft. | lbs. per ft. | lbs. per ft. |
| 2 | 7670 | 8640 | 9590 | 10520 | 11430 | 12320 | 13210 | 14090 | 14950 | 15810 |
| 3 | 5110 | 5760 | 6390 | 7010 | 7620 | 8220 | 8810 | 9390 | 9960 | 10540 |
| 4 | 3840 | 4320 | 4790 | 5260 | 5710 | 6160 | 6600 | 7040 | 7470 | 7900 |
| 5 | 3070 | 3460 | 3840 | 4210 | 4570 | 4930 | 5280 | 5630 | 5980 | 6320 |
| 6 | 2560 | 2880 | 3200 | 3510 | 3810 | 4110 | 4400 | 4700 | 4980 | 5270 |
| 7 | 2190 | 2470 | 2740 | 3010 | 3270 | 3520 | 3770 | 4020 | 4270 | 4520 |
| 8 | 1920 | 2160 | 2400 | 2630 | 2860 | 3080 | 3300 | 3520 | 3740 | 3950 |
| 9 | 1700 | 1920 | 2130 | 2340 | 2540 | 2740 | 2940 | 3180 | 3320 | 3510 |
| 10 | 1530 | 1730 | 1920 | 2100 | 2290 | 2460 | 2640 | 2820 | 2990 | 3160 |
| 11 | 1390 | 1570 | 1740 | 1910 | 2080 | 2240 | 2400 | 2560 | 2720 | 2870 |
| 12 | 1280 | 1440 | 1600 | 1750 | 1900 | 2050 | 2200 | 2350 | 2490 | 2630 |
| 13 | 1180 | 1330 | 1480 | 1620 | 1760 | 1900 | 2030 | 2170 | 2300 | 2430 |
| 14 | 1100 | 1230 | 1370 | 1500 | 1630 | 1760 | 1890 | 2010 | 2140 | 2260 |
| 15 | 1020 | 1150 | 1280 | 1400 | 1520 | 1640 | 1760 | 1880 | 1990 | 2110 |
| 16 | 960 | 1080 | 1200 | 1320 | 1430 | 1540 | 1650 | 1760 | 1870 | 1980 |

For safe loads below heavy lines the deflections will be greater than the allowable limit for plastered ceilings = $\frac{1}{360}$ span.

SAFE LOADS IN POUNDS UNIFORMLY DISTRIBUTED FOR CAMBRIA ANGLES.

UNEQUAL LEGS.

NEUTRAL AXIS PARALLEL TO LONG LEG.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.



| Distance between supports in feet. | Section No. A 112. | | | | | | | | |
|---|-------------------------|-------------------------|-------------------------|-------------------------|-------------------------|-------------------------|-------------------------|-------------------------|-------------------------|
| | 8" x 6" | | | | | | | | |
| | $\frac{1}{2}$ " | $\frac{9}{16}$ " | $\frac{5}{8}$ " | $\frac{11}{16}$ " | $\frac{3}{4}$ " | $\frac{13}{16}$ " | $\frac{7}{8}$ " | $\frac{15}{16}$ " | 1" |
| | 23.0 lbs. per ft. | 25.7 lbs. per ft. | 28.5 lbs. per ft. | 31.2 lbs. per ft. | 33.8 lbs. per ft. | 36.5 lbs. per ft. | 39.1 lbs. per ft. | 41.7 lbs. per ft. | 44.2 lbs. per ft. |
| 4 | 12770 | 14230 | 15670 | 17080 | 18460 | 19830 | 21170 | 22490 | 23790 |
| 5 | 10210 | 11380 | 12530 | 13660 | 14770 | 15860 | 16930 | 17990 | 19030 |
| 6 | 8510 | 9480 | 10440 | 11380 | 12310 | 13220 | 14110 | 14990 | 15860 |
| 7 | 7290 | 8130 | 8950 | 9790 | 10550 | 11330 | 12090 | 12850 | 13590 |
| 8 | 6380 | 7110 | 7830 | 8540 | 9230 | 9910 | 10580 | 11240 | 11890 |
| 9 | 5670 | 6320 | 6960 | 7590 | 8200 | 8810 | 9400 | 9990 | 10570 |
| 10 | 5100 | 5690 | 6260 | 6830 | 7380 | 7930 | 8460 | 8990 | 9510 |
| 11 | 4640 | 5170 | 5690 | 6210 | 6710 | 7210 | 7690 | 8170 | 8650 |
| 12 | 4250 | 4740 | 5220 | 5690 | 6150 | 6610 | 7050 | 7490 | 7930 |
| 13 | 3920 | 4370 | 4820 | 5250 | 5680 | 6100 | 6510 | 6920 | 7320 |
| 14 | 3640 | 4060 | 4470 | 4880 | 5270 | 5660 | 6040 | 6420 | 6790 |
| 15 | 3400 | 3790 | 4170 | 4550 | 4920 | 5280 | 5640 | 5990 | 6340 |
| 16 | 3190 | 3550 | 3910 | 4270 | 4610 | 4950 | 5290 | 5620 | 5940 |
| 17 | 3000 | 3340 | 3680 | 4010 | 4340 | 4660 | 4980 | 5290 | 5590 |
| 18 | 2830 | 3160 | 3480 | 3790 | 4100 | 4400 | 4700 | 4990 | 5280 |
| 19 | 2680 | 2990 | 3290 | 3590 | 3880 | 4170 | 4450 | 4730 | 5000 |
| 20 | 2550 | 2840 | 3130 | 3410 | 3690 | 3960 | 4230 | 4490 | 4750 |
| 21 | 2430 | 2710 | 2980 | 3250 | 3510 | 3770 | 4030 | 4280 | 4530 |
| 22 | 2320 | 2580 | 2840 | 3100 | 3350 | 3600 | 3840 | 4090 | 4320 |
| 23 | 2220 | 2470 | 2720 | 2970 | 3210 | 3440 | 3680 | 3910 | 4130 |
| 24 | 2120 | 2370 | 2610 | 2840 | 3070 | 3300 | 3520 | 3740 | 3960 |

For safe loads below heavy lines the deflections will be greater than the allowable limit for plastered ceilings = $\frac{1}{360}$ span.

SAFE LOADS IN POUNDS UNIFORMLY DISTRIBUTED FOR CAMBRIA ANGLES.

UNEQUAL LEGS.

NEUTRAL AXIS PARALLEL TO SHORT LEG.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.



| Distance between supports in feet. | Section No. A 91. | | | | | |
|------------------------------------|-----------------------------|-------------------|------------------|------------------|------------------|------------------|
| | $2\frac{1}{2}'' \times 2''$ | | | | | |
| | $\frac{3}{16}''$ | $\frac{1}{4}''$ | $\frac{5}{16}''$ | $\frac{3}{8}''$ | $\frac{7}{16}''$ | $\frac{1}{2}''$ |
| | 2.75 lbs. per ft. | 3.62 lbs. per ft. | 4.5 lbs. per ft. | 5.3 lbs. per ft. | 6.1 lbs. per ft. | 6.8 lbs. per ft. |
| 2 | 1560 | 2030 | 2490 | 2920 | 3330 | 3730 |
| 3 | 1040 | 1360 | 1660 | 1940 | 2220 | 2480 |
| 4 | 780 | 1020 | 1240 | 1460 | 1660 | 1860 |
| 5 | 620 | 810 | 990 | 1170 | 1330 | 1490 |
| 6 | 520 | 680 | 830 | 970 | 1110 | 1240 |
| 7 | 450 | 580 | 710 | 830 | 950 | 1070 |
| 8 | 390 | 510 | 620 | 730 | 830 | 930 |
| 9 | 350 | 450 | 550 | 650 | 740 | 830 |
| 10 | 310 | 410 | 500 | 580 | 670 | 750 |
| 11 | 280 | 370 | 450 | 530 | 610 | 680 |
| 12 | 260 | 340 | 410 | 490 | 560 | 620 |

| Distance between supports in feet. | Section No. A 129. | | | | | |
|------------------------------------|--------------------|------------------|------------------|------------------|------------------|------------------|
| | $3'' \times 2''$ | | | | | |
| | $\frac{3}{16}''$ | $\frac{1}{4}''$ | $\frac{5}{16}''$ | $\frac{3}{8}''$ | $\frac{7}{16}''$ | $\frac{1}{2}''$ |
| | 3.07 lbs. per ft. | 4.1 lbs. per ft. | 5.0 lbs. per ft. | 5.9 lbs. per ft. | 6.8 lbs. per ft. | 7.7 lbs. per ft. |
| 2 | 2210 | 2890 | 3540 | 4170 | 4770 | 5350 |
| 3 | 1470 | 1930 | 2360 | 2780 | 3180 | 3570 |
| 4 | 1110 | 1440 | 1770 | 2080 | 2380 | 2670 |
| 5 | 880 | 1160 | 1420 | 1670 | 1910 | 2140 |
| 6 | 740 | 960 | 1180 | 1390 | 1590 | 1780 |
| 7 | 630 | 830 | 1010 | 1190 | 1360 | 1530 |
| 8 | 550 | 720 | 890 | 1040 | 1190 | 1340 |
| 9 | 490 | 640 | 790 | 930 | 1060 | 1190 |
| 10 | 440 | 580 | 710 | 830 | 950 | 1070 |
| 11 | 400 | 530 | 640 | 760 | 870 | 970 |
| 12 | 370 | 480 | 590 | 690 | 800 | 890 |

For safe loads below heavy lines the deflections will be greater than the allowable limit for plastered ceilings = $\frac{1}{325}$ span.

SAFE LOADS IN POUNDS UNIFORMLY DISTRIBUTED FOR CAMBRIA ANGLES.

UNEQUAL LEGS.

NEUTRAL AXIS PARALLEL TO SHORT LEG.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.



| Distance between supports in feet. | Section No. A 93. | | | | | |
|------------------------------------|----------------------------|----------------------------|----------------------------|----------------------------|----------------------------|---------------------------------|
| | 3'' x 2½'' | | | | | |
| | ¼'' 4.5 lbs. per ft. | ⅝'' 5.6 lbs. per ft. | ¾'' 6.6 lbs. per ft. | ⅞'' 7.6 lbs. per ft. | 1'' 8.5 lbs. per ft. | 1 1/16'' 9.5 lbs. per ft. |
| 2 | 2990 | 3670 | 4320 | 4950 | 5560 | 6140 |
| 3 | 2000 | 2450 | 2880 | 3300 | 3700 | 4090 |
| 4 | 1500 | 1840 | 2160 | 2470 | 2780 | 3070 |
| 5 | 1200 | 1470 | 1730 | 1980 | 2220 | 2460 |
| 6 | 1000 | 1220 | 1440 | 1650 | 1850 | 2050 |
| 7 | 860 | 1050 | 1230 | 1410 | 1590 | 1760 |
| 8 | 750 | 920 | 1080 | 1240 | 1390 | 1540 |
| 9 | 670 | 820 | 960 | 1100 | 1230 | 1360 |
| 10 | 600 | 730 | 860 | 990 | 1110 | 1230 |
| 11 | 540 | 670 | 790 | 900 | 1010 | 1120 |
| 12 | 500 | 610 | 720 | 820 | 930 | 1020 |
| 13 | 460 | 560 | 660 | 760 | 850 | 940 |
| 14 | 430 | 520 | 620 | 710 | 790 | 880 |

| Distance between supports in feet | Section No. A 95. | | | | | |
|-----------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------------|
| | 3½'' x 2½'' | | | | | |
| | ¼'' 4.9 lbs. per ft. | ⅝'' 6.1 lbs. per ft. | ¾'' 7.2 lbs. per ft. | ⅞'' 8.3 lbs. per ft. | 1'' 9.4 lbs. per ft. | 1 1/16'' 10.4 lbs. per ft. |
| 2 | 4020 | 4940 | 5830 | 6690 | 7530 | 8330 |
| 3 | 2680 | 3300 | 3890 | 4460 | 5020 | 5560 |
| 4 | 2010 | 2470 | 2920 | 3350 | 3760 | 4170 |
| 5 | 1610 | 1980 | 2330 | 2680 | 3010 | 3330 |
| 6 | 1340 | 1650 | 1940 | 2230 | 2510 | 2780 |
| 7 | 1150 | 1410 | 1670 | 1910 | 2150 | 2380 |
| 8 | 1010 | 1240 | 1460 | 1670 | 1880 | 2080 |
| 9 | 890 | 1100 | 1300 | 1490 | 1670 | 1850 |
| 10 | 800 | 990 | 1170 | 1340 | 1510 | 1670 |
| 11 | 730 | 900 | 1060 | 1220 | 1370 | 1520 |
| 12 | 670 | 820 | 970 | 1120 | 1250 | 1390 |
| 13 | 620 | 760 | 900 | 1030 | 1160 | 1280 |
| 14 | 570 | 710 | 830 | 960 | 1080 | 1190 |
| 15 | 540 | 660 | 780 | 890 | 1000 | 1110 |
| 16 | 500 | 620 | 730 | 840 | 940 | 1040 |

For safe loads below the heavy lines, the deflections will be greater than the allowable limit for plastered ceilings = $\frac{1}{330}$ span.

SAFE LOADS IN POUNDS UNIFORMLY DISTRIBUTED FOR CAMBRIA ANGLES.

UNEQUAL LEGS.

NEUTRAL AXIS PARALLEL TO SHORT LEG.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.



Section No. A 97.

| Distance between supports in feet. | $3\frac{1}{2}'' \times 3''$ | | | | | | | | | |
|------------------------------------|-----------------------------|------------------|------------------|------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| | $\frac{1}{4}''$ | $\frac{5}{16}''$ | $\frac{3}{8}''$ | $\frac{7}{16}''$ | $\frac{1}{2}''$ | $\frac{9}{16}''$ | $\frac{5}{8}''$ | $\frac{11}{16}''$ | $\frac{3}{4}''$ | $\frac{13}{16}''$ |
| | 5.4 lbs. per ft. | 6.6 lbs. per ft. | 7.9 lbs. per ft. | 9.1 lbs. per ft. | 10.2 lbs. per ft. | 11.4 lbs. per ft. | 12.5 lbs. per ft. | 13.6 lbs. per ft. | 14.7 lbs. per ft. | 15.8 lbs. per ft. |
| 2 | 3090 | 5090 | 6010 | 6890 | 7750 | 8590 | 9400 | 10190 | 10960 | 11710 |
| 3 | 2060 | 3390 | 4000 | 4600 | 5170 | 5730 | 6270 | 6790 | 7300 | 7800 |
| 4 | 1550 | 2540 | 3000 | 3450 | 3880 | 4290 | 4700 | 5090 | 5480 | 5850 |
| 5 | 1240 | 2040 | 2400 | 2760 | 3100 | 3440 | 3760 | 4080 | 4380 | 4680 |
| 6 | 1030 | 1700 | 2000 | 2300 | 2580 | 2860 | 3130 | 3400 | 3650 | 3900 |
| 7 | 880 | 1450 | 1720 | 1970 | 2220 | 2450 | 2690 | 2910 | 3130 | 3340 |
| 8 | 770 | 1270 | 1500 | 1720 | 1940 | 2150 | 2350 | 2550 | 2740 | 2930 |
| 9 | 690 | 1130 | 1330 | 1530 | 1720 | 1910 | 2090 | 2260 | 2430 | 2600 |
| 10 | 620 | 1020 | 1200 | 1380 | 1550 | 1720 | 1880 | 2040 | 2190 | 2340 |
| 11 | 560 | 930 | 1090 | 1250 | 1410 | 1560 | 1710 | 1850 | 1990 | 2130 |
| 12 | 520 | 850 | 1000 | 1150 | 1290 | 1430 | 1570 | 1700 | 1830 | 1950 |
| 13 | 480 | 780 | 920 | 1060 | 1190 | 1320 | 1450 | 1570 | 1690 | 1800 |
| 14 | 440 | 730 | 860 | 980 | 1110 | 1230 | 1340 | 1460 | 1570 | 1670 |
| 15 | 410 | 680 | 800 | 920 | 1030 | 1150 | 1250 | 1360 | 1460 | 1560 |
| 16 | 390 | 640 | 750 | 860 | 970 | 1070 | 1180 | 1270 | 1370 | 1460 |

Section No. A 99.

| Distance between supports in feet. | $4'' \times 3''$ | | | | | | | | | |
|------------------------------------|------------------|------------------|------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| | $\frac{5}{16}''$ | $\frac{3}{8}''$ | $\frac{7}{16}''$ | $\frac{1}{2}''$ | $\frac{9}{16}''$ | $\frac{5}{8}''$ | $\frac{11}{16}''$ | $\frac{3}{4}''$ | $\frac{13}{16}''$ | $\frac{7}{8}''$ |
| | 7.2 lbs. per ft. | 8.5 lbs. per ft. | 9.8 lbs. per ft. | 11.1 lbs. per ft. | 12.4 lbs. per ft. | 13.6 lbs. per ft. | 14.8 lbs. per ft. | 16.0 lbs. per ft. | 17.1 lbs. per ft. | 18.3 lbs. per ft. |
| 2 | 6580 | 7780 | 8940 | 10070 | 11170 | 12240 | 13280 | 14300 | 15290 | 16260 |
| 3 | 4390 | 5180 | 5960 | 6710 | 7450 | 8160 | 8860 | 9530 | 10190 | 10840 |
| 4 | 3290 | 3890 | 4470 | 5040 | 5590 | 6120 | 6640 | 7150 | 7650 | 8130 |
| 5 | 2630 | 3110 | 3580 | 4030 | 4470 | 4900 | 5310 | 5720 | 6120 | 6500 |
| 6 | 2190 | 2590 | 2980 | 3360 | 3720 | 4080 | 4430 | 4770 | 5100 | 5420 |
| 7 | 1880 | 2220 | 2550 | 2880 | 3190 | 3500 | 3800 | 4090 | 4370 | 4650 |
| 8 | 1640 | 1940 | 2240 | 2520 | 2790 | 3060 | 3320 | 3580 | 3820 | 4060 |
| 9 | 1460 | 1730 | 1990 | 2240 | 2480 | 2720 | 2950 | 3180 | 3400 | 3610 |
| 10 | 1320 | 1560 | 1790 | 2010 | 2230 | 2450 | 2660 | 2860 | 3060 | 3250 |
| 11 | 1200 | 1410 | 1630 | 1830 | 2030 | 2230 | 2420 | 2600 | 2780 | 2960 |
| 12 | 1100 | 1300 | 1490 | 1680 | 1860 | 2040 | 2210 | 2380 | 2550 | 2710 |
| 13 | 1010 | 1200 | 1380 | 1550 | 1720 | 1880 | 2040 | 2200 | 2350 | 2500 |
| 14 | 940 | 1110 | 1280 | 1440 | 1600 | 1750 | 1900 | 2040 | 2180 | 2320 |
| 15 | 880 | 1040 | 1190 | 1340 | 1490 | 1630 | 1770 | 1910 | 2040 | 2170 |
| 16 | 820 | 970 | 1120 | 1260 | 1400 | 1530 | 1660 | 1790 | 1910 | 2030 |

For safe loads below heavy lines the deflections will be greater than the allowable limit for plastered ceilings = $\frac{1}{360}$ span.

SAFE LOADS IN POUNDS UNIFORMLY DISTRIBUTED FOR CAMBRIA ANGLES.

UNEQUAL LEGS.

NEUTRAL AXIS PARALLEL TO SHORT LEG.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.



| Distance between supports in feet. | Section No. A 131. | | | | | | |
|------------------------------------|------------------------------------|-----------------------------------|-------------------------------------|------------------------------------|-------------------------------------|------------------------------------|--------------------------------------|
| | 4" x 3½" | | | | | | |
| | 5" 16 7.7 lbs. per ft. | 3" 8 9.1 lbs. per ft. | 7" 16 10.6 lbs. per ft. | 1" 2 11.9 lbs. per ft. | 9" 16 13.3 lbs. per ft. | 5" 8 14.7 lbs. per ft. | 11" 16 16.0 lbs. per ft. |
| 2 | 6740 | 7970 | 9160 | 10320 | 11450 | 12550 | 13630 |
| 3 | 4490 | 5310 | 6110 | 6880 | 7640 | 8370 | 9080 |
| 4 | 3370 | 3980 | 4580 | 5160 | 5730 | 6280 | 6810 |
| 5 | 2690 | 3190 | 3660 | 4130 | 4580 | 5020 | 5450 |
| 6 | 2250 | 2660 | 3050 | 3440 | 3820 | 4180 | 4540 |
| 7 | 1920 | 2280 | 2620 | 2950 | 3270 | 3590 | 3890 |
| 8 | 1680 | 1990 | 2290 | 2580 | 2860 | 3140 | 3410 |
| 9 | 1500 | 1770 | 2040 | 2290 | 2550 | 2790 | 3030 |
| 10 | 1350 | 1590 | 1830 | 2060 | 2290 | 2510 | 2730 |
| 11 | 1220 | 1450 | 1670 | 1880 | 2080 | 2280 | 2480 |
| 12 | 1120 | 1330 | 1530 | 1720 | 1910 | 2090 | 2270 |
| 13 | 1040 | 1230 | 1410 | 1590 | 1760 | 1930 | 2100 |
| 14 | 960 | 1140 | 1310 | 1470 | 1640 | 1790 | 1950 |
| 15 | 900 | 1060 | 1220 | 1380 | 1530 | 1670 | 1820 |
| 16 | 840 | 1000 | 1150 | 1290 | 1430 | 1570 | 1700 |

| Distance between supports in feet. | Section No. A 101. | | | | | | | | | |
|------------------------------------|------------------------------------|-----------------------------------|-------------------------------------|------------------------------------|-------------------------------------|------------------------------------|--------------------------------------|------------------------------------|--------------------------------------|------------------------------------|
| | 5" x 3" | | | | | | | | | |
| | 5" 16 8.2 lbs. per ft. | 3" 8 9.8 lbs. per ft. | 7" 16 11.3 lbs. per ft. | 1" 2 12.8 lbs. per ft. | 9" 16 14.3 lbs. per ft. | 5" 8 15.7 lbs. per ft. | 11" 16 17.1 lbs. per ft. | 3" 4 18.5 lbs. per ft. | 13" 16 19.9 lbs. per ft. | 7" 8 21.2 lbs. per ft. |
| 2 | 10060 | 11920 | 13740 | 15510 | 17240 | 18930 | 20580 | 22190 | 23770 | 25310 |
| 3 | 6710 | 7950 | 9160 | 10340 | 11490 | 12620 | 13720 | 14790 | 15850 | 16870 |
| 4 | 5030 | 5960 | 6870 | 7760 | 8620 | 9470 | 10290 | 11100 | 11880 | 12660 |
| 5 | 4020 | 4770 | 5500 | 6210 | 6900 | 7570 | 8230 | 8880 | 9510 | 10120 |
| 6 | 3350 | 3970 | 4580 | 5170 | 5750 | 6310 | 6860 | 7400 | 7920 | 8440 |
| 7 | 2870 | 3410 | 3930 | 4430 | 4930 | 5410 | 5880 | 6340 | 6790 | 7230 |
| 8 | 2520 | 2980 | 3440 | 3880 | 4310 | 4730 | 5140 | 5550 | 5940 | 6330 |
| 9 | 2240 | 2650 | 3050 | 3450 | 3830 | 4210 | 4570 | 4930 | 5280 | 5620 |
| 10 | 2010 | 2380 | 2750 | 3100 | 3450 | 3790 | 4120 | 4440 | 4750 | 5060 |
| 11 | 1830 | 2170 | 2500 | 2820 | 3130 | 3440 | 3740 | 4030 | 4320 | 4600 |
| 12 | 1680 | 1990 | 2290 | 2590 | 2870 | 3160 | 3430 | 3700 | 3960 | 4220 |
| 13 | 1550 | 1830 | 2110 | 2390 | 2650 | 2910 | 3170 | 3410 | 3660 | 3890 |
| 14 | 1440 | 1700 | 1960 | 2220 | 2460 | 2700 | 2940 | 3170 | 3400 | 3620 |
| 15 | 1340 | 1590 | 1830 | 2070 | 2300 | 2520 | 2740 | 2960 | 3170 | 3370 |
| 16 | 1260 | 1490 | 1720 | 1940 | 2160 | 2370 | 2570 | 2770 | 2970 | 3160 |
| 17 | 1180 | 1400 | 1620 | 1830 | 2030 | 2230 | 2420 | 2610 | 2800 | 2980 |
| 18 | 1120 | 1330 | 1530 | 1720 | 1920 | 2100 | 2290 | 2470 | 2640 | 2810 |

For safe loads below heavy lines the deflections will be greater than the allowable limit for plastered ceilings = $\frac{1}{360}$ span.

SAFE LOADS IN POUNDS UNIFORMLY DISTRIBUTED FOR CAMBRIA ANGLES.

UNEQUAL LEGS.

NEUTRAL AXIS PARALLEL TO SHORT LEG.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.



| Distance between supports in feet. | Section No. A 103. | | | | | | | | | | |
|------------------------------------|--------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| | 5" x 3½" | | | | | | | | | | |
| | 5" | 3" | 7" | ½" | 9" | 5" | 11" | 3" | 13" | 7" | 15" |
| | 8.7 lbs. per ft. | 10.4 lbs. per ft. | 12.0 lbs. per ft. | 13.6 lbs. per ft. | 15.2 lbs. per ft. | 16.8 lbs. per ft. | 18.3 lbs. per ft. | 19.8 lbs. per ft. | 21.3 lbs. per ft. | 22.7 lbs. per ft. | 24.2 lbs. per ft. |
| 2 | 10320 | 12240 | 14100 | 15930 | 17710 | 19450 | 21150 | 22810 | 24440 | 26030 | 27590 |
| 3 | 6880 | 8160 | 9400 | 10620 | 11810 | 12970 | 14100 | 15210 | 16290 | 17350 | 18400 |
| 4 | 5160 | 6120 | 7050 | 7960 | 8850 | 9720 | 10570 | 11410 | 12220 | 13020 | 13800 |
| 5 | 4130 | 4890 | 5640 | 6370 | 7080 | 7780 | 8460 | 9120 | 9780 | 10410 | 11040 |
| 6 | 3440 | 4080 | 4700 | 5310 | 5900 | 6480 | 7050 | 7600 | 8150 | 8680 | 9200 |
| 7 | 2950 | 3500 | 4030 | 4550 | 5060 | 5560 | 6040 | 6520 | 6980 | 7440 | 7880 |
| 8 | 2580 | 3060 | 3530 | 3980 | 4430 | 4860 | 5290 | 5700 | 6110 | 6510 | 6900 |
| 9 | 2290 | 2720 | 3130 | 3540 | 3940 | 4320 | 4700 | 5070 | 5430 | 5780 | 6130 |
| 10 | 2060 | 2450 | 2820 | 3190 | 3540 | 3890 | 4230 | 4560 | 4890 | 5210 | 5520 |
| 11 | 1880 | 2220 | 2560 | 2900 | 3220 | 3540 | 3850 | 4150 | 4440 | 4730 | 5020 |
| 12 | 1720 | 2040 | 2350 | 2650 | 2950 | 3240 | 3520 | 3800 | 4070 | 4340 | 4600 |
| 13 | 1590 | 1880 | 2170 | 2450 | 2720 | 2990 | 3250 | 3510 | 3760 | 4000 | 4240 |
| 14 | 1470 | 1750 | 2010 | 2280 | 2530 | 2780 | 3020 | 3260 | 3490 | 3720 | 3940 |
| 15 | 1380 | 1630 | 1880 | 2120 | 2360 | 2590 | 2820 | 3040 | 3260 | 3470 | 3680 |
| 16 | 1290 | 1530 | 1760 | 1990 | 2210 | 2430 | 2640 | 2850 | 3050 | 3250 | 3450 |
| 17 | 1210 | 1440 | 1660 | 1870 | 2080 | 2290 | 2490 | 2680 | 2880 | 3060 | 3250 |
| 18 | 1150 | 1360 | 1570 | 1770 | 1970 | 2160 | 2350 | 2530 | 2720 | 2890 | 3070 |

| Distance between supports in feet. | Section No. A 135. | | | | | |
|------------------------------------|--------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| | 5" x 4" | | | | | |
| | 3" | 7" | ½" | 9" | 5" | 11" |
| | 11.0 lbs. per ft. | 12.8 lbs. per ft. | 14.5 lbs. per ft. | 16.2 lbs. per ft. | 17.8 lbs. per ft. | 19.5 lbs. per ft. |
| 2 | 12500 | 14410 | 16280 | 18100 | 19880 | 21620 |
| 3 | 8330 | 9610 | 10850 | 12070 | 13250 | 14420 |
| 4 | 6250 | 7200 | 8140 | 9050 | 9940 | 10810 |
| 5 | 5000 | 5760 | 6510 | 7240 | 7950 | 8650 |
| 6 | 4170 | 4800 | 5430 | 6030 | 6630 | 7210 |
| 7 | 3570 | 4120 | 4650 | 5170 | 5680 | 6180 |
| 8 | 3120 | 3600 | 4070 | 4520 | 4970 | 5410 |
| 9 | 2780 | 3200 | 3620 | 4020 | 4420 | 4810 |
| 10 | 2500 | 2880 | 3260 | 3620 | 3980 | 4320 |
| 11 | 2270 | 2620 | 2960 | 3290 | 3610 | 3930 |
| 12 | 2080 | 2400 | 2710 | 3020 | 3310 | 3600 |
| 13 | 1920 | 2220 | 2500 | 2780 | 3060 | 3330 |
| 14 | 1790 | 2060 | 2330 | 2590 | 2840 | 3090 |
| 15 | 1670 | 1920 | 2170 | 2410 | 2650 | 2880 |
| 16 | 1560 | 1800 | 2030 | 2260 | 2490 | 2700 |
| 17 | 1470 | 1700 | 1910 | 2130 | 2340 | 2540 |
| 18 | 1390 | 1600 | 1810 | 2010 | 2210 | 2400 |

For safe loads below heavy lines the deflections will be greater than the allowable limit for plastered ceilings = $\frac{1}{320}$ span.

SAFE LOADS IN POUNDS UNIFORMLY DISTRIBUTED FOR CAMBRIA ANGLES.

UNEQUAL LEGS.

NEUTRAL AXIS PARALLEL TO SHORT LEG.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.



| Distance between sup- ports in feet. | Section No. A 105. | | | | | | | | | | |
|--|-------------------------|-------------------------|-------------------------|-------------------------|-------------------------|-------------------------|-------------------------|-------------------------|-------------------------|-------------------------|-------------------------|
| | 6" x 3½" | | | | | | | | | | |
| | 3" 8 | 7" 16 | 1" 2 | 9" 16 | 5" 8 | 11" 16 | 3" 4 | 13" 16 | 7" 8 | 15" 16 | 1" |
| | 11.7 lbs. per ft. | 13.5 lbs. per ft. | 15.3 lbs. per ft. | 17.1 lbs. per ft. | 18.9 lbs. per ft. | 20.6 lbs. per ft. | 22.4 lbs. per ft. | 24.0 lbs. per ft. | 25.7 lbs. per ft. | 27.3 lbs. per ft. | 28.9 lbs. per ft. |
| 2 | 17300 | 19980 | 22600 | 25160 | 27670 | 30130 | 32550 | 34910 | 37230 | 39510 | 41630 |
| 3 | 11540 | 13320 | 15060 | 16770 | 18450 | 20090 | 21700 | 23270 | 24820 | 26340 | 27750 |
| 4 | 8650 | 9990 | 11300 | 12580 | 13840 | 15070 | 16270 | 17460 | 18620 | 19760 | 20810 |
| 5 | 6920 | 7990 | 9040 | 10060 | 11070 | 12050 | 13020 | 13960 | 14890 | 15800 | 16650 |
| 6 | 5770 | 6660 | 7530 | 8390 | 9220 | 10040 | 10850 | 11640 | 12410 | 13170 | 13880 |
| 7 | 4940 | 5710 | 6460 | 7190 | 7910 | 8610 | 9300 | 9970 | 10640 | 11290 | 11890 |
| 8 | 4330 | 4990 | 5650 | 6290 | 6920 | 7530 | 8140 | 8730 | 9310 | 9880 | 10410 |
| 9 | 3850 | 4440 | 5020 | 5590 | 6150 | 6700 | 7230 | 7760 | 8270 | 8780 | 9250 |
| 10 | 3460 | 4000 | 4520 | 5030 | 5530 | 6030 | 6510 | 6980 | 7450 | 7900 | 8330 |
| 11 | 3150 | 3630 | 4110 | 4570 | 5030 | 5480 | 5920 | 6350 | 6770 | 7180 | 7570 |
| 12 | 2880 | 3330 | 3770 | 4190 | 4610 | 5020 | 5420 | 5820 | 6210 | 6590 | 6940 |
| 13 | 2660 | 3070 | 3480 | 3870 | 4260 | 4640 | 5010 | 5370 | 5730 | 6080 | 6400 |
| 14 | 2470 | 2850 | 3230 | 3590 | 3950 | 4300 | 4650 | 4990 | 5320 | 5640 | 5950 |
| 15 | 2310 | 2660 | 3010 | 3350 | 3690 | 4020 | 4340 | 4650 | 4960 | 5270 | 5550 |
| 16 | 2160 | 2500 | 2820 | 3150 | 3460 | 3770 | 4070 | 4360 | 4650 | 4940 | 5200 |
| 17 | 2040 | 2350 | 2660 | 2960 | 3260 | 3550 | 3830 | 4110 | 4380 | 4650 | 4900 |
| 18 | 1920 | 2220 | 2510 | 2800 | 3070 | 3350 | 3620 | 3880 | 4140 | 4390 | 4630 |
| 19 | 1820 | 2100 | 2380 | 2650 | 2910 | 3170 | 3430 | 3680 | 3920 | 4160 | 4380 |
| 20 | 1730 | 2000 | 2260 | 2520 | 2770 | 3010 | 3250 | 3490 | 3720 | 3950 | 4160 |
| 21 | 1650 | 1900 | 2150 | 2400 | 2640 | 2870 | 3100 | 3320 | 3550 | 3760 | 3960 |
| 22 | 1570 | 1810 | 2050 | 2290 | 2520 | 2740 | 2960 | 3170 | 3380 | 3590 | 3780 |

For safe loads below heavy lines the deflections will be greater than the allowable limit for plastered ceilings = $\frac{1}{320}$ span.

SAFE LOADS IN POUNDS UNIFORMLY DISTRIBUTED FOR CAMBRIA ANGLES.

UNEQUAL LEGS.

NEUTRAL AXIS PARALLEL TO SHORT LEG.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.



| Section No. A 107. | | | | | | | | | | | |
|--|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|
| Distance between sup- ports in feet. | 6" x 4" | | | | | | | | | | |
| | 3" | 7" | 1" | 9" | 5" | 11" | 3" | 13" | 7" | 15" | 1" |
| | 12.3 | 14.3 | 16.2 | 18.1 | 20.0 | 21.8 | 23.6 | 25.4 | 27.2 | 28.9 | 30.6 |
| | lbs. per ft. | lbs. per ft. | lbs. per ft. | lbs. per ft. | lbs. per ft. | lbs. per ft. | lbs. per ft. | lbs. per ft. | lbs. per ft. | lbs. per ft. | lbs. per ft. |
| 2 | 17700 | 20430 | 23120 | 25750 | 28320 | 30850 | 33330 | 35760 | 38140 | 40480 | 42780 |
| 3 | 11800 | 13620 | 15410 | 17160 | 18880 | 20570 | 22220 | 23840 | 25430 | 26990 | 28520 |
| 4 | 8850 | 10230 | 11560 | 12870 | 14160 | 15420 | 16660 | 17880 | 19070 | 20240 | 21390 |
| 5 | 7080 | 8170 | 9250 | 10300 | 11330 | 12340 | 13330 | 14300 | 15260 | 16190 | 17110 |
| 6 | 5900 | 6810 | 7710 | 8580 | 9440 | 10280 | 11110 | 11920 | 12710 | 13490 | 14260 |
| 7 | 5060 | 5840 | 6600 | 7360 | 8090 | 8810 | 9520 | 10220 | 10900 | 11570 | 12220 |
| 8 | 4420 | 5110 | 5780 | 6440 | 7080 | 7710 | 8330 | 8940 | 9540 | 10120 | 10700 |
| 9 | 3930 | 4540 | 5140 | 5720 | 6290 | 6860 | 7410 | 7950 | 8480 | 9000 | 9510 |
| 10 | 3540 | 4090 | 4620 | 5150 | 5660 | 6170 | 6670 | 7150 | 7630 | 8100 | 8560 |
| 11 | 3220 | 3720 | 4200 | 4680 | 5150 | 5610 | 6060 | 6500 | 6930 | 7360 | 7780 |
| 12 | 2950 | 3410 | 3850 | 4290 | 4720 | 5140 | 5550 | 5960 | 6360 | 6750 | 7130 |
| 13 | 2720 | 3140 | 3560 | 3960 | 4360 | 4750 | 5130 | 5500 | 5870 | 6230 | 6580 |
| 14 | 2530 | 2920 | 3300 | 3680 | 4050 | 4410 | 4760 | 5110 | 5450 | 5780 | 6110 |
| 15 | 2360 | 2720 | 3080 | 3430 | 3780 | 4110 | 4440 | 4770 | 5090 | 5400 | 5700 |
| 16 | 2210 | 2550 | 2890 | 3220 | 3540 | 3860 | 4170 | 4470 | 4770 | 5060 | 5350 |
| 17 | 2080 | 2400 | 2720 | 3030 | 3330 | 3630 | 3920 | 4210 | 4490 | 4760 | 5030 |
| 18 | 1970 | 2270 | 2570 | 2860 | 3150 | 3430 | 3700 | 3970 | 4240 | 4500 | 4750 |
| 19 | 1860 | 2150 | 2430 | 2710 | 2980 | 3250 | 3510 | 3760 | 4020 | 4260 | 4500 |
| 20 | 1770 | 2040 | 2310 | 2570 | 2830 | 3080 | 3330 | 3580 | 3810 | 4050 | 4280 |
| 21 | 1690 | 1950 | 2200 | 2450 | 2700 | 2940 | 3170 | 3400 | 3630 | 3860 | 4070 |
| 22 | 1610 | 1860 | 2100 | 2340 | 2570 | 2800 | 3030 | 3250 | 3470 | 3680 | 3890 |

For safe loads below heavy lines the deflections will be greater than the allowable limit for plastered ceilings = $\frac{1}{325}$ span.

SAFE LOADS IN POUNDS UNIFORMLY DISTRIBUTED FOR CAMBRIA ANGLES.

UNEQUAL LEGS.

NEUTRAL AXIS PARALLEL TO SHORT LEG.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.



| Distance between supports in feet. | Section No. A 109. | | | | | | | | | |
|---|-------------------------|-------------------------|-------------------------|-------------------------|-------------------------|-------------------------|-------------------------|-------------------------|-------------------------|-------------------------|
| | 7" x 3½" | | | | | | | | | |
| | 7" | 1" | 9" | 5" | 11" | 3" | 13" | 7" | 15" | 1" |
| | 16 | 2 | 16 | 8 | 16 | 4 | 16 | 8 | 16 | |
| | 15.0 lbs. per ft. | 17.0 lbs. per ft. | 19.1 lbs. per ft. | 21.0 lbs. per ft. | 23.0 lbs. per ft. | 24.9 lbs. per ft. | 26.8 lbs. per ft. | 28.7 lbs. per ft. | 30.5 lbs. per ft. | 32.3 lbs. per ft. |
| 4 | 13360 | 15140 | 16900 | 18570 | 20260 | 21910 | 23530 | 25110 | 26670 | 28210 |
| 5 | 10690 | 12120 | 13520 | 14850 | 16210 | 17530 | 18830 | 20090 | 21340 | 22560 |
| 6 | 8910 | 10100 | 11270 | 12380 | 13510 | 14600 | 15690 | 16740 | 17780 | 18800 |
| 7 | 7640 | 8650 | 9660 | 10610 | 11580 | 12520 | 13450 | 14350 | 15240 | 16120 |
| 8 | 6680 | 7570 | 8450 | 9280 | 10130 | 10950 | 11770 | 12560 | 13340 | 14100 |
| 9 | 5940 | 6730 | 7510 | 8250 | 9010 | 9740 | 10460 | 11160 | 11850 | 12540 |
| 10 | 5340 | 6060 | 6760 | 7430 | 8100 | 8760 | 9410 | 10050 | 10670 | 11280 |
| 11 | 4860 | 5510 | 6150 | 6750 | 7370 | 7970 | 8560 | 9130 | 9700 | 10260 |
| 12 | 4450 | 5050 | 5630 | 6190 | 6750 | 7300 | 7840 | 8370 | 8890 | 9400 |
| 13 | 4110 | 4660 | 5200 | 5710 | 6230 | 6740 | 7240 | 7730 | 8210 | 8680 |
| 14 | 3820 | 4330 | 4830 | 5310 | 5790 | 6260 | 6720 | 7180 | 7620 | 8060 |
| 15 | 3560 | 4040 | 4510 | 4950 | 5400 | 5840 | 6280 | 6700 | 7110 | 7520 |
| 16 | 3340 | 3790 | 4230 | 4640 | 5070 | 5480 | 5880 | 6280 | 6670 | 7050 |
| 17 | 3140 | 3560 | 3980 | 4370 | 4770 | 5150 | 5540 | 5910 | 6280 | 6640 |
| 18 | 2970 | 3370 | 3760 | 4130 | 4500 | 4870 | 5230 | 5580 | 5930 | 6270 |
| 19 | 2810 | 3190 | 3560 | 3910 | 4270 | 4610 | 4950 | 5290 | 5620 | 5940 |
| 20 | 2670 | 3030 | 3380 | 3710 | 4050 | 4380 | 4710 | 5020 | 5330 | 5640 |
| 21 | 2550 | 2880 | 3220 | 3540 | 3860 | 4170 | 4480 | 4780 | 5080 | 5370 |
| 22 | 2430 | 2750 | 3070 | 3380 | 3680 | 3980 | 4280 | 4570 | 4850 | 5130 |
| 23 | 2320 | 2630 | 2940 | 3230 | 3520 | 3810 | 4090 | 4370 | 4640 | 4910 |
| 24 | 2230 | 2520 | 2820 | 3090 | 3380 | 3650 | 3920 | 4190 | 4450 | 4700 |

For safe loads below heavy lines the deflections will be greater than the allowable limit for plastered ceilings = $\frac{1}{360}$ span.

SAFE LOADS IN POUNDS UNIFORMLY DISTRIBUTED FOR CAMBRIA ANGLES.

UNEQUAL LEGS.

NEUTRAL AXIS PARALLEL TO SHORT LEG.



Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.

| | | Section No. A 112. | | | | | | | |
|------------------------------------|----|--------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| Distance between supports in feet. | | 8" x 6" | | | | | | | |
| | | 1" | 2" | 3" | 4" | 5" | 6" | 7" | 8" |
| | | 23.0 lbs. per ft. | 25.7 lbs. per ft. | 28.5 lbs. per ft. | 31.2 lbs. per ft. | 33.8 lbs. per ft. | 36.5 lbs. per ft. | 39.1 lbs. per ft. | 41.7 lbs. per ft. |
| 4 | 5 | 21370 | 23860 | 26310 | 28730 | 31110 | 33450 | 35770 | 38040 |
| 6 | 7 | 17090 | 19090 | 21050 | 22980 | 24890 | 26760 | 28610 | 30430 |
| 8 | 9 | 14250 | 15900 | 17540 | 19150 | 20740 | 22300 | 23840 | 25360 |
| 10 | 11 | 12210 | 13630 | 15040 | 16410 | 17770 | 19110 | 20440 | 21740 |
| 12 | 13 | 10680 | 11930 | 13150 | 14360 | 15550 | 16720 | 17880 | 19020 |
| 14 | 15 | 9500 | 10600 | 11690 | 12770 | 13820 | 14860 | 15890 | 16900 |
| 16 | 17 | 8550 | 9540 | 10520 | 11490 | 12440 | 13380 | 14300 | 15210 |
| 18 | 19 | 7770 | 8670 | 9570 | 10440 | 11310 | 12160 | 13000 | 13830 |
| 20 | 21 | 7120 | 7950 | 8770 | 9570 | 10370 | 11150 | 11920 | 12680 |
| 22 | 23 | 6570 | 7340 | 8090 | 8840 | 9570 | 10290 | 11000 | 11700 |
| 24 | 25 | 6100 | 6810 | 7510 | 8200 | 8880 | 9550 | 10220 | 10870 |
| 26 | 27 | 5700 | 6360 | 7010 | 7660 | 8290 | 8920 | 9540 | 10140 |
| 28 | 29 | 5340 | 5960 | 6570 | 7180 | 7770 | 8360 | 8940 | 9510 |
| 30 | 31 | 5020 | 5610 | 6190 | 6760 | 7320 | 7870 | 8410 | 8950 |
| 32 | 33 | 4750 | 5300 | 5840 | 6380 | 6910 | 7430 | 7950 | 8450 |
| 34 | 35 | 4500 | 5020 | 5540 | 6040 | 6550 | 7040 | 7530 | 8010 |
| 36 | 37 | 4270 | 4770 | 5260 | 5740 | 6220 | 6690 | 7150 | 7600 |
| 38 | 39 | 4070 | 4540 | 5010 | 5470 | 5920 | 6370 | 6810 | 7240 |
| 40 | 41 | 3880 | 4330 | 4780 | 5220 | 5650 | 6080 | 6500 | 6910 |
| 42 | 43 | 3710 | 4150 | 4570 | 4990 | 5410 | 5810 | 6220 | 6610 |
| 44 | 45 | 3560 | 3970 | 4380 | 4780 | 5180 | 5570 | 5960 | 6340 |
| 46 | 47 | 3420 | 3810 | 4210 | 4590 | 4970 | 5350 | 5720 | 6080 |
| 48 | 49 | 3280 | 3670 | 4040 | 4420 | 4780 | 5140 | 5500 | 5850 |
| 50 | 51 | 3160 | 3530 | 3890 | 4250 | 4600 | 4950 | 5300 | 5630 |
| 52 | 53 | 3050 | 3410 | 3760 | 4100 | 4440 | 4780 | 5110 | 5430 |

For safe loads below heavy lines the deflections will be greater than the allowable limit for plastered ceilings = $\frac{1}{160}$ span.

GENERAL FORMULÆ FOR FLEXURE OF BEAMS.**NOTATION.**

- A** = Area of Section in square inches.
d = Depth of Cross Section in inches.
l = Length of Span in inches.
L = Length of Span in feet.
p = Stress in extreme fibre of section in pounds per square inch.
X₁ = Distance of Center of Gravity of Section from extreme fibre in inches.
W = Total Load, in pounds, Uniformly Distributed, including the Weight of Beam.
W₁ = Total Superimposed or Live Load, in pounds, Uniformly Distributed.
W₂ = Total Weight of Beam, in pounds, Uniformly Distributed.
W_s = Total Safe Load, in pounds, Uniformly Distributed.
P = Load, in pounds, concentrated at any point.
F = Coefficient of Strength of the Tables of Properties = Safe Load, in pounds, for a fibre stress of 16 000 pounds per square inch for a span of one foot.
F' = Coefficient of Strength of the Tables of Properties = Safe Load, in pounds, for a fibre stress of 12 500 pounds per square inch for a span of one foot.
D = Total Deflection of Beam, in inches, due to weight **W**.
D_{w1} and **D_p** = Deflections of Beams, in inches, due to the weights **W₁** and **P** respectively.
N = Coefficient of Deflection of the Tables of Properties = Deflection, in inches, due to a total load of 1 000 pounds uniformly distributed for a span of one foot.
N' = Coefficient of Deflection of the Tables of Properties = Deflection, in inches, due to a superimposed load of 1 000 pounds, concentrated at the middle of a Beam with a span of one foot.
H = Coefficient of Deflection, in inches, for fibre stress of 16 000 pounds per square inch, for any section used as a Beam subjected to its safe load Uniformly Distributed. (See table, page 98.)
H' = Coefficient of Deflection, in inches, for fibre stress of 12 500 pounds per square inch for any section used as a Beam subjected to its safe load Uniformly Distributed. (See table, page 98.)
M = Total Bending Moment, in inch pounds, due to the Weight of Beam and Superimposed Load.
I = Moment of Inertia, in inches⁴, Axis through Center of Gravity.
I₁ = Moment of Inertia, in inches⁴, Axis parallel to above but not through Center of Gravity.
v = Distance, in inches, between these Axes.
S = Section Modulus in inches³.
r = Radius of Gyration in inches.
E = Modulus of Elasticity, in pounds, per square inch (Steel = 29 000 000).

GENERAL FORMULÆ.

$$S = \frac{I}{X_1} \quad I_1 = I + Av^2 \quad r = \sqrt{\frac{I}{A}}$$

$$M = \frac{pI}{X_1} = pS \therefore p = \frac{MX_1}{I} = \frac{M}{S} \quad \text{Or for Symmetrical Section } M = \frac{2pI}{d}$$

For Beam supported at both ends and Uniformly Loaded:

$$M = \frac{Wl}{8} = \frac{(W_1 + W_2)l}{8} \therefore W = (W_1 + W_2) = \frac{8M}{l} = \frac{8pI}{lX_1} = \frac{8pS}{l}$$

SAFE LOADS.

$$F = \frac{8pS}{l} \text{ where } p = 16\,000 \text{ pounds and } l = 12'' \text{ therefore } F = \frac{2}{3} 16\,000 S$$

$$F' = \frac{8pS}{l} \text{ where } p = 12\,500 \text{ pounds and } l = 12'' \text{ therefore } F' = \frac{2}{3} 12\,500 S$$

To obtain the Safe Load for any span in feet, for fibre stress of 16 000 pounds per square inch:

$$\text{Safe Load} = W_s = \frac{2}{3} \frac{16\,000 S}{L} = \frac{F}{L}$$

To obtain the Safe Load for any span in feet, for fibre stress of 12 500 pounds per square inch:

$$\text{Safe Load} = W_s = \frac{2}{3} \frac{12\,500 S}{L} = \frac{F'}{L}$$

GENERAL FORMULÆ FOR FLEXURE OF BEAMS.

(CONTINUED.)

DEFLECTIONS.

- (1) Beam supported at both ends and Uniformly Loaded:

$$\text{Deflection for Total Load} = D = \frac{5}{384} \frac{Wl^3}{EI} = \frac{5}{384} \frac{(W_1 + W_2) l^3}{EI}$$

$$\text{Deflection for Superimposed Load} = Dw_1 = \frac{5}{384} \frac{W_1 l^3}{EI}$$

- (2) Beam supported at both ends with load concentrated at the middle:

$$\text{Deflection for Total Load} = D = \frac{Pl^3}{48EI} + \frac{5}{384} \frac{W_2 l^3}{EI}$$

$$\text{Deflection for Superimposed Load} = D_p = \frac{Pl^3}{48EI}$$

- (3) Beam fixed at one end, unsupported at the other, and Uniformly Loaded:

$$\text{Deflection for Total Load} = D = \frac{Wl^3}{8EI} = \frac{(W_1 + W_2) l^3}{8EI}$$

$$\text{Deflection for Superimposed Load} = Dw_1 = \frac{W_1 l^3}{8EI}$$

- (4) Beam fixed at one end, and unsupported at the other, with load concentrated at the unsupported end:

$$\text{Deflection for Total Load} = D = \frac{Pl^3}{3EI} + \frac{W_2 l^3}{8EI}$$

$$\text{Deflection for Superimposed Load} = D_p = \frac{Pl^3}{3EI}$$

$$N = \frac{5}{384} \frac{Wl^3}{EI} = \frac{5}{384} \frac{(W_1 + W_2) l^3}{EI}, \text{ where } W = (W_1 + W_2) = 1000 \text{ pounds and } l = 12''$$

$$N' = \frac{Pl^3}{48EI}, \text{ where } P = 1000 \text{ pounds and } l = 12''$$

$$\text{Total Deflection, in inches, due to a Beam Uniformly Loaded for any span in feet} = D = \frac{NWL^3}{1000} = \frac{N(W_1 + W_2)L^3}{1000}$$

$$\text{Total Deflection, in inches, due to a Superimposed Load } P \text{ and the Weight of Beam } W_2 \text{ for any span in feet} = D = \frac{N'PL^3}{1000} + \frac{NW_2L^3}{1000}$$

$$H = \frac{12}{725} L^3 \qquad H' = \frac{3}{232} L^3$$

FOR SYMMETRICAL SECTIONS.

Total Deflection, in inches, for a fibre stress of 16 000 lbs. per square inch

$$= D = \frac{H}{d}$$

Total Deflection, in inches, for a fibre stress of 12 500 lbs. per square inch

$$= D = \frac{H'}{d}$$

FOR UNSYMMETRICAL SECTIONS.

Total Deflection, in inches, for a fibre stress of 16 000 pounds per square inch

$$= D = \frac{H}{2X_1}$$

Total Deflection, in inches, for a fibre stress of 12 500 pounds per square inch

$$= D = \frac{H'}{2X_1}$$

BENDING MOMENTS AND DEFLECTIONS FOR BEAMS OF UNIFORM SECTION.

W = Total Load, in lbs., uniformly distributed, including the weight of beam.

W_1 = Total Superimposed or Live Load, in lbs., uniformly distributed.

W_2 = Total Weight of Beam or Dead Load, in lbs., uniformly distributed.

P, P_1, P_2, P_3 = Loads, in lbs., concentrated at any points.

The ordinates in diagrams give the bending moments for corresponding points on beam. For superimposed load only, make W_2 in formulæ equal to zero.

M = Total Bending Moment, in inch-lbs.

M_{w1}, M_p = Bending Moments, in inch-lbs., due to Weights W_1 and P respectively.

I = Moment of Inertia, in inches⁴.

l = Length of Span, in inches.

E = Modulus of Elasticity, in lbs. per square inch = 29 000 000 for steel.

W_s = Total Safe Load, in lbs., uniformly distributed, including weight of beam = Total Safe Load of Tables.

(1) Beam Supported at both ends and Uniformly Loaded.

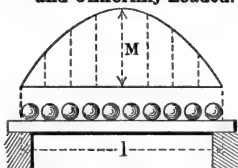


Diagram for Total Load:—

Draw parabola having $M = \frac{Wl}{8}$

Safe Superimposed Load, in lbs., uniformly distributed, $W'_s = W_s - W_2$.

Maximum Bending Moment at middle of beam = $M = \frac{Wl}{8} = \frac{(W_1 + W_2)l}{8}$.

Maximum Shear at points of support = $\frac{W}{2} = \frac{W_1 + W_2}{2}$.

Maximum deflection = $\frac{5}{384} \frac{Wl^3}{EI} = \frac{5}{384} \frac{(W_1 + W_2)l^3}{EI}$.

(2) Beam Supported at both ends with Load Concentrated at the Middle.

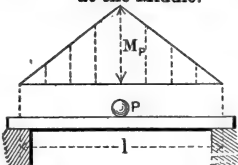


Diagram for Superimposed Load:—

Draw triangle having $M_p = \frac{Pl}{4}$

Diagram, Dead Load, similar to Case (1)

Safe Superimposed Load, in lbs., concentrated, $P_s = \frac{W_s - W_2}{2}$.

Maximum Bending Moment at middle of beam = $M = \frac{Pl}{4} + \frac{W_2 l}{8}$.

Maximum Shear at points of support = $\frac{P + W_2}{2}$.

Max. Deflection = $\frac{Pl^3}{48EI} + \frac{5}{384} \frac{W_2 l^3}{EI}$.

(3) Beam fixed at one end, Unsupported at the other and Uniformly Loaded.

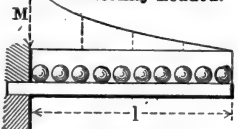


Diagram for Total Load:—

Draw Parabola having $M = \frac{Wl}{2}$

Safe Superimposed Load, in lbs., uniformly distributed, $W'_s = \frac{W_s}{4} - W_2$.

Maximum Bending Moment at point of support = $\frac{Wl}{2} = \frac{(W_1 + W_2)l}{2}$.

Maximum Shear at point of support = $W = W_1 + W_2$.

Max. Deflection = $\frac{Wl^3}{8EI} = \frac{(W_1 + W_2)l^3}{8EI}$.

BENDING MOMENTS AND DEFLECTIONS FOR BEAMS OF UNIFORM SECTION.

W = Total Load, in lbs., uniformly distributed, including the weight of beam.

W_1 = Total Superimposed or Live Load, in lbs., uniformly distributed.

W_2 = Total Weight of Beam or Dead Load, in lbs., uniformly distributed.

P, P_1, P_2, P_3 = Loads, in lbs., concentrated at any points.

The ordinates in diagrams give the bending moments for corresponding points on beam. For superimposed load only, make W_2 in formulæ equal to zero.

M = Total Bending Moment, in inch-lbs.

M_w, M_p = Bending Moments, in inch-lbs., due to Weights W_1 and P respectively.

I = Moment of Inertia, in inches⁴.

l = Length of Span, in inches.

E = Modulus of Elasticity, in lbs. per square inch = 29 000 000 for steel.

W_s = Total Safe Load, in lbs., uniformly distributed, including weight of beam = Total Safe Load of Tables.

- (4) **Beam fixed at one end, and Unsupported at other, with Load Concentrated at the free end.**

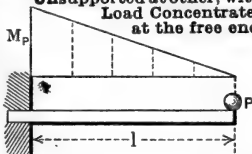


Diagram for Superimposed Load:—
Draw triangle having $M_p = Pl$.

Diagram, Dead Load, similar to Case (3)

Safe Superimposed Load, in lbs., concentrated, $P_s = \frac{W_2 l - 4W_2 l}{8}$.

Maximum Bending Moment at point of support = $Pl + \frac{W_2 l^2}{2}$.

Maximum Shear at point of support = $P + W_2$.

Maximum Deflection = $\frac{Pl^3}{3EI} + \frac{W_2 l^4}{8EI}$.

- (5) **Beam Supported at both ends with Load Concentrated at any point.**

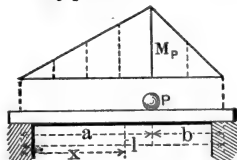


Diagram for Superimposed Load:—

Draw triangle having $M_p = \frac{Pab}{l}$.

Diagram, Dead Load, similar to Case (1)

Safe Superimposed Load, in lbs., concentrated, $P_s = \frac{W_2 l^2 - 4aW_2(1-a)}{8ab}$.

Maximum Bending Moment under load = $\frac{2l}{a(2Pb + W_2 l - W_2 a)}$.

Max. Shear at Sup. near a = $\frac{Pb}{l} + \frac{W_2}{2}$.

Max. Shear at Sup. near b = $\frac{Pa}{l} + \frac{W_2}{2}$.

Deflection at distance x from left support = $\frac{1}{3EI} \left[\frac{2al - a^3}{3} \right]^{\frac{3}{2}}$.

$\left[Pb + \frac{W_2}{8} \left(\sqrt{\frac{2al - a^3}{3}} + \frac{3l^3}{2al - a^2} - 2l \right) \right]$

$x = \sqrt{\frac{2al - a^3}{3}}$ = Distance, from left support, of point of maximum deflection for superimposed load.

- (6) **Beam Supported at both ends with two Symmetrical Loads.**

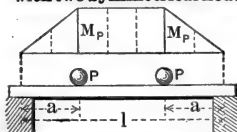


Diagram for Superimposed Load:—
Draw trapezoid having $M_p = Pa$.

Diagram, Dead Load, similar to Case (1)

Safe Superimposed Load, in lbs., concentrated, each, $P_s = \frac{W_2 l - W_2 l}{8a}$.

Maximum Bending Moment at center of beam = $Pa + \frac{W_2 l^2}{8}$.

Maximum Shear at points of support = $\frac{2P + W_2}{2}$.

Maximum Deflection = $\frac{Pa}{24EI} (3l^3 - 4a^2) + \frac{5}{384} \frac{W_2 l^4}{EI}$.

BENDING MOMENTS AND DEFLECTIONS FOR BEAMS OF UNIFORM SECTION.

W = Total Load, in lbs., uniformly distributed, including the weight of beam.

W_1 = Total Superimposed or Live Load, in lbs., uniformly distributed.

W_2 = Total Weight of Beam or Dead Load, in lbs., uniformly distributed.

P, P_1, P_2 = Loads, in lbs., concentrated at any points.

M = Total Bending Moment, in inch-lbs.
 M_w, M_p = Bending Moments, in inch-lbs., due to Weights W_1 and P respectively.

I = Moment of Inertia, in inches⁴.

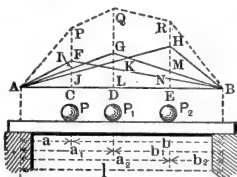
l = Length of Span, in inches.

E = Modulus of Elasticity, in lbs., per square inch = 29 000 000 for steel.

W_s = Total Safe Load, in lbs., uniformly distributed, including the weight of beam = Total Safe Load of Tables.

The ordinates in diagrams give the bending moments for corresponding points on beam. For superimposed load only, make W_2 in formulæ equal to zero.

(7) Beam Supported at both ends with Loads Concentrated at various Points.



The total bending moment at any point produced by all the weights is equal to the sum of the moments at that point produced by each of the weights separately.

Diagram for Dead Load similar to Case (1).

The Maximum Bending Moment occurs at the point where the vertical shear equals zero and will be at one of the loads P, P_1 , or P_2 depending upon their amounts and spacing if W_2 is neglected.

Let R = Reaction at Left Support.

Bending Moment at P =

$$M_p = Ra - \frac{W_2 a^2}{2l}.$$

Bending Moment at P_1 =

$$M_{p1} = Ra_1 - \left[\frac{W_2 a_1^2}{2l} + P(a_1 - a) \right].$$

Bending Moment at $P_2 = M_{p2} = Ra_2 -$

$$\left[\frac{W_2 a_2^2}{2l} + P_1(a_2 - a_1) + P(a_2 - a) \right].$$

Shear or Reaction at Left Support =

$$\frac{P_2 b_2 + P_1 b_1 + Pb + W_2}{1} + \frac{W_2}{2}.$$

Shear or Reaction at Right Support =

$$\frac{P_2 a_2 + P_1 a_1 + Pa + W_2}{1} + \frac{W_2}{2}.$$

Diagram for Superimposed Load:— Draw as in Case (5) the Ordinates FC , GD and HE representing the bending moments due to loads P, P_1 and P_2 respectively. Produce FC to P , making $PC = FC + IC + JC$; GD to Q , making $QD = GD + KD + LD$; and HE to R , making $RE = HE + ME + NE$. Join the points A, P, Q, R and B , then the ordinates between AB and polygon $APQRB$ will represent the bending moments for corresponding points on beam.

BENDING MOMENTS AND DEFLECTIONS FOR BEAMS OF UNIFORM SECTION.

W = Total Load, in lbs., uniformly distributed, including the weight of beam.

W_1 = Total Superimposed or Live Load, in lbs., uniformly distributed.

W_2 = Total Weight of Beam or Dead Load, in lbs., uniformly distributed.

P, P_1, P_2, P_3 = Loads, in lbs., concentrated at any points.

The ordinates in diagrams give the bending moments for corresponding points on beam. For superimposed load only, make W_2 in formulæ equal to zero.

M = Total Bending Moment in inch-lbs.
 M_{W_1}, M_P = Bending Moments, in inch-lbs., due to Weights W_1 and P respectively.

I = Moment of Inertia, in inches⁴.

l = Length of Span, in inches.

E = Modulus of Elasticity, in lbs., per square inch = 29 000 000 for steel.

W_s = Total Safe Load, in lbs., uniformly distributed, including the weight of beam = Total Safe Load of Tables.

(8) Beam Fixed at both ends and Uniformly Loaded.

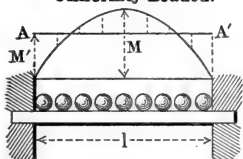


Diagram for Total Load:—Draw parabola having $M = \frac{Wl^2}{8}$. Also $A A'$ parallel to base and at a distance $M' = \frac{Wl^2}{12}$. The Vertical distances between the parabola and line $A A'$ are the moments for corresponding points on beam.

Safe Superimposed Load, in lbs., uniformly distributed, $W'_s = \frac{2}{3} W_s - W_2$.

Distance of points of contra-flexure from supports = .2113l.

Maximum Bending Moment at points of support = $\frac{Wl^2}{12} = \frac{(W_1 + W_2) l^2}{12}$.

Bending Moment at middle of beam = $\frac{Wl^2}{24} = \frac{(W_1 + W_2) l^2}{24}$.

Maximum Shear at points of support = $\frac{Wl}{2}$.

Maximum Deflection = $\frac{Wl^3}{384EI} = \frac{(W_1 + W_2) l^3}{384EI}$.

(9) Beam Fixed at both ends with Load Concentrated at the Middle.

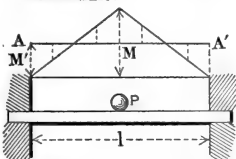


Diagram for Superimposed Load:—Draw triangle having $M = \frac{Pl}{4}$. Also $A A'$ parallel to base and at a distance $M' = \frac{Pl}{8}$. The Vertical distances between the triangle and line $A A'$ are the moments for corresponding points on beam.

Diagram for Dead Load similar to Case (8).

Safe Superimposed Load, in lbs., concentrated, $P_s = W_s - \frac{3}{2} W_2$.

Distance of points of contra-flexure from supports = $\frac{1}{4}l$.

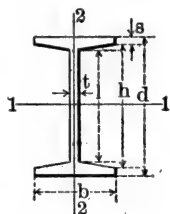
Maximum Bending Moment at points of support = $\frac{Pl}{8} + \frac{W_2 l}{12}$.

Bending Moment at middle of beam = $\frac{Pl}{8} + \frac{W_2 l}{24}$.

Maximum Shear at points of support = $\frac{P + W_2}{2}$.

Maximum Deflection = $\frac{Pl^3}{192EI} + \frac{W_2 l^3}{384EI}$.

VALUES OF MOMENTS OF INERTIA FOR STANDARD AND CAMBRIA SECTIONS.



$$A = td + 2s(b-t) + \frac{(b-t)^2}{12}.$$

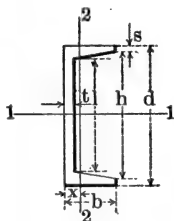
$$I, \text{ Axis } 1-1 = \frac{bd^3}{12} - \frac{h^4-l^4}{8}.$$

$$I', \text{ Axis } 2-2 = \frac{b^3s}{6} + \frac{lt^3}{12} + \frac{b^4-t^4}{288}.$$

$$\text{Slope of flange} = g = \frac{h-l}{b-t} = \frac{1}{6} \text{ for standard sections.}$$

$$h = d - 2s.$$

$$l = h - g(b-t).$$



$$A = td + 2s(b-t) + \frac{(b-t)^2}{6}.$$

$$x = \left[b^3s + \frac{ht^3}{2} + \frac{(b-t)^2(b+2t)}{18} \right] \div A.$$

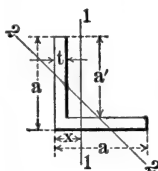
$$I, \text{ Axis } 1-1 = \frac{bd^3}{12} - \frac{h^4-l^4}{16}.$$

$$I', \text{ Axis } 2-2 = \frac{1}{3} \left[2sb^3 + lt^3 + \frac{b^4-t^4}{12} \right] - Ax^2.$$

$$\text{Slope of flange} = g = \frac{h-l}{2(b-t)} = \frac{1}{6} \text{ for standard sections.}$$

$$h = d - 2s.$$

$$l = h - 2g(b-t).$$

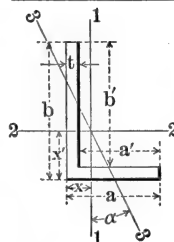


$$A = t(2a-t).$$

$$x = \frac{a^3+at-t^2}{2(2a-t)}.$$

$$I, \text{ Axis } 1-1 = \frac{t(a-x)^3+ax^3-(a-t)(x-t)^3}{3}.$$

$$I', \text{ Axis } 2-2 = \frac{2x^4-2(x-t)^4+t \left[a - \left(2x - \frac{t}{2} \right) \right]^3}{3}.$$



$$A = t(a+b-t).$$

$$x = \frac{t(2a'+b)+a'^2}{2(a'+b)}, \quad x' = \frac{t(2b'+a)+b'^2}{2(b'+a)}.$$

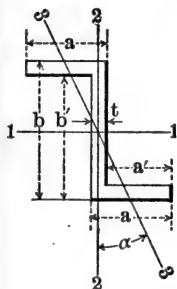
$$\text{Tan. } 2\alpha = + \frac{[(2x-t)b(b-2x')+(2x'-t)(a-t)(a+t-2x)]t}{2(I'-I)}.$$

$$I, \text{ Axis } 1-1 = \frac{t(a-x)^3+bx^3-(b-t)(x-t)^3}{3}.$$

$$I', \text{ Axis } 2-2 = \frac{t(b-x')^3+ax'^3-(a-t)(x'-t)^3}{3}.$$

$$I'', \text{ Axis } 3-3 = \frac{I \cos^2 \alpha - I' \sin^2 \alpha}{\cos 2\alpha}.$$

VALUES OF MOMENTS OF INERTIA FOR STAND- ARD AND CAMBRIA SECTIONS.



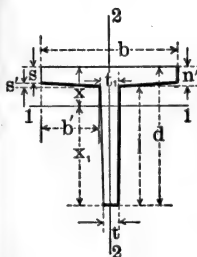
$$A = [b + 2(a - t)] t.$$

$$\tan. 2\alpha = + \frac{(bt - t^2)(a^2 - at)}{I - I'}$$

$$I, \text{ Axis } 1 - 1 = \frac{ab^3 - a'(b - 2t)^3}{12}$$

$$I', \text{ Axis } 2 - 2 = \frac{b(a + a')^3 - 2a'^3b' - 6a'a^2b'}{12}$$

$$I' \text{ Minimum, Axis } 3 - 3 = \frac{I' \cos^2 \alpha - I \sin^2 \alpha}{\cos 2\alpha}$$

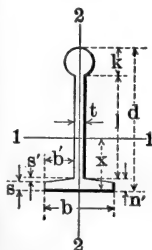


$$A = \frac{1(t + t_1)}{2} + n't_1 + b'(s + n').$$

$$x = \frac{3s^2(b - t_1) + 2b's'(s' + 3s) + 3t_1d^2 - 1(t_1 - t)(3d - l)}{6A}$$

$$I, \text{ Axis } 1 - 1 = \frac{l^3(3t + t_1) + 4bn'^3 - 2b's'^3}{12} - A(x - n')^2$$

$$I', \text{ Axis } 2 - 2 = \frac{sb^3 + s't_1^3 + lt^3}{12} + \frac{s'b'[2b'^2 + (2b' + 3t_1)^2]}{36} + \frac{l(t_1 - t)[(t_1 - t)^2 + 2(t_1 + 2t)^2]}{144}$$



e = Area of head.

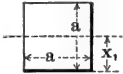
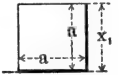
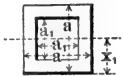

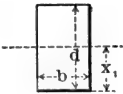
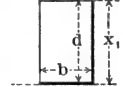
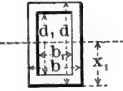
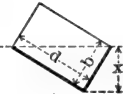
$$A = e + t(d - k) + (b - t)\left(s + \frac{s'}{2}\right).$$

$$x = \frac{e(2d - k) + t(d - k)^2 + (b - t)\left(s^2 + ss' + \frac{s'^2}{3}\right)}{2A}$$

$$I, \text{ Axis } 1 - 1 = e\left[\frac{k^3}{16} + \left(d - \frac{2s + k}{2}\right)^2\right] + \frac{t(1 + s')^3}{3} + \frac{b's'^3 + 2bs^3}{6} - A(x - s)^2.$$

$$I', \text{ Axis } 2 - 2 = \frac{ek^3}{16} + \frac{t^3(1 + s')}{12} + \frac{sb^3}{12} + \frac{s'b'[2b'^2 + (2b' + 3t)^2]}{36}$$

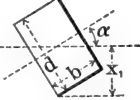
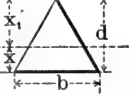
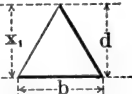

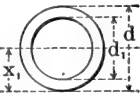
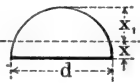
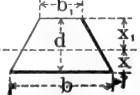
PROPERTIES OF VARIOUS SECTIONS.

| Sections. | Area of Section. A | Distance from Neutral Axis to Extremities of Section. x and x_1 |
|---|-----------------------|--|
|  | a^2 | $x_1 = \frac{a}{2}$ |
|  | a^2 | $*x_1 = a$ |
|  | $a^2 - a_1^2$ | $x_1 = \frac{a}{2}$ |
|  | a^2 | $x_1 = \frac{a}{\sqrt{2}} = .707a$ |
|  | bd | $x_1 = \frac{d}{2}$ |
|  | bd | $*x_1 = d$ |
|  | $bd - b_1d_1$ | $x_1 = \frac{d}{2}$ |
|  | bd | $x_1 = \frac{bd}{\sqrt{b^2 + d^2}}$ *Not the neutral axis. |

PROPERTIES OF VARIOUS SECTIONS.

| Moment of Inertia. I | Section Modulus. $S = \frac{I}{x_1}$ | Radius of Gyration. $r = \sqrt{\frac{I}{A}}$ |
|-------------------------------|---|--|
| $\frac{a^4}{12}$ | $\frac{a^3}{6}$ | $\frac{a}{\sqrt{12}} = .289a$ |
| $\frac{a^4}{3}$ | $\frac{a^3}{3}$ | $\frac{a}{\sqrt{3}} = .577a$ |
| $\frac{a^4 - a_1^4}{12}$ | $\frac{a^4 - a_1^4}{6a}$ | $\sqrt{\frac{a^2 + a_1^2}{12}}$ |
| $\frac{a^4}{12}$ | $\frac{a^3}{6\sqrt{2}} = .118a^3$ | $\frac{a}{\sqrt{12}} = .289a$ |
| $\frac{bd^3}{12}$ | $\frac{bd^2}{6}$ | $\frac{d}{\sqrt{12}} = .289d$ |
| $\frac{bd^3}{3}$ | $\frac{bd^2}{3}$ | $\frac{d}{\sqrt{3}} = .577d$ |
| $\frac{bd^3 - b_1d_1^3}{12}$ | $\frac{bd^3 - b_1d_1^3}{6d}$ | $\sqrt{\frac{bd^3 - b_1d_1^3}{12(bd - b_1d_1)}}$ |
| $\frac{b^3d^3}{6(b^2 + d^2)}$ | $\frac{b^2d^2}{6\sqrt{b^2 + d^2}}$ | $\frac{bd}{\sqrt{6(b^2 + d^2)}}$ |

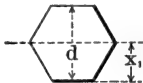

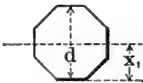
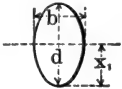
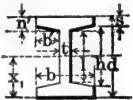
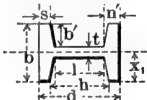
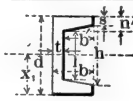

PROPERTIES OF VARIOUS SECTIONS.

| Sections. | Area of Section. A | Distance from Neutral Axis to Extremities of Section. x and x ₁ |
|---|--|---|
|  | bd | $x_1 = \frac{d \cos \alpha + b \sin \alpha}{2}$ |
|  | $\frac{bd}{2}$ | $x = \frac{d}{3}$ $x_1 = \frac{2d}{3}$ |
|  | $\frac{bd}{2}$ | $*x_1 = d$ |
|  | $\frac{\pi d^2}{4} = .785d^2$ | $x_1 = \frac{d}{2}$ |
|  | $\frac{\pi (d^2 - d_1^2)}{4} = .785 (d^2 - d_1^2)$ | $x_1 = \frac{d}{2}$ |
|  | $\frac{\pi d^2}{8} = .393d^2$ | $x = \frac{2d}{3\pi} = .212d$ $x_1 = \frac{(3\pi - 4)d}{6\pi} = .288d$ |
|  | $\frac{b + b_1}{2} \cdot d$ | $x = \frac{b + 2b_1}{b + b_1} \cdot \frac{d}{3}$ $x_1 = \frac{b_1 + 2b}{b + b_1} \cdot \frac{d}{3}$ *Not the neutral axis. |

PROPERTIES OF VARIOUS SECTIONS.

| Moment of Inertia. I | Section Modulus. $S = \frac{I}{x_1}$ | Radius of Gyration. $r = \sqrt{\frac{I}{A}}$ |
|---|---|--|
| $\frac{bd}{12} (d^3 \cos^3 \alpha + b^3 \sin^3 \alpha)$ | $\frac{db}{6} \left(\frac{d^2 \cos^2 \alpha + b^2 \sin^2 \alpha}{d \cos \alpha + b \sin \alpha} \right)$ | $\sqrt{\frac{d^2 \cos^2 \alpha + b^2 \sin^2 \alpha}{12}}$ |
| $\frac{bd^3}{36}$ | $\frac{bd^2}{24}$ | $\frac{d}{\sqrt{18}} = .236d$ |
| Axis through base; $\frac{bd^3}{12}$ Axis through apex; $\frac{bd^3}{4}$ | $\frac{bd^2}{12}$ $\frac{bd^2}{4}$ | $\frac{d}{\sqrt{6}} = .408d$ $\frac{d}{\sqrt{2}} = .707d$ |
| $\frac{\pi d^4}{64} = .049d^4$ | $\frac{\pi d^3}{32} = .098d^3$ | $\frac{d}{4}$ |
| $\frac{\pi(d^4 - d_1^4)}{64} = .049(d^4 - d_1^4)$ | $\frac{\pi(d^4 - d_1^4)}{32d} = .098 \frac{(d^4 - d_1^4)}{d}$ | $\frac{\sqrt{d^2 + d_1^2}}{4}$ |
| $\frac{9\pi^2 - 64}{1152\pi} \cdot d^4 = .007d^4$ | $\frac{9\pi^2 - 64}{192(3\pi - 4)} \cdot d^3 = .024d^3$ | $\frac{\sqrt{9\pi^2 - 64}}{12\pi} \cdot d = .132d$ |
| $\frac{b^3 + 4bb_1 + b_1^3}{36(b + b_1)} \cdot d^3$ | $\frac{b^2 + 4bb_1 + b_1^2}{12(b_1 + 2b)} \cdot d^2$ | $\frac{d}{6(b + b_1)} \sqrt{2(b^2 + 4bb_1 + b_1^2)}$ |

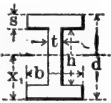
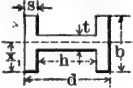
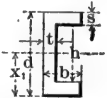
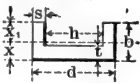
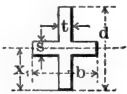
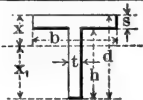
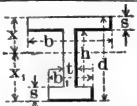
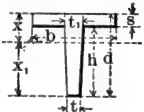
PROPERTIES OF VARIOUS SECTIONS.

| Sections. | Area of Section. A | Distance from Neutral Axis to Extremities of Section. x and x_1 |
|---|---|--|
|  | $\frac{3}{2} d^2 \tan. 30^\circ = .866d^2$ | $x_1 = \frac{d}{2}$ |
|  | $\frac{3}{2} d^2 \tan. 30^\circ = .866d^2$ | $x_1 = \frac{d}{2 \cos 30^\circ} = .577d$ |
|  | $2d^2 \tan. 22\frac{1}{2}^\circ = .828 d^2$ | $x_1 = \frac{d}{2}$ |
|  | $\frac{\pi bd}{4} = .785 bd$ | $x_1 = \frac{d}{2}$ |
|  | $td + 2b' (s + n')$ | $x_1 = \frac{d}{2}$ |
|  | $td + 2b' (s + n')$ | $x_1 = \frac{b}{2}$ |
|  | $td + b' (s + n')$ | $x_1 = \frac{d}{2}$ |
|  | $td + b' (s + n')$ | $x = [b^2s + \frac{ht^3}{2} + \frac{g}{3}(b-t)^3$ $(b+2t)] \div A$ $x_1 = b - x$ |

PROPERTIES OF VARIOUS SECTIONS.

| Moment of Inertia. I | Section Modulus. $S = \frac{I}{x_1}$ | Radius of Gyration. $r = \sqrt{\frac{I}{A}}$ |
|--|---|---|
| $\frac{A}{12} \left[\frac{d^2 (1 + 2 \cos^2 30^\circ)}{4 \cos^2 30^\circ} \right]$ $= .06d^4$ | $\frac{A}{6} \left[\frac{d(1 + 2 \cos^2 30^\circ)}{4 \cos^2 30^\circ} \right] = .12d^3$ | $\frac{d}{4 \cos 30^\circ} \sqrt{\frac{1 + 2 \cos^2 30^\circ}{3}}$ $= .264d$ |
| $\frac{A}{12} \left[\frac{d^2 (1 + 2 \cos^2 30^\circ)}{4 \cos^2 30^\circ} \right]$ $= .06d^4$ | $\frac{A}{6} \left[\frac{d (1 + 2 \cos^2 30^\circ)}{4 \cos 30^\circ} \right]$ $= .104d^3$ | $\frac{d}{4 \cos 30^\circ} \sqrt{\frac{1 + 2 \cos^2 30^\circ}{3}}$ $= .264d$ |
| $\frac{A}{12} \left[\frac{d^2 (1 + 2 \cos^2 22\frac{1}{2}^\circ)}{4 \cos^2 22\frac{1}{2}^\circ} \right]$ $= .055d^4$ | $\frac{A}{6} \left[\frac{d (1 + 2 \cos^2 22\frac{1}{2}^\circ)}{4 \cos 22\frac{1}{2}^\circ} \right]$ $= .109d^3$ | $\frac{d}{4 \cos 22\frac{1}{2}^\circ} \sqrt{\frac{1 + 2 \cos^2 22\frac{1}{2}^\circ}{3}}$ $= .257d$ |
| $\frac{\pi bd^3}{64} = .049bd^3$ | $\frac{\pi bd^2}{32} = .098bd^2$ | $\frac{d}{4}$ |
| $\frac{1}{12} \left[bd^3 - \frac{1}{4g} (h^4 - t^4) \right]$ where $g = \frac{h-1}{b-t}$ | $\frac{2I}{d}$ | $r = \sqrt{\frac{I}{A}}$ |
| $\frac{1}{12} \left[b^3 (d-h) + lt^3 + \frac{g}{4} (b^4 - t^4) \right]$ where $g = \frac{h-1}{b-t}$ | $\frac{2I}{b}$ | $r = \sqrt{\frac{I}{A}}$ |
| $\frac{1}{12} \left[bd^3 - \frac{1}{8g} (h^4 - t^4) \right]$ where $g = \frac{h-1}{2(b-t)}$ | $\frac{2I}{d}$ | $r = \sqrt{\frac{I}{A}}$ |
| $\frac{1}{3} \left[2sb^3 + lt^3 + \frac{g}{2} (b^4 - t^4) - \frac{Ax^2}{h-1} \right]$ where $g = \frac{h-1}{2(b-t)}$ | $\frac{I}{b-x}$ | $r = \sqrt{\frac{I}{A}}$ |

PROPERTIES OF VARIOUS SECTIONS.

| Sections. | Area of Section. A | Distance from Neutral Axis to Extremities of Section. x and x_1 |
|---|-----------------------------|--|
|  | $bd - h(b - t)$ | $x_1 = \frac{d}{2}$ |
|  | $bd - h(b - t)$ | $x_1 = \frac{b}{2}$ |
|  | $bd - h(b - t)$ | $x_1 = \frac{d}{2}$ |
|  | $bd - h(b - t)$ | $x = \frac{2bs^2 + ht^2}{2A}$ $x_1 = b - x$ |
|  | $td + s(b - t)$ | $x_1 = \frac{d}{2}$ |
|  | $bs + ht$ | $x = \frac{d^2t + s^2(b - t)}{2A}$ $x_1 = d - x$ |
|  | $bs + ht + b_1s$ | $x = \frac{td^2 + s^2(b - t) + s(b_1 - t)(2d - s)}{2A}$ $x_1 = d - x$ |
|  | $bs + \frac{h(t + t_1)}{2}$ | $x = \frac{3bs^2 + 3th(d + s) + h(t_1 - t)(h + 3s)}{6A}$ $x_1 = d - x$ |

PROPERTIES OF VARIOUS SECTIONS.

| Moment of Inertia. I | Section Modulus. $S = \frac{I}{x_1}$ | Radius of Gyration. $r = \sqrt{\frac{I}{A}}$ |
|---|---|--|
| $\frac{bd^3 - h^3(b-t)}{12}$ | $\frac{bd^3 - n^3(b-t)}{6d}$ | $\sqrt{\frac{bd^3 - h^3(b-t)}{12[bd - h(b-t)]}}$ |
| $\frac{2sb^3 + ht^3}{12}$ | $\frac{2sb^3 + ht^3}{6b}$ | $\sqrt{\frac{2sb^3 + ht^3}{12[bd - h(b-t)]}}$ |
| $\frac{bd^3 - h^3(b-t)}{12}$ | $\frac{bd^3 - h^3(b-t)}{6d}$ | $\sqrt{\frac{bd^3 - h^3(b-t)}{12[bd - h(b-t)]}}$ |
| $\frac{2sb^3 + ht^3}{3} - Ax^3$ | $\frac{I}{b-x}$ | $\sqrt{\frac{I}{A}}$ |
| $\frac{td^3 + s^3(b-t)}{12}$ | $\frac{td^3 + s^3(b-t)}{6d}$ | $\sqrt{\frac{td^3 + s^3(b-t)}{12[td + s(b-t)]}}$ |
| $\frac{tx_1^3 + bx^3 - (b-t)(x-s)^3}{3}$ | $\frac{I}{d-x}$ | $\sqrt{\frac{tx_1^3 + bx^3 - (b-t)(x-s)^3}{3(bs+ht)}}$ |
| $\frac{bx^3 + b_1x_1^3 - (b-t)(x-s)^3}{3} - \frac{(b_1-t)(x_1-s)^3}{3}$ | $\frac{I}{d-x}$ | $\left[\frac{bx^3 + b_1x_1^3 - (b-t)(x-s)^3}{3(bs+ht+b_1s)} - \frac{(b_1-t)(x_1-s)^3}{3(bs+ht+b_1s)} \right]^{\frac{1}{2}}$ |
| $\frac{4bs^3 + h^3(3t+t_1)}{12} - A(x-s)^3$ | $\frac{I}{d-x}$ | $\sqrt{\frac{I}{A}}$ |

**EXPLANATIONS OF THE TABLES OF PROPERTIES
OF STANDARD AND SPECIAL I-BEAMS, STAND-
ARD AND SPECIAL CHANNELS, AND STANDARD
AND SPECIAL ANGLES WITH EQUAL AND UN-
EQUAL LEGS.**

PROPERTIES OF I-BEAMS.

PAGES 182 TO 185 INCLUSIVE.

The figures or values in the various columns give the section numbers, dimensions, weights, areas and properties of the sections as noted in the different headings.

The columns which require special explanation are as follows:

SECTION MODULUS—Column 8.

This is obtained from the moment of inertia in column 7 by dividing it by the distance from the neutral axis to the most remote fibre, which in this case is one-half the depth of the beam.

COEFFICIENTS OF STRENGTH—Columns 13 and 14.

The coefficients of strength F and F' have been computed for fibre stresses of 16 000 and 12 500 pounds per square inch respectively, as stated in the headings of the columns, and are the safe loads in pounds uniformly distributed, including its own weight, for a beam one foot long. Thus the safe load for any span may be obtained by dividing the proper coefficient by the length of the span in feet.

The coefficients of strength were obtained from the following formulæ:

$$F = \frac{2}{3} \times 16\,000 \times S$$

$$F' = \frac{2}{3} \times 12\,500 \times S$$

in which S is the section modulus.

COEFFICIENTS OF DEFLECTION—Columns 15 and 16.

The Coefficients of Deflection N and N' for uniform and center loads, respectively, were obtained from the following formulæ:

$$N = \frac{Wl^3}{76.8EI} \qquad N' = \frac{Pl^3}{48EI}$$

in which

P and $W = 1\,000$ pounds.

$l = 12$ inches.

$E = 29\,000\,000$.

$I =$ moment of inertia about axis 1-1.

These coefficients are, therefore, the deflections in inches of a beam one foot long with a load of 1 000 pounds, hence, the deflection of a beam for any load and span may be obtained by multiplying the proper coefficient by the cube of the span in feet, and by the number of 1 000-pound units in the given load.

PROPERTIES OF STANDARD AND SPECIAL CHANNELS.**PAGES 186 TO 191 INCLUSIVE.**

The various columns in the Tables of Properties of Standard Channels are similar to those in the Tables of Properties of I-Beams, as explained above, with the addition of column 11, which gives the Section Modulus about an axis through the center of gravity parallel to the web, and column 13, which gives the distance of the center of gravity from the outside of the web.

In this case the Section Modulus $S' = \frac{I'}{b - x}$ the notation being as given at the heads of the columns.

PROPERTIES OF ANGLES.

The values in the Tables of Properties of Standard and Special Angles, with Equal Legs, pages 198 to 203, are those stated in the headings, and those in the Tables of Properties of Standard and Special Angles, with Unequal Legs, on pages 204 to 209, are similar, but with the addition of values for I'' , S'' and r'' about the inclined axis 3-3, the position of which, in order to give the minimum values, was determined by the formula on page 166 or the value of the tangent of $2a$. After determining the position of the inclined axis, the properties corresponding thereto were obtained by the formula on page 166.

MOMENTS OF INERTIA OF RECTANGLES.

Tables of Moments of Inertia of Rectangles, about a transverse axis through the center of gravity, are added on pages 210 to 213 for convenience in calculating the Moments of Inertia, Section Moduli, and Radii of Gyration for compound shapes in which plates are used.

Table I is more convenient when depth of rectangle is expressed without fraction, and is directly applicable to rectangles of various widths, $\frac{1}{4}$ to 1 inch, varying by $\frac{1}{16}$ ths. Table II gives values for 1 inch widths of rectangle only, but for all depths from $\frac{1}{8}$ to $50\frac{15}{16}$ inches, varying by $\frac{1}{16}$ ths. Value for any other width may be obtained from Table II by direct multiplication of tabular value by that other width.

GENERAL FORMULÆ FOR PROPERTIES AND FLEXURE.

Formulæ for obtaining the Properties of Standard Sections are given on pages 166 and 167, and for various usual sections on pages 168 to 175 inclusive.

General formulæ for Flexure of Beams, Bending Moments, and Deflections for various cases of loading are given on pages 160 to 165 inclusive.

EXAMPLES OF APPLICATION OF THE TABLES OF PROPERTIES.

EXAMPLE I.

What is the proper size of I-Beam to carry a load of 35 000 pounds concentrated at the center of a span of 25 feet, the fibre stress not to exceed 16 000 pounds per square inch?

In the Tables of Properties of Standard I-Beams, the column headed F gives the coefficient of strength for a uniform load corresponding to a fibre stress of 16 000 pounds per square inch.

The coefficient of strength for a concentrated load at the center is twice that for the same load uniformly distributed, hence the coefficient necessary to meet the conditions is $35\,000 \times 25 \times 2 = 1\,750\,000$. From the Table of Properties of Standard I-Beams, page 185, column 13, the coefficient F for a 24-inch 80-pound beam is found to be 1 855 310. The weight of the beam itself is $80 \times 25 = 2000$ pounds, which corresponds to a coefficient of $2000 \times 25 = 50\,000$, which deducted from 1 855 310 gives a net coefficient of 1 805 310. A 24-inch beam weighing 80 pounds per foot is, therefore, the proper size.

EXAMPLE II.

What is the deflection of the beam in the preceding example under the given load?

In the Table of Properties of Standard I-Beams, pages 182 to 185 inclusive, the coefficient of deflection for beams with center loads is given in column 16. To obtain the required deflection it is only necessary to multiply the coefficient by the cube of the span and the number of 1 000 pounds units contained in the load.

Thus for the given example the deflection in inches =

$$.0000006 \times 25^3 \times \frac{35\,000}{1\,000} = .328 \text{ inch.}$$

EXAMPLE III.

What is the safe load uniformly distributed that can be placed on an 8-inch standard channel weighing 11.25 pounds per foot, with a clear span of 15 feet for a maximum fibre stress of 12 500 pounds per square inch, the web to be placed vertically?

From the table of Properties of Standard Channels, page 187, column 16, the coefficient of strength F' for the given channel under the conditions named, is found to be 67 300. Hence, the total load may be $67\,300 \div 15 = 4487$ pounds, and, as the channel itself weighs 169 pounds, the net superimposed load which is can safely carry under the given conditions is 4318 pounds.

EXAMPLE IV.

What is the fibre stress in a 5" x 3" angle weighing 8.2 pounds per foot if loaded at the center with a weight of 1500 pounds, used as a beam with a span of 6 feet, the 5-inch leg to be placed vertically?

The bending moment at the center will be

$$\frac{W_1 l}{4} + \frac{W_2 l}{8} = \frac{1\,500 \times 72}{4} + \frac{8.2 \times 6 \times 72}{8} = 27\,443 \text{ inch pounds.}$$

Referring to the Table of Properties of Standard Angles, Unequal Legs, on page 207, the Section Modulus for this angle, corresponding to the axis 2—2, is found to be 1.89.

The maximum fibre stress is obtained by dividing the bending moment by the section modulus, thus: $\frac{27\,443}{1.89} = 14\,520$, which is

the maximum fibre stress in pounds per square inch at the point most remote from the neutral axis, which in this case is the extremity of the longer leg of the angle.

The second term in the above expression for the bending moment is that due to the weight of the angle itself and is inconsiderable, so that in practice it might be neglected for short spans, but should be taken into consideration for the longer ones.

PROPERTIES OF COMPOUND SHAPES.

The moments of inertia, section moduli, and radii of gyration of compound sections used as beams or columns, composed of plates and angles, channels, beams, or any combination of these, may be obtained with the aid of the Tables of Properties as follows:

The first step is to find the center of gravity of the proposed section, which in the case of symmetrical sections is at the center of the figure

For unsymmetrical sections the position of the center of gravity may be determined by multiplying the areas of the component parts by the distances of their centers of gravity from any convenient line, taken as an axis, and dividing the sum of these products by the sum of the areas, which will give the distance of the center of gravity of the compound section from the assumed axis.

The position of the center of gravity for all sizes of angles and channels, is given in the Tables of Properties for these shapes, and is given for various geometrical sections on pages 168 to 175 inclusive, in connection with their other properties.

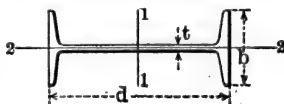
After determining the position of the center of gravity of a compound section, as explained above, the moment of inertia about an axis through its center of gravity may be found by taking the sum of the moments of inertia of each component part about an axis through its own center of gravity, parallel to the axis of the compound section, and adding thereto the sum of products obtained by multiplying the area of each component part by the square of the distance of its center of gravity from the axis of the compound section.

Having thus obtained the moment of inertia of the compound section, the section modulus may be obtained by dividing this moment of inertia by the distance from the neutral axis to the most remote extremity of the section.

The square of the radius of gyration for the compound section may be obtained by dividing the moment of inertia by the total area.

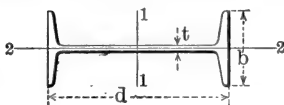
The moment of inertia of a compound section about any axis other than that through its center of gravity may be found in a manner similar to that above described.

PROPERTIES OF STANDARD I-BEAMS.



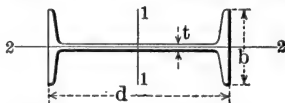
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 |
|-----------------|----------------|------------------|------------------|-------------------|------------------|-----------------------------|---------------------------|------------------------------|-----------------------------|------------------------------|
| Section Number. | Depth of Beam. | Weight per Foot. | Area of Section. | Thickness of Web. | Width of Flange. | Moment of Inertia Axis 1-1. | Section Modulus Axis 1-1. | Radius of Gyration Axis 1-1. | Moment of Inertia Axis 2-2. | Radius of Gyration Axis 2-2. |
| | d | | A | t | b | I | S | r | I' | r' |
| | Inches. | Pounds. | Sq. Ins. | Inch. | Inches. | Inches. ⁴ | Inches. ³ | Inches. | Inches. ⁴ | Inch. |
| B 5 | 3 | 5.50 | 1.63 | .17 | 2.33 | 2.5 | 1.7 | 1.23 | .46 | .53 |
| " | " | 6.50 | 1.91 | .26 | 2.42 | 2.7 | 1.8 | 1.19 | .53 | .52 |
| " | " | 7.50 | 2.21 | .36 | 2.52 | 2.9 | 1.9 | 1.15 | .60 | .52 |
| B 9 | 4 | 7.50 | 2.21 | .19 | 2.66 | 6.0 | 3.0 | 1.64 | .77 | .59 |
| " | " | 8.50 | 2.50 | .26 | 2.73 | 6.4 | 3.2 | 1.59 | .85 | .58 |
| " | " | 9.50 | 2.79 | .34 | 2.81 | 6.7 | 3.4 | 1.54 | .93 | .58 |
| " | " | 10.50 | 3.09 | .41 | 2.88 | 7.1 | 3.6 | 1.52 | 1.01 | .57 |
| B13 | 5 | 9.75 | 2.87 | .21 | 3.00 | 12.1 | 4.8 | 2.05 | 1.23 | .65 |
| " | " | 12.25 | 3.60 | .36 | 3.15 | 13.6 | 5.4 | 1.94 | 1.45 | .63 |
| " | " | 14.75 | 4.34 | .50 | 3.29 | 15.1 | 6.1 | 1.87 | 1.70 | .63 |
| B17 | 6 | 12.25 | 3.61 | .23 | 3.33 | 21.8 | 7.3 | 2.46 | 1.85 | .72 |
| " | " | 14.75 | 4.34 | .35 | 3.45 | 24.0 | 8.0 | 2.35 | 2.09 | .69 |
| " | " | 17.25 | 5.07 | .47 | 3.57 | 26.2 | 8.7 | 2.27 | 2.36 | .68 |
| B21 | 7 | 15.00 | 4.42 | .25 | 3.66 | 36.2 | 10.4 | 2.86 | 2.67 | .78 |
| " | " | 17.50 | 5.15 | .35 | 3.76 | 39.2 | 11.2 | 2.76 | 2.94 | .76 |
| " | " | 20.00 | 5.88 | .46 | 3.87 | 42.2 | 12.1 | 2.68 | 3.24 | .74 |
| B25 | 8 | 18.00 | 5.33 | .27 | 4.00 | 56.9 | 14.2 | 3.27 | 3.78 | .84 |
| " | " | 20.25 | 5.96 | .35 | 4.08 | 60.2 | 15.0 | 3.18 | 4.04 | .82 |
| " | " | 22.75 | 6.69 | .44 | 4.17 | 64.1 | 16.0 | 3.10 | 4.36 | .81 |
| " | " | 25.25 | 7.43 | .53 | 4.26 | 68.0 | 17.0 | 3.03 | 4.71 | .80 |
| B29 | 9 | 21.00 | 6.31 | .29 | 4.33 | 84.9 | 18.9 | 3.67 | 5.16 | .90 |
| " | " | 25.00 | 7.35 | .41 | 4.45 | 91.9 | 20.4 | 3.54 | 5.65 | .88 |
| " | " | 30.00 | 8.82 | .57 | 4.61 | 101.9 | 22.6 | 3.40 | 6.42 | .85 |
| " | " | 35.00 | 10.29 | .73 | 4.77 | 111.8 | 24.8 | 3.30 | 7.31 | .84 |
| B36 | 10 | 25.00 | 7.37 | .31 | 4.66 | 122.1 | 24.4 | 4.07 | 6.89 | .97 |
| " | " | 30.00 | 8.82 | .45 | 4.80 | 134.2 | 26.8 | 3.90 | 7.65 | .93 |
| " | " | 35.00 | 10.29 | .60 | 4.95 | 146.4 | 29.3 | 3.77 | 8.52 | .91 |
| " | " | 40.00 | 11.76 | .75 | 5.10 | 158.7 | 31.7 | 3.67 | 9.50 | .90 |
| B41 | 12 | 31.50 | 9.26 | .35 | 5.00 | 215.8 | 36.0 | 4.83 | 9.50 | 1.01 |
| " | " | 35.00 | 10.29 | .44 | 5.09 | 228.3 | 38.0 | 4.71 | 10.07 | .99 |
| " | " | 40.00 | 11.76 | .56 | 5.21 | 245.9 | 41.0 | 4.57 | 10.95 | .96 |
| B53 | 15 | 42.00 | 12.48 | .41 | 5.50 | 441.8 | 58.9 | 5.95 | 14.62 | 1.08 |
| " | " | 45.00 | 13.24 | .46 | 5.55 | 455.8 | 60.8 | 5.87 | 15.09 | 1.07 |
| " | " | 50.00 | 14.71 | .56 | 5.65 | 483.4 | 64.5 | 5.73 | 16.04 | 1.04 |
| " | " | 55.00 | 16.18 | .66 | 5.75 | 511.0 | 68.1 | 5.62 | 17.06 | 1.03 |
| " | " | 60.00 | 17.65 | .75 | 5.84 | 538.6 | 71.8 | 5.52 | 18.17 | 1.01 |

PROPERTIES OF STANDARD I-BEAMS.



| 12 | 13 | 14 | 15 | 16 | 1 |
|---|---|---|---|---|-------------------------|
| Increase of Thickness of Web for each Pound Increase in Weight. | Coefficient of Strength. | | Coefficient of Deflection. | | Section Number. |
| | For Fibre Stress of 16000 Pounds per Square Inch for Buildings. | For Fibre Stress of 12500 Pounds per Square Inch for Bridges. | Uniform Load. | Center Load. | |
| f | F | F' | N | N' | |
| .098 | 17650 19140 20710 | 13790 14950 16180 | .00031253 .00028827 .00026644 | .00050006 .00046124 .00042630 | B 5 " " |
| .074 | 31810 33890 35980 38070 | 24850 26480 28110 29750 | .00013009 .00012209 .00011500 .00010868 | .00020815 .00019535 .00018400 .00017389 | B 9 " " " |
| .059 | 51590 58100 64630 | 40300 45390 50490 | .00006417 .00005698 .00005122 | .00010267 .00009117 .00008195 | B13 " " |
| .049 | 77460 85270 93110 | 60520 66610 72740 | .00003561 .00003235 .00002963 | .00005698 .00005177 .00004741 | B17 " " |
| .042 | 110410 119400 128560 | 86260 93290 100430 | .00002142 .00001980 .00001839 | .00003427 .00003168 .00002943 | B21 " " |
| .037 | 151660 160510 170970 181430 | 118490 125400 133570 141740 | .00001364 .00001289 .00001210 .00001140 | .00002183 .00002062 .00001936 .00001825 | B25 " " " |
| .033 | 201300 217930 241460 264990 | 157260 170260 188640 207020 | .00000914 .00000844 .00000762 .00000694 | .00001462 .00001350 .00001219 .00001110 | B29 " " " |
| .029 | 260470 286250 312390 338530 | 203500 223630 244050 264480 | .00000635 .00000578 .00000530 .00000489 | .00001017 .00000925 .00000848 .00000782 | B33 " " " |
| .025 | 383670 405800 437170 | 299740 317030 341540 | .00000360 .00000340 .00000316 | .00000575 .00000544 .00000505 | B41 " " |
| .020 | 628270 648310 687530 726740 765960 | 490840 506490 537130 567770 598410 | .00000176 .00000170 .00000161 .00000152 .00000144 | .00000281 .00000272 .00000257 .00000243 .00000231 | B53 " " " " |

PROPERTIES OF STANDARD I-BEAMS.

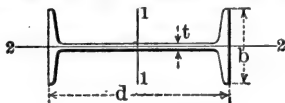


| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 |
|-----------------|----------------|------------------|------------------|--------------------|------------------|-----------------------------|---------------------------|------------------------------|-----------------------------|------------------------------|
| Section Number. | Depth of Beam. | Weight per Foot. | Area of Section. | Thick-ness of Web. | Width of Flange. | Moment of Inertia Axis 1-1. | Section Modulus Axis 1-1. | Radius of Gyration Axis 1-1. | Moment of Inertia Axis 2-2. | Radius of Gyration Axis 2-2. |
| | d | | A | t | b | I | S | r | I' | r' |
| | Inches. | Pounds. | Sq. Ins. | Inch. | Inches. | Inches. ⁴ | Inches. ³ | Inches. | Inches. ⁴ | Inch. |
| B 65 | 18 | 55.0 | 15.93 | .46 | 6.00 | 795.6 | 88.4 | 7.07 | 21.19 | 1.15 |
| " | " | 60.0 | 17.65 | .56 | 6.10 | 841.8 | 93.5 | 6.91 | 22.38 | 1.13 |
| " | " | 65.0 | 19.12 | .64 | 6.18 | 881.5 | 97.9 | 6.79 | 23.47 | 1.11 |
| " | " | 70.0 | 20.59 | .72 | 6.26 | 921.2 | 102.4 | 6.69 | 24.62 | 1.09 |
| B 73 | 20 | 65.0 | 19.08 | .50 | 6.25 | 1169.5 | 117.0 | 7.83 | 27.86 | 1.21 |
| " | " | 70.0 | 20.59 | .58 | 6.33 | 1219.8 | 122.0 | 7.70 | 29.04 | 1.19 |
| " | " | 75.0 | 22.06 | .65 | 6.40 | 1268.8 | 126.9 | 7.58 | 30.25 | 1.17 |
| B 89 | 24 | 80.0 | 23.32 | .50 | 7.00 | 2087.2 | 173.9 | 9.46 | 42.86 | 1.36 |
| " | " | 85.0 | 25.00 | .57 | 7.07 | 2167.8 | 180.7 | 9.31 | 44.35 | 1.33 |
| " | " | 90.0 | 26.47 | .63 | 7.13 | 2238.4 | 186.5 | 9.20 | 45.70 | 1.31 |
| " | " | 95.0 | 27.94 | .69 | 7.19 | 2309.0 | 192.4 | 9.09 | 47.10 | 1.30 |
| " | " | 100.0 | 29.41 | .75 | 7.25 | 2379.6 | 198.3 | 8.99 | 48.55 | 1.28 |

PROPERTIES OF SPECIAL I-BEAMS.

| | | | | | | | | | | |
|-------|----|-------|-------|------|------|--------|-------|------|-------|------|
| B 105 | 12 | 40.0 | 11.84 | .46 | 5.25 | 268.9 | 44.8 | 4.77 | 13.81 | 1.08 |
| " | " | 45.0 | 13.24 | .58 | 5.37 | 285.7 | 47.6 | 4.65 | 14.89 | 1.06 |
| " | " | 50.0 | 14.71 | .70 | 5.49 | 303.4 | 50.6 | 4.54 | 16.12 | 1.05 |
| " | " | 55.0 | 16.18 | .82 | 5.61 | 321.0 | 53.5 | 4.45 | 17.46 | 1.04 |
| B 109 | 15 | 60.0 | 17.67 | .59 | 6.00 | 609.0 | 81.2 | 5.87 | 25.96 | 1.21 |
| " | " | 65.0 | 19.12 | .69 | 6.10 | 636.1 | 84.8 | 5.77 | 27.42 | 1.20 |
| " | " | 70.0 | 20.59 | .78 | 6.19 | 663.7 | 88.5 | 5.68 | 29.00 | 1.19 |
| " | " | 75.0 | 22.06 | .88 | 6.29 | 691.2 | 92.2 | 5.60 | 30.68 | 1.18 |
| " | " | 80.0 | 23.53 | .98 | 6.39 | 718.8 | 95.8 | 5.53 | 32.46 | 1.17 |
| B 113 | 15 | 80.0 | 23.57 | .80 | 6.40 | 789.1 | 105.2 | 5.79 | 41.31 | 1.32 |
| " | " | 85.0 | 25.00 | .90 | 6.50 | 815.9 | 108.8 | 5.71 | 43.46 | 1.32 |
| " | " | 90.0 | 26.47 | .99 | 6.59 | 843.4 | 112.5 | 5.64 | 45.79 | 1.32 |
| " | " | 95.0 | 27.94 | 1.09 | 6.69 | 871.0 | 116.1 | 5.58 | 48.25 | 1.31 |
| " | " | 100.0 | 29.41 | 1.19 | 6.79 | 898.6 | 119.8 | 5.53 | 50.84 | 1.31 |
| B 121 | 20 | 80.0 | 23.73 | .60 | 7.00 | 1466.3 | 146.6 | 7.86 | 45.81 | 1.39 |
| " | " | 85.0 | 25.00 | .66 | 7.06 | 1508.5 | 150.9 | 7.77 | 47.25 | 1.37 |
| " | " | 90.0 | 26.47 | .74 | 7.14 | 1557.5 | 155.8 | 7.67 | 48.98 | 1.36 |
| " | " | 95.0 | 27.94 | .81 | 7.21 | 1606.6 | 160.7 | 7.58 | 50.78 | 1.35 |
| " | " | 100.0 | 29.41 | .88 | 7.28 | 1655.6 | 165.6 | 7.50 | 52.65 | 1.34 |
| B 127 | 24 | 105.0 | 30.98 | .63 | 7.88 | 2811.5 | 234.3 | 9.53 | 78.90 | 1.60 |
| " | " | 110.0 | 32.48 | .69 | 7.94 | 2883.5 | 240.3 | 9.42 | 81.04 | 1.58 |
| " | " | 115.0 | 33.98 | .75 | 8.00 | 2955.5 | 246.3 | 9.33 | 83.23 | 1.56 |

PROPERTIES OF STANDARD I-BEAMS.



| 12 | 18 | 14 | 15 | 16 | 1 |
|---|--|--|----------------------------|--------------|-----------------|
| Increase of Thickness of Web for each Pound Increase in Weight. | Coefficient of Strength. | | Coefficient of Deflection. | | Section Number. |
| | For Fibre Stress of 16 000 Pounds per Square Inch for Buildings. | For Fibre Stress of 12 500 Pounds per Square Inch for Bridges. | Uniform Load. | Center Load. | |
| f | F | F' | N | N' | |
| .016 | 942880 | 736620 | .00000098 | .00000156 | B 65 |
| | 997680 | 779440 | .00000092 | .00000148 | " |
| | 1044740 | 816200 | .00000088 | .00000141 | " |
| | 1091800 | 852970 | .00000084 | .00000135 | " |
| .015 | 1247490 | 974600 | .00000066 | .00000106 | B 73 |
| | 1301110 | 1016490 | .00000064 | .00000102 | " |
| | 1353400 | 1057340 | .00000061 | .00000098 | " |
| .0123 | 1855310 | 1449460 | .00000037 | .00000060 | B 89 |
| | 1926950 | 1505430 | .00000036 | .00000057 | " |
| | 1989700 | 1554450 | .00000035 | .00000056 | " |
| | 2052440 | 1603470 | .00000034 | .00000054 | " |
| | 2115190 | 1652490 | .00000033 | .00000052 | " |

PROPERTIES OF SPECIAL I-BEAMS.

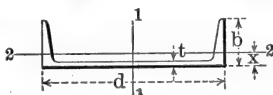
| | | | | | |
|-------|---------|---------|-----------|-----------|-------|
| .025 | 478130 | 373540 | .00000288 | .00000462 | B 105 |
| | 507930 | 396820 | .00000272 | .00000435 | " |
| | 539300 | 421320 | .00000256 | .00000409 | " |
| | 570670 | 445830 | .00000242 | .00000387 | " |
| .020 | 866130 | 676670 | .00000127 | .00000204 | B 109 |
| | 904660 | 706770 | .00000122 | .00000195 | " |
| | 943870 | 737400 | .00000117 | .00000187 | " |
| | 983090 | 768040 | .00000112 | .00000180 | " |
| .020 | 1022300 | 798670 | .00000108 | .00000173 | " |
| | 1122290 | 876790 | .00000098 | .00000157 | B 113 |
| | 1160340 | 906520 | .00000095 | .00000152 | " |
| | 1199550 | 937150 | .00000092 | .00000147 | " |
| .020 | 1238770 | 967790 | .00000089 | .00000143 | " |
| | 1277980 | 998420 | .00000086 | .00000138 | " |
| .015 | 1564060 | 1221920 | .00000053 | .00000085 | B 121 |
| | 1609100 | 1257110 | .00000051 | .00000082 | " |
| | 1661390 | 1297960 | .00000050 | .00000080 | " |
| | 1713670 | 1338810 | .00000048 | .00000077 | " |
| | 1765960 | 1379660 | .00000047 | .00000075 | " |
| .0123 | 2499090 | 1952420 | .00000028 | .00000044 | B 127 |
| | 2563090 | 2002420 | .00000027 | .00000043 | " |
| | 2627090 | 2052420 | .00000026 | .00000042 | " |

PROPERTIES OF STANDARD CHANNELS.



| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
|-------------------------|------------------------------|------------------------|------------------------|---------------------------|------------------------|--------------------------------------|---|---|--------------------------------------|---|---|
| Section Num- ber. | Depth of Chan- nel. | Weight per Foot. | Area of Section. | Thick- ness of Web. | Width of Flange. | Moment of Inertia Axis 1-1. | Section Mod- ulus Axis 1-1. | Radius of Gyra- tion Axis 1-1. | Moment of Inertia Axis 2-2. | Section Mod- ulus Axis 2-2. | Radius of Gyra- tion Axis 2-2. |
| | d | | A | t | b | I | S | r | I' | S' | r' |
| | Inches. | Pounds. | Sq. Ins. | Inch. | Inches. | Inches. ⁴ | Ins. ³ | Inches. | Inches. ⁴ | Ins. ³ | Inch. |
| C 5 | 3 | 4.00 | 1.19 | .17 | 1.41 | 1.6 | 1.1 | 1.17 | .20 | .21 | .41 |
| " | " | 5.00 | 1.47 | .26 | 1.50 | 1.8 | 1.2 | 1.12 | .25 | .24 | .41 |
| " | " | 6.00 | 1.76 | .36 | 1.60 | 2.1 | 1.4 | 1.08 | .31 | .27 | .42 |
| C 9 | 4 | 5.25 | 1.55 | .18 | 1.58 | 3.8 | 1.9 | 1.56 | .32 | .29 | .45 |
| " | " | 6.25 | 1.84 | .25 | 1.65 | 4.2 | 2.1 | 1.51 | .38 | .32 | .45 |
| " | " | 7.25 | 2.13 | .33 | 1.73 | 4.6 | 2.3 | 1.46 | .44 | .35 | .46 |
| C13 | 5 | 6.50 | 1.95 | .19 | 1.75 | 7.4 | 3.0 | 1.95 | .48 | .38 | .50 |
| " | " | 9.00 | 2.65 | .33 | 1.89 | 8.9 | 3.5 | 1.83 | .64 | .45 | .49 |
| " | " | 11.50 | 3.38 | .48 | 2.04 | 10.4 | 4.2 | 1.75 | .82 | .54 | .49 |
| C17 | 6 | 8.00 | 2.38 | .20 | 1.92 | 13.0 | 4.3 | 2.34 | .70 | .50 | .54 |
| " | " | 10.50 | 3.09 | .32 | 2.04 | 15.1 | 5.0 | 2.21 | .88 | .57 | .53 |
| " | " | 13.00 | 3.82 | .44 | 2.16 | 17.3 | 5.8 | 2.13 | 1.07 | .65 | .53 |
| " | " | 15.50 | 4.56 | .56 | 2.28 | 19.5 | 6.5 | 2.07 | 1.28 | .74 | .53 |
| C21 | 7 | 9.75 | 2.85 | .21 | 2.09 | 21.1 | 6.0 | 2.72 | .98 | .63 | .59 |
| " | " | 12.25 | 3.60 | .32 | 2.20 | 24.2 | 6.9 | 2.59 | 1.19 | .71 | .57 |
| " | " | 14.75 | 4.34 | .42 | 2.30 | 27.2 | 7.8 | 2.50 | 1.40 | .79 | .57 |
| " | " | 17.25 | 5.07 | .53 | 2.41 | 30.2 | 8.6 | 2.44 | 1.62 | .87 | .56 |
| " | " | 19.75 | 5.81 | .63 | 2.51 | 33.2 | 9.5 | 2.39 | 1.85 | .96 | .56 |
| C25 | 8 | 11.25 | 3.35 | .22 | 2.26 | 32.3 | 8.1 | 3.10 | 1.33 | .79 | .63 |
| " | " | 13.75 | 4.04 | .31 | 2.35 | 36.0 | 9.0 | 2.98 | 1.55 | .87 | .62 |
| " | " | 16.25 | 4.78 | .40 | 2.44 | 39.9 | 10.0 | 2.89 | 1.78 | .95 | .61 |
| " | " | 18.75 | 5.51 | .49 | 2.53 | 43.8 | 11.0 | 2.82 | 2.01 | 1.02 | .60 |
| " | " | 21.25 | 6.25 | .58 | 2.62 | 47.8 | 11.9 | 2.76 | 2.25 | 1.11 | .60 |
| C29 | 9 | 13.25 | 3.89 | .23 | 2.43 | 47.3 | 10.5 | 3.49 | 1.77 | .97 | .67 |
| " | " | 15.00 | 4.41 | .29 | 2.49 | 50.9 | 11.3 | 3.40 | 1.95 | 1.03 | .66 |
| " | " | 20.00 | 5.88 | .45 | 2.65 | 60.8 | 13.5 | 3.21 | 2.45 | 1.19 | .65 |
| " | " | 25.00 | 7.35 | .61 | 2.81 | 70.7 | 15.7 | 3.10 | 2.98 | 1.36 | .64 |
| C33 | 10 | 15.00 | 4.46 | .24 | 2.60 | 66.9 | 13.4 | 3.87 | 2.30 | 1.17 | .72 |
| " | " | 20.00 | 5.88 | .38 | 2.74 | 78.7 | 15.7 | 3.66 | 2.85 | 1.34 | .70 |
| " | " | 25.00 | 7.35 | .53 | 2.89 | 91.0 | 18.2 | 3.52 | 3.40 | 1.50 | .68 |
| " | " | 30.00 | 8.82 | .68 | 3.04 | 103.2 | 20.6 | 3.42 | 3.99 | 1.67 | .67 |
| " | " | 35.00 | 10.29 | .82 | 3.18 | 115.5 | 23.1 | 3.35 | 4.66 | 1.87 | .67 |
| C41 | 12 | 20.50 | 6.03 | .28 | 2.94 | 128.1 | 21.4 | 4.61 | 3.91 | 1.75 | .81 |
| " | " | 25.00 | 7.35 | .39 | 3.05 | 144.0 | 24.0 | 4.43 | 4.53 | 1.91 | .78 |
| " | " | 30.00 | 8.82 | .51 | 3.17 | 161.6 | 26.9 | 4.28 | 5.21 | 2.09 | .77 |
| " | " | 35.00 | 10.29 | .64 | 3.30 | 179.3 | 29.9 | 4.17 | 5.90 | 2.27 | .76 |
| " | " | 40.00 | 11.76 | .76 | 3.42 | 196.9 | 32.8 | 4.09 | 6.63 | 2.46 | .75 |
| C53 | 15 | 33.00 | 9.90 | .40 | 3.40 | 312.6 | 41.7 | 5.62 | 8.23 | 3.16 | .91 |
| " | " | 35.00 | 10.29 | .43 | 3.43 | 319.9 | 42.7 | 5.57 | 8.48 | 3.22 | .91 |
| " | " | 40.00 | 11.76 | .52 | 3.52 | 347.5 | 46.3 | 5.44 | 9.39 | 3.43 | .89 |
| " | " | 45.00 | 13.24 | .62 | 3.62 | 375.1 | 50.0 | 5.32 | 10.29 | 3.63 | .88 |
| " | " | 50.00 | 14.71 | .72 | 3.72 | 402.7 | 53.7 | 5.23 | 11.22 | 3.85 | .87 |
| " | " | 55.00 | 16.18 | .82 | 3.82 | 430.2 | 57.4 | 5.16 | 12.19 | 4.07 | .87 |

PROPERTIES OF STANDARD CHANNELS.



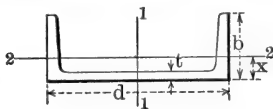
| 13 | 14 | 15 | | 16 | 17 | | 18 | 1 |
|--|---|--|--|----------|----------------------|--------------|----|-----------------|
| Distance of Center of Gravity from Outside of Web. | Increase of Thickness of Web for each Pound Increase in Weight. | Coef. of Strength. | | | Coef. of Deflection. | | | |
| | | Fibre Stress 16 000 Pounds per Sq. Inch for Buildings. | Fibre Stress 12 500 Pounds per Sq. Inch for Bridges. | | Uniform Load. | Center Load. | | Section Number. |
| x Inch. | f Inches. | F | F' | | N | N' | | |
| .44 | .098 | 11630 | 9090 | .0004743 | .0007589 | C 5 | | |
| .44 | | 13140 | 10270 | .0004199 | .0006718 | " | | |
| .46 | | 14710 | 11490 | .0003751 | .0006001 | " | | |
| .46 | .074 | 20230 | 15800 | .0002046 | .0003273 | C 9 | | |
| .46 | | 22270 | 17400 | .0001858 | .0002973 | " | | |
| .46 | | 24360 | 19030 | .0001698 | .0002717 | " | | |
| .49 | .059 | 31640 | 24720 | .0001046 | .0001674 | C13 | | |
| .48 | | 37860 | 29570 | .0000875 | .0001399 | " | | |
| .51 | | 44390 | 34680 | .0000746 | .0001193 | " | | |
| .52 | .049 | 46210 | 36100 | .0000597 | .0000855 | C17 | | |
| .50 | | 53750 | 42000 | .0000513 | .0000821 | " | | |
| .52 | | 61600 | 48120 | .0000448 | .0000717 | " | | |
| .55 | | 69440 | 54250 | .0000397 | .0000636 | " | | |
| .55 | .042 | 64270 | 50210 | .0000368 | .0000588 | C21 | | |
| .53 | | 73650 | 57540 | .0000321 | .0000514 | " | | |
| .53 | | 82740 | 64690 | .0000286 | .0000457 | " | | |
| .55 | | 91950 | 71840 | .0000257 | .0000411 | " | | |
| .58 | | 101100 | 78990 | .0000234 | .0000374 | " | | |
| .58 | .037 | 86140 | 67300 | .0000240 | .0000384 | C25 | | |
| .56 | | 95990 | 75000 | .0000216 | .0000345 | " | | |
| .56 | | 106450 | 83170 | .0000194 | .0000311 | " | | |
| .57 | | 116910 | 91340 | .0000177 | .0000283 | " | | |
| .59 | | 127370 | 99510 | .0000162 | .0000260 | " | | |
| .61 | .033 | 112170 | 87630 | .0000164 | .0000262 | C29 | | |
| .59 | | 120540 | 94170 | .0000158 | .0000244 | " | | |
| .58 | | 144070 | 112550 | .0000128 | .0000204 | " | | |
| .62 | | 167590 | 130930 | .0000110 | .0000176 | " | | |
| .64 | .029 | 142680 | 111470 | .0000116 | .0000186 | C33 | | |
| .61 | | 167940 | 131210 | .0000099 | .0000158 | " | | |
| .63 | | 194090 | 151630 | .0000085 | .0000136 | " | | |
| .65 | | 220230 | 172060 | .0000075 | .0000120 | " | | |
| .69 | | 246380 | 192480 | .0000067 | .0000107 | " | | |
| .70 | .025 | 227750 | 177930 | .0000061 | .0000097 | C41 | | |
| .68 | | 256000 | 200000 | .0000054 | .0000086 | " | | |
| .68 | | 287370 | 224510 | .0000048 | .0000077 | " | | |
| .69 | | 318750 | 249020 | .0000043 | .0000069 | " | | |
| .72 | | 350120 | 273530 | .0000039 | .0000063 | " | | |
| .79 | .020 | 444520 | 347280 | .0000025 | .0000040 | C53 | | |
| .79 | | 455030 | 355500 | .0000024 | .0000039 | " | | |
| .78 | | 494250 | 386130 | .0000022 | .0000036 | " | | |
| .79 | | 533470 | 416770 | .0000021 | .0000033 | " | | |
| .80 | | 572680 | 447410 | .0000019 | .0000031 | " | | |
| .82 | | 611900 | 478050 | .0000018 | .0000029 | " | | |

PROPERTIES OF SHIP AND SPECIAL CHANNELS.

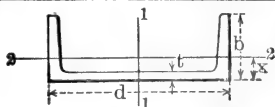


| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 |
|----------------|-------------------|----------------|------------------|--------------------|-----------------|----------------------|------------------|-----------------------------|----------------------------|-------------------------------|-----------------------------|----------------------------|
| Section Number | Depth of Channel. | Wght per Foot. | Area of Section. | Thick-ness of Web. | Width of Flange | Thickness of Flange. | Slope of Flange. | Moment of Inertia Axis 1-1. | Section Mod-ulus Axis 1-1. | Radius of Gyra-tion Axis 1-1. | Moment of Inertia Axis 2-2. | Section Mod-ulus Axis 2-2. |
| | d | | A | t | b | s | | I | S | r | I' | S' |
| | Ins. | Lbs. | Sq. Ins. | Inch. | Ins. | In. | g | Ins. ⁴ | Ins. ³ | Ins. | Ins. ⁴ | Ins. ³ |
| C 269 | 3 | 7.1 | 2.07 | .306 | 1.94 | .26 | .12 | 2.72 | 1.81 | 1.15 | .66 | .52 |
| C 72 | 4 | 10.1 | 2.95 | .394 | 2.09 | .38 | .004 | 6.54 | 3.27 | 1.49 | 1.12 | .79 |
| C 86 | 6 | 15.3 | 4.47 | .34 | 3.50 | .33 | .035 | 25.3 | 8.4 | 2.38 | 5.14 | 2.13 |
| " | " | 17.7 | 5.19 | .46 | 3.62 | " | " | 27.5 | 9.2 | 2.30 | 5.95 | 2.31 |
| C 88 | 6 | 19.0 | 5.58 | .41 | 3.56 | .46 | .02 | 31.1 | 10.4 | 2.36 | 6.79 | 2.85 |
| " | " | 21.6 | 6.36 | .54 | 3.69 | " | " | 33.4 | 11.1 | 2.29 | 7.85 | 3.10 |
| " | " | 23.4 | 6.87 | .63 | 3.78 | " | " | 34.9 | 11.6 | 2.25 | 8.53 | 3.25 |
| C 89 | 7 | 20.9 | 6.15 | .45 | 3.45 | .48 | .02 | 44.6 | 12.7 | 2.69 | 6.74 | 2.81 |
| " | " | 23.8 | 6.99 | .57 | 3.57 | " | " | 48.0 | 13.7 | 2.62 | 7.63 | 3.02 |
| C 101 | 8 | 21.5 | 6.30 | .40 | 3.50 | .48 | .02 | 60.7 | 15.2 | 3.07 | 7.20 | 2.94 |
| " | " | 24.7 | 7.26 | .52 | 3.62 | " | " | 65.8 | 16.4 | 3.01 | 8.25 | 3.17 |
| C 103 | 8 | 23.8 | 7.00 | .50 | 3.50 | .48 | .02 | 63.6 | 15.7 | 3.01 | 7.42 | 2.96 |
| " | " | 27.1 | 7.96 | .62 | 3.62 | " | " | 68.7 | 17.2 | 2.94 | 8.41 | 3.18 |
| C 90 | 10 | 21.9 | 6.44 | .38 | 3.38 | .41 | .02 | 92.0 | 18.4 | 3.78 | 6.29 | 2.51 |
| " | " | 26.0 | 7.64 | .50 | 3.50 | " | " | 102.0 | 20.4 | 3.66 | 7.17 | 2.70 |
| " | " | 27.4 | 8.04 | .54 | 3.54 | " | " | 105.4 | 21.1 | 3.62 | 7.45 | 2.76 |
| " | " | 31.5 | 9.24 | .66 | 3.66 | " | " | 115.4 | 23.1 | 3.54 | 8.30 | 2.94 |
| C 105 | 12 | 35.0 | 10.30 | .47 | 3.77 | .65 | .03 | 215.7 | 36.0 | 4.58 | 12.98 | 4.79 |
| " | " | 40.0 | 11.76 | .60 | 3.90 | " | " | 233.3 | 38.9 | 4.45 | 14.61 | 5.13 |
| " | " | 44.3 | 13.02 | .70 | 4.00 | " | " | 248.4 | 41.4 | 4.37 | 15.99 | 5.41 |
| " | " | 46.3 | 13.62 | .75 | 4.05 | " | " | 255.6 | 42.6 | 4.33 | 16.64 | 5.56 |
| " | " | 48.4 | 14.22 | .80 | 4.10 | " | " | 262.8 | 43.8 | 4.30 | 17.31 | 5.68 |
| " | " | 50.0 | 14.70 | .84 | 4.14 | " | " | 268.6 | 44.8 | 4.27 | 17.84 | 5.79 |
| C 95 | 13 | 32.0 | 9.30 | .38 | 4.00 | .34 | .15 | 237.5 | 36.5 | 5.05 | 11.54 | 3.86 |
| " | " | 35.0 | 10.29 | .45 | 4.08 | " | " | 251.5 | 38.7 | 4.94 | 12.54 | 4.06 |
| " | " | 37.0 | 10.88 | .50 | 4.12 | " | " | 259.8 | 40.0 | 4.89 | 13.10 | 4.17 |
| " | " | 40.0 | 11.76 | .56 | 4.19 | " | " | 272.2 | 41.9 | 4.81 | 13.94 | 4.33 |
| " | " | 45.0 | 13.24 | .68 | 4.30 | " | " | 292.9 | 45.1 | 4.70 | 15.32 | 4.59 |
| " | " | 50.0 | 14.71 | .79 | 4.42 | " | " | 313.7 | 48.3 | 4.62 | 16.71 | 4.86 |
| " | " | 55.0 | 16.18 | .90 | 4.53 | " | " | 334.4 | 51.4 | 4.55 | 18.14 | 5.14 |
| C 65 | 18 | 45.0 | 13.25 | .47 | 3.77 | .45 | .17 | 584.3 | 64.9 | 6.64 | 12.89 | 4.40 |
| " | " | 50.0 | 14.71 | .55 | 3.85 | " | " | 623.1 | 69.2 | 6.51 | 13.90 | 4.61 |
| " | " | 55.0 | 16.18 | .63 | 3.93 | " | " | 662.0 | 73.6 | 6.40 | 14.93 | 4.82 |
| " | " | 60.0 | 17.65 | .72 | 4.02 | " | " | 703.3 | 78.1 | 6.31 | 15.96 | 5.03 |

PROPERTIES OF SHIP AND SPECIAL CHANNELS.



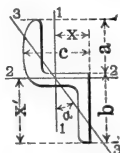
| 14 | 15 | 16 | 17 | 18 | 19 | 20 | 1 |
|------------------------------|--|---|---|---|----------------------|--------------|-----------------|
| Radius of Gyration Axis 2-2. | Distance of Center of Gravity from Outside of Web. | Increase of Thickness of Web for each Lb. Increase in Weight. | Coef. of Strength. | | Coef. of Deflection. | | Section Number. |
| | | | Fibre Stress 16 000 Lbs. per Sq. Inch. for Buildings. | Fibre Stress 12 500 Lbs. per Sq. Inch. for Bridges. | Uniform Load. | Center Load. | |
| r' | x | f | F | F' | N | N' | |
| Inch. | Inch. | Inch. | | | | | |
| .50 | .65 | .098 | 19310 | 15090 | .0002857 | .0004571 | C 269 |
| .62 | .67 | .074 | 34880 | 27250 | .0001186 | .0001898 | C 72 |
| 1.07 | 1.08 | .049 | 89160 | 69660 | .0000307 | .0000491 | C 86 |
| 1.07 | 1.04 | " | 97680 | 76310 | .0000283 | .0000452 | " |
| 1.10 | 1.18 | .049 | 110450 | 86290 | .0000250 | .0000400 | C 88 |
| 1.11 | 1.16 | " | 118770 | 92790 | .0000232 | .0000372 | " |
| 1.11 | 1.15 | " | 124270 | 97080 | .0000222 | .0000356 | " |
| 1.05 | 1.05 | .042 | 135950 | 106210 | .0000174 | .0000278 | C 89 |
| 1.05 | 1.04 | " | 146350 | 114330 | .0000162 | .0000259 | " |
| 1.07 | 1.05 | .037 | 161930 | 126510 | .0000128 | .0000204 | C 101 |
| 1.07 | 1.02 | " | 174930 | 136670 | .0000118 | .0000189 | " |
| 1.03 | .99 | .037 | 167470 | 130830 | .0000122 | .0000195 | C 103 |
| 1.03 | .98 | " | 183470 | 143330 | .0000113 | .0000181 | " |
| .99 | .87 | .029 | 196310 | 153360 | .0000085 | .0000135 | C 90 |
| .97 | .84 | " | 217650 | 170030 | .0000077 | .0000123 | " |
| .96 | .84 | " | 224760 | 175580 | .0000074 | .0000118 | " |
| .95 | .84 | " | 246100 | 192250 | .0000068 | .0000108 | " |
| 1.12 | 1.07 | .0245 | 383550 | 299650 | .0000036 | .0000058 | C 105 |
| 1.11 | 1.05 | " | 414790 | 324060 | .0000033 | .0000053 | " |
| 1.11 | 1.05 | " | 441670 | 345060 | .0000031 | .0000050 | " |
| 1.11 | 1.05 | " | 454470 | 355060 | .0000030 | .0000049 | " |
| 1.10 | 1.05 | " | 467270 | 369750 | .0000030 | .0000047 | " |
| 1.10 | 1.06 | " | 477510 | 373060 | .0000029 | .0000046 | " |
| 1.11 | 1.01 | .023 | 389710 | 304460 | .0000033 | .0000052 | C 95 |
| 1.10 | .99 | " | 412750 | 322460 | .0000031 | .0000049 | " |
| 1.10 | .98 | " | 426340 | 333080 | .0000030 | .0000048 | " |
| 1.09 | .97 | " | 446740 | 349010 | .0000029 | .0000046 | " |
| 1.08 | .97 | " | 480720 | 375560 | .0000027 | .0000042 | " |
| 1.07 | .98 | " | 514710 | 402120 | .0000025 | .0000040 | " |
| 1.06 | 1.00 | " | 548700 | 428670 | .0000023 | .0000037 | " |
| .99 | .84 | .016 | 692270 | 540830 | .0000014 | .0000022 | C 65 |
| .97 | .83 | " | 738520 | 576970 | .0000012 | .0000020 | " |
| .96 | .83 | " | 784600 | 612970 | .0000012 | .0000019 | " |
| .95 | .85 | " | 833560 | 651220 | .0000011 | .0000018 | " |



PROPERTIES OF STANDARD SHIP CHANNELS.

General slope of flange = 2° or .035.

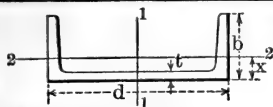
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
|-----------------|-------------------|-----------------|------------------|--------------------|------------------|---------------------------|-----------------------------|----------------------------|-------------------------------|-----------------------------|----------------------------|
| Section Number. | Depth of Channel. | W'ght per Foot. | Area of Section. | Thick-ness of Web. | Width of Flange. | Thick-ness at Mid Flange. | Moment of Inertia Axis 1-1. | Section Mod-ulus Axis 1-1. | Radius of Gyra-tion Axis 1-1. | Moment of Inertia Axis 2-2. | Section Mod-ulus Axis 2-2. |
| | d | | A | t | b | | I | S | r | I' | S' |
| | Ins. | Lbs. | Sq. Ins. | Inch. | Ins. | Inch. | Ins. ⁴ | Ins. ³ | Ins. | Ins. ⁴ | Ins. ³ |
| C 55 | 6 | 16.8 | 4.92 | .325 | 3.45 | .475 | 28.5 | 9.5 | 2.41 | 5.69 | 2.49 |
| "(BSC8) | " | 17.8 | 5.22 | .375 | 3.50 | " | 29.4 | 9.8 | 2.38 | 6.09 | 2.58 |
| " | " | 19.8 | 5.82 | .475 | 3.60 | " | 31.2 | 10.4 | 2.32 | 6.86 | 2.77 |
| C 57 | 7 | 18.9 | 5.55 | .350 | 3.45 | .500 | 42.8 | 12.2 | 2.78 | 6.31 | 2.69 |
| "(BSC10) | " | 20.1 | 5.90 | .400 | 3.50 | " | 44.2 | 12.6 | 2.74 | 6.73 | 2.78 |
| " | " | 22.5 | 6.60 | .500 | 3.60 | " | 47.1 | 13.5 | 2.67 | 7.54 | 2.98 |
| C 59 | 8 | 21.2 | 6.23 | .375 | 3.45 | .525 | 61.2 | 15.3 | 3.13 | 6.92 | 2.89 |
| "(BSC13) | " | 22.6 | 6.63 | .425 | 3.50 | " | 63.3 | 15.8 | 3.09 | 7.36 | 2.98 |
| " | " | 25.3 | 7.43 | .525 | 3.60 | " | 67.6 | 16.9 | 3.02 | 8.21 | 3.18 |
| C 60 | 9 | 23.7 | 6.96 | .400 | 3.45 | .550 | 84.3 | 18.7 | 3.48 | 7.52 | 3.08 |
| "(BSC17) | " | 25.2 | 7.41 | .450 | 3.50 | " | 87.3 | 19.4 | 3.43 | 7.97 | 3.17 |
| " | " | 28.3 | 8.31 | .550 | 3.60 | " | 93.4 | 20.7 | 3.35 | 8.85 | 3.38 |
| " | " | 31.3 | 9.21 | .650 | 3.70 | " | 99.4 | 22.1 | 3.29 | 9.71 | 3.57 |
| C 61 | 10 | 24.6 | 7.23 | .375 | 3.40 | .575 | 108.6 | 21.7 | 3.88 | 7.62 | 3.15 |
| " | " | 26.3 | 7.73 | .425 | 3.45 | " | 112.7 | 22.5 | 3.82 | 8.10 | 3.25 |
| "(BSC20) | " | 28.0 | 8.23 | .475 | 3.50 | " | 116.9 | 23.4 | 3.77 | 8.56 | 3.37 |
| " | " | 31.4 | 9.23 | .575 | 3.60 | " | 125.2 | 25.0 | 3.69 | 9.47 | 3.60 |
| " | " | 34.8 | 10.23 | .675 | 3.70 | " | 133.6 | 26.7 | 3.61 | 10.37 | 3.80 |
| C 63 | 12 | 30.6 | 9.00 | .450 | 3.45 | .600 | 181.8 | 30.3 | 4.50 | 8.89 | 3.48 |
| "(BSC25) | " | 32.7 | 9.60 | .500 | 3.50 | " | 189.0 | 31.5 | 4.44 | 9.37 | 3.58 |
| " | " | 36.8 | 10.80 | .600 | 3.60 | " | 203.4 | 33.9 | 4.34 | 10.31 | 3.80 |
| " | " | 40.8 | 12.00 | .700 | 3.70 | " | 217.8 | 36.3 | 4.26 | 11.26 | 4.01 |



PROPERTIES OF Z-BAR HATCH SECTION.

STANDARD SHIP SECTION.

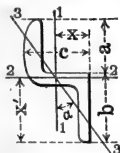
| Section Number. | Size $a \times b \times c$. | Weight per Foot. | Area of Section. | THICKNESS. | | | Moment of Inertia Axis 1-1. | Section Modulus Axis 2-2. |
|-----------------|---|------------------|------------------|---------------|----------------|---------------|-----------------------------|---------------------------|
| | | | | Web. | Plain Leg. | Rounded Leg. | | |
| | | | | Ins. | Ins. | Ins. | | |
| Z 101 | $2 \frac{1}{2} \times 3 \times 2 \frac{3}{4}$ | 13.6 | 3.98 | $\frac{1}{2}$ | $\frac{1}{16}$ | $\frac{3}{4}$ | 3.57 | 2.52 |



PROPERTIES OF STANDARD SHIP CHANNELS.

General slope of flange = 2° or .035.

| 13 | 14 | 15 | 16 | | 17 | 18 | | 19 | 1 |
|--|--|---|--|---|-------------------------------|-----------------|--------------------|----|---|
| Radii of Gyra- tion Axis 2-2. | Dis- tance of Center of Gravi- ty from Outside of Web. | In- crease of Thick- ness of Web for each Lb. In- crease in Weight. | Coefficient of Strength. | | Coefficient of Deflection. | | Section Number. | | |
| | | | Fibre Stress 16 000 Lbs per Sq. Inch. for Buildings. | Fibre Stress 12 500 Lbs. per Sq. Inch. for Bridges. | Uniform Load. | Center Load. | | | |
| | | | F | F' | N | N' | | | |
| r' | x | f | | | | | | | |
| Inch | Inch. | Inch. | | | | | | | |
| 1.08 | 1.17 | .049 | 101500 | 79300 | .0000271 | .0000434 | C 55 | | |
| 1.08 | 1.15 | " | 104700 | 81800 | .0000264 | .0000422 | " (BSC 8) | | |
| 1.09 | 1.13 | " | 111000 | 86800 | .0000249 | .0000398 | " | | |
| 1.07 | 1.11 | .042 | 130410 | 101880 | .0000182 | .0000290 | C 57 | | |
| 1.07 | 1.09 | " | 134770 | 105290 | .0000176 | .0000281 | " (BSC 10) | | |
| 1.07 | 1.07 | " | 143480 | 112090 | .0000165 | .0000264 | " | | |
| 1.05 | 1.05 | .037 | 163080 | 127410 | .0000127 | .0000203 | C 59 | | |
| 1.05 | 1.04 | " | 163770 | 131850 | .0000123 | .0000196 | " (BSC 13) | | |
| 1.05 | 1.02 | " | 180150 | 140740 | .0000115 | .0000184 | " | | |
| 1.04 | 1.01 | .033 | 199730 | 156040 | .0000092 | .0000148 | C 60 | | |
| 1.04 | 1.00 | " | 206930 | 161660 | .0000089 | .0000142 | " (BSC 17) | | |
| 1.03 | .98 | " | 221330 | 172910 | .0000083 | .0000133 | " | | |
| 1.03 | .98 | " | 235730 | 184160 | .0000078 | .0000125 | " | | |
| 1.03 | .98 | .029 | 231610 | 180940 | .0000072 | .0000115 | C 61 | | |
| 1.02 | .97 | " | 240500 | 187890 | .0000069 | .0000111 | " | | |
| 1.02 | .96 | " | 249390 | 194830 | .0000067 | .0000107 | " (BSC 20) | | |
| 1.01 | .95 | " | 267160 | 208720 | .0000062 | .0000100 | " | | |
| 1.01 | .95 | " | 284940 | 222610 | .0000058 | .0000093 | " | | |
| .99 | .90 | .025 | 323290 | 252570 | .0000044 | .0000070 | C 63 | | |
| .99 | .89 | " | 336090 | 262570 | .0000041 | .0000066 | " (BSC 25) | | |
| .98 | .89 | " | 361690 | 282570 | .0000039 | .0000061 | " | | |
| .97 | .89 | " | 387290 | 302570 | .0000036 | .0000057 | " | | |

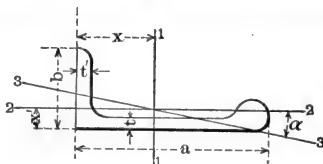


PROPERTIES OF Z-BAR HATCH SECTION.

STANDARD SHIP SECTION.

| Radius of Gyration Axis 1-1. | Distance of Center of Gravity x | Moment of Inertia Axis 2-2. | Section Modulus Axis 2-2. | Radius of Gyration Axis 2-2. | Distance of Center of Gravity x' | Tangent of Angle α | Least Radius of Gyration Axis 3-3. | Section Number. |
|------------------------------|---------------------------------|-----------------------------|---------------------------|------------------------------|----------------------------------|---------------------------|------------------------------------|-----------------|
| Ins. | Ins. | Ins. ⁴ | Ins. ³ | Ins. | Ins. | | Ins. | |
| .95 | 1.42 | 6.98 | 2.39 | 1.33 | 2.93 | 1.560 | .55 | Z-101 |

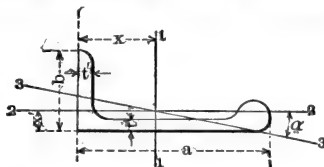
PROPERTIES OF BULB ANGLES.



| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|--------------------|--------------------------|------------------------|------------------------|------------------------------|--------------------------------|--------------------------------------|---------------------------------|
| Section Number. | Size. | Weight per Foot. | Area of Section. | Thickness of Bulb Leg. | Thickness of Plain Leg. | Moment of Inertia Axis 1-1. | Section Modulus Axis 1-1. |
| | $a \times b$ | | A | t | t' | I | S |
| | Inches. | | Sq. Ins. | Ins. | Ins. | Ins. ⁴ | Ins. ³ |
| * A174 | $4 \times 3\frac{1}{2}$ | 11.7 | 3.42 | $\frac{3}{8}$ | $\frac{3}{8}$ | 7.7 | 3.25 |
| * A176 | $5 \times 4\frac{1}{2}$ | 19.2 | 5.64 | $\frac{1}{2}$ | $\frac{1}{2}$ | 20.7 | 7.89 |
| A 171 | $5 \times 2\frac{1}{2}$ | 10.2 | 3.00 | $\frac{1}{2}$ | $\frac{3}{8}$ to $\frac{1}{2}$ | 10.4 | 4.05 |
| A 177 | 6×3 | 11.8 | 3.47 | $\frac{5}{16}$ | .34 | 16.8 | 5.10 |
| " | " | 13.5 | 3.95 | $\frac{3}{8}$ | .39 | 18.5 | 5.56 |
| " | " | 15.0 | 4.41 | $\frac{7}{16}$ | .43 | 20.1 | 6.02 |
| A 178 | $6 \times 3\frac{1}{2}$ | 12.5 | 3.66 | $\frac{5}{16}$ | .37 | 18.0 | 5.16 |
| " | " | 14.1 | 4.13 | $\frac{3}{8}$ | .41 | 19.6 | 5.62 |
| " | " | 15.7 | 4.60 | $\frac{7}{16}$ | .45 | 21.3 | 6.11 |
| " | " | 17.3 | 5.07 | $\frac{1}{2}$ | .49 | 22.8 | 6.53 |
| " | " | 18.9 | 5.53 | $\frac{9}{16}$ | .53 | 24.4 | 6.97 |
| " | " | 20.5 | 6.02 | $\frac{5}{8}$ | .58 | 25.9 | 7.42 |
| A 179 | $7 \times 3\frac{1}{2}$ | 15.7 | 4.61 | $\frac{3}{8}$ | .43 | 29.3 | 7.21 |
| " | " | 17.5 | 5.13 | $\frac{7}{16}$ | .46 | 31.6 | 7.79 |
| " | " | 19.1 | 5.60 | $\frac{1}{2}$ | .48 | 33.7 | 8.36 |
| A 181 | $8 \times 3\frac{1}{2}$ | 17.4 | 5.09 | $\frac{3}{8}$ | .42 | 42.8 | 9.54 |
| " | " | 19.3 | 5.64 | $\frac{7}{16}$ | .44 | 45.3 | 10.15 |
| " | " | 21.5 | 6.30 | $\frac{1}{2}$ | .50 | 50.1 | 11.14 |
| A 183 | $9 \times 3\frac{1}{2}$ | 20.3 | 5.96 | $\frac{1}{2}$ | .44 | 62.6 | 12.78 |
| " | " | 22.6 | 6.62 | $\frac{3}{4}$ | .48 | 68.0 | 13.81 |
| " | " | 24.8 | 7.27 | $\frac{7}{8}$ | .52 | 72.7 | 14.75 |
| A 185 | $10 \times 3\frac{1}{2}$ | 23.6 | 6.91 | $\frac{7}{16}$ | .47 | 88.6 | 16.62 |
| " | " | 26.1 | 7.64 | $\frac{1}{2}$ | .51 | 95.6 | 17.81 |
| " | " | 28.5 | 8.35 | $\frac{9}{16}$ | .55 | 102.2 | 19.00 |

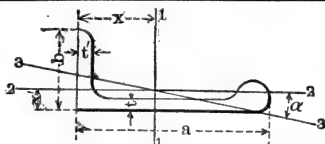
*Top Guard Angle.

PROPERTIES OF BULB ANGLES.



| 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 1 |
|------------------------------|--|-----------------------------|---------------------------|------------------------------|---|-------------------|------------------------------------|-----------------|
| Radius of Gyration Axis 1-1. | Distance Center of Gravity from back of Plain Leg. | Moment of Inertia Axis 2-2. | Section Modulus Axis 2-2. | Radius of Gyration Axis 2-2. | Distance Center of Gravity from back of Bulb Leg. | Tangent of Angle. | Least Radius of Gyration Axis 3-3. | Section Number. |
| r | x | I' | S' | r' | x' | α | r'' | |
| Ins. | Ins. | Ins. ⁴ | Ins. ³ | Ins. | Ins. | | Ins. | |
| 1.50 | 1.73 | 3.07 | 1.19 | .95 | .94 | .398 | .81 | A174* |
| 1.92 | 2.38 | 7.96 | 2.41 | 1.19 | 1.19 | .385 | 1.01 | A176* |
| 1.86 | 2.43 | 3.47 | 1.81 | 1.08 | .59 | .198 | 1.03 | A171 |
| 2.20 | 2.70 | 1.88 | .79 | .74 | .63 | .161 | .65 | A177 |
| 2.16 | 2.67 | 2.11 | .90 | .73 | .65 | .161 | .65 | " |
| 2.14 | 2.66 | 2.33 | 1.00 | .73 | .67 | .159 | .65 | " |
| 2.22 | 2.51 | 3.27 | 1.21 | .95 | .80 | .250 | .79 | A178 |
| 2.18 | 2.50 | 3.60 | 1.33 | .93 | .80 | .247 | .79 | " |
| 2.15 | 2.52 | 3.92 | 1.46 | .92 | .81 | .244 | .78 | " |
| 2.12 | 2.50 | 4.21 | 1.57 | .91 | .82 | .239 | .78 | " |
| 2.10 | 2.51 | 4.50 | 1.69 | .90 | .84 | .238 | .77 | " |
| 2.08 | 2.50 | 4.85 | 1.84 | .90 | .86 | .236 | .77 | " |
| 2.52 | 2.94 | 3.70 | 1.85 | .90 | .75 | .193 | .77 | A179 |
| 2.48 | 2.94 | 3.99 | 1.46 | .88 | .76 | .190 | .76 | " |
| 2.45 | 2.97 | 4.16 | 1.52 | .86 | .76 | .183 | .75 | " |
| 2.90 | 3.52 | 3.73 | 1.33 | .86 | .70 | .143 | .76 | A181 |
| 2.83 | 3.54 | 3.95 | 1.42 | .84 | .71 | .138 | .75 | " |
| 2.82 | 3.50 | 4.41 | 1.59 | .83 | .73 | .136 | .75 | " |
| 3.24 | 4.10 | 4.00 | 1.42 | .82 | .68 | .110 | .73 | A183 |
| 3.20 | 4.08 | 4.37 | 1.56 | .81 | .70 | .109 | .73 | " |
| 3.16 | 4.07 | 4.71 | 1.69 | .80 | .71 | .108 | .73 | " |
| 3.58 | 4.67 | 4.34 | 1.53 | .79 | .67 | .087 | .73 | A185 |
| 3.54 | 4.63 | 4.73 | 1.68 | .79 | .68 | .087 | .73 | " |
| 3.50 | 4.61 | 5.09 | 1.82 | .78 | .70 | .086 | .72 | " |

*Top Guard Angle.

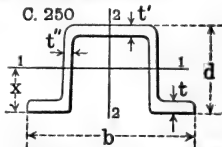
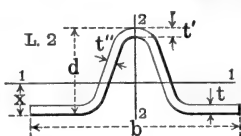


PROPERTIES OF STANDARD BULB ANGLES.

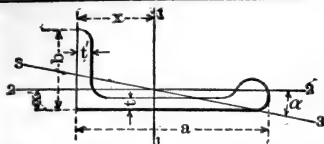
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|-----------------|------------|------------------|------------------|------------------------|-------------------------|-----------------------------|---------------------------|
| Section Number. | Size. | Weight per Foot. | Area of Section. | Thickness of Bulb Leg. | Thickness of Plain Leg. | Moment of Inertia Axis 1-1. | Section Modulus Axis 1-1. |
| | a x b | | A | t | t' | I | S. |
| | Inches. | Lbs. | Sq. Ins. | Ins. | Ins. | Ins. ⁴ | Ins. ³ |
| A 187 | 6 x 3 | 12.2 | 3.58 | .350 | | 16.6 | 4.9 |
| " (BSBA 4) | " | 12.8 | 3.76 | .375 | | 17.4 | 5.1 |
| " | " | 14.1 | 4.14 | .425 | .375 | 18.8 | 5.5 |
| " | " | 15.6 | 4.58 | .475 | | 20.2 | 5.9 |
| A 188 | 7 x 3 1/2 | 15.3 | 4.50 | .375 | | 28.6 | 7.2 |
| " (BSBA 8) | " | 16.8 | 4.94 | .425 | .425 | 30.9 | 7.7 |
| " | " | 18.6 | 5.46 | .475 | | 33.2 | 8.2 |
| " | " | 20.0 | 5.90 | .525 | | 35.5 | 8.8 |
| A 189 | 8 x 3 1/2 | 18.0 | 5.29 | .400 | | 43.8 | 9.8 |
| " (BSBA 12) | " | 19.6 | 5.78 | .450 | .450 | 47.1 | 10.6 |
| " | " | 21.6 | 6.34 | .500 | | 50.4 | 11.2 |
| " | " | 23.2 | 6.83 | .550 | | 53.7 | 11.9 |
| A 190 | 9 x 3 1/2 | 20.9 | 6.14 | .425 | | 63.8 | 13.1 |
| " (BSBA 16) | " | 22.7 | 6.68 | .475 | .475 | 68.4 | 13.9 |
| " | " | 24.8 | 7.29 | .525 | | 73.1 | 14.8 |
| " | " | 26.6 | 7.82 | .575 | | 77.6 | 15.6 |
| " | " | 28.6 | 8.41 | .625 | | 81.8 | 16.4 |
| A 191 | 10 x 3 1/2 | 24.9 | 7.32 | .475 | | 92.1 | 17.2 |
| " (BSBA 18) | " | 26.9 | 7.90 | .525 | .525 | 98.2 | 18.3 |
| " | " | 29.1 | 8.55 | .575 | | 104.3 | 19.2 |
| " | " | 31.1 | 9.14 | .625 | | 110.4 | 20.3 |
| " | " | 33.2 | 9.77 | .675 | | 115.9 | 21.2 |
| " | " | 35.2 | 10.35 | .725 | | 122.0 | 22.3 |

PROPERTIES OF CAR SIDE STAKE AND DOOR

SPREADER BAR SECTIONS.



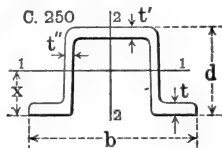
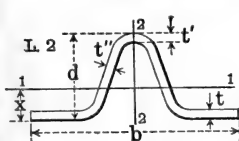
| Section Number. | Size b x d | Weight per Foot. | Area of Section. | THICKNESS | | | Moment of Inertia Axis 1-1. |
|-----------------|---------------|---------------------|---------------------|-----------|--------|----------|-----------------------------------|
| | | | | Base t | Top t' | Sides t" | |
| | Ins. | Lbs. | Sq. In. | Ins. | Ins. | Ins. | Ins. ⁴ |
| L 2 | 7 x 2 3/4 | 7.2 | 2.10 | 3/16 | 3/8 | 3/16 | 1.99 |
| " | 7 x 2 13/16 | 8.7 | 2.54 | 1/4 | 7/16 | .210 | 2.90 |
| " | 7 x 2 15/16 | 11.7 | 3.41 | 3/8 | 9/16 | .254 | 4.55 |
| C 250 | 7 1/2 x 4 | 19.8 | 5.81 | 1/2 | .483 | .320 | 11.78 |



PROPERTIES OF STANDARD BULB ANGLES.

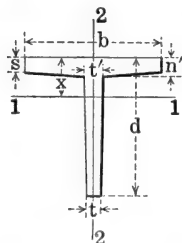
| 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 1 |
|------------------------------|--|-----------------------------|---------------------------|------------------------------|---|-------------------|------------------------------------|-----------------|
| Radius of Gyration Axis 1-1. | Distance Center of Gravity from back of Plain Leg. | Moment of Inertia Axis 2-2. | Section Modulus Axis 2-2. | Radius of Gyration Axis 2-2. | Distance Center of Gravity from back of Bulb Leg. | Tangent of Angle. | Least Radius of Gyration Axis 3-3. | Section Number. |
| r | x | I' | S' | r' | x' | a | r'' | |
| Ins. | Ins. | Ins. ⁴ | Ins. ³ | Ins. | Ins. | | Ins. | |
| 2.16 | 2.59 | 1.9 | .83 | .74 | .63 | .173 | .65 | A 187 |
| 2.15 | 2.60 | 2.1 | .87 | .74 | .64 | .174 | .65 | " (BSBA 4) |
| 2.13 | 2.60 | 2.3 | .96 | .75 | .66 | .176 | .65 | " |
| 2.10 | 2.55 | 2.5 | 1.1 | .74 | .67 | .178 | .66 | " |
| 2.52 | 2.99 | 3.4 | 1.2 | .87 | .72 | .177 | .75 | A 188 |
| 2.50 | 3.00 | 3.7 | 1.4 | .87 | .74 | .178 | .76 | " (BSBA 8) |
| 2.47 | 2.94 | 4.1 | 1.5 | .88 | .75 | .180 | .76 | " |
| 2.45 | 2.95 | 4.5 | 1.6 | .87 | .77 | .182 | .77 | " |
| 2.88 | 3.54 | 3.7 | 1.3 | .83 | .70 | .136 | .74 | A 189 |
| 2.85 | 3.54 | 4.0 | 1.4 | .84 | .71 | .136 | .75 | " (BSBA 12) |
| 2.82 | 3.48 | 4.4 | 1.6 | .83 | .73 | .138 | .75 | " |
| 2.81 | 3.49 | 4.8 | 1.7 | .84 | .75 | .139 | .76 | " |
| 3.22 | 4.10 | 3.9 | 1.4 | .80 | .68 | .105 | .73 | A 190 |
| 3.20 | 4.10 | 4.3 | 1.5 | .81 | .70 | .106 | .74 | " (BSBA 16) |
| 3.17 | 4.03 | 4.7 | 1.7 | .80 | .71 | .107 | .74 | " |
| 3.15 | 4.03 | 5.1 | 1.8 | .81 | .73 | .108 | .75 | " |
| 3.12 | 3.98 | 5.4 | 2.0 | .80 | .74 | .110 | .75 | " |
| 3.55 | 4.63 | 4.4 | 1.6 | .78 | .68 | .085 | .72 | A 191 |
| 3.53 | 4.62 | 4.8 | 1.7 | .78 | .69 | .085 | .72 | " (BSBA 18) |
| 3.49 | 4.56 | 5.1 | 1.9 | .77 | .70 | .086 | .73 | " |
| 3.48 | 4.56 | 5.6 | 2.0 | .78 | .72 | .087 | .74 | " |
| 3.44 | 4.52 | 5.8 | 2.1 | .77 | .74 | .089 | .74 | " |
| 3.43 | 4.53 | 6.3 | 2.3 | .78 | .76 | .090 | .75 | " |

PROPERTIES OF CAR SIDE STAKE AND DOOR SPREADER BAR SECTIONS.



| Section Modulus Axis 1-1. | Radius of Gyration Axis 1-1. | Distance to Center of Gravity x . | Moment of Inertia Axis 2-2. | Section Modulus Axis 2-2. | Radius of Gyration Axis 2-2. | Section Number. |
|---------------------------|------------------------------|-------------------------------------|-----------------------------|---------------------------|------------------------------|-----------------|
| Ins. ³ | Ins. | Ins. | Ins. ⁴ | Ins. ³ | Ins. | |
| 1.16 | .97 | 1.04 | 5.45 | 1.56 | 1.61 | L 2 |
| 1.53 | 1.07 | .91 | 7.23 | 2.07 | 1.69 | " |
| 2.12 | 1.15 | .79 | 10.81 | 3.09 | 1.78 | " |
| 5.77 | 1.42 | 2.04 | 26.2 | 7.00 | 2.12 | C 250 |

PROPERTIES OF T-BARS.



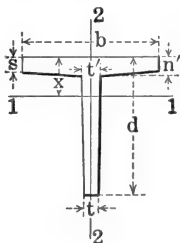
EQUAL LEGS.

| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
|----------------|-----------------|-----------------|---------------------------------|---------------------------------|-----------------|-----------------|--|----------------------------|
| Section Number | Dimensions | | | | Weight per Foot | Area of Section | Distance of Center of Gravity from Outside of Flange | Moment of Inertia Axis 1-1 |
| | Width of Flange | Depth of Bar | Thickness of Flange | Thickness of Stem | | | | |
| | b | d | s to n' | t to t' | | A | x | I |
| | Inches | Inches | Inch | Inch | Pounds | Sq. Ins. | Inch | Inches ⁴ |
| T 5 | 1 | 1 | $\frac{1}{8}$ to $\frac{5}{32}$ | $\frac{1}{8}$ to $\frac{5}{32}$ | .89 | .26 | .29 | .02 |
| T181 | $1\frac{1}{8}$ | $1\frac{1}{8}$ | $\frac{3}{16}$ " $\frac{1}{4}$ | $\frac{3}{32}$ " $\frac{7}{32}$ | 1.37 | .40 | .33 | .04 |
| T183 | $1\frac{3}{16}$ | $1\frac{3}{16}$ | $\frac{3}{16}$ " $\frac{1}{4}$ | $\frac{3}{32}$ " $\frac{7}{32}$ | 1.51 | .44 | .34 | .05 |
| T187 | $1\frac{1}{4}$ | $1\frac{1}{4}$ | $\frac{3}{16}$ " $\frac{1}{4}$ | $\frac{3}{32}$ " $\frac{7}{32}$ | 1.60 | .47 | .36 | .06 |
| T188 | $1\frac{1}{4}$ | $1\frac{1}{4}$ | $\frac{3}{16}$ " $\frac{3}{8}$ | $\frac{3}{16}$ " $\frac{9}{32}$ | 1.70 | .50 | .40 | .07 |
| T191 | $1\frac{1}{2}$ | $1\frac{1}{2}$ | $\frac{3}{16}$ " $\frac{3}{8}$ | $\frac{3}{16}$ " $\frac{7}{32}$ | 1.94 | .57 | .44 | .11 |
| T193 | $1\frac{1}{2}$ | $1\frac{1}{2}$ | $\frac{1}{4}$ " $\frac{3}{8}$ | $\frac{1}{4}$ " $\frac{9}{32}$ | 2.47 | .73 | .47 | .15 |
| T194 | $1\frac{3}{4}$ | $1\frac{3}{4}$ | $\frac{1}{4}$ " $\frac{5}{16}$ | $\frac{1}{4}$ " $\frac{5}{16}$ | 3.09 | .91 | .54 | .23 |
| T 37 | 2 | 2 | $\frac{1}{4}$ " $\frac{5}{16}$ | $\frac{1}{4}$ " $\frac{5}{16}$ | 3.56 | 1.05 | .59 | .37 |
| T 39 | 2 | 2 | $\frac{5}{16}$ " $\frac{3}{8}$ | $\frac{5}{16}$ " $\frac{3}{8}$ | 4.3 | 1.26 | .61 | .44 |
| T 41 | $2\frac{1}{4}$ | $2\frac{1}{4}$ | $\frac{1}{4}$ " $\frac{5}{16}$ | $\frac{1}{4}$ " $\frac{5}{16}$ | 4.1 | 1.19 | .65 | .52 |
| T 42 | $2\frac{1}{4}$ | $2\frac{1}{4}$ | $\frac{5}{16}$ " $\frac{3}{8}$ | $\frac{5}{16}$ " $\frac{3}{8}$ | 4.9 | 1.43 | .68 | .65 |
| T 47 | $2\frac{1}{2}$ | $2\frac{1}{2}$ | $\frac{1}{4}$ " $\frac{5}{16}$ | $\frac{1}{4}$ " $\frac{5}{16}$ | 4.6 | 1.33 | .71 | .74 |
| T 49 | $2\frac{1}{2}$ | $2\frac{1}{2}$ | $\frac{5}{16}$ " $\frac{3}{8}$ | $\frac{5}{16}$ " $\frac{3}{8}$ | 5.5 | 1.60 | .74 | .88 |

UNEQUAL LEGS.

| | | | | | | | | |
|------|----------------|-----------------|---------------------------------|----------------------------------|------|-----|-----|-----|
| T 16 | $1\frac{1}{4}$ | $1\frac{1}{16}$ | $\frac{3}{16}$ to $\frac{1}{4}$ | $\frac{5}{32}$ to $\frac{7}{32}$ | 1.48 | .43 | .30 | .04 |
| T 18 | $1\frac{1}{4}$ | $1\frac{1}{8}$ | $\frac{3}{16}$ " $\frac{1}{4}$ | $\frac{3}{16}$ " $\frac{1}{4}$ | 1.56 | .46 | .34 | .05 |
| T 20 | $1\frac{1}{2}$ | $1\frac{1}{4}$ | $\frac{1}{8}$ " $\frac{5}{32}$ | $\frac{1}{8}$ " $\frac{5}{32}$ | 1.25 | .37 | .33 | .05 |

PROPERTIES OF T-BARS.



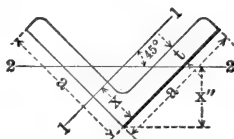
EQUAL LEGS.

| 10 | 11 | 12 | 13 | 14 | 15 | 16 | 1 |
|--------------------------------|-----------------------------------|----------------------------------|--------------------------------|-----------------------------------|---|--|-------------------|
| Section Modulus Axis 1-1 | Radius of Gyration Axis 1-1 | Moment of Inertia Axis 2-2 | Section Modulus Axis 2-2 | Radius of Gyration Axis 2-2 | Coef. of Strength | | Section Number |
| | | | | | For Fibre Stress of 16 000 Lbs. per Square Inch. | For Fibre Stress of 12 500 Lbs. per Square Inch | |
| S | r | I' | S' | r' | | | |
| Inches ³ | Inch | Inches ⁴ | Inches ³ | Inch | F | F' | |
| .03 | .30 | .01 | .02 | .21 | 320 | 250 | T 5 |
| .05 | .31 | .02 | .04 | .24 | 530 | 410 | T181 |
| .06 | .33 | .03 | .05 | .26 | 610 | 480 | T183 |
| .06 | .35 | .03 | .05 | .27 | 680 | 530 | T187 |
| .08 | .37 | .03 | .05 | .26 | 820 | 640 | T188 |
| .11 | .45 | .06 | .08 | .32 | 1170 | 910 | T191 |
| .14 | .45 | .08 | .10 | .32 | 1490 | 1160 | T193 |
| .19 | .51 | .12 | .14 | .37 | 2020 | 1580 | T194 |
| .26 | .59 | .18 | .18 | .42 | 2770 | 2160 | T 37 |
| .31 | .59 | .23 | .23 | .43 | 3300 | 2580 | T 39 |
| .32 | .66 | .25 | .22 | .46 | 3410 | 2660 | T 41 |
| .41 | .67 | .33 | .29 | .48 | 4370 | 3410 | T 42 |
| .42 | .75 | .34 | .27 | .51 | 4420 | 3450 | T 47 |
| .50 | .74 | .44 | .35 | .52 | 5330 | 4160 | T 49 |

UNEQUAL LEGS.

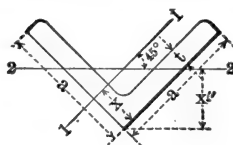
| | | | | | | | |
|-----|-----|-----|-----|-----|-----|-----|-------------|
| .05 | .29 | .03 | .05 | .28 | 500 | 390 | T 16 |
| .06 | .32 | .03 | .05 | .27 | 640 | 500 | T 18 |
| .05 | .37 | .04 | .05 | .32 | 530 | 410 | T 20 |

PROPERTIES OF STANDARD ANGLES. EQUAL LEGS.



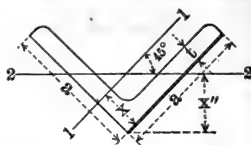
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|--------------------|--------------|------------|------------------------|------------------------|---|-----------------------------------|---------------------------------|
| Section Number. | Dimensions. | Thickness. | Weight per Foot. | Area of Section. | Distance of Center of Gravity from Back of Leg. | Moment of Inertia Axis 1-1. | Section Modulus Axis 1-1. |
| | a x a | t | | A | x | I | S |
| | Inches. | Inch. | | Sq. Ins. | Inch. | Inches. ⁴ | Inches. ³ |
| A11 | 1½ x 1½ | ⅛ | 1.23 | .36 | .42 | .08 | .072 |
| " | " | ⅜ | 1.80 | .53 | .44 | .11 | .104 |
| " | " | ¼ | 2.34 | .69 | .47 | .14 | .134 |
| " | " | ⅝ | 2.86 | .84 | .49 | .16 | .162 |
| " | " | ⅜ | 3.35 | .98 | .51 | .19 | .188 |
| A15 | 2 x 2 | ⅛ | 1.65 | .48 | .55 | .19 | .13 |
| " | " | ⅜ | 2.44 | .72 | .57 | .27 | .19 |
| " | " | ¼ | 3.19 | .94 | .59 | .35 | .25 |
| " | " | ⅝ | 3.92 | 1.15 | .61 | .42 | .30 |
| " | " | ⅜ | 4.7 | 1.36 | .64 | .48 | .35 |
| " | " | ⅞ | 5.3 | 1.56 | .66 | .54 | .40 |
| " | " | ½ | 6.0 | 1.75 | .68 | .59 | .45 |
| A17 | 2½ x 2½ | ⅛ | 2.08 | .61 | .67 | .38 | .20 |
| " | " | ⅜ | 3.07 | .90 | .69 | .55 | .30 |
| " | " | ¼ | 4.1 | 1.19 | .72 | .70 | .39 |
| " | " | ⅝ | 5.0 | 1.47 | .74 | .85 | .48 |
| " | " | ⅜ | 5.9 | 1.73 | .76 | .98 | .57 |
| " | " | ⅞ | 6.8 | 2.00 | .78 | 1.11 | .65 |
| " | " | ½ | 7.7 | 2.25 | .81 | 1.23 | .73 |
| A19 | 3 x 3 | ¼ | 4.9 | 1.44 | .84 | 1.24 | .58 |
| " | " | ⅝ | 6.1 | 1.78 | .87 | 1.51 | .71 |
| " | " | ⅜ | 7.2 | 2.11 | .89 | 1.76 | .83 |
| " | " | ⅞ | 8.3 | 2.43 | .91 | 1.99 | .95 |
| " | " | ½ | 9.4 | 2.75 | .93 | 2.22 | 1.07 |
| " | " | ⅝ | 10.4 | 3.06 | .95 | 2.43 | 1.19 |

PROPERTIES OF STANDARD ANGLES. EQUAL LEGS.



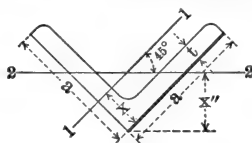
| 9 | 10 | 11 | 12 | 13 | 1 |
|---------------------------------|---|--------------------------------------|------------------------------|---------------------------------------|-----------------|
| Radius of Gyration Axis 1-1. | Distance of Center of Gravity from External Apex. | Least Moment of Inertia Axis 2-2. | Section Modulus Axis 2-2. | Least Radius of Gyration Axis 2-2. | Section Number. |
| r | x'' | I'' | S'' | r'' | |
| Inch. | Inches. | Inches. ⁴ | Inches. ³ | Inch. | |
| .47 | .60 | .031 | .053 | .30 | A11 |
| .46 | .63 | .045 | .072 | .29 | " |
| .45 | .66 | .058 | .088 | .29 | " |
| .44 | .69 | .070 | .101 | .29 | " |
| .44 | .72 | .082 | .114 | .29 | " |
| .63 | .78 | .08 | .10 | .40 | A15 |
| .62 | .80 | .11 | .14 | .39 | " |
| .61 | .84 | .14 | .17 | .39 | " |
| .60 | .87 | .17 | .20 | .39 | " |
| .59 | .90 | .20 | .22 | .39 | " |
| .59 | .93 | .23 | .25 | .38 | " |
| .58 | .96 | .26 | .27 | .38 | " |
| .79 | .95 | .15 | .16 | .50 | A17 |
| .78 | .98 | .22 | .22 | .49 | " |
| .77 | 1.01 | .29 | .28 | .49 | " |
| .76 | 1.05 | .35 | .33 | .49 | " |
| .75 | 1.08 | .41 | .38 | .48 | " |
| .75 | 1.11 | .46 | .42 | .48 | " |
| .74 | 1.14 | .52 | .46 | .48 | " |
| .93 | 1.19 | .50 | .42 | .59 | A19 |
| .92 | 1.22 | .61 | .50 | .59 | " |
| .91 | 1.26 | .72 | .57 | .58 | " |
| .91 | 1.29 | .82 | .64 | .58 | " |
| .90 | 1.32 | .92 | .70 | .58 | " |
| .89 | 1.35 | 1.02 | .76 | .58 | " |

**PROPERTIES OF
STANDARD ANGLES.
EQUAL LEGS.**



| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|-----------------|---------------|------------|------------------|------------------|---|-----------------------------|---------------------------|
| Section Number. | Dimensions. | Thickness. | Weight per Foot. | Area of Section. | Distance of Center of Gravity from Back of Leg. | Moment of Inertia Axis 1-1. | Section Modulus Axis 1-1. |
| | a x a | t | | A | x | I | S |
| | Inches. | Inch. | Pounds. | Sq. Ins. | Inches. | Inches. ⁴ | Inches. ³ |
| A21 | 3 1/2 x 3 1/2 | 1/4 | 5.8 | 1.69 | .97 | 2.01 | .79 |
| " | " | 3/8 | 7.2 | 2.09 | .99 | 2.45 | .98 |
| " | " | 1/2 | 8.5 | 2.48 | 1.01 | 2.87 | 1.16 |
| " | " | 5/8 | 9.8 | 2.87 | 1.04 | 3.26 | 1.32 |
| " | " | 3/4 | 11.1 | 3.25 | 1.06 | 3.64 | 1.49 |
| " | " | 7/8 | 12.4 | 3.62 | 1.08 | 3.99 | 1.65 |
| " | " | 1 | 13.6 | 3.98 | 1.10 | 4.33 | 1.81 |
| " | " | 1 1/8 | 14.8 | 4.34 | 1.12 | 4.65 | 1.96 |
| " | " | 1 1/4 | 16.0 | 4.69 | 1.15 | 4.96 | 2.11 |
| " | " | 1 1/2 | 17.1 | 5.03 | 1.17 | 5.25 | 2.25 |
| " | " | 1 3/8 | 18.3 | 5.36 | 1.19 | 5.53 | 2.39 |
| A23 | 4 x 4 | 1/4 | 8.2 | 2.40 | 1.12 | 3.71 | 1.29 |
| " | " | 3/8 | 9.8 | 2.86 | 1.14 | 4.36 | 1.52 |
| " | " | 1/2 | 11.3 | 3.31 | 1.16 | 4.97 | 1.75 |
| " | " | 5/8 | 12.8 | 3.75 | 1.18 | 5.56 | 1.97 |
| " | " | 3/4 | 14.3 | 4.18 | 1.21 | 6.12 | 2.19 |
| " | " | 7/8 | 15.7 | 4.61 | 1.23 | 6.66 | 2.40 |
| " | " | 1 | 17.1 | 5.03 | 1.25 | 7.17 | 2.61 |
| " | " | 1 1/8 | 18.5 | 5.44 | 1.27 | 7.66 | 2.81 |
| " | " | 1 1/4 | 19.9 | 5.84 | 1.29 | 8.14 | 3.01 |
| " | " | 1 1/2 | 21.2 | 6.23 | 1.31 | 8.59 | 3.20 |
| A27 | 6 x 6 | 3/8 | 14.9 | 4.36 | 1.64 | 15.39 | 3.53 |
| " | " | 1/2 | 17.2 | 5.06 | 1.66 | 17.68 | 4.07 |
| " | " | 5/8 | 19.6 | 5.75 | 1.68 | 19.91 | 4.61 |
| " | " | 3/4 | 21.9 | 6.43 | 1.71 | 22.07 | 5.14 |
| " | " | 7/8 | 24.2 | 7.11 | 1.73 | 24.16 | 5.66 |
| " | " | 1 | 26.5 | 7.78 | 1.75 | 26.19 | 6.17 |
| " | " | 1 1/8 | 28.7 | 8.44 | 1.78 | 28.15 | 6.66 |
| " | " | 1 1/4 | 31.0 | 9.09 | 1.80 | 30.06 | 7.15 |
| " | " | 1 1/2 | 33.1 | 9.73 | 1.82 | 31.92 | 7.63 |
| " | " | 1 3/8 | 35.3 | 10.37 | 1.84 | 33.72 | 8.11 |
| " | " | 1 | 37.4 | 11.00 | 1.86 | 35.46 | 8.57 |
| A35 | 8 x 8 | 1/2 | 26.4 | 7.75 | 2.19 | 48.65 | 8.37 |
| " | " | 3/4 | 29.6 | 8.68 | 2.21 | 54.09 | 9.34 |
| " | " | 5/8 | 32.7 | 9.61 | 2.23 | 59.43 | 10.30 |
| " | " | 1 | 35.8 | 10.53 | 2.25 | 64.64 | 11.25 |
| " | " | 1 1/8 | 38.9 | 11.44 | 2.28 | 69.74 | 12.18 |
| " | " | 1 1/4 | 42.0 | 12.34 | 2.30 | 74.72 | 13.11 |
| " | " | 1 1/2 | 45.0 | 13.23 | 2.32 | 79.58 | 14.02 |
| " | " | 1 3/8 | 48.1 | 14.12 | 2.34 | 84.34 | 14.91 |
| " | " | 1 | 51.0 | 15.00 | 2.37 | 88.98 | 15.80 |
| " | " | 1 1/8 | 54.0 | 15.87 | 2.39 | 93.53 | 16.67 |
| " | " | 1 1/4 | 56.9 | 16.73 | 2.41 | 97.97 | 17.53 |

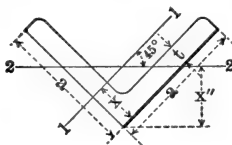
**PROPERTIES OF
STANDARD ANGLES.
EQUAL LEGS.**



| 9 | 10 | 11 | 12 | 13 | 1 |
|------------------------------|---|-----------------------------------|---------------------------|------------------------------------|-----------------|
| Radius of Gyration Axis 1-1. | Distance of Center of Gravity from External Apex. | Least Moment of Inertia Axis 2-2. | Section Modulus Axis 2-2. | Least Radius of Gyration Axis 2-2. | Section Number. |
| r | x'' | I'' | S'' | r'' | |
| Inches. | Inches. | Inches. ⁴ | Inches. ³ | Inch. | |
| 1.09 | 1.37 | .80 | .59 | .69 | A21 |
| 1.08 | 1.40 | .99 | .71 | .69 | " |
| 1.07 | 1.43 | 1.16 | .81 | .68 | " |
| 1.07 | 1.46 | 1.33 | .91 | .68 | " |
| 1.06 | 1.50 | 1.50 | 1.00 | .68 | " |
| 1.05 | 1.53 | 1.66 | 1.09 | .68 | " |
| 1.04 | 1.56 | 1.82 | 1.17 | .68 | " |
| 1.04 | 1.59 | 1.97 | 1.24 | .67 | " |
| 1.03 | 1.62 | 2.13 | 1.31 | .67 | " |
| 1.02 | 1.65 | 2.28 | 1.38 | .67 | " |
| 1.02 | 1.68 | 2.43 | 1.45 | .67 | " |
| 1.24 | 1.58 | 1.50 | .95 | .79 | A23 |
| 1.23 | 1.61 | 1.77 | 1.10 | .79 | " |
| 1.23 | 1.64 | 2.02 | 1.23 | .78 | " |
| 1.22 | 1.67 | 2.28 | 1.36 | .78 | " |
| 1.21 | 1.71 | 2.52 | 1.48 | .78 | " |
| 1.20 | 1.74 | 2.76 | 1.59 | .77 | " |
| 1.19 | 1.77 | 3.00 | 1.70 | .77 | " |
| 1.19 | 1.80 | 3.23 | 1.80 | .77 | " |
| 1.18 | 1.83 | 3.46 | 1.89 | .77 | " |
| 1.17 | 1.86 | 3.69 | 1.99 | .77 | " |
| 1.88 | 2.32 | 6.19 | 2.67 | 1.19 | A27 |
| 1.87 | 2.34 | 7.13 | 3.04 | 1.19 | " |
| 1.86 | 2.38 | 8.04 | 3.37 | 1.18 | " |
| 1.85 | 2.41 | 8.94 | 3.70 | 1.18 | " |
| 1.84 | 2.45 | 9.81 | 4.01 | 1.17 | " |
| 1.83 | 2.48 | 10.67 | 4.31 | 1.17 | " |
| 1.83 | 2.51 | 11.52 | 4.59 | 1.17 | " |
| 1.82 | 2.54 | 12.35 | 4.86 | 1.17 | " |
| 1.81 | 2.57 | 13.17 | 5.12 | 1.16 | " |
| 1.80 | 2.60 | 13.98 | 5.37 | 1.16 | " |
| 1.80 | 2.64 | 14.78 | 5.61 | 1.16 | " |
| 2.51 | 3.09 | 19.56 | 6.33 | 1.59 | A35 |
| 2.50 | 3.12 | 21.79 | 6.98 | 1.58 | " |
| 2.49 | 3.16 | 23.97 | 7.60 | 1.58 | " |
| 2.48 | 3.19 | 26.13 | 8.20 | 1.58 | " |
| 2.47 | 3.22 | 28.24 | 8.77 | 1.57 | " |
| 2.46 | 3.25 | 30.33 | 9.33 | 1.57 | " |
| 2.45 | 3.28 | 32.38 | 9.86 | 1.56 | " |
| 2.44 | 3.32 | 34.40 | 10.38 | 1.56 | " |
| 2.44 | 3.35 | 36.40 | 10.88 | 1.56 | " |
| 2.43 | 3.38 | 38.38 | 11.36 | 1.56 | " |
| 2.42 | 3.41 | 40.33 | 11.83 | 1.55 | " |

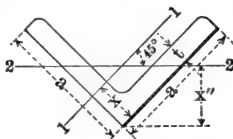
PROPERTIES OF SPECIAL ANGLES.

EQUAL LEGS.



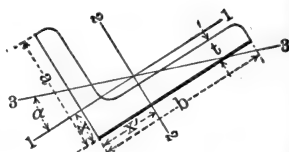
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|-----------------|------------------------------------|----------------|------------------|------------------|---|-----------------------------|---------------------------|
| Section Number. | Dimensions. | Thickness | Weight per Foot. | Area of Section. | Distance of Center of Gravity from Back of Leg. | Moment of Inertia Axis 1-1. | Section Modulus Axis 1-1. |
| | $a \times a$ | t | | A | x | I | S |
| | Inches. | Inch. | Pounds. | Sq. Ins. | Inch. | Inches. ⁴ | Inches. ³ |
| A36 | $\frac{3}{4} \times \frac{3}{4}$ | $\frac{1}{8}$ | .59 | .17 | .23 | .009 | .017 |
| " | " | $\frac{1}{4}$ | .84 | .25 | .25 | .012 | .024 |
| A37 | 1×1 | $\frac{1}{8}$ | .80 | .23 | .30 | .022 | .031 |
| " | " | $\frac{3}{16}$ | 1.16 | .34 | .32 | .030 | .044 |
| " | " | $\frac{1}{4}$ | 1.49 | .44 | .34 | .037 | .056 |
| A38 | $1\frac{1}{4} \times 1\frac{1}{4}$ | $\frac{1}{8}$ | 1.01 | .30 | .36 | .044 | .049 |
| " | " | $\frac{1}{4}$ | 1.48 | .43 | .38 | .061 | .071 |
| " | " | $\frac{1}{2}$ | 1.92 | .56 | .40 | .077 | .091 |
| A40 | $1\frac{3}{4} \times 1\frac{3}{4}$ | $\frac{1}{8}$ | 1.44 | .42 | .48 | .13 | .10 |
| " | " | $\frac{1}{4}$ | 2.12 | .62 | .51 | .18 | .14 |
| " | " | $\frac{1}{2}$ | 2.77 | .81 | .53 | .23 | .19 |
| " | " | $\frac{3}{8}$ | 3.39 | 1.00 | .55 | .27 | .23 |
| " | " | $\frac{1}{2}$ | 3.99 | 1.17 | .57 | .31 | .26 |
| A41 | $2\frac{1}{4} \times 2\frac{1}{4}$ | $\frac{1}{8}$ | 2.75 | .81 | .63 | .39 | .24 |
| " | " | $\frac{1}{4}$ | 3.62 | 1.06 | .65 | .50 | .32 |
| " | " | $\frac{1}{2}$ | 4.5 | 1.31 | .68 | .61 | .39 |
| A43 | $2\frac{3}{4} \times 2\frac{3}{4}$ | $\frac{1}{4}$ | 4.5 | 1.31 | .78 | .95 | .48 |
| " | " | $\frac{3}{8}$ | 5.6 | 1.62 | .80 | 1.15 | .59 |
| " | " | $\frac{1}{2}$ | 6.6 | 1.92 | .82 | 1.33 | .69 |
| A47 | 5×5 | $\frac{3}{8}$ | 12.3 | 3.61 | 1.39 | 8.74 | 2.42 |
| " | " | $\frac{1}{2}$ | 14.3 | 4.18 | 1.41 | 10.02 | 2.79 |
| " | " | $\frac{1}{2}$ | 16.2 | 4.75 | 1.43 | 11.25 | 3.16 |
| " | " | $\frac{3}{4}$ | 18.1 | 5.31 | 1.46 | 12.44 | 3.51 |
| " | " | $\frac{5}{8}$ | 20.0 | 5.86 | 1.48 | 13.58 | 3.86 |
| " | " | $\frac{1}{2}$ | 21.8 | 6.40 | 1.50 | 14.68 | 4.20 |
| " | " | $\frac{3}{4}$ | 23.6 | 6.94 | 1.52 | 15.74 | 4.52 |

PROPERTIES OF SPECIAL ANGLES.
EQUAL LEGS.



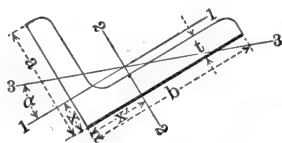
| 9 | 10 | 11 | 12 | 13 | 1 |
|---------------------------------------|--|---|---------------------------------|--|--------------------|
| Radius of Gyration Axis 1-1. | Distance of Center of Gravity from External Apex. | Least Moment of Inertia Axis 2-2. | Section Modulus Axis 2-2. | Least Radius of Gyration Axis 2-2. | Section Number. |
| r | x'' | I'' | S'' | r'' | |
| Inch. | Inch. | Inches. ⁴ | Inches. ³ | Inch. | |
| .22 | .33 | .004 | .011 | .14 | A36 |
| .22 | .36 | .005 | .014 | .14 | " |
| .30 | .42 | .009 | .021 | .19 | A37 |
| .30 | .45 | .013 | .028 | .19 | " |
| .29 | .48 | .016 | .034 | .19 | " |
| .38 | .51 | .018 | .035 | .24 | A38 |
| .38 | .54 | .025 | .047 | .24 | " |
| .37 | .57 | .033 | .057 | .24 | " |
| .55 | .68 | .051 | .076 | .35 | A40 |
| .54 | .72 | .073 | .10 | .34 | " |
| .53 | .75 | .094 | .13 | .34 | " |
| .52 | .78 | .113 | .15 | .34 | " |
| .51 | .81 | .133 | .16 | .34 | " |
| .70 | .89 | .16 | .18 | .44 | A41 |
| .69 | .92 | .21 | .22 | .44 | " |
| .68 | .96 | .25 | .26 | .44 | " |
| .85 | 1.10 | .33 | .35 | .54 | A43 |
| .84 | 1.13 | .47 | .41 | .54 | " |
| .83 | 1.17 | .55 | .47 | .53 | " |
| 1.56 | 1.96 | 3.53 | 1.79 | .99 | A47 |
| 1.55 | 2.00 | 4.05 | 2.03 | .98 | " |
| 1.54 | 2.03 | 4.56 | 2.25 | .98 | " |
| 1.53 | 2.06 | 5.06 | 2.46 | .98 | " |
| 1.52 | 2.09 | 5.55 | 2.66 | .97 | " |
| 1.51 | 2.12 | 6.03 | 2.84 | .97 | " |
| 1.50 | 2.15 | 6.53 | 3.04 | .97 | " |

PROPERTIES OF
STANDARD ANGLES.
UNEQUAL LEGS.



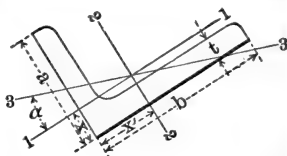
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|-----------------|-------------|-----------|------------------|------------------|--|-----------------------------|---------------------------|
| Section Number. | Dimensions. | Thickness | Weight per Foot. | Area of Section. | Distance of Center of Gravity from Back of Longer Leg. | Moment of Inertia Axis 1-1. | Section Modulus Axis 1-1. |
| | b x a | t | | A | x | I | S |
| | Inches. | Inch. | Pounds. | Sq. Ins. | Inch. | Inches. ⁴ | Inches. ³ |
| A91 | 2½ x 2 | ⅜ | 2.75 | .81 | .51 | .29 | .20 |
| " | " | ¼ | 3.62 | 1.06 | .54 | .37 | .25 |
| " | " | ⅜ | 4.5 | 1.31 | .56 | .45 | .31 |
| " | " | ⅝ | 5.3 | 1.55 | .58 | .51 | .36 |
| " | " | ⅞ | 6.1 | 1.78 | .60 | .58 | .41 |
| " | " | 1½ | 6.8 | 2.00 | .63 | .64 | .46 |
| A93 | 3 x 2½ | ¼ | 4.5 | 1.31 | .66 | .74 | .40 |
| " | " | ⅜ | 5.6 | 1.62 | .68 | .90 | .49 |
| " | " | ⅝ | 6.6 | 1.92 | .71 | 1.04 | .58 |
| " | " | ⅞ | 7.6 | 2.22 | .73 | 1.18 | .66 |
| " | " | 1½ | 8.5 | 2.50 | .75 | 1.30 | .74 |
| " | " | 1⅞ | 9.5 | 2.78 | .77 | 1.42 | .82 |
| A95 | 3½ x 2½ | ¼ | 4.9 | 1.44 | .61 | .78 | .41 |
| " | " | ⅜ | 6.1 | 1.78 | .64 | .94 | .50 |
| " | " | ⅝ | 7.2 | 2.11 | .66 | 1.09 | .59 |
| " | " | ⅞ | 8.3 | 2.43 | .68 | 1.23 | .68 |
| " | " | 1½ | 9.4 | 2.75 | .70 | 1.36 | .76 |
| " | " | 1⅞ | 10.4 | 3.06 | .73 | 1.49 | .84 |
| A97 | 3½ x 3 | ¼ | 5.4 | 1.56 | .79 | 1.30 | .58 |
| " | " | ⅜ | 6.6 | 1.93 | .81 | 1.58 | .72 |
| " | " | ⅝ | 7.9 | 2.30 | .83 | 1.85 | .85 |
| " | " | ⅞ | 9.1 | 2.65 | .85 | 2.09 | .98 |
| " | " | 1½ | 10.2 | 3.00 | .88 | 2.33 | 1.10 |
| " | " | 1⅞ | 11.4 | 3.34 | .90 | 2.55 | 1.21 |
| " | " | 2 | 12.5 | 3.67 | .92 | 2.76 | 1.33 |
| " | " | 2½ | 13.6 | 4.00 | .94 | 2.96 | 1.44 |
| " | " | 3 | 14.7 | 4.31 | .96 | 3.15 | 1.54 |
| " | " | 3½ | 15.8 | 4.62 | .98 | 3.33 | 1.65 |
| " | " | 4 | 16.8 | 4.92 | 1.00 | 3.50 | 1.75 |
| A99 | 4 x 3 | ⅜ | 7.2 | 2.09 | .76 | 1.65 | .73 |
| " | " | ⅝ | 8.5 | 2.48 | .78 | 1.92 | .87 |
| " | " | ⅞ | 9.8 | 2.87 | .80 | 2.18 | .99 |
| " | " | 1½ | 11.1 | 3.25 | .83 | 2.42 | 1.12 |
| " | " | 1⅞ | 12.4 | 3.62 | .85 | 2.66 | 1.23 |
| " | " | 2 | 13.6 | 3.98 | .87 | 2.87 | 1.35 |
| " | " | 2½ | 14.8 | 4.34 | .89 | 3.08 | 1.46 |
| " | " | 3 | 16.0 | 4.69 | .92 | 3.28 | 1.57 |
| " | " | 3½ | 17.1 | 5.03 | .94 | 3.47 | 1.68 |
| " | " | 4 | 18.3 | 5.36 | .96 | 3.66 | 1.79 |

**PROPERTIES OF
STANDARD ANGLES.
UNEQUAL LEGS.**



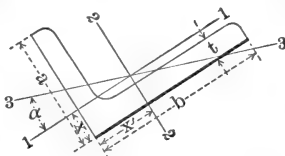
| 9 | 10 | 11 | 12 | 13 | 14 | 15 | 1 |
|------------------------------|---|-----------------------------|---------------------------|------------------------------|-------------------|------------------------------------|-----------------|
| Radius of Gyration Axis 1-1. | Distance of Center of Gravity from back of Shorter Leg. | Moment of Inertia Axis 2-2. | Section Modulus Axis 2-2. | Radius of Gyration Axis 2-2. | Tangent of Angle. | Least Radius of Gyration Axis 3-3. | Section Number. |
| r | x' | I' | S' | r' | α | r'' | |
| Inch. | Inch. | Inches. ⁴ | Inches. ³ | Inches. | | Inch. | |
| .60 | .76 | .51 | .29 | .79 | .632 | .43 | A91 |
| .59 | .79 | .65 | .38 | .78 | .626 | .42 | " |
| .58 | .81 | .79 | .47 | .78 | .620 | .42 | " |
| .58 | .83 | .91 | .55 | .77 | .614 | .42 | " |
| .57 | .85 | 1.03 | .62 | .76 | .607 | .42 | " |
| .56 | .88 | 1.14 | .70 | .75 | .600 | .42 | " |
| .75 | .91 | 1.17 | .56 | .95 | .684 | .53 | A93 |
| .74 | .93 | 1.42 | .69 | .94 | .680 | .53 | " |
| .74 | .96 | 1.66 | .81 | .93 | .676 | .52 | " |
| .73 | .98 | 1.88 | .93 | .92 | .672 | .52 | " |
| .72 | 1.00 | 2.08 | 1.04 | .91 | .666 | .52 | " |
| .72 | 1.02 | 2.28 | 1.15 | .91 | .661 | .52 | " |
| .74 | 1.11 | 1.80 | .75 | 1.12 | .506 | .54 | A95 |
| .73 | 1.14 | 2.19 | .93 | 1.11 | .501 | .54 | " |
| .72 | 1.16 | 2.56 | 1.09 | 1.10 | .496 | .54 | " |
| .71 | 1.18 | 2.91 | 1.26 | 1.09 | .491 | .54 | " |
| .70 | 1.20 | 3.24 | 1.41 | 1.09 | .486 | .53 | " |
| .70 | 1.23 | 3.55 | 1.56 | 1.08 | .480 | .53 | " |
| .91 | 1.04 | 1.91 | .78 | 1.11 | .727 | .63 | A97 |
| .90 | 1.06 | 2.33 | .95 | 1.10 | .724 | .63 | " |
| .90 | 1.08 | 2.72 | 1.13 | 1.09 | .721 | .62 | " |
| .89 | 1.10 | 3.10 | 1.29 | 1.08 | .718 | .62 | " |
| .88 | 1.13 | 3.45 | 1.45 | 1.07 | .714 | .62 | " |
| .87 | 1.15 | 3.79 | 1.61 | 1.07 | .711 | .62 | " |
| .87 | 1.17 | 4.11 | 1.76 | 1.06 | .707 | .62 | " |
| .86 | 1.19 | 4.41 | 1.91 | 1.05 | .703 | .62 | " |
| .85 | 1.21 | 4.70 | 2.05 | 1.04 | .698 | .62 | " |
| .85 | 1.23 | 4.98 | 2.20 | 1.04 | .694 | .62 | " |
| .84 | 1.25 | 5.24 | 2.33 | 1.03 | .689 | .63 | " |
| .89 | 1.26 | 3.38 | 1.23 | 1.27 | .554 | .65 | A99 |
| .88 | 1.28 | 3.96 | 1.46 | 1.26 | .551 | .64 | " |
| .87 | 1.30 | 4.52 | 1.68 | 1.25 | .547 | .64 | " |
| .86 | 1.33 | 5.05 | 1.89 | 1.25 | .543 | .64 | " |
| .86 | 1.35 | 5.55 | 2.09 | 1.24 | .538 | .64 | " |
| .85 | 1.37 | 6.03 | 2.30 | 1.23 | .534 | .64 | " |
| .84 | 1.39 | 6.49 | 2.49 | 1.22 | .529 | .64 | " |
| .84 | 1.42 | 6.93 | 2.68 | 1.22 | .524 | .64 | " |
| .83 | 1.44 | 7.35 | 2.87 | 1.21 | .518 | .64 | " |
| .83 | 1.46 | 7.75 | 3.05 | 1.20 | .512 | .64 | " |

**PROPERTIES OF
STANDARD ANGLES.
UNEQUAL LEGS.**



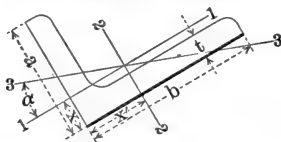
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|-----------------|--------------|---------------|------------------|------------------|--|-----------------------------|---------------------------|
| Section Number. | Dimensions. | Thickness. | Weight per Foot. | Area of Section. | Distance of Center of Gravity from Back of Longer Leg. | Moment of Inertia Axis 1-1. | Section Modulus Axis 1-1. |
| | $b \times a$ | t | | A | x | I | S |
| | Inches. | Inch. | Pounds. | Sq. Ins. | Inch. | Inches. ⁴ | Inches. ³ |
| A101 | 5 x 3 | $\frac{1}{8}$ | 8.2 | 2.40 | .68 | 1.75 | .75 |
| " | " | $\frac{1}{4}$ | 9.8 | 2.86 | .70 | 2.04 | .89 |
| " | " | $\frac{3}{8}$ | 11.3 | 3.31 | .73 | 2.32 | 1.02 |
| " | " | $\frac{1}{2}$ | 12.8 | 3.75 | .75 | 2.58 | 1.15 |
| " | " | $\frac{5}{8}$ | 14.3 | 4.18 | .77 | 2.83 | 1.27 |
| " | " | $\frac{3}{4}$ | 15.7 | 4.61 | .80 | 3.06 | 1.39 |
| " | " | $\frac{7}{8}$ | 17.1 | 5.03 | .82 | 3.29 | 1.51 |
| " | " | 1 | 18.5 | 5.44 | .84 | 3.51 | 1.62 |
| " | " | $\frac{1}{8}$ | 19.9 | 5.84 | .86 | 3.71 | 1.74 |
| " | " | $\frac{1}{4}$ | 21.2 | 6.23 | .88 | 3.91 | 1.85 |
| A103 | 5 x 3½ | $\frac{1}{8}$ | 8.7 | 2.56 | .84 | 2.72 | 1.02 |
| " | " | $\frac{1}{4}$ | 10.4 | 3.05 | .86 | 3.18 | 1.21 |
| " | " | $\frac{3}{8}$ | 12.0 | 3.53 | .88 | 3.63 | 1.39 |
| " | " | $\frac{1}{2}$ | 13.6 | 4.00 | .91 | 4.05 | 1.56 |
| " | " | $\frac{5}{8}$ | 15.2 | 4.47 | .93 | 4.45 | 1.73 |
| " | " | $\frac{3}{4}$ | 16.8 | 4.92 | .95 | 4.83 | 1.90 |
| " | " | $\frac{7}{8}$ | 18.3 | 5.37 | .97 | 5.20 | 2.06 |
| " | " | 1 | 19.8 | 5.81 | 1.00 | 5.55 | 2.22 |
| " | " | $\frac{1}{8}$ | 21.3 | 6.25 | 1.02 | 5.89 | 2.37 |
| " | " | $\frac{1}{4}$ | 22.7 | 6.67 | 1.04 | 6.21 | 2.52 |
| " | " | $\frac{1}{2}$ | 24.2 | 7.09 | 1.06 | 6.52 | 2.67 |
| A105 | 6 x 3½ | $\frac{3}{8}$ | 11.7 | 3.42 | .79 | 3.34 | 1.23 |
| " | " | $\frac{1}{2}$ | 13.5 | 3.97 | .81 | 3.81 | 1.41 |
| " | " | $\frac{5}{8}$ | 15.3 | 4.50 | .83 | 4.25 | 1.59 |
| " | " | $\frac{3}{4}$ | 17.1 | 5.03 | .86 | 4.67 | 1.77 |
| " | " | $\frac{7}{8}$ | 18.9 | 5.55 | .88 | 5.08 | 1.94 |
| " | " | 1 | 20.6 | 6.06 | .90 | 5.47 | 2.11 |
| " | " | $\frac{1}{8}$ | 22.4 | 6.56 | .93 | 5.84 | 2.27 |
| " | " | $\frac{1}{4}$ | 24.0 | 7.06 | .95 | 6.20 | 2.43 |
| " | " | $\frac{3}{8}$ | 25.7 | 7.55 | .97 | 6.55 | 2.59 |
| " | " | $\frac{1}{2}$ | 27.3 | 8.03 | .99 | 6.88 | 2.74 |
| " | " | 1 | 28.9 | 8.50 | 1.01 | 7.21 | 2.90 |
| A107 | 6 x 4 | $\frac{3}{8}$ | 12.3 | 3.61 | .94 | 4.90 | 1.60 |
| " | " | $\frac{1}{2}$ | 14.3 | 4.18 | .96 | 5.60 | 1.85 |
| " | " | $\frac{5}{8}$ | 16.2 | 4.75 | .99 | 6.27 | 2.08 |
| " | " | $\frac{3}{4}$ | 18.1 | 5.31 | 1.01 | 6.91 | 2.31 |
| " | " | $\frac{7}{8}$ | 20.0 | 5.86 | 1.03 | 7.52 | 2.54 |
| " | " | 1 | 21.8 | 6.40 | 1.06 | 8.11 | 2.76 |
| " | " | $\frac{1}{8}$ | 23.6 | 6.94 | 1.08 | 8.68 | 2.97 |
| " | " | $\frac{1}{4}$ | 25.4 | 7.47 | 1.10 | 9.23 | 3.18 |
| " | " | $\frac{3}{8}$ | 27.2 | 7.98 | 1.12 | 9.75 | 3.39 |
| " | " | $\frac{1}{2}$ | 28.9 | 8.50 | 1.14 | 10.26 | 3.59 |
| " | " | 1 | 30.6 | 9.00 | 1.17 | 10.75 | 3.79 |

**PROPERTIES OF
STANDARD ANGLES.
UNEQUAL LEGS.**



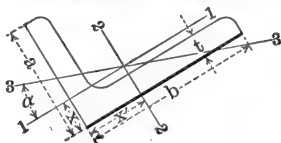
| 9 | 10 | 11 | 12 | 13 | 14 | 15 | 1 |
|------------------------------|---|-----------------------------|---------------------------|------------------------------|-------------------|------------------------------------|-----------------|
| Radius of Gyration Axis 1-1. | Distance of Center of Gravity from Back of Shorter Leg. | Moment of Inertia Axis 2-2. | Section Modulus Axis 2-2. | Radius of Gyration Axis 2-2. | Tangent of Angle. | Least Radius of Gyration Axis 3-3. | Section Number. |
| r | x' | I' | S' | r' | α | r'' | |
| Inch. | Inches. | Inches. ⁴ | Inches. ³ | Inch. | | Inch. | |
| .85 | 1.68 | 6.26 | 1.89 | 1.61 | .368 | .66 | A101 |
| .84 | 1.70 | 7.37 | 2.24 | 1.61 | .364 | .65 | " |
| .84 | 1.73 | 8.43 | 2.58 | 1.60 | .361 | .65 | " |
| .83 | 1.75 | 9.45 | 2.91 | 1.59 | .357 | .65 | " |
| .82 | 1.77 | 10.43 | 3.23 | 1.58 | .353 | .65 | " |
| .82 | 1.80 | 11.37 | 3.55 | 1.57 | .349 | .64 | " |
| .81 | 1.82 | 12.28 | 3.86 | 1.56 | .345 | .64 | " |
| .80 | 1.84 | 13.15 | 4.16 | 1.55 | .340 | .64 | " |
| .80 | 1.86 | 13.98 | 4.46 | 1.55 | .336 | .64 | " |
| .79 | 1.88 | 14.78 | 4.75 | 1.54 | .331 | .64 | " |
| 1.03 | 1.59 | 6.60 | 1.94 | 1.61 | .489 | .77 | A103 |
| 1.02 | 1.61 | 7.78 | 2.29 | 1.60 | .485 | .76 | " |
| 1.01 | 1.63 | 8.90 | 2.64 | 1.59 | .482 | .76 | " |
| 1.01 | 1.66 | 9.99 | 2.99 | 1.58 | .479 | .75 | " |
| 1.00 | 1.68 | 11.03 | 3.32 | 1.57 | .476 | .75 | " |
| .99 | 1.70 | 12.03 | 3.65 | 1.56 | .472 | .75 | " |
| .98 | 1.72 | 12.99 | 3.97 | 1.56 | .468 | .75 | " |
| .98 | 1.75 | 13.92 | 4.28 | 1.55 | .464 | .75 | " |
| .97 | 1.77 | 14.81 | 4.58 | 1.54 | .460 | .75 | " |
| .96 | 1.79 | 15.67 | 4.88 | 1.53 | .455 | .75 | " |
| .96 | 1.81 | 16.49 | 5.17 | 1.53 | .451 | .75 | " |
| .99 | 2.04 | 12.86 | 3.24 | 1.94 | .350 | .77 | A105 |
| .98 | 2.06 | 14.76 | 3.75 | 1.93 | .347 | .76 | " |
| .97 | 2.08 | 16.59 | 4.24 | 1.92 | .344 | .76 | " |
| .96 | 2.11 | 18.37 | 4.72 | 1.91 | .341 | .75 | " |
| .96 | 2.13 | 20.08 | 5.19 | 1.90 | .338 | .75 | " |
| .95 | 2.15 | 21.74 | 5.65 | 1.89 | .334 | .75 | " |
| .94 | 2.18 | 23.34 | 6.10 | 1.89 | .331 | .75 | " |
| .94 | 2.20 | 24.89 | 6.55 | 1.88 | .327 | .75 | " |
| .93 | 2.22 | 26.39 | 6.98 | 1.87 | .323 | .75 | " |
| .93 | 2.24 | 27.84 | 7.41 | 1.86 | .320 | .75 | " |
| .92 | 2.26 | 29.15 | 7.80 | 1.85 | .317 | .75 | " |
| 1.17 | 1.94 | 13.47 | 3.32 | 1.93 | .446 | .88 | A107 |
| 1.16 | 1.96 | 15.46 | 3.83 | 1.92 | .443 | .87 | " |
| 1.15 | 1.99 | 17.40 | 4.33 | 1.91 | .440 | .87 | " |
| 1.14 | 2.01 | 19.26 | 4.83 | 1.90 | .438 | .87 | " |
| 1.13 | 2.03 | 21.07 | 5.31 | 1.90 | .434 | .86 | " |
| 1.13 | 2.06 | 22.82 | 5.78 | 1.89 | .431 | .86 | " |
| 1.12 | 2.08 | 24.51 | 6.25 | 1.88 | .428 | .86 | " |
| 1.11 | 2.10 | 26.15 | 6.70 | 1.87 | .425 | .86 | " |
| 1.11 | 2.12 | 27.73 | 7.15 | 1.86 | .421 | .86 | " |
| 1.10 | 2.14 | 29.26 | 7.59 | 1.86 | .418 | .86 | " |
| 1.09 | 2.17 | 30.75 | 8.02 | 1.85 | .414 | .86 | " |

PROPERTIES OF SPECIAL ANGLES. UNEQUAL LEGS.



| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|-----------------|--------------|----------------|------------------|------------------|--|-----------------------------|---------------------------|
| Section Number. | Dimensions. | Thickness. | Weight per Foot. | Area of Section. | Distance of Center of Gravity from Back of Longer Leg. | Moment of Inertia Axis 1-1. | Section Modulus Axis 1-1. |
| | $b \times a$ | t | | A | x | I | S |
| | Inches. | Inch. | Pounds. | Sq. Ins. | Inch. | Inches. ⁴ | Inches. ³ |
| A129 | 3 x 2 | $\frac{1}{8}$ | 3.07 | .90 | .47 | .31 | .20 |
| " | " | $\frac{1}{4}$ | 4.1 | 1.19 | .49 | .39 | .26 |
| " | " | $\frac{3}{8}$ | 5.0 | 1.47 | .51 | .47 | .32 |
| " | " | $\frac{1}{2}$ | 5.9 | 1.73 | .54 | .54 | .37 |
| " | " | $\frac{3}{4}$ | 6.8 | 2.00 | .56 | .61 | .42 |
| " | " | $\frac{1}{2}$ | 7.7 | 2.25 | .58 | .67 | .47 |
| A131 | 4 x 3½ | $\frac{5}{16}$ | 7.7 | 2.25 | .93 | 2.55 | .99 |
| " | " | $\frac{3}{8}$ | 9.1 | 2.67 | .96 | 2.99 | 1.17 |
| " | " | $\frac{1}{2}$ | 10.6 | 3.09 | .98 | 3.40 | 1.35 |
| " | " | $\frac{3}{4}$ | 11.9 | 3.50 | 1.00 | 3.79 | 1.52 |
| " | " | $\frac{1}{2}$ | 13.3 | 3.90 | 1.02 | 4.17 | 1.68 |
| " | " | $\frac{3}{8}$ | 14.7 | 4.30 | 1.04 | 4.49 | 1.83 |
| " | " | $\frac{1}{2}$ | 16.0 | 4.68 | 1.07 | 4.86 | 2.00 |
| A135 | 5 x 4 | $\frac{3}{8}$ | 11.0 | 3.23 | 1.03 | 4.66 | 1.57 |
| " | " | $\frac{1}{2}$ | 12.8 | 3.75 | 1.05 | 5.32 | 1.81 |
| " | " | $\frac{3}{4}$ | 14.5 | 4.25 | 1.07 | 5.96 | 2.04 |
| " | " | $\frac{1}{2}$ | 16.2 | 4.75 | 1.10 | 6.56 | 2.26 |
| " | " | $\frac{3}{8}$ | 17.8 | 5.23 | 1.12 | 7.14 | 2.48 |
| " | " | $\frac{1}{2}$ | 19.5 | 5.72 | 1.14 | 7.70 | 2.69 |
| A109 | 7 x 3½ | $\frac{1}{8}$ | 15.0 | 4.40 | .75 | 3.95 | 1.44 |
| " | " | $\frac{1}{2}$ | 17.0 | 5.00 | .78 | 4.41 | 1.62 |
| " | " | $\frac{3}{8}$ | 19.1 | 5.59 | .80 | 4.86 | 1.80 |
| " | " | $\frac{1}{2}$ | 21.0 | 6.17 | .82 | 5.28 | 1.97 |
| " | " | $\frac{3}{4}$ | 23.0 | 6.75 | .85 | 5.69 | 2.14 |
| " | " | $\frac{1}{2}$ | 24.9 | 7.31 | .87 | 6.08 | 2.31 |
| " | " | $\frac{3}{8}$ | 26.8 | 7.87 | .89 | 6.46 | 2.48 |
| " | " | $\frac{1}{2}$ | 28.7 | 8.42 | .91 | 6.83 | 2.64 |
| " | " | $\frac{3}{8}$ | 30.5 | 8.97 | .94 | 7.18 | 2.80 |
| " | " | $\frac{1}{2}$ | 32.3 | 9.50 | .96 | 7.53 | 2.96 |
| A112 | 8 x 6 | $\frac{1}{2}$ | 23.0 | 6.75 | 1.47 | 21.68 | 4.79 |
| " | " | $\frac{3}{8}$ | 25.7 | 7.56 | 1.50 | 24.04 | 5.34 |
| " | " | $\frac{1}{2}$ | 28.5 | 8.36 | 1.52 | 26.33 | 5.88 |
| " | " | $\frac{3}{4}$ | 31.2 | 9.15 | 1.54 | 28.56 | 6.40 |
| " | " | $\frac{1}{2}$ | 33.8 | 9.94 | 1.56 | 30.72 | 6.92 |
| " | " | $\frac{3}{8}$ | 36.5 | 10.72 | 1.59 | 32.82 | 7.44 |
| " | " | $\frac{1}{2}$ | 39.1 | 11.48 | 1.61 | 34.86 | 7.94 |
| " | " | $\frac{3}{8}$ | 41.7 | 12.25 | 1.63 | 36.85 | 8.43 |
| " | " | $\frac{1}{2}$ | 44.2 | 13.00 | 1.65 | 38.78 | 8.92 |

PROPERTIES OF SPECIAL ANGLES. UNEQUAL LEGS.



| 9 | 10 | 11 | 12 | 13 | 14 | 15 | 1 |
|------------------------------|---|-----------------------------|---------------------------|------------------------------|-------------------|------------------------------|-----------------|
| Radius of Gyration Axis 1-1. | Distance of Center of Gravity from Back of Shorter Leg. | Moment of Inertia Axis 2-2. | Section Modulus Axis 2-2. | Radius of Gyration Axis 2-2. | Tangent of Angle. | Radius of Gyration Axis 3-3. | Section Number. |
| r | x' | I' | S' | r' | α | r'' | |
| Inch. | Inches. | Inches. ⁴ | Inches. ³ | Inches. | | Inch. | |
| .58 | .97 | .84 | .41 | .97 | .446 | .44 | A129 |
| .57 | .99 | 1.09 | .54 | .96 | .440 | .43 | " |
| .57 | 1.02 | 1.32 | .66 | .95 | .434 | .43 | " |
| .56 | 1.04 | 1.53 | .78 | .94 | .428 | .43 | " |
| .55 | 1.06 | 1.73 | .89 | .93 | .421 | .43 | " |
| .55 | 1.08 | 1.92 | 1.00 | .92 | .414 | .43 | " |
| 1.07 | 1.18 | 3.56 | 1.26 | 1.26 | .757 | .73 | A131 |
| 1.06 | 1.21 | 4.18 | 1.49 | 1.25 | .755 | .73 | " |
| 1.05 | 1.23 | 4.76 | 1.72 | 1.24 | .753 | .72 | " |
| 1.04 | 1.25 | 5.32 | 1.94 | 1.23 | .750 | .72 | " |
| 1.03 | 1.27 | 5.86 | 2.15 | 1.23 | .747 | .72 | " |
| 1.02 | 1.29 | 6.37 | 2.35 | 1.22 | .742 | .72 | " |
| 1.02 | 1.32 | 6.86 | 2.56 | 1.21 | .742 | .72 | " |
| 1.20 | 1.53 | 8.14 | 2.34 | 1.59 | .631 | .85 | A135 |
| 1.19 | 1.55 | 9.32 | 2.70 | 1.58 | .629 | .85 | " |
| 1.18 | 1.57 | 10.46 | 3.05 | 1.57 | .626 | .85 | " |
| 1.18 | 1.60 | 11.55 | 3.39 | 1.56 | .623 | .85 | " |
| 1.17 | 1.62 | 12.61 | 3.73 | 1.55 | .620 | .84 | " |
| 1.16 | 1.64 | 13.62 | 4.05 | 1.54 | .617 | .84 | " |
| .95 | 2.50 | 22.56 | 5.01 | 2.26 | .267 | .76 | A109 |
| .94 | 2.53 | 25.41 | 5.68 | 2.25 | .264 | .75 | " |
| .93 | 2.55 | 28.18 | 6.34 | 2.25 | .262 | .75 | " |
| .93 | 2.57 | 30.86 | 6.96 | 2.24 | .259 | .75 | " |
| .92 | 2.60 | 33.47 | 7.60 | 2.23 | .257 | .74 | " |
| .91 | 2.62 | 35.99 | 8.22 | 2.22 | .253 | .74 | " |
| .91 | 2.64 | 38.45 | 8.83 | 2.21 | .250 | .74 | " |
| .90 | 2.66 | 40.82 | 9.42 | 2.20 | .247 | .74 | " |
| .89 | 2.69 | 43.13 | 10.00 | 2.19 | .244 | .74 | " |
| .89 | 2.71 | 45.37 | 10.58 | 2.19 | .241 | .74 | " |
| 1.79 | 2.47 | 44.31 | 8.02 | 2.56 | .558 | 1.30 | A112 |
| 1.78 | 2.50 | 49.26 | 8.95 | 2.55 | .556 | 1.30 | " |
| 1.77 | 2.52 | 54.10 | 9.87 | 2.54 | .554 | 1.29 | " |
| 1.77 | 2.54 | 58.82 | 10.77 | 2.54 | .554 | 1.29 | " |
| 1.76 | 2.56 | 63.42 | 11.67 | 2.53 | .553 | 1.28 | " |
| 1.75 | 2.59 | 67.92 | 12.55 | 2.52 | .549 | 1.28 | " |
| 1.74 | 2.61 | 72.32 | 13.41 | 2.51 | .546 | 1.28 | " |
| 1.73 | 2.63 | 76.59 | 14.27 | 2.50 | .545 | 1.28 | " |
| 1.73 | 2.65 | 80.78 | 15.11 | 2.49 | .543 | 1.28 | " |

MOMENTS OF INERTIA OF RECTANGLES. I

Neutral Axis

Depths 2 to 60 inches; widths $\frac{1}{4}$ to 1 inch, varying by $\frac{1}{8}$ inch.

| Depth in Inches. | Width of Rectangle in Inches. | | | | | | |
|------------------------|-------------------------------|----------------|---------------|----------------|---------------|----------------|---------------|
| | $\frac{1}{4}$ | $\frac{5}{16}$ | $\frac{3}{8}$ | $\frac{7}{16}$ | $\frac{1}{2}$ | $\frac{9}{16}$ | $\frac{5}{8}$ |
| 2 | .17 | .21 | .25 | .29 | .33 | .38 | .42 |
| 3 | .56 | .70 | .84 | .98 | 1.13 | 1.27 | 1.41 |
| 4 | 1.33 | 1.67 | 2.00 | 2.33 | 2.67 | 3.00 | 3.33 |
| 5 | 2.60 | 3.26 | 3.91 | 4.56 | 5.21 | 5.86 | 6.51 |
| 6 | 4.50 | 5.63 | 6.75 | 7.88 | 9.00 | 10.13 | 11.25 |
| 7 | 7.15 | 8.93 | 10.72 | 12.51 | 14.29 | 16.08 | 17.86 |
| 8 | 10.67 | 13.33 | 16.00 | 18.67 | 21.33 | 24.00 | 26.67 |
| 9 | 15.19 | 18.98 | 22.78 | 26.58 | 30.38 | 34.17 | 37.97 |
| 10 | 20.83 | 26.04 | 31.25 | 36.46 | 41.67 | 46.87 | 52.08 |
| 11 | 27.73 | 34.66 | 41.59 | 48.53 | 55.46 | 62.39 | 69.32 |
| 12 | 36.00 | 45.00 | 54.00 | 63.00 | 72.00 | 81.00 | 90.00 |
| 13 | 45.77 | 57.21 | 68.66 | 80.10 | 91.54 | 102.98 | 114.43 |
| 14 | 57.17 | 71.46 | 85.75 | 100.04 | 114.33 | 128.63 | 142.92 |
| 15 | 70.31 | 87.89 | 105.47 | 123.05 | 140.63 | 158.20 | 175.78 |
| 16 | 85.33 | 106.67 | 128.00 | 149.33 | 170.67 | 192.00 | 213.33 |
| 17 | 102.35 | 127.94 | 153.53 | 179.12 | 204.71 | 230.30 | 255.89 |
| 18 | 121.50 | 151.88 | 182.25 | 212.63 | 243.00 | 273.38 | 303.75 |
| 19 | 142.90 | 178.62 | 214.34 | 250.07 | 285.79 | 321.52 | 357.24 |
| 20 | 166.67 | 208.33 | 250.00 | 291.67 | 333.33 | 375.00 | 416.67 |
| 21 | 192.94 | 241.17 | 289.41 | 337.64 | 385.88 | 434.11 | 482.34 |
| 22 | 221.83 | 277.29 | 332.75 | 388.21 | 443.67 | 499.13 | 554.58 |
| 23 | 253.48 | 316.85 | 380.22 | 443.59 | 506.96 | 570.33 | 633.70 |
| 24 | 288.00 | 360.00 | 432.00 | 504.00 | 576.00 | 648.00 | 720.00 |
| 25 | 325.52 | 406.90 | 488.28 | 569.66 | 651.04 | 732.42 | 813.80 |
| 26 | 366.17 | 457.71 | 549.25 | 640.79 | 732.33 | 823.88 | 915.42 |
| 27 | 410.06 | 512.58 | 615.09 | 717.61 | 820.13 | 922.64 | 1025.16 |
| 28 | 457.33 | 571.67 | 686.00 | 800.33 | 914.67 | 1029.00 | 1143.33 |
| 29 | 508.10 | 635.13 | 762.16 | 889.18 | 1016.21 | 1143.23 | 1270.26 |
| 30 | 562.50 | 703.13 | 843.75 | 984.38 | 1125.00 | 1265.63 | 1406.25 |
| 32 | 682.67 | 853.33 | 1024.00 | 1194.67 | 1365.33 | 1536.00 | 1706.67 |
| 34 | 818.83 | 1023.54 | 1228.25 | 1432.96 | 1637.67 | 1842.38 | 2047.08 |
| 36 | 972.00 | 1215.00 | 1458.00 | 1701.00 | 1944.00 | 2187.00 | 2430.00 |
| 38 | 1143.17 | 1428.96 | 1714.75 | 2000.54 | 2286.33 | 2572.13 | 2857.92 |
| 40 | 1333.33 | 1666.67 | 2000.00 | 2333.33 | 2666.67 | 3000.00 | 3333.33 |
| 42 | 1543.50 | 1929.38 | 2315.25 | 2701.13 | 3087.00 | 3472.88 | 3858.75 |
| 44 | 1774.67 | 2218.33 | 2662.00 | 3105.67 | 3549.33 | 3993.00 | 4436.67 |
| 46 | 2027.83 | 2534.79 | 3041.75 | 3548.71 | 4055.67 | 4562.63 | 5069.58 |
| 48 | 2304.00 | 2880.00 | 3456.00 | 4032.00 | 4608.00 | 5184.00 | 5760.00 |
| 50 | 2604.17 | 3255.21 | 3906.25 | 4557.29 | 5208.33 | 5859.38 | 6510.42 |
| 52 | 2929.33 | 3661.67 | 4394.00 | 5126.33 | 5858.67 | 6591.00 | 7323.33 |
| 54 | 3280.50 | 4100.63 | 4920.75 | 5740.88 | 6561.00 | 7381.13 | 8201.25 |
| 56 | 3658.67 | 4573.33 | 5488.00 | 6402.67 | 7317.33 | 8232.00 | 9146.67 |
| 58 | 4064.83 | 5081.04 | 6097.25 | 7113.46 | 8129.67 | 9145.87 | 10162.08 |
| 60 | 4500.00 | 5625.00 | 6750.00 | 7875.00 | 9000.00 | 10125.00 | 11250.00 |

MOMENTS OF INERTIA OF RECTANGLES. I

Neutral  Axis

Depths 2 to 60 inches; widths $\frac{1}{8}$ to 1 inch, varying by $\frac{1}{16}$ inch.

| Width of Rectangle in Inches. | | | | | | Depth in Inches. |
|-------------------------------|---------------|---------------|---------------|---------------|----------|------------------------|
| $\frac{1}{16}$ | $\frac{3}{4}$ | $\frac{1}{8}$ | $\frac{7}{8}$ | $\frac{1}{2}$ | 1 | |
| .46 | .50 | .54 | .58 | .63 | .67 | 2 |
| 1.55 | 1.69 | 1.83 | 1.97 | 2.11 | 2.25 | 3 |
| 3.67 | 4.00 | 4.33 | 4.67 | 5.00 | 5.33 | 4 |
| 7.16 | 7.81 | 8.46 | 9.11 | 9.77 | 10.42 | 5 |
| 12.38 | 13.50 | 14.63 | 15.75 | 16.88 | 18.00 | 6 |
| 19.65 | 21.44 | 23.22 | 25.01 | 26.80 | 28.58 | 7 |
| 29.33 | 32.00 | 34.67 | 37.33 | 40.00 | 42.67 | 8 |
| 41.77 | 45.56 | 49.36 | 53.16 | 56.95 | 60.75 | 9 |
| 57.29 | 62.50 | 67.71 | 72.92 | 78.13 | 83.33 | 10 |
| 76.26 | 83.19 | 90.12 | 97.05 | 103.98 | 110.92 | 11 |
| 99.00 | 108.00 | 117.00 | 126.00 | 135.00 | 144.00 | 12 |
| 125.87 | 137.31 | 148.75 | 160.20 | 171.64 | 183.08 | 13 |
| 157.21 | 171.50 | 185.79 | 200.08 | 214.38 | 228.67 | 14 |
| 193.36 | 210.94 | 228.52 | 246.09 | 263.67 | 281.25 | 15 |
| 234.67 | 256.00 | 277.33 | 298.67 | 320.00 | 341.33 | 16 |
| 281.47 | 307.06 | 332.65 | 358.24 | 383.83 | 409.42 | 17 |
| 334.13 | 364.50 | 394.88 | 425.25 | 455.63 | 486.00 | 18 |
| 392.96 | 428.69 | 464.41 | 500.14 | 535.86 | 571.58 | 19 |
| 458.33 | 500.00 | 541.67 | 583.33 | 625.00 | 666.67 | 20 |
| 530.58 | 578.81 | 627.05 | 675.28 | 723.52 | 771.75 | 21 |
| 610.04 | 665.50 | 720.96 | 776.42 | 831.87 | 887.33 | 22 |
| 697.07 | 760.44 | 823.81 | 887.18 | 950.55 | 1013.92 | 23 |
| 792.00 | 864.00 | 936.00 | 1008.00 | 1080.00 | 1152.00 | 24 |
| 895.18 | 976.56 | 1057.94 | 1139.32 | 1220.70 | 1302.08 | 25 |
| 1006.96 | 1098.50 | 1190.04 | 1281.58 | 1373.13 | 1464.67 | 26 |
| 1127.67 | 1230.19 | 1332.70 | 1435.22 | 1537.73 | 1640.25 | 27 |
| 1257.67 | 1372.00 | 1486.33 | 1600.67 | 1715.00 | 1829.33 | 28 |
| 1397.29 | 1524.31 | 1651.34 | 1778.36 | 1905.39 | 2032.42 | 29 |
| 1546.88 | 1687.50 | 1828.13 | 1968.75 | 2109.38 | 2250.00 | 30 |
| 1877.33 | 2048.00 | 2218.67 | 2389.33 | 2560.00 | 2730.67 | 32 |
| 2251.79 | 2456.50 | 2661.21 | 2865.92 | 3070.63 | 3275.33 | 34 |
| 2673.00 | 2916.00 | 3159.00 | 3402.00 | 3645.00 | 3888.00 | 36 |
| 3143.71 | 3429.50 | 3715.29 | 4001.08 | 4286.88 | 4572.67 | 38 |
| 3666.67 | 4000.00 | 4333.33 | 4666.67 | 5000.00 | 5333.33 | 40 |
| 4244.63 | 4630.50 | 5016.38 | 5402.25 | 5788.13 | 6174.00 | 42 |
| 4880.33 | 5324.00 | 5767.67 | 6211.33 | 6655.00 | 7098.67 | 44 |
| 5576.54 | 6083.50 | 6590.46 | 7097.42 | 7604.38 | 8111.33 | 46 |
| 6336.00 | 6912.00 | 7488.00 | 8064.00 | 8640.00 | 9216.00 | 48 |
| 7161.46 | 7812.50 | 8463.54 | 9114.58 | 9765.63 | 10416.67 | 50 |
| 8055.67 | 8788.00 | 9520.33 | 10252.67 | 10985.00 | 11717.33 | 52 |
| 9021.38 | 9841.50 | 10661.63 | 11481.75 | 12301.88 | 13122.00 | 54 |
| 10061.33 | 10976.00 | 11890.67 | 12805.33 | 13720.00 | 14634.67 | 56 |
| 11178.29 | 12194.50 | 13210.71 | 14226.92 | 15243.12 | 16259.33 | 58 |
| 12375.00 | 13500.00 | 14625.00 | 15750.00 | 16875.00 | 18000.00 | 60 |

MOMENTS OF INERTIA OF RECTANGLES. II

ONE INCH WIDE.

NEUTRAL  AXIS

Value for any width may be obtained from tabular value by direct multiplication.

| Depth in Inches. | Additional Depth in Fractions of an Inch. | | | | | | | |
|------------------------|---|----------------|---------------|----------------|---------------|----------------|---------------|----------------|
| | 0 | $\frac{1}{16}$ | $\frac{1}{8}$ | $\frac{3}{16}$ | $\frac{1}{4}$ | $\frac{5}{16}$ | $\frac{3}{8}$ | $\frac{7}{16}$ |
| 0 | | .00002 | .00016 | .00055 | .00130 | .00254 | .00439 | .00698 |
| 1 | .08333 | .09995 | .11865 | .13955 | .16276 | .18842 | .21663 | .24754 |
| 2 | .66667 | .73114 | .79964 | .87229 | .94922 | 1.0305 | 1.1164 | 1.2068 |
| 3 | 2.2500 | 2.3936 | 2.5431 | 2.6988 | 2.8607 | 3.0289 | 3.2036 | 3.3849 |
| 4 | 5.3333 | 5.5873 | 5.8491 | 6.1190 | 6.3971 | 6.6802 | 6.9783 | 7.2817 |
| 5 | 10.417 | 10.812 | 11.218 | 11.633 | 12.059 | 12.494 | 12.941 | 13.397 |
| 6 | 18.000 | 18.568 | 19.149 | 19.741 | 20.345 | 20.961 | 21.590 | 22.232 |
| 7 | 28.583 | 29.356 | 30.142 | 30.942 | 31.757 | 32.585 | 33.428 | 34.285 |
| 8 | 42.667 | 43.674 | 44.698 | 45.737 | 46.793 | 47.864 | 48.952 | 50.056 |
| 9 | 60.750 | 62.024 | 63.317 | 64.626 | 65.954 | 67.300 | 68.665 | 70.047 |
| 10 | 83.333 | 84.906 | 86.498 | 88.109 | 89.741 | 91.392 | 93.064 | 94.756 |
| 11 | 110.92 | 112.82 | 114.74 | 116.69 | 118.65 | 120.64 | 122.65 | 124.68 |
| 12 | 144.00 | 146.26 | 148.55 | 150.86 | 153.19 | 155.55 | 157.93 | 160.33 |
| 13 | 183.08 | 185.74 | 188.42 | 191.12 | 193.85 | 196.61 | 199.39 | 202.20 |
| 14 | 228.67 | 231.74 | 234.85 | 237.98 | 241.14 | 244.32 | 247.54 | 250.78 |
| 15 | 281.25 | 284.78 | 288.34 | 291.93 | 295.55 | 299.20 | 302.87 | 306.58 |
| 16 | 341.33 | 345.35 | 349.40 | 353.47 | 357.58 | 361.73 | 365.90 | 370.11 |
| 17 | 409.42 | 413.95 | 418.52 | 423.11 | 427.75 | 432.41 | 437.11 | 441.85 |
| 18 | 486.00 | 491.41 | 496.20 | 501.35 | 506.53 | 511.75 | 517.01 | 522.31 |
| 19 | 571.58 | 577.24 | 582.94 | 588.67 | 594.44 | 600.25 | 606.10 | 611.98 |
| 20 | 666.67 | 672.94 | 679.24 | 685.59 | 691.84 | 698.41 | 704.87 | 711.38 |
| 21 | 771.75 | 778.66 | 785.61 | 792.61 | 799.65 | 806.72 | 813.84 | 821.00 |
| 22 | 887.33 | 894.92 | 902.54 | 910.21 | 917.93 | 925.68 | 933.49 | 941.33 |
| 23 | 1013.9 | 1022.2 | 1030.5 | 1038.9 | 1047.3 | 1055.8 | 1064.3 | 1072.9 |
| 24 | 1152.0 | 1161.0 | 1170.1 | 1178.4 | 1188.4 | 1197.6 | 1206.8 | 1216.2 |
| 25 | 1302.1 | 1311.9 | 1321.7 | 1331.6 | 1341.5 | 1351.5 | 1361.6 | 1371.6 |
| 26 | 1464.7 | 1475.3 | 1485.9 | 1496.6 | 1507.3 | 1518.1 | 1529.0 | 1539.9 |
| 27 | 1640.2 | 1651.7 | 1663.1 | 1674.7 | 1686.2 | 1697.9 | 1709.5 | 1721.3 |
| 28 | 1829.3 | 1841.6 | 1853.9 | 1866.3 | 1878.8 | 1891.3 | 1903.8 | 1916.4 |
| 29 | 2032.4 | 2045.6 | 2058.8 | 2072.1 | 2085.4 | 2098.8 | 2112.3 | 2125.8 |
| 30 | 2250.0 | 2264.1 | 2278.2 | 2292.4 | 2306.7 | 2321.0 | 2335.4 | 2349.9 |
| 31 | 2482.6 | 2497.6 | 2512.7 | 2527.9 | 2543.1 | 2558.4 | 2573.8 | 2589.2 |
| 32 | 2730.7 | 2746.7 | 2762.8 | 2778.9 | 2795.2 | 2811.4 | 2827.8 | 2844.2 |
| 33 | 2994.7 | 3011.8 | 3028.9 | 3046.1 | 3063.3 | 3080.4 | 3098.0 | 3115.4 |
| 34 | 3275.3 | 3293.4 | 3311.6 | 3329.8 | 3348.1 | 3366.5 | 3384.9 | 3403.4 |
| 35 | 3572.9 | 3592.0 | 3611.3 | 3630.6 | 3650.0 | 3669.5 | 3689.0 | 3708.6 |
| 36 | 3888.0 | 3908.3 | 3928.6 | 3949.1 | 3969.6 | 3990.1 | 4010.8 | 4031.5 |
| 37 | 4221.1 | 4242.5 | 4264.0 | 4285.6 | 4307.3 | 4328.9 | 4350.7 | 4372.6 |
| 38 | 4572.7 | 4595.3 | 4617.9 | 4640.7 | 4663.5 | 4686.4 | 4719.4 | 4732.4 |
| 39 | 4943.3 | 4967.0 | 4990.9 | 5014.9 | 5038.9 | 5063.0 | 5087.2 | 5111.5 |
| 40 | 5333.3 | 5358.4 | 5383.5 | 5408.7 | 5433.9 | 5459.3 | 5484.7 | 5510.2 |
| 41 | 5743.4 | 5769.7 | 5796.1 | 5822.6 | 5849.1 | 5875.7 | 5902.5 | 5929.2 |
| 42 | 6174.0 | 6201.6 | 6229.3 | 6257.1 | 6284.9 | 6312.8 | 6340.9 | 6368.9 |
| 43 | 6625.6 | 6654.5 | 6683.5 | 6703.5 | 6741.8 | 6771.1 | 6800.4 | 6829.9 |
| 44 | 7098.7 | 7129.0 | 7159.3 | 7189.0 | 7220.3 | 7251.0 | 7281.7 | 7312.5 |
| 45 | 7593.8 | 7625.4 | 7657.2 | 7689.1 | 7721.0 | 7753.0 | 7785.2 | 7817.4 |
| 46 | 8111.3 | 8144.7 | 8177.6 | 8210.9 | 8244.3 | 8277.8 | 8311.3 | 8345.0 |
| 47 | 8651.9 | 8686.5 | 8721.1 | 8755.9 | 8790.7 | 8825.6 | 8860.7 | 8895.8 |
| 48 | 9216.0 | 9252.0 | 9288.2 | 9324.4 | 9360.7 | 9397.2 | 9433.7 | 9470.3 |
| 49 | 9804.1 | 9841.6 | 9879.3 | 9917.1 | 9954.9 | 9992.9 | 10031 | 10071 |
| 50 | 10417 | 10456 | 10495 | 10534 | 10574 | 10613 | 10653 | 10692 |

MOMENTS OF INERTIA OF RECTANGLES. II**ONE INCH WIDE.**

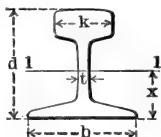
NEUTRAL

AXIS

Value for any width may be obtained from
tabular value by direct multiplication.

| Additional Depth in Fractions of an Inch. | | | | | | | | Depth in Inches. |
|---|----------------|---------------|-----------------|---------------|-----------------|---------------|-----------------|------------------------|
| $\frac{1}{2}$ | $\frac{9}{16}$ | $\frac{5}{8}$ | $\frac{11}{16}$ | $\frac{3}{4}$ | $\frac{13}{16}$ | $\frac{7}{8}$ | $\frac{15}{16}$ | |
| .01041 | .01483 | .02034 | .02708 | .03516 | .04469 | .05583 | .06866 | 0 |
| .28125 | .31789 | .35758 | .40045 | .44661 | .49620 | .54932 | .60610 | 1 |
| 1.3021 | 1.4022 | 1.5073 | 1.6176 | 1.7331 | 1.8539 | 1.9803 | 2.1123 | 2 |
| 3.5729 | 3.7678 | 3.9696 | 4.1784 | 4.3945 | 4.6179 | 4.8488 | 5.0872 | 3 |
| 7.5937 | 7.9146 | 8.2443 | 8.5831 | 8.9310 | 9.2882 | 9.6548 | 10.031 | 4 |
| 13.865 | 14.343 | 14.832 | 15.331 | 15.843 | 16.365 | 16.898 | 17.443 | 5 |
| 22.885 | 23.552 | 24.231 | 24.924 | 25.629 | 26.347 | 27.079 | 27.825 | 6 |
| 35.156 | 36.043 | 36.944 | 37.859 | 38.790 | 39.736 | 40.698 | 41.674 | 7 |
| 51.177 | 52.314 | 53.468 | 54.639 | 55.827 | 57.032 | 58.254 | 59.493 | 8 |
| 71.448 | 72.867 | 74.305 | 75.762 | 77.238 | 78.733 | 80.247 | 81.780 | 9 |
| 96.469 | 98.203 | 99.955 | 101.73 | 103.52 | 105.34 | 107.18 | 109.04 | 10 |
| 126.74 | 128.82 | 130.92 | 133.04 | 135.19 | 137.35 | 139.55 | 141.76 | 11 |
| 162.76 | 165.21 | 167.69 | 170.19 | 172.72 | 175.28 | 177.85 | 180.46 | 12 |
| 205.03 | 207.89 | 210.78 | 213.69 | 216.63 | 219.60 | 222.60 | 225.62 | 13 |
| 254.05 | 257.35 | 260.68 | 264.04 | 267.42 | 270.83 | 274.28 | 277.75 | 14 |
| 310.32 | 314.09 | 317.89 | 321.72 | 325.58 | 329.47 | 333.40 | 337.35 | 15 |
| 374.34 | 378.61 | 382.92 | 387.25 | 391.62 | 396.02 | 400.45 | 404.92 | 16 |
| 446.61 | 451.42 | 456.25 | 461.12 | 466.03 | 470.97 | 475.94 | 480.95 | 17 |
| 527.63 | 533.00 | 538.40 | 543.84 | 549.32 | 554.83 | 560.38 | 565.96 | 18 |
| 617.91 | 623.87 | 629.87 | 635.90 | 641.98 | 648.09 | 654.24 | 660.44 | 19 |
| 717.93 | 724.51 | 731.14 | 737.81 | 744.51 | 751.26 | 758.05 | 764.88 | 20 |
| 828.20 | 835.44 | 842.73 | 850.05 | 857.43 | 864.84 | 872.29 | 879.79 | 21 |
| 949.22 | 957.15 | 965.13 | 973.15 | 981.21 | 989.32 | 997.47 | 1005.7 | 22 |
| 1081.5 | 1090.1 | 1098.8 | 1107.6 | 1116.4 | 1125.2 | 1134.1 | 1143.0 | 23 |
| 1225.5 | 1234.9 | 1244.4 | 1253.9 | 1263.4 | 1273.0 | 1282.6 | 1292.3 | 24 |
| 1381.8 | 1392.0 | 1402.2 | 1412.5 | 1422.8 | 1433.2 | 1443.6 | 1454.1 | 25 |
| 1550.8 | 1561.8 | 1572.8 | 1584.0 | 1595.1 | 1606.3 | 1617.6 | 1628.9 | 26 |
| 1733.1 | 1744.9 | 1756.8 | 1768.8 | 1780.8 | 1792.8 | 1804.9 | 1817.1 | 27 |
| 1929.1 | 1941.8 | 1954.6 | 1967.4 | 1980.3 | 1993.2 | 2006.2 | 2019.3 | 28 |
| 2139.4 | 2153.0 | 2166.7 | 2180.4 | 2194.2 | 2208.1 | 2222.0 | 2236.0 | 29 |
| 2364.4 | 2378.9 | 2393.6 | 2408.3 | 2423.0 | 2437.8 | 2452.7 | 2467.6 | 30 |
| 2604.7 | 2620.2 | 2635.8 | 2651.4 | 2667.2 | 2682.9 | 2698.8 | 2714.7 | 31 |
| 2860.7 | 2877.2 | 2893.8 | 2910.5 | 2927.2 | 2944.0 | 2960.8 | 2977.8 | 32 |
| 3132.9 | 3150.5 | 3168.1 | 3185.8 | 3203.6 | 3221.4 | 3239.3 | 3257.3 | 33 |
| 3422.0 | 3440.6 | 3459.3 | 3478.1 | 3496.9 | 3515.8 | 3534.8 | 3553.8 | 34 |
| 3728.2 | 3748.0 | 3767.8 | 3787.6 | 3807.6 | 3827.6 | 3847.6 | 3867.8 | 35 |
| 4052.3 | 4073.1 | 4094.0 | 4115.0 | 4136.1 | 4157.2 | 4178.4 | 4199.7 | 36 |
| 4394.5 | 4416.5 | 4438.6 | 4460.8 | 4483.0 | 4505.3 | 4527.7 | 4550.1 | 37 |
| 4755.5 | 4778.7 | 4802.0 | 4825.4 | 4848.8 | 4872.3 | 4895.9 | 4919.5 | 38 |
| 5135.8 | 5160.2 | 5184.7 | 5209.3 | 5239.6 | 5285.3 | 5283.5 | 5308.4 | 39 |
| 5535.8 | 5561.5 | 5587.3 | 5613.1 | 5639.0 | 5665.0 | 5691.0 | 5717.2 | 40 |
| 5956.1 | 5983.1 | 6010.1 | 6037.0 | 6064.4 | 6091.7 | 6119.0 | 6146.5 | 41 |
| 6397.1 | 6425.4 | 6453.7 | 6482.2 | 6510.7 | 6539.3 | 6568.0 | 6596.7 | 42 |
| 6867.7 | 6889.0 | 6918.7 | 6948.5 | 6978.3 | 7008.3 | 7038.3 | 7068.5 | 43 |
| 7343.4 | 7374.4 | 7405.5 | 7436.6 | 7467.9 | 7499.2 | 7530.6 | 7562.1 | 44 |
| 7849.7 | 7882.1 | 7914.6 | 7947.1 | 7979.8 | 8012.5 | 8045.4 | 8078.3 | 45 |
| 8378.7 | 8412.5 | 8446.5 | 8480.5 | 8514.6 | 8548.8 | 8583.1 | 8617.4 | 46 |
| 8931.0 | 8966.3 | 9001.7 | 9037.2 | 9072.7 | 9108.4 | 9144.2 | 9180.0 | 47 |
| 9507.0 | 9544.1 | 9580.7 | 9617.7 | 9654.8 | 9692.0 | 9729.2 | 9766.6 | 48 |
| 10107 | 10146 | 10184 | 10223 | 10261 | 10300 | 10339 | 10378 | 49 |
| 10732 | 10772 | 10812 | 10852 | 10892 | 10933 | 10973 | 11014 | 50 |

PROPERTIES AND PRINCIPAL DIMENSIONS OF STANDARD T-RAILS.

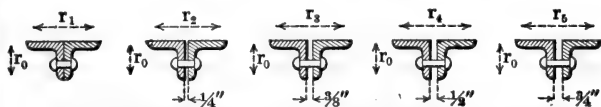


| Stand- ard. (See Foot Note.) | Section Number. | Weight per Yard. | Area. | b | d | k | t | Neutral Axis 1-1. | | |
|--|--------------------|------------------------|----------|-----------------|------------------|------------------|----------------|-------------------|--------------------------|---------------------|
| | | | | | | | | \bar{x} | Moment of Inertia. | Section Modulus. |
| | | Pounds. | Sq. Ins. | Inches. | Inches. | Inches. | Inch. | Inches. | I | S |
| | 580 | 12 | 1.17 | 2 | 2 | 1 | $\frac{1}{8}$ | .96 | .67 | .64 |
| | 579 | 16 | 1.56 | $2\frac{3}{8}$ | $2\frac{3}{8}$ | $1\frac{11}{16}$ | $\frac{1}{4}$ | 1.14 | 1.23 | .99 |
| | 578 | 20 | 1.98 | $2\frac{5}{8}$ | $2\frac{5}{8}$ | $1\frac{13}{16}$ | $\frac{1}{4}$ | 1.25 | 1.93 | 1.41 |
| | 577 | 25 | 2.40 | $2\frac{3}{4}$ | $2\frac{3}{4}$ | $1\frac{1}{2}$ | $\frac{1}{4}$ | 1.33 | 2.50 | 1.76 |
| | 576 | 30 | 3.02 | $3\frac{1}{8}$ | $3\frac{1}{8}$ | $1\frac{11}{16}$ | $\frac{3}{8}$ | 1.52 | 4.10 | 2.55 |
| | 575 | 35 | 3.42 | $3\frac{5}{16}$ | $3\frac{5}{16}$ | $1\frac{3}{4}$ | $\frac{2}{4}$ | 1.54 | 5.14 | 2.90 |
| C | 545 | 40 | 3.94 | $3\frac{1}{2}$ | $3\frac{1}{2}$ | $1\frac{7}{8}$ | $\frac{3}{8}$ | 1.69 | 6.52 | 3.60 |
| C | 549 | 45 | 4.40 | $3\frac{1}{8}$ | $3\frac{1}{8}$ | 2 | $\frac{2}{4}$ | 1.76 | 8.09 | 4.19 |
| C | 542 | 50 | 4.87 | $3\frac{7}{8}$ | $3\frac{7}{8}$ | $2\frac{1}{8}$ | $\frac{1}{8}$ | 1.86 | 9.82 | 4.86 |
| C | 537 | 55 | 5.38 | $4\frac{1}{16}$ | $4\frac{1}{16}$ | $2\frac{1}{4}$ | $\frac{1}{8}$ | 1.98 | 12.03 | 5.78 |
| A | 568 | 60 | 5.86 | 4 | $4\frac{1}{2}$ | $2\frac{1}{4}$ | $\frac{1}{8}$ | 2.13 | 15.41 | 6.50 |
| C | 533 | 60 | 5.93 | $4\frac{1}{4}$ | $4\frac{1}{4}$ | $2\frac{3}{8}$ | $\frac{3}{8}$ | 2.06 | 14.56 | 6.65 |
| B | 571 | 60 | 5.87 | $3\frac{1}{8}$ | $4\frac{3}{16}$ | $2\frac{1}{8}$ | $\frac{3}{8}$ | 1.95 | 13.30 | 5.94 |
| C | 534 | 65 | 6.33 | $4\frac{1}{16}$ | $4\frac{1}{16}$ | $2\frac{1}{2}$ | $\frac{1}{2}$ | 2.15 | 16.72 | 7.30 |
| A | 567 | 70 | 6.82 | $4\frac{1}{4}$ | $4\frac{3}{4}$ | $2\frac{3}{8}$ | $\frac{1}{2}$ | 2.20 | 21.05 | 8.26 |
| C | 532 | 70 | 6.81 | $4\frac{5}{8}$ | $4\frac{5}{8}$ | $2\frac{7}{16}$ | $\frac{3}{8}$ | 2.22 | 20.06 | 8.32 |
| B | 570 | 70 | 6.89 | $4\frac{3}{4}$ | $4\frac{3}{4}$ | $2\frac{3}{8}$ | $\frac{3}{8}$ | 2.16 | 18.60 | 7.78 |
| C | 529 | 75 | 7.33 | $4\frac{1}{8}$ | $4\frac{1}{8}$ | $2\frac{1}{2}$ | $\frac{1}{2}$ | 2.29 | 23.11 | 9.17 |
| A | 566 | 80 | 7.86 | $4\frac{5}{8}$ | $5\frac{1}{8}$ | $2\frac{1}{2}$ | $\frac{3}{8}$ | 2.31 | 28.80 | 10.21 |
| C | 530 | 80 | 7.86 | 5 | 5 | $2\frac{1}{2}$ | $\frac{3}{8}$ | 2.41 | 26.35 | 10.17 |
| B | 569 | 80 | 7.91 | $4\frac{7}{16}$ | $4\frac{11}{16}$ | $2\frac{7}{16}$ | $\frac{3}{8}$ | 2.27 | 25.10 | 9.40 |
| C | 531 | 85 | 8.33 | $5\frac{1}{16}$ | $5\frac{1}{16}$ | $2\frac{3}{8}$ | $\frac{1}{8}$ | 2.47 | 30.34 | 11.15 |
| A | 563 | 90 | 8.82 | $5\frac{1}{8}$ | $5\frac{3}{8}$ | $2\frac{9}{16}$ | $\frac{1}{8}$ | 2.54 | 38.70 | 12.52 |
| C | 535 | 90 | 8.83 | $5\frac{3}{8}$ | $5\frac{3}{8}$ | $2\frac{5}{8}$ | $\frac{1}{8}$ | 2.57 | 34.43 | 12.25 |
| B | 561 | 90 | 8.87 | $4\frac{9}{16}$ | $5\frac{1}{4}$ | $2\frac{9}{16}$ | $\frac{1}{8}$ | 2.45 | 32.30 | 11.45 |
| C | 550 | 95 | 9.28 | $5\frac{9}{16}$ | $5\frac{9}{16}$ | $2\frac{11}{16}$ | $\frac{1}{8}$ | 2.67 | 38.58 | 13.85 |
| A | 565 | 100 | 9.84 | $5\frac{1}{2}$ | 6 | $2\frac{3}{4}$ | $\frac{1}{8}$ | 2.75 | 48.94 | 15.07 |
| C | 536 | 100 | 9.84 | $5\frac{3}{4}$ | $5\frac{3}{4}$ | $2\frac{3}{4}$ | $\frac{9}{16}$ | 2.73 | 43.42 | 14.38 |
| B | 564 | 100 | 9.85 | $5\frac{3}{4}$ | $5\frac{1}{2}$ | $2\frac{11}{16}$ | $\frac{1}{8}$ | 2.63 | 41.30 | 13.72 |
| M | 572 | 110 | 10.75 | $5\frac{1}{2}$ | 6 | $2\frac{11}{16}$ | $\frac{1}{8}$ | 2.80 | 56.00 | 17.50 |
| M | 573 | 120 | 11.76 | $5\frac{3}{4}$ | $6\frac{1}{4}$ | $2\frac{7}{8}$ | $\frac{5}{8}$ | 2.89 | 60.04 | 17.87 |
| M | 574 | 130 | 12.76 | 6 | $6\frac{1}{2}$ | $2\frac{11}{16}$ | $\frac{1}{2}$ | 3.00 | 71.02 | 20.29 |
| | 539 | 150 | 14.71 | 6 | 6 | $4\frac{1}{4}$ | 1 | 3.00 | 69.30 | 23.10 |

For detail dimensions of Section No. 539, see page 26.

A; B;—Type A; Type B; American Railway Association Standard.
C;—American Society of Civil Engineers Standard.
M;—Manufacturers Standard.

RADII OF GYRATION FOR TWO ANGLES PLACED BACK TO BACK. ANGLES WITH EQUAL LEGS.



Radii of gyration correspond to directions indicated by arrowheads.

| Section Number. | Dimensions. | Thickness. | Area of Two Angles. | Radii of Gyration. | | | | | |
|-----------------|-------------|------------|---------------------|--------------------|----------------|----------------|----------------|----------------|----------------|
| | | | | r ₀ | r ₁ | r ₂ | r ₃ | r ₄ | r ₅ |
| Inches. | Inch. | Sq. Ins. | | | | | | | |
| A11 | 1½ x 1½ | ⅜ | 1.06 | 0.64 | 0.64 | 0.73 | 0.78 | 0.83 | 0.94 |
| " | " | ⅝ | 1.68 | 0.44 | 0.66 | 0.76 | 0.81 | 0.86 | 0.97 |
| " | " | *⅝ | 1.97 | 0.44 | 0.67 | 0.77 | 0.82 | 0.88 | 0.99 |
| *A40 | 1¾ x 1¾ | ⅜ | .84 | 0.55 | 0.73 | 0.82 | 0.86 | 0.91 | 1.02 |
| " | " | ⅝ | 1.24 | 0.54 | 0.74 | 0.83 | 0.88 | 0.93 | 1.03 |
| " | " | ⅝ | 2.34 | 0.51 | 0.76 | 0.86 | 0.91 | 0.97 | 1.07 |
| A15 | 2 x 2 | *⅝ | .97 | 0.63 | 0.84 | 0.92 | 0.97 | 1.02 | 1.12 |
| " | " | ⅝ | 1.44 | 0.62 | 0.84 | 0.93 | 0.98 | 1.03 | 1.13 |
| " | " | ⅝ | 2.30 | 0.60 | 0.86 | 0.95 | 1.00 | 1.05 | 1.16 |
| " | " | ⅝ | 3.12 | 0.59 | 0.88 | 0.98 | 1.03 | 1.08 | 1.19 |
| *A41 | 2¼ x 2¼ | ⅝ | 1.62 | 0.70 | 0.94 | 1.03 | 1.08 | 1.12 | 1.22 |
| " | " | ⅝ | 2.62 | 0.68 | 0.96 | 1.05 | 1.10 | 1.15 | 1.25 |
| A17 | 2½ x 2½ | *⅝ | 1.22 | 0.79 | 1.04 | 1.12 | 1.17 | 1.21 | 1.31 |
| " | " | ⅝ | 2.38 | 0.77 | 1.05 | 1.14 | 1.19 | 1.24 | 1.34 |
| " | " | ⅝ | 3.46 | 0.75 | 1.07 | 1.16 | 1.21 | 1.26 | 1.36 |
| " | " | ⅝ | 4.50 | 0.74 | 1.09 | 1.19 | 1.24 | 1.29 | 1.39 |
| *A43 | 2¾ x 2¾ | ⅝ | 2.62 | 0.85 | 1.15 | 1.24 | 1.29 | 1.34 | 1.43 |
| " | " | ⅝ | 3.24 | 0.84 | 1.16 | 1.25 | 1.30 | 1.35 | 1.45 |
| " | " | ⅝ | 3.84 | 0.83 | 1.17 | 1.26 | 1.31 | 1.35 | 1.45 |
| A19 | 3 x 3 | ⅝ | 2.88 | 0.93 | 1.26 | 1.34 | 1.39 | 1.43 | 1.53 |
| " | " | ⅝ | 4.86 | 0.91 | 1.28 | 1.37 | 1.42 | 1.47 | 1.57 |
| " | " | ⅝ | 6.12 | 0.89 | 1.30 | 1.39 | 1.44 | 1.49 | 1.59 |
| A21 | 3½ x 3½ | ⅝ | 3.38 | 1.09 | 1.46 | 1.54 | 1.59 | 1.64 | 1.73 |
| " | " | ⅝ | 7.96 | 1.04 | 1.52 | 1.61 | 1.66 | 1.71 | 1.81 |
| " | " | ⅝ | 10.06 | 1.02 | 1.55 | 1.65 | 1.70 | 1.75 | 1.85 |
| A23 | 4 x 4 | ⅝ | 4.80 | 1.24 | 1.67 | 1.76 | 1.80 | 1.85 | 1.94 |
| " | " | ⅝ | 8.36 | 1.21 | 1.71 | 1.80 | 1.85 | 1.89 | 1.99 |
| " | " | ⅝ | 11.68 | 1.18 | 1.75 | 1.85 | 1.89 | 1.94 | 2.04 |
| *A47 | 5 x 5 | ⅝ | 7.22 | 1.56 | 2.09 | 2.17 | 2.22 | 2.26 | 2.35 |
| " | " | ⅝ | 9.50 | 1.54 | 2.10 | 2.19 | 2.24 | 2.28 | 2.38 |
| " | " | ⅝ | 13.88 | 1.50 | 2.14 | 2.25 | 2.27 | 2.32 | 2.42 |
| A27 | 6 x 6 | ⅝ | 10.12 | 1.87 | 2.50 | 2.58 | 2.63 | 2.67 | 2.76 |
| " | " | ⅝ | 14.22 | 1.84 | 2.53 | 2.62 | 2.66 | 2.71 | 2.80 |
| " | " | ⅝ | 19.46 | 1.81 | 2.57 | 2.66 | 2.70 | 2.75 | 2.85 |
| A35 | 8 x 8 | ⅝ | 15.50 | 2.51 | 3.32 | 3.41 | 3.45 | 3.49 | 3.58 |
| " | " | ⅝ | 19.22 | 2.49 | 3.34 | 3.43 | 3.47 | 3.51 | 3.60 |
| " | " | ⅝ | 22.88 | 2.47 | 3.36 | 3.44 | 3.49 | 3.53 | 3.62 |
| " | " | ⅝ | 26.46 | 2.45 | 3.38 | 3.46 | 3.51 | 3.55 | 3.64 |
| " | " | ⅝ | 30.00 | 2.44 | 3.40 | 3.48 | 3.53 | 3.57 | 3.67 |
| " | " | ⅝ | 33.46 | 2.42 | 3.42 | 3.51 | 3.55 | 3.60 | 3.69 |

Angles marked * are special sections.

RADII OF GYRATION FOR TWO ANGLES PLACED BACK TO BACK. ANGLES WITH UNEQUAL LEGS.

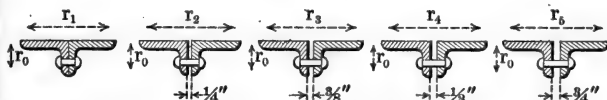


Radii of gyration correspond to directions indicated by arrowheads.

| Section Number. | Dimensions. Inches. | Thickness Inch. | Area of Two Angles. Sq. Ins. | Radii of Gyration. | | | | | |
|-----------------|------------------------|--------------------|---------------------------------|--------------------|----------------|----------------|----------------|----------------|----------------|
| | | | | r ₀ | r ₁ | r ₂ | r ₃ | r ₄ | r ₅ |
| A91 | 2½ x 2 | 1/8 | 1.62 | 0.79 | 0.79 | 0.88 | 0.92 | 0.97 | 1.07 |
| " | " | 3/8 | 3.10 | 0.77 | 0.82 | 0.91 | 0.96 | 1.01 | 1.12 |
| " | " | 1/2 | 4.00 | 0.75 | 0.84 | 0.94 | 0.99 | 1.04 | 1.15 |
| *A129 | 3 x 2 | 1/8 | 1.80 | 0.97 | 0.75 | 0.83 | 0.88 | 0.93 | 1.03 |
| " | " | 3/8 | 2.94 | 0.95 | 0.76 | 0.85 | 0.90 | 0.95 | 1.05 |
| " | " | 1/2 | 4.00 | 0.93 | 0.79 | 0.88 | 0.93 | 0.98 | 1.09 |
| A93 | 3 x 2½ | 1/4 | 2.62 | 0.95 | 1.00 | 1.09 | 1.13 | 1.18 | 1.28 |
| " | " | 3/8 | 3.84 | 0.93 | 1.02 | 1.11 | 1.16 | 1.21 | 1.31 |
| " | " | 1/2 | 5.56 | 0.91 | 1.05 | 1.15 | 1.20 | 1.25 | 1.35 |
| A95 | 3½ x 2½ | 1/4 | 2.88 | 1.12 | 0.96 | 1.04 | 1.09 | 1.13 | 1.23 |
| " | " | 1/2 | 5.50 | 1.09 | 1.00 | 1.09 | 1.14 | 1.19 | 1.29 |
| " | " | 1/2 | 6.12 | 1.08 | 1.01 | 1.10 | 1.15 | 1.20 | 1.31 |
| A97 | 3½ x 3 | 1/4 | 3.12 | 1.11 | 1.20 | 1.29 | 1.34 | 1.38 | 1.48 |
| " | " | 1/8 | 6.68 | 1.07 | 1.25 | 1.34 | 1.39 | 1.44 | 1.54 |
| " | " | 1/8 | 9.24 | 1.04 | 1.30 | 1.40 | 1.45 | 1.50 | 1.60 |
| A99 | 4 x 3 | 1/8 | 4.18 | 1.27 | 1.17 | 1.25 | 1.30 | 1.34 | 1.44 |
| " | " | 3/8 | 7.24 | 1.24 | 1.21 | 1.30 | 1.34 | 1.39 | 1.49 |
| " | " | 1/2 | 10.06 | 1.21 | 1.25 | 1.35 | 1.40 | 1.45 | 1.55 |
| *A131 | 4 x 3½ | 1/8 | 4.50 | 1.26 | 1.42 | 1.50 | 1.55 | 1.59 | 1.69 |
| " | " | 3/8 | 7.00 | 1.23 | 1.44 | 1.53 | 1.58 | 1.63 | 1.73 |
| " | " | 1/2 | 8.60 | 1.22 | 1.46 | 1.55 | 1.60 | 1.65 | 1.75 |
| A101 | 5 x 3 | 1/8 | 4.80 | 1.61 | 1.09 | 1.17 | 1.22 | 1.26 | 1.36 |
| " | " | 3/8 | 8.36 | 1.58 | 1.13 | 1.22 | 1.26 | 1.31 | 1.41 |
| " | " | 1/2 | 11.68 | 1.55 | 1.17 | 1.27 | 1.32 | 1.37 | 1.47 |
| A103 | 5 x 3½ | 3/8 | 6.10 | 1.60 | 1.34 | 1.42 | 1.46 | 1.51 | 1.60 |
| " | " | 1/2 | 9.84 | 1.56 | 1.37 | 1.46 | 1.51 | 1.56 | 1.66 |
| " | " | 3/4 | 13.34 | 1.53 | 1.42 | 1.51 | 1.56 | 1.61 | 1.71 |
| *A135 | 5 x 4 | 3/8 | 6.46 | 1.59 | 1.58 | 1.66 | 1.71 | 1.75 | 1.85 |
| " | " | 1/2 | 8.50 | 1.57 | 1.60 | 1.68 | 1.73 | 1.78 | 1.87 |
| " | " | 3/4 | 10.46 | 1.55 | 1.62 | 1.71 | 1.75 | 1.80 | 1.90 |
| A105 | 6 x 3½ | 3/8 | 6.84 | 1.94 | 1.26 | 1.34 | 1.39 | 1.43 | 1.53 |
| " | " | 1/2 | 11.10 | 1.90 | 1.30 | 1.39 | 1.43 | 1.48 | 1.58 |
| " | " | 3/4 | 15.10 | 1.87 | 1.34 | 1.44 | 1.49 | 1.53 | 1.64 |
| A107 | 6 x 4 | 3/8 | 7.22 | 1.93 | 1.50 | 1.58 | 1.62 | 1.67 | 1.76 |
| " | " | 1/2 | 11.72 | 1.90 | 1.53 | 1.62 | 1.67 | 1.71 | 1.81 |
| " | " | 3/4 | 15.96 | 1.86 | 1.58 | 1.67 | 1.71 | 1.76 | 1.86 |
| *A109 | 7 x 3½ | 1/8 | 8.80 | 2.26 | 1.16 | 1.29 | 1.33 | 1.38 | 1.47 |
| " | " | 3/8 | 10.00 | 2.25 | 1.22 | 1.30 | 1.35 | 1.39 | 1.48 |
| " | " | 1/2 | 12.34 | 2.24 | 1.24 | 1.32 | 1.37 | 1.42 | 1.51 |
| " | " | 3/4 | 15.74 | 2.21 | 1.27 | 1.36 | 1.41 | 1.46 | 1.56 |
| " | " | 1 | 19.00 | 2.19 | 1.31 | 1.40 | 1.45 | 1.50 | 1.60 |

Angles marked * are special sections.

**RADII OF GYRATION FOR TWO ANGLES
PLACED BACK TO BACK.
ANGLES WITH UNEQUAL LEGS.**



Radii of gyration correspond to directions indicated by arrowheads.

| Section Number. | Dimensions. | Thickness. | Area of Two Angles. Sq. Ins. | Radii of Gyration. | | | | | |
|-----------------|-------------|------------|---------------------------------|--------------------|----------------|----------------|----------------|----------------|----------------|
| | Inches. | Inch. | | r ₀ | r ₁ | r ₂ | r ₃ | r ₄ | r ₅ |
| A91 | 2½ x 2 | ⅜ | 1.62 | 0.60 | 1.10 | 1.19 | 1.24 | 1.29 | 1.39 |
| " | " | ⅝ | 3.10 | 0.58 | 1.13 | 1.23 | 1.28 | 1.33 | 1.43 |
| " | " | ½ | 4.00 | 0.56 | 1.15 | 1.25 | 1.30 | 1.35 | 1.46 |
| *A129 | 3 x 2 | ⅜ | 1.80 | 0.58 | 1.37 | 1.46 | 1.51 | 1.56 | 1.66 |
| " | " | ⅝ | 2.94 | 0.57 | 1.39 | 1.48 | 1.53 | 1.58 | 1.68 |
| " | " | ½ | 4.00 | 0.55 | 1.41 | 1.51 | 1.56 | 1.61 | 1.71 |
| A93 | 3 x 2½ | ¼ | 2.62 | 0.75 | 1.31 | 1.40 | 1.45 | 1.50 | 1.60 |
| " | " | ⅝ | 3.84 | 0.74 | 1.33 | 1.42 | 1.47 | 1.52 | 1.63 |
| " | " | ½ | 5.56 | 0.72 | 1.37 | 1.46 | 1.51 | 1.56 | 1.66 |
| A95 | 3½ x 2½ | ¼ | 2.88 | 0.74 | 1.58 | 1.67 | 1.72 | 1.76 | 1.86 |
| " | " | ⅝ | 5.50 | 0.70 | 1.62 | 1.72 | 1.77 | 1.81 | 1.92 |
| " | " | ½ | 6.12 | 0.70 | 1.64 | 1.73 | 1.78 | 1.83 | 1.93 |
| A97 | 3½ x 3 | ¼ | 3.12 | 0.91 | 1.52 | 1.61 | 1.66 | 1.70 | 1.80 |
| " | " | ⅝ | 6.68 | 0.87 | 1.57 | 1.66 | 1.71 | 1.76 | 1.86 |
| " | " | ½ | 9.24 | 0.85 | 1.61 | 1.71 | 1.76 | 1.81 | 1.91 |
| A99 | 4 x 3 | ⅜ | 4.18 | 0.89 | 1.79 | 1.88 | 1.93 | 1.97 | 2.07 |
| " | " | ⅝ | 7.24 | 0.86 | 1.83 | 1.93 | 1.97 | 2.02 | 2.12 |
| " | " | ½ | 10.06 | 0.83 | 1.88 | 1.97 | 2.02 | 2.08 | 2.18 |
| *A131 | 4 x 3½ | ⅜ | 4.50 | 1.07 | 1.73 | 1.81 | 1.86 | 1.91 | 2.00 |
| " | " | ⅝ | 7.00 | 1.04 | 1.76 | 1.85 | 1.89 | 1.94 | 2.04 |
| " | " | ½ | 8.60 | 1.02 | 1.78 | 1.87 | 1.92 | 1.97 | 2.07 |
| A101 | 5 x 3 | ⅜ | 4.80 | 0.85 | 2.33 | 2.42 | 2.47 | 2.52 | 2.61 |
| " | " | ⅝ | 8.86 | 0.82 | 2.37 | 2.47 | 2.52 | 2.57 | 2.67 |
| " | " | ½ | 11.68 | 0.80 | 2.42 | 2.52 | 2.57 | 2.62 | 2.72 |
| A103 | 5 x 3½ | ⅜ | 6.10 | 1.02 | 2.27 | 2.36 | 2.41 | 2.45 | 2.55 |
| " | " | ⅝ | 9.84 | 0.99 | 2.31 | 2.40 | 2.45 | 2.50 | 2.60 |
| " | " | ½ | 13.34 | 0.96 | 2.36 | 2.45 | 2.50 | 2.55 | 2.65 |
| *A135 | 5 x 4 | ⅜ | 6.46 | 1.20 | 2.20 | 2.29 | 2.34 | 2.38 | 2.48 |
| " | " | ⅝ | 8.50 | 1.18 | 2.22 | 2.31 | 2.36 | 2.41 | 2.50 |
| " | " | ½ | 10.46 | 1.17 | 2.24 | 2.33 | 2.38 | 2.43 | 2.53 |
| A105 | 6 x 3½ | ⅜ | 6.84 | 0.99 | 2.81 | 2.90 | 2.95 | 3.00 | 3.09 |
| " | " | ⅝ | 11.10 | 0.96 | 2.86 | 2.95 | 3.00 | 3.05 | 3.15 |
| " | " | ½ | 15.10 | 0.93 | 2.90 | 3.00 | 3.05 | 3.10 | 3.20 |
| A107 | 6 x 4 | ⅜ | 7.22 | 1.17 | 2.74 | 2.83 | 2.87 | 2.92 | 3.02 |
| " | " | ⅝ | 11.72 | 1.13 | 2.78 | 2.87 | 2.92 | 2.97 | 3.06 |
| " | " | ½ | 15.96 | 1.11 | 2.82 | 2.92 | 2.97 | 3.02 | 3.12 |
| *A109 | 7 x 3½ | ⅜ | 8.80 | 0.95 | 3.37 | 3.47 | 3.52 | 3.56 | 3.66 |
| " | " | ⅝ | 10.00 | 0.94 | 3.39 | 3.48 | 3.53 | 3.58 | 3.67 |
| " | " | ½ | 12.34 | 0.93 | 3.40 | 3.50 | 3.55 | 3.60 | 3.70 |
| " | " | ⅝ | 15.74 | 0.91 | 3.45 | 3.54 | 3.59 | 3.64 | 3.74 |
| " | " | 1 | 19.00 | 0.89 | 3.48 | 3.58 | 3.63 | 3.68 | 3.78 |

Angles marked * are special sections.

STRENGTH OF STEEL COLUMNS OR STRUTS.

For various values of $\frac{L}{r}$ in which L = length in feet and r = radius of gyration in inches.

P = ultimate strength in lbs. per square inch.

FOR SOFT STEEL.

$$P = \frac{45\,000}{1 + \frac{(12\,L)^2}{36\,000\,r^2}} \quad \text{Pin and square bearing} \quad P = \frac{45\,000}{1 + \frac{(12\,L)^2}{24\,000\,r^2}} \quad \text{Pin bearing} \quad P = \frac{45\,000}{1 + \frac{(12\,L)^2}{18\,000\,r^2}}$$

To obtain safe unit stress:

For quiescent loads, as in buildings, divide by 4.

For moving loads, as in bridges, divide by 5.

| $\frac{L}{r}$ | Ultimate Strength in lbs. per Square Inch. | | | $\frac{L}{r}$ | Ultimate Strength in lbs. per Square Inch. | | |
|---------------|---|-----------------|-------|---------------|---|-----------------|-------|
| | Square. | Pin and Square. | Pin. | | Square. | Pin and Square. | Pin. |
| 3.0 | 43437 | 42694 | 41978 | 7.6 | 36554 | 33419 | 30779 |
| 3.2 | 43230 | 42395 | 41593 | 7.8 | 36193 | 32966 | 30268 |
| 3.4 | 43011 | 42081 | 41190 | | | | |
| 3.6 | 42782 | 41754 | 40773 | 8.0 | 35828 | 32514 | 29762 |
| 3.8 | 42543 | 41412 | 40340 | 8.2 | 35462 | 32064 | 29260 |
| | | | | 8.4 | 35095 | 31615 | 28763 |
| 4.0 | 42294 | 41058 | 39893 | 8.6 | 34727 | 31169 | 28272 |
| 4.2 | 42035 | 40693 | 39435 | 8.8 | 34358 | 30724 | 27787 |
| 4.4 | 41765 | 40317 | 38966 | | | | |
| 4.6 | 41488 | 39930 | 38485 | 9.0 | 33988 | 30282 | 27306 |
| 4.8 | 41203 | 39534 | 37998 | 9.2 | 33611 | 29844 | 26832 |
| | | | | 9.4 | 33249 | 29408 | 26364 |
| 5.0 | 40910 | 39130 | 37500 | 9.6 | 32880 | 28977 | 25903 |
| 5.2 | 40608 | 38807 | 36997 | 9.8 | 32511 | 28549 | 25448 |
| 5.4 | 40299 | 38300 | 36488 | | | | |
| 5.6 | 39984 | 37874 | 35975 | 10.0 | 32143 | 28125 | 25000 |
| 5.8 | 39663 | 37443 | 35457 | 10.2 | 31776 | 27706 | 24559 |
| | | | | 10.4 | 31411 | 27290 | 24125 |
| 6.0 | 39335 | 37006 | 34938 | 10.6 | 31054 | 26879 | 23698 |
| 6.2 | 39003 | 36566 | 34416 | 10.8 | 30684 | 26474 | 23279 |
| 6.4 | 38665 | 36122 | 33894 | | | | |
| 6.6 | 38323 | 35676 | 33371 | 11.0 | 30324 | 26072 | 22866 |
| 6.8 | 37976 | 35219 | 32849 | 11.2 | 29965 | 25675 | 22460 |
| | | | | 11.4 | 29608 | 25285 | 22063 |
| 7.0 | 37616 | 34776 | 32328 | 11.6 | 29247 | 24899 | 21671 |
| 7.2 | 37272 | 34324 | 31809 | 11.8 | 28903 | 24517 | 21288 |
| 7.4 | 36914 | 33872 | 31292 | | | | |

STRENGTH OF STEEL COLUMNS OR STRUTS.

For various values of $\frac{L}{r}$ in which L = length in feet and r = radius of gyration in inches.

P = ultimate strength in lbs. per square inch.

FOR SOFT STEEL.

Square bearing

Pin and square bearing

Pin bearing

$$P = \frac{45\,000}{1 + \frac{(12L)^2}{36\,000r^2}}$$

$$P = \frac{45\,000}{1 + \frac{(12L)^2}{24\,000r^2}}$$

$$P = \frac{45\,000}{1 + \frac{(12L)^2}{18\,000r^2}}$$

To obtain safe unit stress:

For quiescent loads, as in buildings, divide by 4.

For moving loads, as in bridges, divide by 5.

| $\frac{L}{r}$ | Ultimate Strength in lbs. per Square Inch. | | | $\frac{L}{r}$ | Ultimate Strength in lbs. per Square Inch. | | |
|---------------|---|--------------------|-------|---------------|---|--------------------|-------|
| | Square. | Pin and Square. | Pin. | | Square. | Pin and Square. | Pin. |
| 12.0 | 28553 | 24142 | 20911 | 16.6 | 21406 | 16960 | 14043 |
| 12.2 | 28207 | 23771 | 20542 | 16.8 | 21137 | 16708 | 13812 |
| 12.4 | 27863 | 23406 | 20179 | | | | |
| 12.6 | 27522 | 23046 | 19823 | 17.0 | 20872 | 16459 | 13584 |
| 12.8 | 27185 | 22693 | 19474 | 17.2 | 20611 | 16216 | 13366 |
| | | | | 17.4 | 20353 | 15977 | 13150 |
| 13.0 | 26850 | 22343 | 19133 | 17.6 | 20098 | 15742 | 12938 |
| 13.2 | 26524 | 22005 | 18797 | 17.8 | 19847 | 15512 | 12731 |
| 13.4 | 26189 | 21662 | 18469 | | | | |
| 13.6 | 25864 | 21329 | 18148 | 18.0 | 19599 | 15286 | 12528 |
| 13.8 | 25543 | 21002 | 17833 | 18.2 | 19351 | 15063 | 12329 |
| | | | | 18.4 | 19114 | 14845 | 12135 |
| 14.0 | 25224 | 20680 | 17523 | 18.6 | 18878 | 14630 | 11944 |
| 14.2 | 24909 | 20363 | 17221 | 18.8 | 18644 | 14420 | 11757 |
| 14.4 | 24598 | 20052 | 16925 | | | | |
| 14.6 | 24290 | 19746 | 16634 | 19.0 | 18418 | 14218 | 11579 |
| 14.8 | 23985 | 19445 | 16350 | 19.2 | 18185 | 14010 | 11394 |
| | | | | 19.4 | 17961 | 13811 | 11219 |
| 15.0 | 23684 | 19148 | 16071 | 19.6 | 17740 | 13616 | 11048 |
| 15.2 | 23387 | 18858 | 15799 | 19.8 | 17519 | 13422 | 10877 |
| 15.4 | 23093 | 18572 | 15532 | | | | |
| 15.6 | 22803 | 18288 | 15270 | 20.0 | 17308 | 13235 | 10715 |
| 15.8 | 22516 | 18015 | 15105 | 20.2 | 17096 | 13050 | 10553 |
| | | | | 20.4 | 16888 | 12868 | 10434 |
| 16.0 | 22234 | 17744 | 14764 | 20.6 | 16682 | 12690 | 10249 |
| 16.2 | 21954 | 17478 | 14518 | 20.8 | 16480 | 12515 | 10087 |
| 16.4 | 21678 | 17216 | 14279 | | | | |

STRENGTH OF STEEL COLUMNS OR STRUTS.

For various values of $\frac{L}{r}$ in which L = length in feet and r = radius of gyration in inches.

P = ultimate strength in lbs. per square inch.

FOR MEDIUM STEEL.

$$P = \frac{50\,000}{1 + \frac{(12L)^2}{36\,000r^2}} \quad \text{Pin and square bearing} \quad P = \frac{50\,000}{1 + \frac{(12L)^2}{24\,000r^2}} \quad \text{Pin bearing} \quad P = \frac{50\,000}{1 + \frac{(12L)^2}{18\,000r^2}}$$

To obtain safe unit stress:

For quiescent loads, as in buildings, divide by 4.

For moving loads, as in bridges, divide by 5.

| $\frac{L}{r}$ | Ultimate Strength in lbs. per Square Inch. | | | $\frac{L}{r}$ | Ultimate Strength in lbs. per Square Inch. | | |
|---------------|---|-----------------|-------|---------------|---|-----------------|-------|
| | Square. | Pin and Square. | Pin. | | Square. | Pin and Square. | Pin. |
| 3.0 | 48263 | 47438 | 46642 | 7.6 | 40616 | 37132 | 34199 |
| 3.2 | 48033 | 47106 | 46214 | 7.8 | 40214 | 36629 | 33631 |
| 3.4 | 47790 | 46757 | 45767 | | | | |
| 3.6 | 47536 | 46393 | 45303 | 8.0 | 39809 | 36127 | 33069 |
| 3.8 | 47270 | 46013 | 44822 | 8.2 | 39402 | 35627 | 32511 |
| | | | | 8.4 | 38994 | 35128 | 31959 |
| 4.0 | 46993 | 45620 | 44325 | 8.6 | 38585 | 34632 | 31413 |
| 4.2 | 46705 | 45214 | 43817 | 8.8 | 38175 | 34138 | 30874 |
| 4.4 | 46406 | 44797 | 43295 | | | | |
| 4.6 | 46098 | 44367 | 42761 | 9.0 | 37764 | 33647 | 30340 |
| 4.8 | 45781 | 43927 | 42220 | 9.2 | 37354 | 33160 | 29813 |
| | | | | 9.4 | 36943 | 32676 | 29293 |
| 5.0 | 45455 | 43478 | 41667 | 9.6 | 36533 | 32197 | 28781 |
| 5.2 | 45120 | 43020 | 41108 | 9.8 | 36123 | 31721 | 28275 |
| 5.4 | 44777 | 42555 | 40542 | | | | |
| 5.6 | 44427 | 42082 | 39972 | 10.0 | 35714 | 31250 | 27778 |
| 5.8 | 44070 | 41603 | 39397 | 10.2 | 35307 | 30784 | 27288 |
| | | | | 10.4 | 34901 | 30322 | 26806 |
| 6.0 | 43706 | 41118 | 38820 | 10.6 | 34496 | 29866 | 26331 |
| 6.2 | 43337 | 40629 | 38240 | 10.8 | 34093 | 29415 | 25865 |
| 6.4 | 42961 | 40136 | 37660 | | | | |
| 6.6 | 42581 | 39640 | 37079 | 11.0 | 33693 | 28969 | 25407 |
| 6.8 | 42196 | 39141 | 36499 | 11.2 | 33294 | 28528 | 24956 |
| | | | | 11.4 | 32898 | 28094 | 24514 |
| 7.0 | 41806 | 38640 | 35920 | 11.6 | 32505 | 27665 | 24079 |
| 7.2 | 41413 | 38138 | 35343 | 11.8 | 32114 | 27241 | 23653 |
| 7.4 | 41016 | 37635 | 34769 | | | | |

STRENGTH OF STEEL COLUMNS OR STRUTS.

For various values of $\frac{L}{r}$ in which L = length in feet and r = radius of gyration in inches.

P = ultimate strength in lbs. per square inch.

FOR MEDIUM STEEL.

$$P = \frac{50\,000}{1 + \frac{(12L)^2}{36\,000r^2}} \quad \text{Pin and square bearing} \quad P = \frac{50\,000}{1 + \frac{(12L)^2}{24\,000r^2}} \quad \text{Pin bearing} \quad P = \frac{50\,000}{1 + \frac{(12L)^2}{18\,000r^2}}$$

To obtain safe unit stress:

For quiescent loads, as in buildings, divide by 4.

For moving loads, as in bridges, divide by 5.

| $\frac{L}{r}$ | Ultimate Strength in lbs. per Square Inch. | | | $\frac{L}{r}$ | Ultimate Strength in lbs. per Square Inch. | | |
|---------------|---|-----------------|-------|---------------|---|-----------------|-------|
| | Square. | Pin and Square. | Pin. | | Square. | Pin and Square. | Pin. |
| 12.0 | 31726 | 26824 | 23234 | 16.6 | 23784 | 18844 | 15603 |
| 12.2 | 31341 | 26412 | 22824 | 16.8 | 23486 | 18564 | 15347 |
| 12.4 | 30959 | 26007 | 22421 | | | | |
| 12.6 | 30580 | 25607 | 22026 | 17.0 | 23191 | 18288 | 15097 |
| 12.8 | 30205 | 25214 | 21638 | 17.2 | 22901 | 18018 | 14851 |
| | | | | 17.4 | 22614 | 17752 | 14611 |
| 13.0 | 29833 | 24826 | 21259 | 17.6 | 22331 | 17491 | 14376 |
| 13.2 | 29464 | 24445 | 20886 | 17.8 | 22052 | 17235 | 14145 |
| 13.4 | 29099 | 24069 | 20521 | | | | |
| 13.6 | 28738 | 23699 | 20164 | 18.0 | 21777 | 16984 | 13920 |
| 13.8 | 28381 | 23336 | 19814 | 18.2 | 21506 | 16737 | 13699 |
| | | | | 18.4 | 21238 | 16494 | 13483 |
| 14.0 | 28027 | 22978 | 19470 | 18.6 | 20975 | 16256 | 13271 |
| 14.2 | 27677 | 22626 | 19134 | 18.8 | 20715 | 16022 | 13063 |
| 14.4 | 27331 | 22280 | 18805 | | | | |
| 14.6 | 26989 | 21940 | 18482 | 19.0 | 20458 | 15793 | 12860 |
| 14.8 | 26650 | 21605 | 18167 | 19.2 | 20206 | 15567 | 12661 |
| | | | | 19.4 | 19957 | 15346 | 12466 |
| 15.0 | 26316 | 21276 | 17857 | 19.6 | 19711 | 15129 | 12275 |
| 15.2 | 25985 | 20953 | 17554 | 19.8 | 19466 | 14913 | 12086 |
| 15.4 | 25659 | 20636 | 17258 | | | | |
| 15.6 | 25337 | 20320 | 16967 | 20.0 | 19231 | 14706 | 11905 |
| 15.8 | 25018 | 20017 | 16683 | 20.2 | 18996 | 14500 | 11725 |
| | | | | 20.4 | 18764 | 14298 | 11549 |
| 16.0 | 24704 | 19716 | 16404 | 20.6 | 18536 | 14100 | 11377 |
| 16.2 | 24393 | 19420 | 16131 | 20.8 | 18311 | 13905 | 11208 |
| 16.4 | 24087 | 19129 | 15865 | | | | |

EXAMPLE OF THE USE OF THE TABLES OF RADII OF GYRATION FOR TWO ANGLES PLACED BACK TO BACK AND THE TABLES OF STRENGTH OF STEEL COLUMNS OR STRUTS.

PAGES 215 TO 221 INCLUSIVE

What is the size of truss member required to safely sustain 50 000 pounds in compression, the safety factor being 4, the unsupported length 8 feet, the gusset plates at each end being $\frac{3}{8}$ " thick?

Assume for trial two 4" x 3" x $\frac{5}{16}$ " angles with the long legs together. Referring to page 216, the least Radius of Gyration, comparing values in columns r_0 and r_3 is found to be 1.27. The ratio of the length of the column in feet to the Least Radius of Gyration in inches, $\frac{L}{r}$ is, there-

fore, $\frac{8}{1.27} = 6.3$.

Referring to the table of Strength of Steel Columns or Struts for medium steel, page 220, the ultimate strength of a column in which $\frac{L}{r} = 6.3$ is found by interpolation between the values for 6.2 and 6.4

to be 43 149 pounds per square inch, which, divided by the safety factor 4, gives 10 787 pounds as the safe unit stress per square inch. Multiplying the safe unit stress per square inch, 10 787 pounds, by 4.18, the area of the two angles in square inches, gives 45 090 pounds as the total safe load. This is slightly less than the specified load of 50 000 pounds, and, therefore, it will be necessary to increase the assumed section. Assume the angles to be 4" x 3" x $\frac{3}{8}$ ", for which the Least Radius of Gyration is found by interpolation to be 1.26, and, by

the same process used above, $\frac{L}{r}$ is found to be 6.35, which corre-

sponds to an ultimate strength of 43 055 pounds per square inch, or a safe unit stress of 10 764 pounds per square inch, which, if multiplied by the area of the two angles, 4.96 square inches, gives a safe total load of 53 389 pounds, which is ample to meet the conditions stated.

EXPLANATION OF TABLES RELATING TO DIMENSIONS AND SAFE LOADS OF STEEL COLUMNS OF VARIOUS SECTIONS.

PAGES 224 TO 301 INCLUSIVE

Tables of Dimensions for Plate and Angle Columns are given on pages 224 and 225, the Moments of Inertia and Section Moduli about two rectangular axes are given on pages 226 to 228 and the Safe Loads for various lengths, calculated for the Radius of Gyration about each of the two rectangular axes, are given on pages 248 to 267 inclusive.

Tables of Dimensions for Latticed Channel Columns are given on pages 230, the Moments of Inertia and Section Moduli about two rectangular axes are given on page 231, the Safe Loads for various lengths

based upon the Least Radius of Gyration, are given on pages 268 to 271, and data relating to the proper sizes of lattice bars and stay-plates to be used with these columns are given on pages 272 and 273.

On pages 232 and 233 are given the Principal Dimensions of Plate and Channel Columns with comparatively narrow plates called, for convenience of reference, Series A, and on pages 234 and 235 for Series B, which differs from Series A, in having wider plates. Moments of Inertia and Section Moduli about two rectangular axes are given for Series A and B on pages 236 to 242 inclusive, and the Safe Loads for different lengths, based upon the Least Radius of Gyration, are given on pages 274 to 301 inclusive.

Safe Loads for I-Beams used as Columns or Struts are given on pages 244 to 247, and the dimensions of these sections can be obtained from the tables on pages 186 to 189 inclusive.

The Plate and Channel Columns given in Series A are particularly useful in buildings or locations in which it is desired to keep the extreme dimensions of the cross section as small as possible for this style of column, although in this series the Radius of Gyration about the central axis parallel to the channel webs is somewhat smaller than the Radius of Gyration about the axis perpendicular to the channel webs. This makes the narrower columns of Series A somewhat less economical of material than the wider columns of Series B, which, however, is small in amount for columns of ordinary story length of 10 feet to 14 feet, such as are used in skeleton buildings.

In Series B of Plate and Channel Columns with wider plates, the Radii of Gyration about the two axes are practically equal for the intermediate thicknesses and these columns are slightly more economical of material than those of Series A, although they require somewhat more space on account of their wider sections.

The Safe Loads for columns of various kinds, as given on pages 244 to 301 inclusive, are expressed in thousands of pounds, and have been figured by the use of Gordon's formula, as stated at the heads of the various tables, using the safety factor 4, which relates to static or quiescent loads such as occur in ordinary buildings.

On page 229 is given a table showing the Distances Back to Back for Spacing Two Channels of the same size in order to produce equal Moments of Inertia about the two rectangular axes. This table will be found to be useful in designing compression members of trusses, etc.

The Safe Loads of the tables are assumed to be centrally applied, and for convenience in computing the proper sizes required to support eccentric loads the tables of Moments of Inertia and Section Moduli for the different sections of columns are given.

The Safe Loads in the various tables are figured for extreme ratios from 30 to 150 for $\frac{l}{r}$, in which l is the length of the column and r the Least Radius of Gyration, both expressed in inches.

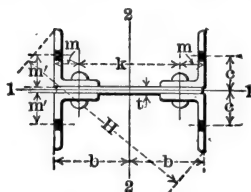
The weights of columns stated in the tables are per lineal foot of shaft, and do not include any allowances for bases, brackets or other connections, as these depend upon the particular details and requirements of each case.

Loads for other safety factors can be figured from the tables by inverse proportion, thus:

New safety factor : 4 :: load from tables : new loads.

Drawings of typical details of steel columns are given on page 243.

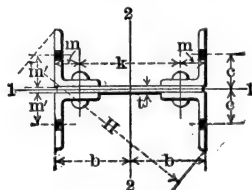
DIMENSIONS FOR PLATE AND ANGLE COLUMNS.



| Size of Angles. | Size of Plates. | Weight of Column. | Area of Column Section. | b | c | m | m' | k | H |
|-----------------|-----------------|-------------------|-------------------------|---------|---------|---------|---------|---------|--------------|
| Inches. | Inches. | Lbs. per Ft. | Sq. Ins. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. |
| 3" x 2½" x ¼" | 6" x ¼" | 23.1 44.2 | 6.74 13.00 | 3½" | 1⅞" | 1⅝" | 1¾" | 3½" | 8½" 9" |
| 3" x 2½" x ¼" | 8" x ¼" | 24.8 47.6 | 7.24 14.00 | 4½" | 1⅞" | 1⅝" | 1¾" | 5½" | 10⅝" 10½" |
| 3" x 2½" x ¼" | 10" x ¼" | 26.5 51.0 | 7.74 15.00 | 5½" | 1⅞" | 1⅝" | 1¾" | 7½" | 12" 12½" |
| 3" x 2½" x ¼" | 12" x ¼" | 28.2 54.4 | 8.24 16.00 | 6½" | 1⅞" | 1⅝" | 1¾" | 9½" | 13¼" 13½" |
| 3½" x 2½" x ¼" | 7" x ¼" | 25.6 59.5 | 7.51 17.49 | 3⅝" | 2⅜" | 1⅝" | 2¼" | 4½" | 10¼" 10½" |
| 3½" x 2½" x ¼" | 8" x ¼" | 26.4 62.0 | 7.76 18.24 | 4½" | 2⅜" | 1⅝" | 2¼" | 5½" | 11" 11⅞" |
| 3½" x 2½" x ¼" | 10" x ¼" | 28.1 67.1 | 8.26 19.74 | 5½" | 2⅜" | 1⅝" | 2¼" | 7½" | 12¼" 12½" |
| 3½" x 2½" x ¼" | 12" x ¼" | 29.8 72.2 | 8.76 21.24 | 6½" | 2⅜" | 1⅝" | 2¼" | 9½" | 14¼" 14½" |
| 4" x 3" x ⅝" | 8" x ⅝" | 37.3 97.0 | 10.86 28.44 | 4½" | 2⅞" | 1¾" | 2¼" | 4¾" | 11½" 12⅝" |
| 4" x 3" x ⅝" | 10" x ⅝" | 39.4 103.0 | 11.49 30.19 | 5½" | 2⅞" | 1¾" | 2¼" | 6¾" | 13¼" 13⅞" |
| 4" x 3" x ⅝" | 12" x ⅝" | 41.6 108.9 | 12.11 31.94 | 6½" | 2⅞" | 1¾" | 2¼" | 8¾" | 14½" 15⅝" |
| 4" x 3" x ⅝" | 14" x ⅝" | 43.7 114.9 | 12.74 33.69 | 7½" | 2⅞" | 1¾" | 2¼" | 10¾" | 16¼" 16½" |

Dimensions m' and c may be varied to suit requirements.

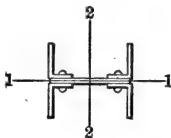
DIMENSIONS FOR PLATE AND ANGLE COLUMNS.



| Size of Angles. | Size of Plates. | Weight of Column. | Area of Column Section. | b | c | m | m' | k | H |
|---|--------------------------|-------------------|-------------------------|-----------------|----------------------------------|----------------|----------------|-----------------|------------------------------------|
| Inches. | Inches. | Lbs. per Ft. | Sq. Ins. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. |
| $5 \times 3\frac{1}{2} \times \frac{1}{16}$ | $10 \times \frac{1}{16}$ | 45.4 128.7 | 13.37 37.74 | $5\frac{1}{8}$ | $2\frac{1}{8}$ $2\frac{1}{4}$ | $2\frac{1}{4}$ | $2\frac{1}{4}$ | $5\frac{1}{4}$ | $14\frac{1}{8}$ 15 |
| $5 \times 3\frac{1}{2} \times \frac{1}{16}$ | $12 \times \frac{1}{16}$ | 47.6 135.1 | 13.99 39.61 | $6\frac{1}{8}$ | $2\frac{1}{8}$ $2\frac{1}{4}$ | $2\frac{1}{4}$ | $2\frac{1}{4}$ | $7\frac{1}{4}$ | 16 $16\frac{1}{8}$ |
| $5 \times 3\frac{1}{2} \times \frac{1}{16}$ | $14 \times \frac{1}{16}$ | 49.7 141.5 | 14.62 41.49 | $7\frac{1}{8}$ | $2\frac{1}{8}$ $2\frac{1}{4}$ | $2\frac{1}{4}$ | $2\frac{1}{4}$ | $9\frac{1}{4}$ | $17\frac{1}{8}$ $17\frac{1}{4}$ |
| $5 \times 3\frac{1}{2} \times \frac{1}{16}$ | $16 \times \frac{1}{16}$ | 51.8 147.8 | 15.24 43.36 | $8\frac{1}{8}$ | $2\frac{1}{8}$ $2\frac{1}{4}$ | $2\frac{1}{4}$ | $2\frac{1}{4}$ | $11\frac{1}{4}$ | $19\frac{1}{4}$ $19\frac{1}{8}$ |
| $6 \times 3\frac{1}{2} \times \frac{3}{16}$ | $12 \times \frac{3}{16}$ | 62.1 166.4 | 18.18 46.00 | $6\frac{1}{8}$ | $2\frac{1}{8}$ $2\frac{1}{4}$ | $2\frac{1}{4}$ | $2\frac{1}{4}$ | $7\frac{1}{4}$ | $17\frac{1}{8}$ $17\frac{1}{4}$ |
| $6 \times 3\frac{1}{2} \times \frac{3}{16}$ | $14 \times \frac{3}{16}$ | 64.7 168.2 | 18.93 48.00 | $7\frac{1}{8}$ | $2\frac{1}{8}$ $2\frac{1}{4}$ | $2\frac{1}{4}$ | $2\frac{1}{4}$ | $9\frac{1}{4}$ | $18\frac{3}{8}$ $19\frac{1}{8}$ |
| $6 \times 3\frac{1}{2} \times \frac{3}{16}$ | $16 \times \frac{3}{16}$ | 67.2 170.0 | 19.68 50.00 | $8\frac{1}{8}$ | $2\frac{1}{8}$ $2\frac{1}{4}$ | $2\frac{1}{4}$ | $2\frac{1}{4}$ | $11\frac{1}{4}$ | $20\frac{1}{8}$ $20\frac{1}{4}$ |
| $6 \times 3\frac{1}{2} \times \frac{3}{16}$ | $18 \times \frac{3}{16}$ | 69.8 176.8 | 20.43 52.00 | $9\frac{1}{8}$ | $2\frac{1}{8}$ $2\frac{1}{4}$ | $2\frac{1}{4}$ | $2\frac{1}{4}$ | $13\frac{1}{4}$ | $22\frac{1}{8}$ $22\frac{1}{4}$ |
| $7 \times 3\frac{1}{2} \times \frac{1}{4}$ | $14 \times \frac{1}{4}$ | 80.8 176.8 | 23.73 52.00 | $7\frac{1}{8}$ | $2\frac{1}{2}$ $2\frac{3}{4}$ | $2\frac{1}{4}$ | $2\frac{1}{4}$ | $9\frac{1}{4}$ | $20\frac{1}{8}$ $20\frac{1}{4}$ |
| $7 \times 3\frac{1}{2} \times \frac{1}{4}$ | $16 \times \frac{1}{4}$ | 83.8 183.6 | 24.60 54.00 | $8\frac{1}{8}$ | $2\frac{1}{2}$ $2\frac{3}{4}$ | $2\frac{1}{4}$ | $2\frac{1}{4}$ | $11\frac{1}{4}$ | $21\frac{1}{4}$ $22\frac{3}{8}$ |
| $7 \times 3\frac{1}{2} \times \frac{1}{4}$ | $18 \times \frac{1}{4}$ | 86.8 190.4 | 25.48 56.00 | $9\frac{1}{8}$ | $2\frac{1}{2}$ $2\frac{3}{4}$ | $2\frac{1}{4}$ | $2\frac{1}{4}$ | $13\frac{1}{4}$ | $23\frac{1}{4}$ $23\frac{3}{8}$ |
| $7 \times 3\frac{1}{2} \times \frac{1}{4}$ | $20 \times \frac{1}{4}$ | 89.8 197.2 | 26.35 58.00 | $10\frac{1}{8}$ | $2\frac{1}{2}$ $2\frac{3}{4}$ | $2\frac{1}{4}$ | $2\frac{1}{4}$ | $15\frac{1}{4}$ | $24\frac{1}{4}$ $25\frac{1}{8}$ |

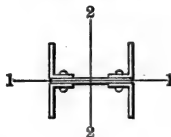
Dimensions m' and c may be varied to suit requirements.

MOMENTS OF INERTIA AND SECTION MODULI FOR PLATE AND ANGLE COLUMNS.



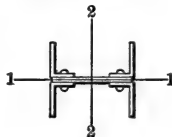
| Size of Angles. | Size of Plate. | Axis 1-1. | | Axis 2-2. | | Size of Plate. | Axis 1-1. | | Axis 2-2. | |
|-----------------------|----------------------|-----------------------|---------------------|-----------------------|---------------------|----------------------|-----------------------|---------------------|-----------------------|---------------------|
| | | Moment of Inertia. | Section Modulus. | Moment of Inertia. | Section Modulus. | | Moment of Inertia. | Section Modulus. | Moment of Inertia. | Section Modulus. |
| Inches. | Inches. | Ins. ⁴ | Ins. ³ | Ins. ⁴ | Ins. ³ | Inches. | Ins. ⁴ | Ins. ³ | Ins. ⁴ | Ins. ³ |
| 3 x 2½ x ¼ | 6 x ¼ | 10.3 | 3.3 | 39.4 | 12.6 | 8 x ¼ | 10.3 | 3.3 | 76.7 | 18.6 |
| " " ⅜ | " " ⅜ | 13.4 | 4.3 | 47.9 | 15.3 | " " ⅜ | 13.4 | 4.3 | 93.7 | 22.7 |
| " " ½ | " " ½ | 16.7 | 5.2 | 55.9 | 17.9 | " " ½ | 16.7 | 5.3 | 110.1 | 26.7 |
| " " ⅝ | " " ⅝ | 20.2 | 6.3 | 63.5 | 20.3 | " " ⅝ | 20.3 | 6.3 | 125.6 | 30.5 |
| " " ¾ | " " ¾ | 24.0 | 7.4 | 70.6 | 22.6 | " " ¾ | 24.0 | 7.4 | 140.5 | 34.1 |
| " " ⅞ | " " ⅞ | 28.1 | 8.6 | 77.3 | 24.8 | " " ⅞ | 28.1 | 8.6 | 154.6 | 37.5 |
| 3 x 2½ x ¼ | 10 x ¼ | 10.3 | 3.3 | 128.4 | 25.1 | 12 x ¼ | 10.3 | 3.3 | 195.7 | 32.0 |
| " " ⅜ | " " ⅜ | 13.4 | 4.3 | 157.5 | 30.7 | " " ⅜ | 13.4 | 4.3 | 240.5 | 39.3 |
| " " ½ | " " ½ | 16.7 | 5.3 | 185.6 | 36.2 | " " ½ | 16.7 | 5.3 | 284.0 | 46.4 |
| " " ⅝ | " " ⅝ | 20.3 | 6.3 | 212.5 | 41.5 | " " ⅝ | 20.3 | 6.3 | 325.8 | 53.2 |
| " " ¾ | " " ¾ | 24.1 | 7.4 | 238.3 | 46.5 | " " ¾ | 24.1 | 7.4 | 366.1 | 59.8 |
| " " ⅞ | " " ⅞ | 28.1 | 8.6 | 263.1 | 51.3 | " " ⅞ | 28.2 | 8.6 | 405.1 | 66.1 |
| 3½ x 2½ x ¼ | 7 x ¼ | 16.0 | 4.4 | 62.4 | 17.2 | 8 x ¼ | 16.0 | 4.4 | 84.7 | 20.5 |
| " " ⅜ | " " ⅜ | 20.7 | 5.7 | 76.2 | 21.0 | " " ⅜ | 20.7 | 5.7 | 103.6 | 25.1 |
| " " ½ | " " ½ | 25.6 | 6.9 | 89.3 | 24.6 | " " ½ | 25.6 | 6.9 | 121.7 | 29.5 |
| " " ⅝ | " " ⅝ | 30.8 | 8.3 | 101.7 | 28.1 | " " ⅝ | 30.8 | 8.3 | 138.9 | 33.7 |
| " " ¾ | " " ¾ | 36.3 | 9.7 | 113.6 | 31.3 | " " ¾ | 36.3 | 9.7 | 155.5 | 37.7 |
| " " ⅞ | " " ⅞ | 42.1 | 11.1 | 124.8 | 34.4 | " " ⅞ | 42.1 | 11.1 | 171.2 | 41.5 |
| 3½ x 2½ x ¼ | 10 x ¼ | 16.0 | 4.4 | 140.9 | 27.5 | 12 x ¼ | 16.0 | 4.4 | 213.7 | 34.9 |
| " " ⅜ | " " ⅜ | 20.7 | 5.7 | 173.0 | 33.8 | " " ⅜ | 20.7 | 5.7 | 262.9 | 42.9 |
| " " ½ | " " ½ | 25.6 | 6.9 | 203.9 | 39.8 | " " ½ | 25.6 | 7.0 | 310.5 | 50.7 |
| " " ⅝ | " " ⅝ | 30.8 | 8.3 | 233.5 | 45.6 | " " ⅝ | 30.8 | 8.3 | 356.2 | 58.2 |
| " " ¾ | " " ¾ | 36.3 | 9.7 | 262.1 | 51.1 | " " ¾ | 36.4 | 9.7 | 400.7 | 65.4 |
| " " ⅞ | " " ⅞ | 42.2 | 11.2 | 289.4 | 56.5 | " " ⅞ | 42.2 | 11.2 | 443.4 | 72.4 |

MOMENTS OF INERTIA AND SECTION MODULI FOR PLATE AND ANGLE COLUMNS.



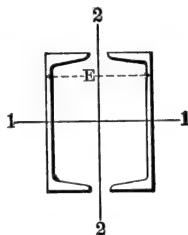
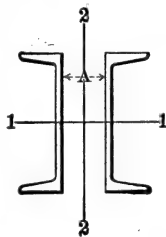
| Size of Angles. | Size of Plate. | Axis 1-1. | | Axis 2-2. | | Size of Plate. | Axis 1-1. | | Axis 2-2. | | |
|-----------------------|----------------------|--------------------------|---------------------|--------------------------|---------------------|----------------------|--------------------------|---------------------|-------------------|-------------------|-------|
| | | Moment of Inertia. | Section Modulus. | Moment of Inertia. | Section Modulus. | | Moment of Inertia. | Section Modulus. | | | |
| Inches. | Inches. | Ina. ⁴ | Ina. ³ | Ina. ⁴ | Ina. ³ | Inches. | Ina. ⁴ | Ina. ³ | Ina. ⁴ | Ina. ³ | |
| 4 x 3 | $\frac{1}{8}$ | 8x $\frac{1}{8}$ | 30.3 | 7.3 | 114.6 | 27.8 | 10x $\frac{1}{8}$ | 30.3 | 7.3 | 192.0 | 37.5 |
| " | $\frac{3}{8}$ | " $\frac{3}{8}$ | 37.4 | 8.9 | 134.8 | 32.7 | " $\frac{3}{8}$ | 37.4 | 8.9 | 226.4 | 44.2 |
| " | $\frac{1}{2}$ | " $\frac{1}{2}$ | 44.8 | 10.6 | 154.0 | 37.3 | " $\frac{1}{2}$ | 44.8 | 10.6 | 259.5 | 50.6 |
| " | $\frac{5}{8}$ | " $\frac{5}{8}$ | 52.6 | 12.4 | 172.4 | 41.8 | " $\frac{5}{8}$ | 52.6 | 12.4 | 291.5 | 56.9 |
| " | $\frac{3}{4}$ | " $\frac{3}{4}$ | 60.8 | 14.2 | 190.0 | 46.1 | " $\frac{3}{4}$ | 60.9 | 14.2 | 322.2 | 62.9 |
| " | $\frac{7}{8}$ | " $\frac{7}{8}$ | 69.5 | 16.1 | 206.9 | 50.2 | " $\frac{7}{8}$ | 69.5 | 16.1 | 352.0 | 68.7 |
| " | 1 | "1 | 78.6 | 18.1 | 223.0 | 54.1 | "1 | 78.6 | 18.1 | 380.5 | 74.2 |
| " | 1 $\frac{1}{8}$ | "1 $\frac{1}{8}$ | 88.1 | 20.1 | 238.3 | 57.8 | "1 $\frac{1}{8}$ | 88.2 | 20.2 | 408.0 | 79.6 |
| " | 1 $\frac{1}{4}$ | "1 $\frac{1}{4}$ | 98.1 | 22.3 | 253.0 | 61.3 | "1 $\frac{1}{4}$ | 98.2 | 22.3 | 434.4 | 84.7 |
| " | 1 $\frac{1}{2}$ | "1 $\frac{1}{2}$ | 108.5 | 24.4 | 267.0 | 64.7 | "1 $\frac{1}{2}$ | 108.6 | 24.5 | 459.8 | 89.7 |
| 4 x 3 | $\frac{3}{8}$ | 12x $\frac{3}{8}$ | 30.3 | 7.3 | 292.3 | 47.7 | 14x $\frac{3}{8}$ | 30.3 | 7.3 | 416.8 | 58.5 |
| " | $\frac{1}{2}$ | " $\frac{1}{2}$ | 37.4 | 8.9 | 345.5 | 56.4 | " $\frac{1}{2}$ | 37.4 | 8.9 | 493.4 | 69.3 |
| " | $\frac{5}{8}$ | " $\frac{5}{8}$ | 44.8 | 10.6 | 396.7 | 64.8 | " $\frac{5}{8}$ | 44.8 | 10.6 | 567.4 | 79.6 |
| " | $\frac{3}{4}$ | " $\frac{3}{4}$ | 52.6 | 12.4 | 446.6 | 72.9 | " $\frac{3}{4}$ | 52.7 | 12.4 | 639.7 | 89.8 |
| " | $\frac{7}{8}$ | " $\frac{7}{8}$ | 60.9 | 14.2 | 494.7 | 80.8 | " $\frac{7}{8}$ | 60.9 | 14.2 | 709.6 | 99.6 |
| " | 1 | "1 | 69.6 | 16.1 | 541.5 | 88.4 | "1 | 69.6 | 16.1 | 777.8 | 109.2 |
| " | 1 $\frac{1}{8}$ | "1 $\frac{1}{8}$ | 78.7 | 18.1 | 586.5 | 95.8 | "1 $\frac{1}{8}$ | 78.7 | 18.1 | 843.7 | 118.4 |
| " | 1 $\frac{1}{4}$ | "1 $\frac{1}{4}$ | 88.2 | 20.2 | 630.1 | 102.9 | "1 $\frac{1}{4}$ | 88.3 | 20.2 | 907.7 | 127.4 |
| " | 1 $\frac{1}{2}$ | "1 $\frac{1}{2}$ | 98.2 | 22.3 | 672.2 | 109.8 | "1 $\frac{1}{2}$ | 98.3 | 22.3 | 969.8 | 136.1 |
| " | 1 $\frac{3}{4}$ | "1 $\frac{3}{4}$ | 108.7 | 24.5 | 713.1 | 116.4 | "1 $\frac{3}{4}$ | 108.8 | 24.5 | 1030.1 | 144.6 |
| 5 x 3 $\frac{1}{2}$ | $\frac{1}{8}$ | 10x $\frac{1}{8}$ | 57.6 | 11.2 | 225.0 | 43.9 | 12x $\frac{1}{8}$ | 57.6 | 11.2 | 341.9 | 55.8 |
| " | $\frac{3}{8}$ | " $\frac{3}{8}$ | 70.6 | 13.6 | 265.7 | 51.8 | " $\frac{3}{8}$ | 70.6 | 13.6 | 404.6 | 66.1 |
| " | $\frac{1}{2}$ | " $\frac{1}{2}$ | 84.1 | 16.1 | 304.8 | 59.5 | " $\frac{1}{2}$ | 84.1 | 16.1 | 465.2 | 75.9 |
| " | $\frac{5}{8}$ | " $\frac{5}{8}$ | 98.2 | 18.7 | 342.6 | 66.9 | " $\frac{5}{8}$ | 98.2 | 18.7 | 524.0 | 85.5 |
| " | $\frac{3}{4}$ | " $\frac{3}{4}$ | 112.9 | 21.4 | 379.1 | 74.0 | " $\frac{3}{4}$ | 112.9 | 21.4 | 581.0 | 94.9 |
| " | $\frac{7}{8}$ | " $\frac{7}{8}$ | 128.2 | 24.1 | 414.4 | 80.9 | " $\frac{7}{8}$ | 128.2 | 24.1 | 636.4 | 103.9 |
| " | 1 | "1 | 144.1 | 27.0 | 448.2 | 87.5 | "1 | 144.1 | 27.0 | 689.8 | 112.6 |
| " | 1 $\frac{1}{8}$ | "1 $\frac{1}{8}$ | 160.6 | 29.9 | 481.1 | 93.9 | "1 $\frac{1}{8}$ | 160.7 | 29.9 | 741.8 | 121.1 |
| " | 1 $\frac{1}{4}$ | "1 $\frac{1}{4}$ | 177.8 | 32.9 | 512.6 | 100.0 | "1 $\frac{1}{4}$ | 177.9 | 32.9 | 792.1 | 129.3 |
| " | 1 $\frac{1}{2}$ | "1 $\frac{1}{2}$ | 195.7 | 36.0 | 543.1 | 106.0 | "1 $\frac{1}{2}$ | 195.8 | 36.0 | 841.0 | 137.3 |
| " | 1 $\frac{3}{4}$ | "1 $\frac{3}{4}$ | 214.2 | 39.2 | 572.5 | 111.7 | "1 $\frac{3}{4}$ | 214.3 | 39.2 | 888.2 | 145.0 |
| 5 x 3 $\frac{1}{2}$ | $\frac{3}{8}$ | 14x $\frac{3}{8}$ | 57.6 | 11.2 | 486.8 | 68.3 | 16x $\frac{3}{8}$ | 57.6 | 11.2 | 660.8 | 81.3 |
| " | $\frac{1}{2}$ | " $\frac{1}{2}$ | 70.6 | 13.6 | 576.9 | 81.0 | " $\frac{1}{2}$ | 70.6 | 13.6 | 784.0 | 96.5 |
| " | $\frac{5}{8}$ | " $\frac{5}{8}$ | 84.1 | 16.1 | 664.2 | 93.2 | " $\frac{5}{8}$ | 84.1 | 16.1 | 903.8 | 111.2 |
| " | $\frac{3}{4}$ | " $\frac{3}{4}$ | 98.2 | 18.7 | 749.3 | 105.2 | " $\frac{3}{4}$ | 98.3 | 18.7 | 1020.6 | 125.6 |
| " | $\frac{7}{8}$ | " $\frac{7}{8}$ | 112.9 | 21.4 | 832.1 | 116.8 | " $\frac{7}{8}$ | 113.0 | 21.4 | 1134.7 | 139.7 |
| " | 1 | "1 | 128.3 | 24.1 | 912.7 | 128.1 | "1 | 128.3 | 24.2 | 1245.9 | 153.3 |
| " | 1 $\frac{1}{8}$ | "1 $\frac{1}{8}$ | 144.2 | 27.0 | 990.8 | 139.1 | "1 $\frac{1}{8}$ | 144.2 | 27.0 | 1354.0 | 166.6 |
| " | 1 $\frac{1}{4}$ | "1 $\frac{1}{4}$ | 160.8 | 29.9 | 1067.1 | 149.8 | "1 $\frac{1}{4}$ | 160.8 | 29.9 | 1459.8 | 179.7 |
| " | 1 $\frac{1}{2}$ | "1 $\frac{1}{2}$ | 178.0 | 32.9 | 1141.0 | 160.1 | "1 $\frac{1}{2}$ | 178.1 | 32.9 | 1562.6 | 192.3 |
| " | 1 $\frac{3}{4}$ | "1 $\frac{3}{4}$ | 195.9 | 36.0 | 1213.2 | 170.3 | "1 $\frac{3}{4}$ | 196.0 | 36.0 | 1663.3 | 204.7 |
| " | 1 $\frac{7}{8}$ | "1 $\frac{7}{8}$ | 214.4 | 39.2 | 1283.1 | 180.1 | "1 $\frac{7}{8}$ | 214.6 | 39.2 | 1761.0 | 216.7 |

MOMENTS OF INERTIA AND SECTION MODULI FOR PLATE AND ANGLE COLUMNS.



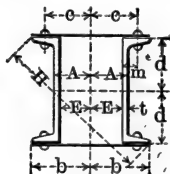
| Size of Angles. | Size of Plate. | Axis 1-1. | | Axis 2-2. | | Size of Plate. | Axis 1-1. | | Axis 2-2. | |
|-----------------------|----------------------|--------------------------|---------------------|--------------------------|---------------------|----------------------|--------------------------|---------------------|--------------------------|---------------------|
| | | Moment of Inertia. | Section Modulus. | Moment of Inertia. | Section Modulus. | | Moment of Inertia. | Section Modulus. | Moment of Inertia. | Section Modulus. |
| Inches. | Inches. | Ins. ⁴ | Ins. ³ | Ins. ⁴ | Ins. ³ | Inches. | Ins. ⁴ | Ins. ³ | Ins. ⁴ | Ins. ³ |
| 6 x 3½ x ¾ | 12x¾ | 119.2 | 19.3 | 457.5 | 74.7 | 14x¾ | 119.2 | 19.3 | 649.1 | 91.1 |
| " | " 1½ | 141.5 | 22.8 | 526.2 | 85.9 | " 1½ | 141.5 | 22.8 | 747.7 | 104.9 |
| " | " 1½ | 164.5 | 26.3 | 593.0 | 96.8 | " 1½ | 164.5 | 26.3 | 843.9 | 118.4 |
| " | " 1½ | 188.3 | 30.0 | 657.9 | 107.4 | " 1½ | 188.3 | 30.0 | 937.6 | 131.6 |
| " | " 1½ | 212.9 | 33.7 | 720.9 | 117.7 | " 1½ | 212.9 | 33.7 | 1028.8 | 144.4 |
| " | " 1½ | 238.3 | 37.6 | 781.8 | 127.6 | " 1½ | 238.3 | 37.6 | 1117.3 | 156.8 |
| " | " 1½ | 264.5 | 41.5 | 841.2 | 137.3 | " 1½ | 264.6 | 41.5 | 1203.9 | 169.0 |
| " | " 1½ | 291.5 | 45.5 | 898.5 | 146.7 | " 1½ | 291.6 | 45.5 | 1287.9 | 180.8 |
| " | " 1½ | 319.5 | 49.6 | 954.4 | 155.8 | " 1½ | 319.6 | 49.6 | 1370.0 | 192.3 |
| " | " 1½ | 348.2 | 53.8 | 1008.4 | 164.6 | " 1½ | 348.4 | 53.9 | 1449.5 | 203.4 |
| " | " 1 | 377.5 | 58.1 | 1060.8 | 173.2 | " 1 | 377.7 | 58.1 | 1526.9 | 214.3 |
| 6 x 3½ x ¾ | 16x¾ | 119.2 | 19.3 | 878.6 | 108.1 | 18x¾ | 119.3 | 19.3 | 1147.4 | 125.7 |
| " | " 1½ | 141.5 | 22.8 | 1013.2 | 124.7 | " 1½ | 141.5 | 22.8 | 1324.4 | 145.1 |
| " | " 1½ | 164.5 | 26.3 | 1144.7 | 140.9 | " 1½ | 164.6 | 26.3 | 1497.5 | 164.1 |
| " | " 1½ | 188.4 | 30.0 | 1273.2 | 156.7 | " 1½ | 188.4 | 30.0 | 1667.1 | 182.7 |
| " | " 1½ | 213.0 | 33.7 | 1398.6 | 172.1 | " 1½ | 213.0 | 33.7 | 1832.8 | 200.9 |
| " | " 1½ | 238.4 | 37.6 | 1520.6 | 187.2 | " 1½ | 238.4 | 37.6 | 1994.3 | 218.6 |
| " | " 1½ | 264.6 | 41.5 | 1640.2 | 201.9 | " 1½ | 264.7 | 41.5 | 2152.9 | 235.9 |
| " | " 1½ | 291.7 | 45.5 | 1756.4 | 216.2 | " 1½ | 291.8 | 45.5 | 2307.4 | 252.9 |
| " | " 1½ | 319.7 | 49.7 | 1870.4 | 230.2 | " 1½ | 319.8 | 49.7 | 2459.2 | 269.5 |
| " | " 1½ | 348.5 | 53.9 | 1981.1 | 243.8 | " 1½ | 348.6 | 53.9 | 2606.8 | 285.7 |
| " | " 1 | 377.8 | 58.1 | 2089.1 | 257.1 | " 1 | 378.0 | 58.2 | 2751.3 | 301.5 |
| 7 x 3½ x 1 | 14x1 | 220.8 | 30.6 | 831.2 | 116.7 | 16x1 | 220.8 | 30.6 | 1122.6 | 138.2 |
| " | " 1½ | 255.8 | 35.3 | 938.4 | 131.7 | " 1½ | 255.8 | 35.3 | 1268.8 | 156.2 |
| " | " 1½ | 292.7 | 40.2 | 1043.0 | 146.4 | " 1½ | 292.7 | 40.2 | 1411.6 | 173.7 |
| " | " 1½ | 328.5 | 44.9 | 1144.6 | 160.7 | " 1½ | 328.5 | 44.9 | 1550.9 | 190.9 |
| " | " 1½ | 367.3 | 50.0 | 1243.9 | 174.6 | " 1½ | 367.4 | 50.0 | 1687.2 | 207.7 |
| " | " 1½ | 406.6 | 55.1 | 1340.7 | 188.2 | " 1½ | 406.7 | 55.1 | 1820.5 | 224.0 |
| " | " 1½ | 447.2 | 60.4 | 1434.8 | 201.4 | " 1½ | 447.3 | 60.4 | 1950.3 | 240.0 |
| " | " 1½ | 488.3 | 65.7 | 1526.7 | 214.3 | " 1½ | 488.4 | 65.7 | 2077.4 | 255.7 |
| " | " 1½ | 530.8 | 71.1 | 1615.9 | 226.8 | " 1½ | 530.9 | 71.1 | 2201.1 | 270.9 |
| " | " 1 | 574.3 | 76.6 | 1702.8 | 239.0 | " 1 | 574.5 | 76.6 | 2322.0 | 285.8 |
| 7 x 3½ x 1 | 18x1 | 220.8 | 30.6 | 1463.2 | 160.4 | 20x1 | 220.8 | 30.6 | 1854.8 | 183.2 |
| " | " 1½ | 255.9 | 35.3 | 1655.1 | 181.4 | " 1½ | 255.9 | 35.3 | 2099.4 | 207.4 |
| " | " 1½ | 292.8 | 40.2 | 1843.0 | 202.0 | " 1½ | 292.8 | 40.2 | 2339.4 | 231.1 |
| " | " 1½ | 328.6 | 44.9 | 2026.6 | 222.1 | " 1½ | 328.6 | 44.9 | 2574.2 | 254.2 |
| " | " 1½ | 367.4 | 50.0 | 2206.4 | 241.8 | " 1½ | 367.5 | 50.0 | 2804.4 | 277.0 |
| " | " 1½ | 406.7 | 55.2 | 2382.7 | 261.1 | " 1½ | 406.8 | 55.2 | 3030.5 | 299.3 |
| " | " 1½ | 447.4 | 60.4 | 2554.7 | 280.0 | " 1½ | 447.5 | 60.4 | 3251.4 | 321.1 |
| " | " 1½ | 488.5 | 65.7 | 2723.5 | 298.5 | " 1½ | 488.6 | 65.7 | 3468.5 | 342.6 |
| " | " 1½ | 531.0 | 71.1 | 2888.1 | 316.5 | " 1½ | 531.2 | 71.1 | 3680.5 | 363.5 |
| " | " 1 | 574.7 | 76.6 | 3049.1 | 334.2 | " 1 | 574.8 | 76.6 | 3888.3 | 384.0 |

SPACING OF CHANNELS FOR EQUAL MOMENTS OF INERTIA ABOUT THE TWO RECT-ANGULAR AXES 1-1 AND 2-2.



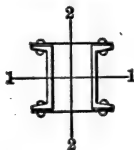
| Section Num- ber. | Depth of Chan- nel. | Weight per foot of one Chan- nel. | Area of Section of one Chan- nel. | A | E | Section Num- ber. | Depth of Chan- nel. | Weight per foot of one Chan- nel. | Area of Section of one Chan- nel. | A | E |
|-------------------------|------------------------------|---|---|---------|---------|-------------------------|------------------------------|---|---|---------|---------|
| | Inches. | Pounds. | Sq. Ins. | Inches. | Inches. | | Inches. | Pounds. | Sq. Ins. | Inches. | Inches. |
| C5 | 3 | 4.00 | 1.19 | 1.29 | 3.05 | C33 | 10 | 15.00 | 4.46 | 6.33 | 8.89 |
| " | " | 5.00 | 1.47 | 1.17 | 2.93 | " | " | 20.00 | 5.88 | 5.96 | 8.40 |
| " | " | 6.00 | 1.76 | 1.10 | 2.94 | " | " | 25.00 | 7.35 | 5.66 | 8.14 |
| C9 | 4 | 5.25 | 1.55 | 2.08 | 3.92 | " | " | 30.00 | 8.82 | 5.41 | 8.01 |
| " | " | 6.25 | 1.84 | 1.96 | 3.80 | " | " | 35.00 | 10.29 | 5.18 | 7.94 |
| " | " | 7.25 | 2.13 | 1.88 | 3.72 | C41 | 12 | 20.50 | 6.03 | 7.68 | 10.48 |
| C13 | 5 | 6.50 | 1.95 | 2.79 | 4.75 | " | " | 25.00 | 7.35 | 7.35 | 10.07 |
| " | " | 9.00 | 2.65 | 2.57 | 4.49 | " | " | 30.00 | 8.82 | 7.06 | 9.78 |
| " | " | 11.50 | 3.38 | 2.35 | 4.39 | " | " | 35.00 | 10.29 | 6.83 | 9.59 |
| C17 | 6 | 8.00 | 2.38 | 3.51 | 5.59 | " | " | 40.00 | 11.76 | 6.60 | 9.48 |
| " | " | 10.50 | 3.09 | 3.29 | 5.29 | C95 | 13 | 32.00 | 9.30 | 7.84 | 11.88 |
| " | " | 13.00 | 3.82 | 3.08 | 5.16 | " | " | 35.00 | 10.29 | 7.66 | 11.62 |
| " | " | 15.50 | 4.56 | 2.90 | 5.10 | " | " | 37.00 | 10.88 | 7.56 | 11.48 |
| C21 | 7 | 9.75 | 2.85 | 4.21 | 6.41 | " | " | 40.00 | 11.76 | 7.44 | 11.32 |
| " | " | 12.25 | 3.60 | 4.00 | 6.12 | " | " | 45.00 | 13.24 | 7.22 | 11.10 |
| " | " | 14.75 | 4.34 | 3.82 | 5.94 | " | " | 50.00 | 14.71 | 7.02 | 10.94 |
| " | " | 17.25 | 5.07 | 3.65 | 5.85 | " | " | 55.00 | 16.18 | 6.84 | 10.84 |
| " | " | 19.75 | 5.81 | 3.49 | 5.81 | C53 | 15 | 33.00 | 9.90 | 9.51 | 12.67 |
| C25 | 8 | 11.25 | 3.35 | 4.92 | 7.24 | " | " | 35.00 | 10.29 | 9.42 | 12.58 |
| " | " | 13.75 | 4.04 | 4.72 | 6.96 | " | " | 40.00 | 11.76 | 9.16 | 12.28 |
| " | " | 16.25 | 4.78 | 4.53 | 6.77 | " | " | 45.00 | 13.24 | 8.92 | 12.08 |
| " | " | 18.75 | 5.51 | 4.37 | 6.65 | " | " | 50.00 | 14.71 | 8.72 | 11.92 |
| " | " | 21.25 | 6.25 | 4.22 | 6.58 | " | " | 55.00 | 16.18 | 8.53 | 11.81 |
| C29 | 9 | 13.25 | 3.89 | 5.62 | 8.06 | C65 | 18 | 45.00 | 13.25 | 11.48 | 14.84 |
| " | " | 15.00 | 4.41 | 5.48 | 7.84 | " | " | 50.00 | 14.71 | 11.20 | 14.52 |
| " | " | 20.00 | 5.88 | 5.14 | 7.46 | " | " | 55.00 | 16.18 | 10.98 | 14.30 |
| " | " | 25.00 | 7.35 | 4.83 | 7.31 | " | " | 60.00 | 17.65 | 10.78 | 14.18 |

DIMENSIONS FOR LATTICED CHANNEL COLUMNS.



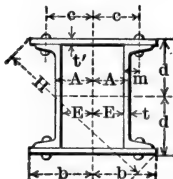
| Depth of Channel and Section Number. | Weight per Foot. | t | b | d | H | c | E | A | m |
|--------------------------------------|------------------|-------|-----------------|-----------------|------------------|-----------------|-----------------|-----------------|-----------------|
| | Pounds. | Inch. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. |
| 6" C17 | 8.00 | .20 | 3 $\frac{1}{4}$ | 3 | 9 $\frac{3}{8}$ | 2 $\frac{1}{2}$ | 1 $\frac{1}{4}$ | 2 | 1 $\frac{1}{4}$ |
| | 10.50 | .32 | " | " | " | " | 1 $\frac{1}{4}$ | " | 1 $\frac{1}{4}$ |
| | 13.00 | .44 | " | " | " | " | 1 $\frac{1}{4}$ | " | 1 $\frac{1}{4}$ |
| | 15.50 | .56 | " | " | " | " | 1 $\frac{1}{4}$ | " | 1 $\frac{1}{4}$ |
| 7" C21 | 9.75 | .21 | 4 $\frac{1}{4}$ | 3 $\frac{1}{2}$ | 11 | 3 $\frac{3}{8}$ | 2 $\frac{1}{4}$ | 2 $\frac{1}{2}$ | 1 $\frac{1}{4}$ |
| | 12.25 | .32 | " | " | " | " | 2 $\frac{1}{4}$ | " | 1 $\frac{1}{4}$ |
| | 14.75 | .42 | " | " | " | " | 1 $\frac{1}{4}$ | " | 1 $\frac{1}{4}$ |
| | 17.25 | .53 | " | " | " | " | 1 $\frac{1}{4}$ | " | 1 $\frac{1}{4}$ |
| 8" C25 | 11.25 | .22 | 4 $\frac{1}{2}$ | 4 | 12 $\frac{1}{2}$ | 3 $\frac{1}{4}$ | 2 $\frac{1}{2}$ | 2 $\frac{1}{4}$ | 1 $\frac{1}{4}$ |
| | 13.75 | .31 | " | " | " | " | 2 $\frac{1}{4}$ | " | 1 $\frac{1}{4}$ |
| | 16.25 | .40 | " | " | " | " | 2 $\frac{1}{4}$ | " | 1 $\frac{1}{4}$ |
| | 18.75 | .49 | " | " | " | " | 2 $\frac{1}{4}$ | " | 1 $\frac{1}{4}$ |
| 9" C29 | 21.25 | .58 | " | " | " | " | 2 $\frac{1}{4}$ | " | 1 $\frac{1}{4}$ |
| | 13.25 | .23 | 5 $\frac{1}{4}$ | 4 $\frac{1}{2}$ | 13 $\frac{1}{4}$ | 4 $\frac{1}{8}$ | 2 $\frac{3}{4}$ | 3 | 1 $\frac{3}{8}$ |
| | 15.00 | .29 | " | " | " | " | 2 $\frac{1}{4}$ | " | 1 $\frac{1}{4}$ |
| | 20.00 | .45 | " | " | " | " | 2 $\frac{1}{4}$ | " | 1 $\frac{1}{4}$ |
| 10" C33 | 25.00 | .61 | " | " | " | " | 2 $\frac{3}{8}$ | " | 1 $\frac{1}{4}$ |
| | 15.00 | .24 | 5 $\frac{3}{4}$ | 5 | 15 $\frac{1}{4}$ | 4 $\frac{1}{8}$ | 3 $\frac{1}{8}$ | 3 $\frac{1}{4}$ | 1 $\frac{1}{2}$ |
| | 20.00 | .38 | " | " | " | " | 3 | " | 1 $\frac{5}{8}$ |
| | 25.00 | .53 | " | " | " | " | 2 $\frac{1}{4}$ | " | 1 $\frac{1}{4}$ |
| 12" C41 | 30.00 | .68 | " | " | " | " | 2 $\frac{1}{4}$ | " | 1 $\frac{1}{4}$ |
| | 35.00 | .82 | " | " | " | " | 2 $\frac{1}{4}$ | " | 2 $\frac{1}{4}$ |
| | 20.50 | .28 | 6 $\frac{1}{4}$ | 6 | 18 $\frac{3}{8}$ | 5 $\frac{1}{8}$ | 3 $\frac{1}{8}$ | 4 $\frac{1}{4}$ | 1 $\frac{1}{4}$ |
| | 25.00 | .39 | " | " | " | " | 3 $\frac{1}{4}$ | " | 1 $\frac{1}{8}$ |
| 15" C53 | 30.00 | .51 | " | " | " | " | 3 $\frac{1}{8}$ | " | 2 |
| | 35.00 | .64 | " | " | " | " | 3 $\frac{1}{8}$ | " | 2 $\frac{1}{8}$ |
| | 40.00 | .76 | " | " | " | " | 3 $\frac{1}{8}$ | " | 2 $\frac{1}{4}$ |
| | 33.00 | .40 | 8 $\frac{1}{8}$ | 7 $\frac{1}{2}$ | 22 $\frac{1}{8}$ | 6 $\frac{1}{8}$ | 4 $\frac{1}{4}$ | 5 $\frac{1}{8}$ | 1 $\frac{1}{8}$ |
| 15" C53 | 35.00 | .43 | " | " | " | " | 4 $\frac{1}{4}$ | " | 1 $\frac{1}{4}$ |
| | 40.00 | .52 | " | " | " | " | 4 $\frac{1}{8}$ | " | 2 |
| | 45.00 | .62 | " | " | " | " | 4 $\frac{1}{8}$ | " | 2 $\frac{1}{8}$ |
| | 50.00 | .72 | " | " | " | " | 4 $\frac{1}{4}$ | " | 2 $\frac{1}{4}$ |
| 15" C53 | 55.00 | .82 | " | " | " | " | 4 $\frac{1}{4}$ | " | 2 $\frac{1}{4}$ |

PROPERTIES OF LATTICED CHANNEL COLUMNS.



| Depth of Channel and Section Number. | Weight per Foot. | Axis 1-1. | | Axis 2-2. | |
|--|------------------------|-----------------------|----------------------|-----------------------|----------------------|
| | | Moment of Inertia. | Section Modulus. | Moment of Inertia. | Section Modulus. |
| | Pounds. | Inches. ⁴ | Inches. ³ | Inches. ⁴ | Inches. ³ |
| 8" C17 | 8.00 | 26.0 | 8.7 | 27.0 | 7.3 |
| | 10.50 | 30.2 | 10.1 | 31.1 | 8.4 |
| | 13.00 | 34.6 | 11.5 | 35.2 | 9.5 |
| | 15.50 | 39.0 | 13.0 | 38.7 | 10.4 |
| 7" C21 | 9.75 | 42.2 | 12.1 | 44.0 | 10.8 |
| | 12.25 | 48.4 | 13.8 | 50.5 | 11.9 |
| | 14.75 | 54.4 | 15.5 | 56.4 | 13.3 |
| | 17.25 | 60.4 | 17.3 | 61.4 | 14.4 |
| 8" C25 | 11.25 | 64.6 | 16.2 | 67.5 | 14.0 |
| | 13.75 | 72.0 | 18.0 | 75.8 | 15.8 |
| | 16.25 | 79.8 | 20.0 | 84.5 | 17.6 |
| | 18.75 | 87.7 | 21.9 | 92.3 | 19.3 |
| 9" C29 | 21.25 | 95.6 | 23.9 | 99.7 | 20.8 |
| | 13.25 | 94.6 | 21.0 | 92.4 | 17.8 |
| | 15.00 | 101.8 | 22.6 | 100.0 | 19.2 |
| | 20.00 | 121.6 | 27.0 | 120.1 | 23.1 |
| 10" C33 | 25.00 | 141.4 | 31.4 | 139.1 | 26.8 |
| | 15.00 | 133.8 | 26.8 | 131.7 | 23.0 |
| | 20.00 | 157.4 | 31.5 | 158.5 | 27.6 |
| | 25.00 | 182.0 | 36.4 | 183.3 | 32.0 |
| 12" C41 | 30.00 | 206.4 | 41.3 | 205.4 | 35.8 |
| | 35.00 | 231.0 | 46.2 | 226.0 | 39.4 |
| | 20.50 | 256.2 | 42.7 | 256.9 | 37.9 |
| | 25.00 | 288.0 | 48.0 | 295.6 | 43.6 |
| 15" C53 | 30.00 | 323.2 | 53.9 | 335.8 | 49.5 |
| | 35.00 | 358.6 | 59.8 | 370.5 | 54.6 |
| | 40.00 | 393.8 | 65.6 | 405.7 | 59.8 |
| | 33.00 | 625.2 | 83.4 | 618.7 | 76.1 |
| 15" C53 | 35.00 | 639.8 | 85.3 | 636.1 | 78.3 |
| | 40.00 | 695.0 | 92.7 | 700.8 | 86.3 |
| | 45.00 | 750.2 | 100.0 | 763.0 | 93.9 |
| | 50.00 | 805.4 | 107.4 | 819.5 | 100.9 |
| 15" C53 | 55.00 | 860.4 | 114.7 | 874.3 | 107.6 |

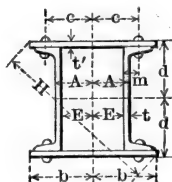
DIMENSIONS FOR PLATE AND CHANNEL COLUMNS.



SERIES A.

| Depth of Channel and Section No. | Weight per Foot. | Size of Plates. | | t | b | d | H | c | E | A | m |
|----------------------------------|------------------|-----------------|---------------|-------|----------------|----------------|-----------------|----------------|----------------|----------------|----------------|
| | | Width. | Thick-ness t' | | | | | | | | |
| | Pounds. | Inches. | Inch. | Inch. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. |
| 6" C17 | 8.0 | 8 | $\frac{1}{4}$ | .20 | 4 | $3\frac{1}{4}$ | $10\frac{1}{8}$ | $2\frac{7}{8}$ | $1\frac{1}{2}$ | 2 | $1\frac{1}{8}$ |
| | 10.5 | " | $\frac{1}{4}$ | .32 | " | $3\frac{3}{8}$ | $10\frac{1}{8}$ | " | $1\frac{1}{2}$ | " | $1\frac{1}{8}$ |
| | " | " | $\frac{5}{8}$ | " | " | $3\frac{3}{8}$ | $10\frac{1}{8}$ | " | $1\frac{1}{2}$ | " | $1\frac{1}{8}$ |
| | 13.0 | " | $\frac{1}{4}$ | .44 | " | $3\frac{3}{4}$ | $10\frac{1}{8}$ | " | $1\frac{1}{2}$ | " | $1\frac{1}{8}$ |
| | 15.5 | " | $\frac{5}{8}$ | .56 | " | $3\frac{3}{4}$ | $10\frac{1}{8}$ | " | $1\frac{1}{2}$ | " | $1\frac{1}{8}$ |
| 7" C21 | 9.75 | 9 | $\frac{1}{4}$ | .21 | $4\frac{1}{2}$ | $3\frac{3}{4}$ | $11\frac{1}{4}$ | $3\frac{1}{4}$ | $2\frac{1}{2}$ | $2\frac{1}{4}$ | $1\frac{1}{8}$ |
| | 12.25 | " | $\frac{1}{4}$ | .32 | " | $4\frac{1}{8}$ | $12\frac{1}{8}$ | " | $1\frac{1}{2}$ | " | $1\frac{1}{8}$ |
| | " | " | $\frac{5}{8}$ | " | " | $4\frac{1}{8}$ | $12\frac{1}{8}$ | " | $1\frac{1}{2}$ | " | $1\frac{1}{8}$ |
| | 14.75 | " | $\frac{1}{4}$ | .42 | " | $3\frac{3}{4}$ | $11\frac{1}{4}$ | " | $1\frac{1}{2}$ | " | $1\frac{1}{8}$ |
| | " | " | $\frac{5}{8}$ | " | " | $4\frac{1}{8}$ | $12\frac{1}{8}$ | " | $1\frac{1}{2}$ | " | $1\frac{1}{8}$ |
| | 17.25 | " | $\frac{1}{4}$ | .53 | " | $3\frac{3}{4}$ | $11\frac{1}{4}$ | " | $1\frac{1}{2}$ | " | $1\frac{1}{8}$ |
| 8" C25 | 19.75 | " | $\frac{1}{4}$ | .68 | " | $4\frac{1}{8}$ | $12\frac{1}{8}$ | " | $1\frac{1}{2}$ | " | $1\frac{1}{8}$ |
| | " | " | $\frac{5}{8}$ | " | " | $4\frac{1}{8}$ | $12\frac{1}{8}$ | " | $1\frac{1}{2}$ | " | $1\frac{1}{8}$ |
| | 11.25 | 10 | $\frac{1}{4}$ | .22 | 5 | $4\frac{1}{4}$ | $13\frac{1}{8}$ | $3\frac{3}{8}$ | $2\frac{1}{2}$ | $2\frac{1}{4}$ | $1\frac{1}{4}$ |
| | " | " | $\frac{5}{8}$ | " | " | $4\frac{1}{4}$ | $13\frac{1}{8}$ | " | $2\frac{1}{2}$ | " | $1\frac{1}{4}$ |
| | 13.75 | " | $\frac{1}{4}$ | .31 | " | $4\frac{1}{4}$ | $13\frac{1}{8}$ | " | $2\frac{1}{2}$ | " | $1\frac{1}{4}$ |
| | " | " | $\frac{5}{8}$ | " | " | $4\frac{1}{4}$ | $13\frac{1}{8}$ | " | $2\frac{1}{2}$ | " | $1\frac{1}{4}$ |
| 9" C29 | 16.25 | " | $\frac{1}{4}$ | .40 | " | $4\frac{1}{4}$ | $13\frac{1}{8}$ | " | $2\frac{1}{2}$ | " | $1\frac{1}{4}$ |
| | " | " | $\frac{5}{8}$ | " | " | $4\frac{1}{4}$ | $13\frac{1}{8}$ | " | $2\frac{1}{2}$ | " | $1\frac{1}{4}$ |
| | 18.75 | " | $\frac{1}{4}$ | .49 | " | $4\frac{1}{4}$ | $13\frac{1}{8}$ | " | $2\frac{1}{2}$ | " | $1\frac{1}{4}$ |
| | " | " | $\frac{5}{8}$ | " | " | $4\frac{1}{4}$ | $13\frac{1}{8}$ | " | $2\frac{1}{2}$ | " | $1\frac{1}{4}$ |
| | 21.25 | " | $\frac{1}{4}$ | .58 | " | $4\frac{1}{4}$ | $13\frac{1}{8}$ | " | $2\frac{1}{2}$ | " | $1\frac{1}{4}$ |
| 9" C29 | 13.25 | 11 | $\frac{1}{4}$ | .23 | $5\frac{1}{2}$ | $4\frac{1}{4}$ | $14\frac{1}{2}$ | $4\frac{1}{8}$ | $2\frac{3}{4}$ | 3 | $1\frac{1}{4}$ |
| | " | " | $\frac{5}{8}$ | " | " | $5\frac{1}{8}$ | $15\frac{1}{8}$ | " | $2\frac{3}{4}$ | " | $1\frac{1}{4}$ |
| | 15.00 | " | $\frac{1}{4}$ | .29 | " | $4\frac{1}{4}$ | $14\frac{1}{2}$ | " | $2\frac{3}{4}$ | " | $1\frac{1}{4}$ |
| | " | " | $\frac{5}{8}$ | " | " | $5\frac{1}{8}$ | $15\frac{1}{8}$ | " | $2\frac{3}{4}$ | " | $1\frac{1}{4}$ |
| | 20.00 | " | $\frac{1}{4}$ | .45 | " | $4\frac{1}{4}$ | $14\frac{1}{2}$ | " | $2\frac{3}{4}$ | " | $1\frac{1}{4}$ |
| 9" C29 | " | " | $\frac{5}{8}$ | " | " | $5\frac{1}{8}$ | $15\frac{1}{8}$ | " | $2\frac{3}{4}$ | " | $1\frac{1}{4}$ |
| | 25.00 | " | $\frac{1}{4}$ | .61 | " | $4\frac{1}{4}$ | $14\frac{1}{2}$ | " | $2\frac{3}{4}$ | " | $1\frac{1}{4}$ |
| | " | " | $\frac{5}{8}$ | " | " | $5\frac{1}{8}$ | $15\frac{1}{8}$ | " | $2\frac{3}{4}$ | " | $1\frac{1}{4}$ |

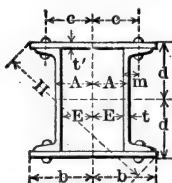
DIMENSIONS FOR PLATE AND CHANNEL COLUMNS.



SERIES A.

| Depth of Channel and Section No. | Weight per Foot. | Size of Plates. | | t | b | d | H | c | E | A | m |
|----------------------------------|------------------|-----------------|---------------|-------|----------------|----------------|------------------|----------------|-----------------|----------------|----------------|
| | | Width. | Thick-ness t' | | | | | | | | |
| | Pounds. | Inches. | Inch. | Inch. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. |
| 10' C33 | 15.0 | 12 | $\frac{1}{4}$ | .24 | 6 | $5\frac{1}{4}$ | $15\frac{1}{16}$ | $4\frac{1}{2}$ | 3 | $3\frac{3}{4}$ | $1\frac{1}{2}$ |
| | 20.0 | " | $\frac{1}{4}$ | .38 | " | $5\frac{1}{4}$ | $15\frac{1}{16}$ | " | $2\frac{3}{8}$ | " | $1\frac{5}{8}$ |
| | 25.0 | " | $\frac{1}{4}$ | .53 | " | $5\frac{1}{4}$ | $15\frac{1}{16}$ | " | $2\frac{3}{4}$ | " | $1\frac{3}{4}$ |
| | 30.0 | " | $\frac{1}{4}$ | .68 | " | $5\frac{1}{4}$ | $15\frac{1}{16}$ | " | $2\frac{1}{2}$ | " | $1\frac{1}{8}$ |
| | 35.0 | " | $\frac{1}{4}$ | .82 | " | $5\frac{1}{4}$ | $15\frac{1}{16}$ | " | $2\frac{1}{8}$ | " | $2\frac{1}{8}$ |
| 12' C41 | 20.5 | 14 | $\frac{1}{4}$ | .28 | 7 | $6\frac{1}{4}$ | $18\frac{3}{4}$ | $5\frac{5}{8}$ | $3\frac{3}{8}$ | $4\frac{1}{8}$ | $1\frac{3}{4}$ |
| | 25.0 | " | $\frac{1}{4}$ | .39 | " | $6\frac{1}{4}$ | $18\frac{3}{4}$ | " | $3\frac{3}{4}$ | " | $1\frac{7}{8}$ |
| | 30.0 | " | $\frac{1}{4}$ | .51 | " | $6\frac{1}{4}$ | $18\frac{3}{4}$ | " | $3\frac{5}{8}$ | " | 2 |
| | 35.0 | " | $\frac{1}{4}$ | .64 | " | $6\frac{1}{4}$ | $18\frac{3}{4}$ | " | $3\frac{1}{2}$ | " | $2\frac{1}{8}$ |
| | 40.0 | " | $\frac{1}{4}$ | .76 | " | $6\frac{1}{4}$ | $18\frac{3}{4}$ | " | $3\frac{3}{8}$ | " | $2\frac{1}{4}$ |
| 15' C53 | 38.0 | 17 | $\frac{3}{8}$ | .40 | $8\frac{1}{2}$ | $7\frac{7}{8}$ | $23\frac{1}{16}$ | $6\frac{3}{4}$ | $4\frac{1}{8}$ | $5\frac{1}{4}$ | $1\frac{7}{8}$ |
| | 35.0 | " | $\frac{3}{8}$ | .43 | " | $7\frac{7}{8}$ | $23\frac{1}{16}$ | " | $4\frac{1}{16}$ | " | $1\frac{1}{8}$ |
| | 40.0 | " | $\frac{3}{8}$ | .52 | " | $7\frac{7}{8}$ | $23\frac{1}{16}$ | " | $4\frac{1}{4}$ | " | 2 |
| | 45.0 | " | $\frac{3}{8}$ | .62 | " | $7\frac{7}{8}$ | $23\frac{1}{16}$ | " | $4\frac{1}{8}$ | " | $2\frac{1}{8}$ |
| | 50.0 | " | $\frac{3}{8}$ | .72 | " | $8\frac{1}{4}$ | $23\frac{1}{16}$ | " | $4\frac{1}{16}$ | " | $2\frac{1}{4}$ |
| | 55.0 | " | $\frac{3}{8}$ | .82 | " | $7\frac{7}{8}$ | $23\frac{1}{16}$ | " | $4\frac{1}{8}$ | " | $2\frac{1}{8}$ |

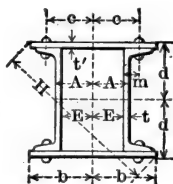
DIMENSIONS FOR PLATE AND CHANNEL COLUMNS.



SERIES B.

| Depth of Channel and Section No. | Weight per Foot. | Size of Plates. | | t | b | d | H | c | E | A | m |
|----------------------------------|------------------|-----------------|---------------|-------|----------------|----------------|-----------------|----------------|----------------|----------------|----------------|
| | | Width. | Thick-ness t' | | | | | | | | |
| | Pounds. | Inches. | Inch. | Inch. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. |
| 6" C17 | 8.0 | 9 | $\frac{1}{4}$ | .20 | $4\frac{1}{2}$ | $3\frac{1}{4}$ | $11\frac{1}{8}$ | $3\frac{3}{8}$ | $2\frac{1}{4}$ | $2\frac{1}{2}$ | $1\frac{1}{4}$ |
| | 10.5 | " | $\frac{5}{8}$ | .32 | " | $3\frac{5}{8}$ | $11\frac{1}{8}$ | " | $2\frac{1}{4}$ | " | $1\frac{1}{4}$ |
| | 13.0 | " | $\frac{1}{4}$ | .44 | " | $3\frac{1}{4}$ | $11\frac{1}{8}$ | " | $2\frac{1}{4}$ | " | $1\frac{1}{4}$ |
| | 15.5 | " | $\frac{5}{8}$ | .56 | " | $3\frac{1}{4}$ | $11\frac{1}{8}$ | " | $1\frac{1}{4}$ | " | $1\frac{1}{4}$ |
| 7" C21 | 9.75 | 11 | $\frac{1}{4}$ | .21 | $5\frac{1}{2}$ | $3\frac{3}{4}$ | $13\frac{1}{8}$ | $4\frac{1}{4}$ | $3\frac{1}{4}$ | $3\frac{1}{4}$ | $1\frac{1}{4}$ |
| | 12.25 | " | $\frac{5}{8}$ | .32 | " | $4\frac{1}{8}$ | $13\frac{3}{4}$ | " | $2\frac{1}{4}$ | " | $1\frac{1}{4}$ |
| | 14.75 | " | $\frac{1}{4}$ | .42 | " | $3\frac{3}{4}$ | $13\frac{3}{4}$ | " | $2\frac{1}{4}$ | " | $1\frac{1}{4}$ |
| | 17.25 | " | $\frac{5}{8}$ | .53 | " | $3\frac{3}{4}$ | $13\frac{3}{4}$ | " | $2\frac{1}{4}$ | " | $1\frac{1}{2}$ |
| | 19.75 | " | $\frac{1}{4}$ | .63 | " | $3\frac{3}{4}$ | $13\frac{3}{4}$ | " | $2\frac{3}{8}$ | " | $1\frac{1}{2}$ |
| | " | " | $\frac{5}{8}$ | " | " | $4\frac{1}{8}$ | $13\frac{3}{4}$ | " | " | " | " |
| 8" C25 | 11.25 | 12 | $\frac{1}{4}$ | .22 | 6 | $4\frac{1}{4}$ | $14\frac{1}{4}$ | $4\frac{5}{8}$ | $3\frac{1}{4}$ | $3\frac{5}{8}$ | $1\frac{1}{4}$ |
| | 13.75 | " | $\frac{5}{8}$ | .31 | " | $4\frac{1}{8}$ | $15\frac{1}{2}$ | " | $3\frac{1}{4}$ | " | $1\frac{1}{4}$ |
| | 16.25 | " | $\frac{1}{4}$ | .40 | " | $4\frac{1}{4}$ | $14\frac{1}{4}$ | " | $3\frac{1}{4}$ | " | $1\frac{1}{2}$ |
| | 18.75 | " | $\frac{5}{8}$ | .49 | " | $4\frac{1}{8}$ | $15\frac{1}{2}$ | " | $3\frac{3}{8}$ | " | $1\frac{1}{2}$ |
| | 21.25 | " | $\frac{1}{4}$ | .58 | " | $4\frac{1}{4}$ | $14\frac{1}{4}$ | " | $3\frac{1}{4}$ | " | $1\frac{1}{4}$ |
| 9" C29 | 13.25 | 13 | $\frac{1}{4}$ | .23 | $6\frac{1}{2}$ | $4\frac{1}{4}$ | $16\frac{1}{8}$ | $5\frac{1}{8}$ | $3\frac{3}{4}$ | 4 | $1\frac{1}{2}$ |
| | 15.00 | " | $\frac{5}{8}$ | .29 | " | $4\frac{1}{8}$ | $16\frac{1}{8}$ | " | $3\frac{1}{4}$ | " | $1\frac{1}{4}$ |
| | 20.00 | " | $\frac{1}{4}$ | .45 | " | $4\frac{1}{4}$ | $16\frac{1}{8}$ | " | $3\frac{1}{4}$ | " | $1\frac{1}{4}$ |
| | " | " | $\frac{5}{8}$ | .61 | " | $4\frac{1}{8}$ | $16\frac{1}{8}$ | " | $3\frac{3}{8}$ | " | $1\frac{1}{4}$ |
| | 25.00 | " | $\frac{1}{4}$ | " | " | $4\frac{1}{4}$ | $16\frac{1}{8}$ | " | " | " | " |

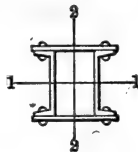
DIMENSIONS FOR PLATE AND CHANNEL COLUMNS.



SERIES B.

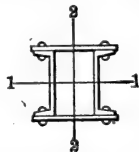
| Depth of Channel and Section No. | Weight per Foot. | Size of Plates. | | t | b | d | H | c | E | A | m |
|----------------------------------|------------------|-----------------|----------------|-------|----------------|----------------|-----------------|----------------|----------------|----------------|----------------|
| | | Width. | Thick-ness. t' | | | | | | | | |
| | Pounds. | Inches. | Inch. | Inch. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. |
| 10" C33 | 15.0 | 15 | $\frac{1}{4}$ | .24 | $7\frac{1}{2}$ | $5\frac{1}{4}$ | $18\frac{1}{4}$ | 6 | $4\frac{1}{2}$ | $4\frac{1}{4}$ | $1\frac{1}{2}$ |
| | 20.0 | " | $\frac{1}{4}$ | .38 | " | $5\frac{1}{4}$ | $18\frac{1}{4}$ | " | $4\frac{1}{2}$ | " | $1\frac{3}{8}$ |
| | 25.0 | " | $\frac{1}{4}$ | .53 | " | $5\frac{1}{4}$ | $18\frac{1}{4}$ | " | $4\frac{1}{4}$ | " | $1\frac{3}{4}$ |
| | 30.0 | " | $\frac{1}{4}$ | .68 | " | $5\frac{1}{4}$ | $18\frac{1}{4}$ | " | $4\frac{1}{4}$ | " | $1\frac{1}{2}$ |
| | 35.0 | " | $\frac{1}{4}$ | .82 | " | $5\frac{1}{4}$ | $18\frac{1}{4}$ | " | $3\frac{1}{4}$ | " | $2\frac{1}{4}$ |
| 12" C41 | 20.5 | 16 | $\frac{1}{4}$ | .28 | 8 | $6\frac{1}{4}$ | $20\frac{1}{4}$ | $6\frac{3}{8}$ | $4\frac{1}{2}$ | $5\frac{1}{8}$ | $1\frac{3}{4}$ |
| | 25.0 | " | $\frac{1}{4}$ | .39 | " | $6\frac{1}{4}$ | $20\frac{1}{4}$ | " | $4\frac{1}{4}$ | " | $1\frac{1}{2}$ |
| | 30.0 | " | $\frac{1}{4}$ | .51 | " | $6\frac{1}{4}$ | $20\frac{1}{4}$ | " | $4\frac{1}{2}$ | " | 2 |
| | 35.0 | " | $\frac{1}{4}$ | .64 | " | $6\frac{1}{4}$ | $20\frac{1}{4}$ | " | $4\frac{1}{4}$ | " | $2\frac{1}{8}$ |
| | 40.0 | " | $\frac{1}{4}$ | .78 | " | $6\frac{1}{4}$ | $20\frac{1}{4}$ | " | $4\frac{1}{2}$ | " | $2\frac{1}{4}$ |
| 15" C53 | 33.0 | 20 | $\frac{3}{8}$ | .40 | 10 | $7\frac{7}{8}$ | $25\frac{1}{8}$ | $8\frac{1}{4}$ | $6\frac{3}{8}$ | $6\frac{1}{4}$ | $1\frac{3}{8}$ |
| | 35.0 | " | $\frac{3}{8}$ | .43 | " | $7\frac{7}{8}$ | $25\frac{1}{8}$ | " | $6\frac{1}{4}$ | " | $1\frac{1}{2}$ |
| | 40.0 | " | $\frac{3}{8}$ | .52 | " | $8\frac{1}{4}$ | $25\frac{1}{8}$ | " | $6\frac{1}{4}$ | " | 2 |
| | 45.0 | " | $\frac{3}{8}$ | .62 | " | $8\frac{1}{4}$ | $25\frac{1}{8}$ | " | $6\frac{1}{8}$ | " | $2\frac{1}{8}$ |
| | 50.0 | " | $\frac{3}{8}$ | .72 | " | $7\frac{7}{8}$ | $25\frac{1}{8}$ | " | $6\frac{1}{4}$ | " | $2\frac{1}{4}$ |
| | 55.0 | " | $\frac{3}{8}$ | .82 | " | $7\frac{7}{8}$ | $25\frac{1}{8}$ | " | $5\frac{1}{4}$ | " | $2\frac{1}{4}$ |

**MOMENTS OF INERTIA AND
SECTION MODULI FOR
PLATE AND CHAN-
NEL COLUMNS.**



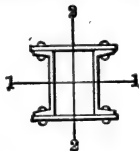
| Depth of Channel and Section Number. | Weight per Foot. | SERIES A. | | | | | | SERIES B. | | | | | |
|--------------------------------------|------------------|-----------------|------|---------------------|------------------|--------------------|------------------|------------------|------------------|--------------------|------------------|---------------------|------|
| | | Width of Plate. | | Axis 1-1. | | Axis 2-2. | | Width of Plate. | | Axis 1-1. | | Axis 2-2. | |
| | | | | Thickness of Plate. | | Moment of Inertia. | Section Modulus. | | | Moment of Inertia. | Section Modulus. | Thickness of Plate. | |
| | | In. | In. | In. ⁴ | In. ³ | | | In. ⁴ | In. ³ | | | In. | In. |
| 6" C 17 | 8.00 | 8 | 1/4 | 65.1 | 20.0 | 48.4 | 12.1 | 9 | 1/4 | 70.0 | 21.5 | 69.6 | 15.5 |
| | " | " | 5/16 | 75.9 | 22.9 | 53.7 | 13.4 | " | 5/16 | 82.1 | 24.8 | 77.2 | 17.2 |
| | " | " | 3/8 | 87.0 | 25.8 | 59.0 | 14.8 | " | 3/8 | 94.7 | 28.1 | 84.8 | 18.9 |
| | " | " | 1/2 | 98.6 | 28.7 | 64.4 | 16.1 | " | 1/2 | 107.8 | 31.4 | 92.4 | 20.5 |
| | " | " | 5/8 | 110.7 | 31.6 | 69.7 | 17.4 | " | 5/8 | 121.3 | 34.6 | 100.0 | 22.2 |
| | " | " | 3/4 | 123.1 | 34.6 | 75.0 | 18.8 | " | 3/4 | 135.3 | 38.0 | 107.6 | 23.9 |
| 6" C 17 | " | " | 7/8 | 136.1 | 37.5 | 80.4 | 20.1 | " | 7/8 | 149.8 | 41.3 | 115.2 | 25.6 |
| | 10.50 | 8 | 1/4 | 69.3 | 21.3 | 52.5 | 13.1 | 9 | 1/4 | 74.2 | 22.8 | 76.5 | 17.0 |
| | " | " | 5/16 | 80.1 | 24.2 | 57.8 | 14.5 | " | 5/16 | 86.3 | 26.1 | 84.1 | 18.7 |
| | " | " | 3/8 | 91.2 | 27.0 | 63.1 | 15.8 | " | 3/8 | 98.9 | 29.3 | 91.7 | 20.4 |
| | " | " | 1/2 | 102.8 | 29.9 | 68.5 | 17.1 | " | 1/2 | 112.0 | 32.6 | 99.3 | 22.1 |
| | " | " | 5/8 | 114.9 | 32.8 | 73.8 | 18.5 | " | 5/8 | 125.5 | 35.8 | 106.9 | 23.8 |
| 6" C 17 | " | " | 3/4 | 127.3 | 35.7 | 79.1 | 19.8 | " | 3/4 | 139.5 | 39.2 | 114.5 | 25.4 |
| | " | " | 7/8 | 140.3 | 38.7 | 84.5 | 21.1 | " | 7/8 | 154.0 | 42.5 | 122.1 | 27.1 |
| | 13.00 | 8 | 1/4 | 73.7 | 22.7 | 56.5 | 14.1 | 9 | 1/4 | 78.6 | 24.2 | 83.4 | 18.5 |
| | " | " | 5/16 | 84.5 | 25.5 | 61.9 | 15.5 | " | 5/16 | 90.7 | 27.4 | 91.0 | 20.2 |
| | " | " | 3/8 | 95.6 | 28.3 | 67.2 | 16.8 | " | 3/8 | 103.3 | 30.6 | 98.6 | 21.9 |
| | " | " | 1/2 | 107.2 | 31.2 | 72.5 | 18.1 | " | 1/2 | 116.4 | 33.9 | 106.2 | 23.6 |
| 6" C 17 | " | " | 5/8 | 119.3 | 34.1 | 77.9 | 19.5 | " | 5/8 | 129.9 | 37.1 | 113.7 | 25.3 |
| | " | " | 3/4 | 131.7 | 37.0 | 83.2 | 20.8 | " | 3/4 | 143.9 | 40.4 | 121.3 | 27.0 |
| | " | " | 7/8 | 144.7 | 39.9 | 88.5 | 22.1 | " | 7/8 | 158.4 | 43.7 | 128.9 | 28.7 |
| | 15.50 | 8 | 1/4 | 78.1 | 24.0 | 60.0 | 15.0 | 9 | 1/4 | 83.0 | 25.5 | 89.5 | 19.9 |
| | " | " | 5/16 | 88.9 | 26.8 | 65.4 | 16.3 | " | 5/16 | 95.1 | 28.7 | 97.1 | 21.6 |
| | " | " | 3/8 | 100.0 | 29.6 | 70.7 | 17.7 | " | 3/8 | 107.7 | 31.9 | 104.7 | 23.3 |
| 6" C 17 | " | " | 1/2 | 111.8 | 32.5 | 76.0 | 19.0 | " | 1/2 | 120.8 | 35.1 | 112.3 | 25.0 |
| | " | " | 5/8 | 123.7 | 35.3 | 81.4 | 20.3 | " | 5/8 | 134.3 | 38.4 | 119.9 | 26.6 |
| | " | " | 3/4 | 136.1 | 38.2 | 86.7 | 21.7 | " | 3/4 | 148.3 | 41.6 | 127.4 | 28.3 |
| | " | " | 7/8 | 149.1 | 41.1 | 92.0 | 23.0 | " | 7/8 | 162.8 | 44.9 | 135.0 | 30.0 |

MOMENTS OF INERTIA AND SECTION MODULI FOR PLATE AND CHAN- NEL COLUMNS.



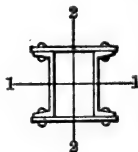
| Depth of Channel and Section Number. | Weight per Foot. | SERIES A. | | | | | | SERIES B. | | | | | |
|--------------------------------------|------------------|------------------|-----|--------------------|------------------|--------------------|------------------|------------------|-----|--------------------|------------------|--------------------|------------------|
| | | Width of Plate. | | Axis 1-1. | | Axis 2-2. | | Width of Plate. | | Axis 1-1. | | Axis 2-2. | |
| | | Thickness Plate. | In. | Moment of Inertia. | Section Modulus. | Moment of Inertia. | Section Modulus. | Thickness Plate. | In. | Moment of Inertia. | Section Modulus. | Moment of Inertia. | Section Modulus. |
| | | | | | | | | | | | | | |
| 7" C21 | 9.75 | 9 | 1/4 | 101.4 | 27.0 | 70.6 | 15.7 | 11 | 1/4 | 114.5 | 30.5 | 130.9 | 23.8 |
| | " | " | 1/8 | 117.4 | 30.8 | 78.1 | 17.4 | " | 1/8 | 134.2 | 35.2 | 144.7 | 26.3 |
| | " | " | 3/8 | 134.1 | 34.6 | 85.8 | 19.1 | " | 3/8 | 154.5 | 39.9 | 158.6 | 28.8 |
| | " | " | 1/2 | 151.3 | 38.4 | 93.4 | 20.8 | " | 1/2 | 175.5 | 44.6 | 172.5 | 31.4 |
| | " | " | 5/8 | 169.0 | 42.2 | 101.0 | 22.4 | " | 5/8 | 197.1 | 49.3 | 186.3 | 33.9 |
| | " | " | 3/4 | 187.2 | 46.1 | 108.5 | 24.1 | " | 3/4 | 219.5 | 54.0 | 200.2 | 36.4 |
| | " | " | 7/8 | 206.2 | 50.0 | 116.1 | 25.8 | " | 7/8 | 242.5 | 58.8 | 214.1 | 38.9 |
| | " | " | 1 | 225.6 | 53.9 | 123.8 | 27.5 | " | 1 | 266.3 | 63.6 | 227.9 | 41.4 |
| 7" C21 | 12.25 | 9 | 1/4 | 107.6 | 28.7 | 76.3 | 17.0 | 11 | 1/4 | 120.7 | 32.2 | 144.0 | 26.2 |
| | " | " | 1/8 | 123.6 | 32.4 | 83.9 | 18.6 | " | 1/8 | 140.4 | 36.8 | 157.9 | 28.7 |
| | " | " | 3/8 | 140.3 | 36.2 | 91.5 | 20.3 | " | 3/8 | 160.7 | 41.5 | 171.8 | 31.2 |
| | " | " | 1/2 | 157.5 | 40.0 | 99.1 | 22.0 | " | 1/2 | 181.7 | 46.1 | 185.6 | 33.8 |
| | " | " | 5/8 | 175.2 | 43.8 | 106.7 | 23.7 | " | 5/8 | 203.3 | 50.8 | 199.5 | 36.3 |
| | " | " | 3/4 | 193.4 | 47.6 | 114.3 | 25.4 | " | 3/4 | 225.7 | 55.6 | 213.4 | 38.8 |
| | " | " | 7/8 | 212.4 | 51.5 | 121.9 | 27.1 | " | 7/8 | 248.7 | 60.3 | 227.2 | 41.3 |
| | " | " | 1 | 231.8 | 55.4 | 129.5 | 28.8 | " | 1 | 272.5 | 65.1 | 241.1 | 43.8 |
| 7" C21 | 14.75 | 9 | 1/4 | 113.6 | 30.3 | 81.5 | 18.1 | 11 | 1/4 | 126.7 | 33.8 | 156.3 | 28.4 |
| | " | " | 1/8 | 129.6 | 34.0 | 89.1 | 19.8 | " | 1/8 | 146.4 | 38.4 | 170.1 | 30.9 |
| | " | " | 3/8 | 146.3 | 37.7 | 96.7 | 21.5 | " | 3/8 | 166.7 | 43.0 | 184.0 | 33.5 |
| | " | " | 1/2 | 163.5 | 41.5 | 104.3 | 23.2 | " | 1/2 | 187.7 | 47.7 | 197.8 | 36.0 |
| | " | " | 5/8 | 181.2 | 45.3 | 111.9 | 24.9 | " | 5/8 | 209.3 | 52.3 | 211.7 | 38.5 |
| | " | " | 3/4 | 199.4 | 49.1 | 119.5 | 26.5 | " | 3/4 | 231.7 | 57.0 | 225.6 | 41.0 |
| | " | " | 7/8 | 218.4 | 53.0 | 127.1 | 28.2 | " | 7/8 | 254.7 | 61.8 | 239.4 | 43.5 |
| | " | " | 1 | 237.8 | 56.8 | 134.7 | 29.9 | " | 1 | 278.5 | 66.5 | 253.3 | 46.1 |
| 7" C21 | 17.25 | 9 | 1/4 | 125.7 | 60.6 | 142.3 | 31.6 | " | 3/4 | 302.9 | 71.3 | 267.2 | 48.6 |
| | " | 9 | 1/4 | 119.6 | 31.9 | 85.9 | 19.1 | 11 | 1/4 | 132.7 | 35.4 | 167.1 | 30.4 |
| | " | " | 1/8 | 135.6 | 35.6 | 93.4 | 20.8 | " | 1/8 | 152.4 | 40.0 | 181.0 | 32.9 |
| | " | " | 3/8 | 152.3 | 39.3 | 101.1 | 22.5 | " | 3/8 | 172.7 | 44.6 | 194.9 | 35.4 |
| | " | " | 1/2 | 169.5 | 43.1 | 108.7 | 24.2 | " | 1/2 | 193.7 | 49.2 | 208.7 | 38.0 |
| | " | " | 5/8 | 187.2 | 46.8 | 116.2 | 25.8 | " | 5/8 | 215.3 | 53.8 | 222.6 | 40.5 |
| | " | " | 3/4 | 205.4 | 50.6 | 123.8 | 27.5 | " | 3/4 | 237.7 | 58.5 | 236.5 | 43.0 |
| | " | " | 7/8 | 224.4 | 54.4 | 131.4 | 29.2 | " | 7/8 | 260.7 | 63.2 | 250.3 | 45.5 |
| 7" C21 | 19.75 | 9 | 1/4 | 243.8 | 58.2 | 139.1 | 30.9 | " | 1 | 284.5 | 67.9 | 264.2 | 48.0 |
| | " | " | 3/4 | 263.7 | 62.1 | 146.6 | 32.6 | " | 3/4 | 308.9 | 72.7 | 278.1 | 50.6 |
| | " | 9 | 1/4 | 125.6 | 33.5 | 90.3 | 20.1 | 11 | 1/4 | 138.7 | 37.0 | 178.2 | 32.4 |
| | " | " | 1/8 | 141.6 | 37.1 | 97.9 | 21.8 | " | 1/8 | 158.4 | 41.5 | 192.0 | 34.9 |
| | " | " | 3/8 | 158.3 | 40.8 | 105.5 | 23.4 | " | 3/8 | 178.7 | 46.1 | 205.9 | 37.4 |
| | " | " | 1/2 | 175.5 | 44.6 | 113.1 | 25.1 | " | 1/2 | 199.7 | 50.7 | 219.7 | 40.0 |
| | " | " | 5/8 | 193.2 | 48.3 | 120.7 | 26.8 | " | 5/8 | 221.3 | 55.3 | 233.6 | 42.5 |
| | " | " | 3/4 | 211.4 | 52.0 | 128.3 | 28.5 | " | 3/4 | 243.7 | 60.0 | 247.5 | 45.0 |
| 7" C21 | " | " | 7/8 | 230.4 | 55.9 | 135.9 | 30.2 | " | 7/8 | 266.7 | 64.7 | 261.3 | 47.5 |
| | " | " | 1 | 249.8 | 59.7 | 143.5 | 31.9 | " | 1 | 290.5 | 69.4 | 275.2 | 50.0 |
| | | | 3/4 | 269.7 | 63.5 | 151.1 | 33.6 | | 3/4 | 314.9 | 74.1 | 289.1 | 52.6 |

MOMENTS OF INERTIA AND SECTION MODULI FOR PLATE AND CHAN- NEL COLUMNS.



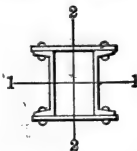
| Depth of Channel and Section Number. | Weight per Foot. | SERIES A. | | | | | | SERIES B. | | | | | |
|--------------------------------------|------------------|-----------------|-------|--------------------|-------------------|--------------------|-------------------|-------------------|-------|--------------------|-------------------|--------------------|-------------------|
| | | Width of Plate. | | Axis 1-1. | | Axis 2-2. | | Width of Plate. | | Axis 1-1. | | Axis 2-2. | |
| | | | | Moment of Inertia. | Section Modulus. | Moment of Inertia. | Section Modulus. | | | Moment of Inertia. | Section Modulus. | Moment of Inertia. | Section Modulus. |
| | | Lbs. | In. | In. | Ins. ⁴ | Ins. ³ | Ins. ⁴ | Ins. ³ | In. | In. | Ins. ⁴ | Ins. ³ | Ins. ⁴ |
| 8" C 25 | 11.25 | 10 | 1/4 | 149.7 | 35.2 | 104.0 | 20.8 | 12 | 1/4 | 166.7 | 39.2 | 181.1 | 30.2 |
| | " | " | 3/8 | 172.6 | 40.0 | 114.4 | 22.9 | " | 3/8 | 194.2 | 45.0 | 199.1 | 33.2 |
| | " | " | 1/2 | 196.2 | 44.9 | 124.9 | 25.0 | " | 1/2 | 222.5 | 50.9 | 217.1 | 36.2 |
| | " | " | 5/8 | 220.5 | 49.7 | 135.3 | 27.1 | " | 5/8 | 251.7 | 56.7 | 235.1 | 39.2 |
| | " | " | 3/4 | 245.4 | 54.5 | 145.7 | 29.1 | " | 3/4 | 281.6 | 62.6 | 253.1 | 42.2 |
| | " | " | 7/8 | 271.1 | 59.4 | 156.1 | 31.2 | " | 7/8 | 312.4 | 68.5 | 271.1 | 45.2 |
| | " | " | 1 | 297.5 | 64.3 | 166.5 | 33.3 | " | 1 | 344.1 | 74.4 | 289.1 | 48.2 |
| | " | " | 1 1/8 | 324.6 | 69.2 | 176.9 | 35.4 | " | 1 1/8 | 376.6 | 80.3 | 307.1 | 51.2 |
| 8" C 26 | 13.75 | 10 | 1/4 | 352.4 | 74.2 | 187.4 | 37.5 | " | 1 1/8 | 410.0 | 86.3 | 325.1 | 54.2 |
| | " | " | 3/8 | 157.1 | 37.0 | 111.6 | 22.3 | 12 | 1/4 | 174.1 | 41.0 | 196.4 | 32.7 |
| | " | " | 1/2 | 180.0 | 41.7 | 122.0 | 24.4 | " | 3/8 | 201.6 | 46.8 | 214.4 | 35.7 |
| | " | " | 5/8 | 203.6 | 46.5 | 132.4 | 26.5 | " | 1/2 | 229.9 | 52.6 | 232.4 | 38.7 |
| | " | " | 3/4 | 227.9 | 51.4 | 142.8 | 28.6 | " | 5/8 | 259.1 | 58.4 | 250.4 | 41.7 |
| | " | " | 7/8 | 252.8 | 56.2 | 153.2 | 30.6 | " | 3/4 | 289.0 | 64.2 | 268.4 | 44.7 |
| | " | " | 1 | 278.5 | 61.0 | 163.6 | 32.7 | " | 7/8 | 319.8 | 70.1 | 286.4 | 47.7 |
| | " | " | 1 1/8 | 304.9 | 65.9 | 174.1 | 34.8 | " | 1 | 351.5 | 76.0 | 304.4 | 50.7 |
| 8" C 25 | 16.25 | 10 | 1/4 | 332.0 | 70.8 | 184.5 | 36.9 | " | 1 1/8 | 384.0 | 81.9 | 322.4 | 53.7 |
| | " | " | 3/8 | 359.8 | 75.8 | 194.9 | 39.0 | " | 3/8 | 417.4 | 87.9 | 340.4 | 56.7 |
| | " | " | 1/2 | 164.9 | 38.8 | 119.4 | 23.9 | 12 | 1/4 | 181.9 | 42.8 | 212.5 | 35.4 |
| | " | " | 5/8 | 187.8 | 43.6 | 129.8 | 26.0 | " | 3/8 | 209.4 | 48.6 | 230.5 | 38.4 |
| | " | " | 3/4 | 211.4 | 48.3 | 140.2 | 28.0 | " | 1/2 | 237.7 | 54.3 | 248.5 | 41.4 |
| | " | " | 7/8 | 235.7 | 53.1 | 150.6 | 30.1 | " | 5/8 | 266.9 | 60.1 | 266.5 | 44.4 |
| | " | " | 1 | 260.6 | 57.9 | 161.0 | 32.2 | " | 3/4 | 296.8 | 66.0 | 284.5 | 47.4 |
| | " | " | 1 1/8 | 286.3 | 62.8 | 171.5 | 34.3 | " | 7/8 | 327.6 | 71.8 | 302.5 | 50.4 |
| 8" C 25 | 18.75 | 10 | 1/4 | 312.7 | 67.6 | 181.9 | 36.4 | " | 1 | 359.3 | 77.7 | 320.5 | 53.4 |
| | " | " | 3/8 | 339.8 | 72.5 | 192.3 | 38.5 | " | 1 1/8 | 391.8 | 83.6 | 338.5 | 56.4 |
| | " | " | 1/2 | 367.6 | 77.4 | 202.7 | 40.5 | " | 3/8 | 425.2 | 89.5 | 356.5 | 59.4 |
| | " | " | 5/8 | 172.7 | 40.6 | 126.3 | 25.3 | 12 | 1/4 | 189.7 | 44.6 | 227.3 | 37.9 |
| | " | " | 3/4 | 195.6 | 45.4 | 136.7 | 27.4 | " | 3/8 | 217.2 | 50.4 | 245.3 | 40.9 |
| | " | " | 7/8 | 219.2 | 50.1 | 147.2 | 29.4 | " | 1/2 | 245.5 | 56.1 | 263.3 | 43.9 |
| | " | " | 1 | 243.5 | 54.9 | 157.6 | 31.5 | " | 5/8 | 274.7 | 61.9 | 281.3 | 46.9 |
| | " | " | 1 1/8 | 268.4 | 59.7 | 168.0 | 33.6 | " | 3/4 | 304.6 | 67.7 | 299.3 | 49.9 |
| 8" C 25 | 21.25 | 10 | 1/4 | 294.1 | 64.5 | 178.4 | 35.7 | " | 1 | 335.4 | 73.5 | 317.3 | 52.9 |
| | " | " | 3/8 | 320.5 | 69.3 | 188.8 | 37.8 | " | 1 1/8 | 367.1 | 79.4 | 335.3 | 55.9 |
| | " | " | 1/2 | 347.6 | 74.2 | 199.2 | 39.9 | " | 3/8 | 399.6 | 85.2 | 353.3 | 58.9 |
| | " | " | 5/8 | 375.4 | 79.0 | 209.7 | 41.9 | " | 1/2 | 433.0 | 91.2 | 371.3 | 61.9 |
| | " | " | 3/4 | 180.7 | 42.5 | 133.0 | 26.6 | 12 | 1/4 | 197.7 | 46.5 | 241.7 | 40.3 |
| | " | " | 7/8 | 203.6 | 47.2 | 143.4 | 28.7 | " | 3/8 | 225.2 | 52.2 | 259.7 | 43.3 |
| | " | " | 1 | 227.2 | 51.9 | 153.8 | 30.8 | " | 1/2 | 253.5 | 58.0 | 277.7 | 46.3 |
| | " | " | 1 1/8 | 251.5 | 56.7 | 164.2 | 32.8 | " | 5/8 | 282.7 | 63.7 | 295.7 | 49.3 |
| 8" C 25 | " | " | 3/4 | 276.4 | 61.4 | 174.6 | 34.9 | " | 3/4 | 312.6 | 69.5 | 313.7 | 52.3 |
| | " | " | 7/8 | 302.1 | 66.2 | 185.0 | 37.0 | " | 1 | 343.4 | 75.3 | 331.7 | 55.3 |
| | " | " | 1 | 328.5 | 71.0 | 195.5 | 39.1 | " | 1 1/8 | 375.1 | 81.1 | 349.7 | 58.3 |
| | " | " | 1 1/8 | 355.6 | 75.9 | 205.9 | 41.2 | " | 3/8 | 407.6 | 87.0 | 367.7 | 61.3 |
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**MOMENTS OF INERTIA AND
SECTION MODULI FOR
PLATE AND CHAN-
NEL COLUMNS.**



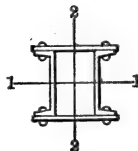
| Depth of Channel and Section Number. | Weight per Foot. | SERIES A. | | | | | | SERIES B. | | | | | |
|--------------------------------------|------------------|---------------------|-----|--------------------|-------------------|--------------------|-------------------|---------------------|-----|--------------------|-------------------|--------------------|-------------------|
| | | Width of Plate. | | Axis 1-1. | | Axis 2-2. | | Width of Plate. | | Axis 1-1. | | Axis 2-2. | |
| | | Thickness of Plate. | | Moment of Inertia. | Section Modulus. | Moment of Inertia. | Section Modulus. | Thickness of Plate. | | Moment of Inertia. | Section Modulus. | Moment of Inertia. | Section Modulus. |
| | | In. | In. | Ins. ⁴ | Ins. ³ | Ins. ⁴ | Ins. ³ | In. | In. | Ins. ⁴ | Ins. ³ | Ins. ⁴ | Ins. ³ |
| 9" C 29 | 13.25 | 11 | 1/4 | 212.3 | 44.7 | 147.9 | 26.9 | 13 | 1/4 | 233.7 | 49.2 | 244.3 | 37.6 |
| | " | " | 1/8 | 243.8 | 50.7 | 161.8 | 29.4 | " | 1/8 | 270.8 | 56.3 | 267.2 | 41.1 |
| | " | " | 3/8 | 276.0 | 56.6 | 175.6 | 31.9 | " | 3/8 | 308.9 | 63.4 | 290.1 | 44.6 |
| | " | " | 1/2 | 309.0 | 62.6 | 189.4 | 34.4 | " | 1/2 | 348.1 | 70.5 | 313.0 | 48.2 |
| | " | " | 5/8 | 343.0 | 68.6 | 203.3 | 37.0 | " | 5/8 | 388.2 | 77.6 | 335.9 | 51.7 |
| | " | " | 3/4 | 377.9 | 74.7 | 217.3 | 39.5 | " | 3/4 | 429.3 | 84.8 | 358.8 | 55.2 |
| | " | " | 7/8 | 413.5 | 80.7 | 231.1 | 42.0 | " | 7/8 | 471.5 | 92.0 | 381.6 | 58.7 |
| | " | " | 1 | 449.9 | 86.7 | 244.9 | 44.5 | " | 1 | 514.7 | 99.2 | 404.5 | 62.2 |
| 9" C 29 | " | " | 3/4 | 487.5 | 92.9 | 258.8 | 47.1 | " | 3/4 | 558.9 | 106.5 | 427.4 | 65.8 |
| | 15.00 | 11 | 1/4 | 219.5 | 46.2 | 155.4 | 28.3 | 13 | 1/4 | 240.9 | 50.7 | 258.5 | 39.8 |
| | " | " | 1/8 | 251.0 | 52.2 | 169.3 | 30.8 | " | 1/8 | 278.0 | 57.8 | 281.4 | 43.3 |
| | " | " | 3/8 | 283.2 | 58.1 | 183.1 | 33.3 | " | 3/8 | 316.1 | 64.9 | 304.3 | 46.8 |
| | " | " | 1/2 | 316.2 | 64.0 | 197.0 | 35.8 | " | 1/2 | 355.3 | 72.0 | 327.2 | 50.3 |
| | " | " | 5/8 | 350.2 | 70.0 | 210.9 | 38.3 | " | 5/8 | 395.4 | 79.1 | 350.1 | 53.9 |
| | " | " | 3/4 | 385.1 | 76.1 | 224.8 | 40.9 | " | 3/4 | 436.5 | 86.2 | 373.0 | 57.4 |
| | " | " | 7/8 | 420.7 | 82.1 | 238.6 | 43.4 | " | 7/8 | 478.7 | 93.4 | 395.8 | 60.9 |
| 9" C 29 | " | " | 1 | 457.1 | 88.1 | 252.4 | 45.9 | " | 1 | 521.9 | 100.6 | 418.7 | 64.4 |
| | " | " | 3/4 | 494.7 | 94.2 | 266.3 | 48.4 | " | 3/4 | 566.1 | 107.8 | 441.6 | 67.9 |
| | 20.00 | 11 | 1/4 | 239.3 | 50.4 | 175.6 | 31.9 | 13 | 1/4 | 260.7 | 54.9 | 297.0 | 45.7 |
| | " | " | 1/8 | 270.8 | 56.3 | 189.5 | 34.5 | " | 1/8 | 297.8 | 61.9 | 319.9 | 49.2 |
| | " | " | 3/8 | 303.0 | 62.2 | 203.3 | 37.0 | " | 3/8 | 335.9 | 68.9 | 342.8 | 52.7 |
| | " | " | 1/2 | 336.0 | 68.0 | 217.1 | 39.5 | " | 1/2 | 375.1 | 76.0 | 365.7 | 56.3 |
| | " | " | 5/8 | 370.0 | 74.0 | 231.0 | 42.0 | " | 5/8 | 415.2 | 83.0 | 388.6 | 59.8 |
| | " | " | 3/4 | 404.9 | 80.0 | 244.9 | 44.5 | " | 3/4 | 456.3 | 90.1 | 411.5 | 63.3 |
| 9" C 29 | " | " | 7/8 | 440.5 | 86.0 | 258.8 | 47.1 | " | 7/8 | 498.5 | 97.3 | 434.3 | 66.8 |
| | " | " | 1 | 476.9 | 91.9 | 272.6 | 49.6 | " | 1 | 541.7 | 104.4 | 457.2 | 70.3 |
| | " | " | 3/4 | 514.5 | 98.0 | 286.5 | 52.1 | " | 3/4 | 585.9 | 111.6 | 480.1 | 73.9 |
| | 25.00 | 11 | 1/4 | 259.1 | 54.5 | 194.6 | 35.4 | 13 | 1/4 | 280.5 | 59.1 | 333.9 | 51.4 |
| | " | " | 1/8 | 290.6 | 60.4 | 208.5 | 37.9 | " | 1/8 | 317.6 | 66.0 | 356.8 | 54.9 |
| | " | " | 3/8 | 322.8 | 66.2 | 222.3 | 40.4 | " | 3/8 | 355.7 | 73.0 | 379.7 | 58.4 |
| | " | " | 1/2 | 355.8 | 72.1 | 236.1 | 42.9 | " | 1/2 | 394.9 | 80.0 | 402.5 | 61.9 |
| | " | " | 5/8 | 389.8 | 78.0 | 250.1 | 45.5 | " | 5/8 | 435.0 | 87.0 | 425.4 | 65.5 |
| 9" C 29 | " | " | 3/4 | 424.7 | 83.9 | 264.0 | 48.0 | " | 3/4 | 476.1 | 94.1 | 448.3 | 69.0 |
| | " | " | 7/8 | 460.3 | 89.8 | 277.8 | 50.5 | " | 7/8 | 518.3 | 101.1 | 471.2 | 72.5 |
| | " | " | 1 | 496.7 | 95.8 | 291.6 | 53.0 | " | 1 | 561.5 | 108.2 | 494.1 | 76.0 |
| | " | " | 3/4 | 534.3 | 101.8 | 305.5 | 55.6 | " | 3/4 | 605.7 | 115.4 | 517.0 | 79.5 |

MOMENTS OF INERTIA AND SECTION MODULI FOR PLATE AND CHAN- NEL COLUMNS.



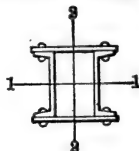
| Depth of Channel and Section Number. | Weight per Foot. | SERIES A. | | | | | | SERIES B. | | | | | |
|--------------------------------------|------------------|-----------------|------------------|--------------------|-------------------|--------------------|-------------------|-----------------|------------------|--------------------|-------------------|--------------------|-------------------|
| | | Width of Plate. | Thickness Plate. | Axis 1-1. | | Axis 2-2. | | Width of Plate. | Thickness Plate. | Axis 1-1. | | Axis 2-2. | |
| | | | | Moment of Inertia. | Section Modulus. | Moment of Inertia. | Section Modulus. | | | Moment of Inertia. | Section Modulus. | Moment of Inertia. | Section Modulus. |
| | | | | Ins. ⁴ | Ins. ³ | Ins. ⁴ | Ins. ³ | | | Ins. ⁴ | Ins. ³ | Ins. ⁴ | Ins. ³ |
| 10" C 33 | 15.0 | 12 | 1/4 | 291.4 | 55.5 | 195.4 | 32.6 | 15 | 1/4 | 330.8 | 63.0 | 381.8 | 50.9 |
| | " | " | 3/8 | 333.3 | 62.7 | 213.4 | 35.6 | " | 3/8 | 383.3 | 72.1 | 417.0 | 55.6 |
| | " | " | 1/2 | 376.1 | 70.0 | 231.4 | 38.6 | " | 1/2 | 436.7 | 81.2 | 452.1 | 60.3 |
| | " | " | 5/8 | 419.9 | 77.2 | 249.4 | 41.6 | " | 5/8 | 491.6 | 90.4 | 487.3 | 65.0 |
| | " | " | 3/4 | 464.8 | 84.5 | 267.4 | 44.6 | " | 3/4 | 547.6 | 99.6 | 522.4 | 69.7 |
| | " | " | 7/8 | 510.7 | 91.8 | 285.4 | 47.6 | " | 7/8 | 605.1 | 108.8 | 557.6 | 74.3 |
| | " | " | 1 | 557.6 | 99.1 | 303.4 | 50.6 | " | 1 | 663.6 | 118.0 | 592.7 | 79.0 |
| | " | " | 1 1/4 | 605.6 | 106.5 | 321.4 | 53.6 | " | 1 1/4 | 723.7 | 127.3 | 627.9 | 83.7 |
| 10" C 38 | " | " | 3/4 | 654.7 | 113.9 | 339.4 | 56.6 | " | 3/4 | 784.9 | 136.5 | 663.1 | 88.4 |
| | 20.0 | 12 | 1/4 | 315.0 | 60.0 | 220.1 | 36.7 | 15 | 1/4 | 354.4 | 67.5 | 438.0 | 58.4 |
| | " | " | 3/8 | 356.9 | 67.2 | 238.1 | 39.7 | " | 3/8 | 406.9 | 76.6 | 473.1 | 63.1 |
| | " | " | 1/2 | 399.7 | 74.4 | 256.1 | 42.7 | " | 1/2 | 460.3 | 85.6 | 508.3 | 67.8 |
| | " | " | 5/8 | 443.5 | 81.6 | 274.1 | 45.7 | " | 5/8 | 515.2 | 94.8 | 543.4 | 72.5 |
| | " | " | 3/4 | 488.4 | 88.8 | 292.1 | 48.7 | " | 3/4 | 571.2 | 103.9 | 578.6 | 77.2 |
| | " | " | 7/8 | 534.3 | 96.1 | 310.1 | 51.7 | " | 7/8 | 628.7 | 113.0 | 613.8 | 81.8 |
| | " | " | 1 | 581.2 | 103.3 | 328.1 | 54.7 | " | 1 | 687.2 | 122.2 | 648.9 | 86.5 |
| 10" C 43 | " | " | 1 1/4 | 629.2 | 110.6 | 346.1 | 57.7 | " | 1 1/4 | 747.3 | 131.4 | 684.1 | 91.2 |
| | " | " | 3/4 | 678.3 | 118.0 | 364.1 | 60.7 | " | 3/4 | 808.5 | 140.6 | 719.2 | 95.9 |
| | 25.0 | 12 | 1/4 | 339.6 | 64.7 | 242.8 | 40.5 | 15 | 1/4 | 379.0 | 72.2 | 491.8 | 65.6 |
| | " | " | 3/8 | 381.5 | 71.8 | 260.8 | 43.5 | " | 3/8 | 431.5 | 81.2 | 526.9 | 70.3 |
| | " | " | 1/2 | 424.3 | 78.9 | 278.8 | 46.5 | " | 1/2 | 484.9 | 90.2 | 562.1 | 75.0 |
| | " | " | 5/8 | 468.1 | 86.1 | 296.8 | 49.5 | " | 5/8 | 539.8 | 99.3 | 587.3 | 79.6 |
| | " | " | 3/4 | 513.0 | 93.3 | 314.8 | 52.5 | " | 3/4 | 595.8 | 108.3 | 632.4 | 84.3 |
| | " | " | 7/8 | 558.9 | 100.5 | 332.8 | 55.5 | " | 7/8 | 653.3 | 117.4 | 667.6 | 89.0 |
| 10" C 48 | " | " | 1 | 605.8 | 107.7 | 350.8 | 58.5 | " | 1 | 711.8 | 126.5 | 702.7 | 93.7 |
| | " | " | 1 1/4 | 653.8 | 115.0 | 368.8 | 61.5 | " | 1 1/4 | 771.9 | 135.7 | 737.9 | 98.4 |
| | " | " | 3/4 | 702.9 | 122.2 | 386.8 | 64.5 | " | 3/4 | 833.1 | 144.9 | 773.0 | 103.1 |
| | 30.0 | 12 | 1/4 | 364.0 | 69.3 | 262.9 | 43.8 | 15 | 1/4 | 403.4 | 76.8 | 541.6 | 72.2 |
| | " | " | 3/8 | 405.9 | 76.4 | 280.9 | 46.8 | " | 3/8 | 455.9 | 85.8 | 576.8 | 76.9 |
| | " | " | 1/2 | 448.7 | 83.5 | 298.9 | 49.8 | " | 1/2 | 509.3 | 94.8 | 611.9 | 81.6 |
| | " | " | 5/8 | 492.5 | 90.6 | 316.9 | 52.8 | " | 5/8 | 564.2 | 103.8 | 647.1 | 86.3 |
| | " | " | 3/4 | 537.4 | 97.7 | 334.9 | 55.8 | " | 3/4 | 620.2 | 112.8 | 682.2 | 91.0 |
| 10" C 53 | " | " | 7/8 | 583.3 | 104.9 | 352.9 | 58.8 | " | 7/8 | 677.7 | 121.8 | 717.4 | 95.7 |
| | " | " | 1 | 630.2 | 112.0 | 370.9 | 61.8 | " | 1 | 736.2 | 130.9 | 752.5 | 100.3 |
| | " | " | 1 1/4 | 678.2 | 119.3 | 388.9 | 64.8 | " | 1 1/4 | 796.3 | 140.0 | 787.7 | 105.0 |
| | " | " | 3/4 | 727.3 | 126.5 | 406.9 | 67.8 | " | 3/4 | 857.5 | 149.1 | 822.9 | 109.7 |
| | 35.0 | 12 | 1/4 | 388.6 | 74.0 | 281.7 | 46.9 | 15 | 1/4 | 428.0 | 81.5 | 589.2 | 78.6 |
| | " | " | 3/8 | 430.5 | 81.0 | 299.7 | 49.9 | " | 3/8 | 480.5 | 90.4 | 624.4 | 83.3 |
| | " | " | 1/2 | 473.3 | 88.1 | 317.7 | 52.9 | " | 1/2 | 533.9 | 99.3 | 659.5 | 87.9 |
| | " | " | 5/8 | 517.1 | 95.1 | 335.7 | 55.9 | " | 5/8 | 588.8 | 108.3 | 694.7 | 92.6 |
| 10" C 58 | " | " | 3/4 | 562.0 | 102.2 | 353.7 | 58.9 | " | 3/4 | 644.8 | 117.2 | 729.8 | 97.3 |
| | " | " | 7/8 | 607.9 | 109.3 | 371.7 | 61.9 | " | 7/8 | 702.3 | 126.3 | 765.0 | 102.0 |
| | " | " | 1 | 654.8 | 116.4 | 389.7 | 64.9 | " | 1 | 760.8 | 135.3 | 800.2 | 106.7 |
| | " | " | 1 1/4 | 702.8 | 123.6 | 407.7 | 67.9 | " | 1 1/4 | 820.9 | 144.3 | 835.3 | 111.4 |
| | " | " | 3/4 | 751.9 | 130.8 | 425.7 | 70.9 | " | 3/4 | 882.1 | 153.4 | 870.5 | 116.1 |

**MOMENTS OF INERTIA AND
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PLATE AND CHAN-
NEL COLUMNS.**

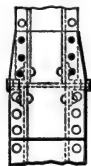
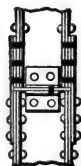
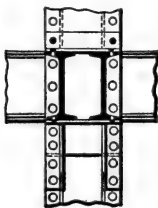
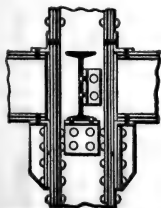
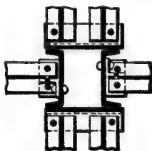
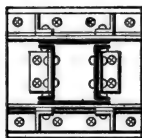
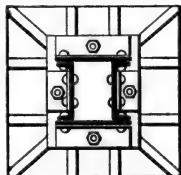
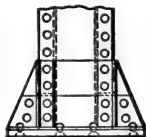
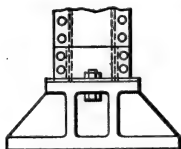
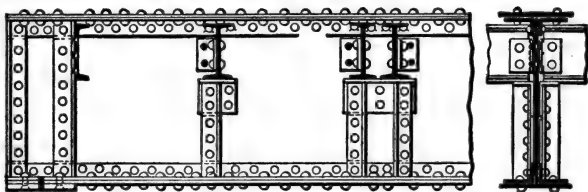


| Depth of Channel and Section Number. | Weight per Foot. | SERIES A. | | | | | | SERIES B. | | | | | |
|--------------------------------------|------------------|-----------------|------|--------------------|-------------------|--------------------|-------------------|-------------------|------|--------------------|-------------------|--------------------|-------------------|
| | | Width of Plate. | | Axis 1-1. | | Axis 2-2. | | Width of Plate. | | Axis 1-1. | | Axis 2-2. | |
| | | | | Moment of Inertia. | Section Modulus. | Moment of Inertia. | Section Modulus. | | | Moment of Inertia. | Section Modulus. | Moment of Inertia. | Section Modulus. |
| | | Lbs. | In. | In. | Ins. ⁴ | Ins. ³ | Ins. ⁴ | Ins. ³ | In. | In. | Ins. ⁴ | Ins. ³ | Ins. ⁴ |
| 12" C41 | 20.5 | 14 | 1/4 | 518.9 | 83.0 | 371.3 | 53.0 | 16 | 1/4 | 556.4 | 89.0 | 549.3 | 68.7 |
| | " | " | 5/16 | 587.9 | 93.1 | 399.9 | 57.1 | " | 5/16 | 635.3 | 100.6 | 592.0 | 74.0 |
| | " | " | 3/8 | 658.3 | 103.3 | 428.4 | 61.2 | " | 3/8 | 715.8 | 112.3 | 634.6 | 79.3 |
| | " | " | 1/2 | 730.1 | 113.4 | 457.0 | 65.3 | " | 1/2 | 797.8 | 123.9 | 677.3 | 84.7 |
| | " | " | 5/8 | 803.4 | 123.6 | 485.6 | 69.4 | " | 5/8 | 881.5 | 135.6 | 720.0 | 90.0 |
| | " | " | 3/4 | 878.0 | 133.8 | 514.2 | 73.5 | " | 3/4 | 966.9 | 147.3 | 762.6 | 95.3 |
| | " | " | 7/8 | 954.1 | 144.0 | 542.8 | 77.5 | " | 7/8 | 1053.8 | 159.1 | 805.3 | 100.7 |
| 12" C41 | 25.0 | 14 | 1/4 | 1031.6 | 154.3 | 571.4 | 81.6 | 16 | 1/4 | 1142.4 | 170.8 | 848.0 | 106.0 |
| | " | " | 5/16 | 1110.6 | 164.5 | 599.9 | 85.7 | " | 5/16 | 1232.7 | 182.6 | 890.6 | 111.3 |
| | " | " | 3/8 | 550.7 | 88.1 | 409.9 | 58.6 | 16 | 3/8 | 588.2 | 94.1 | 610.8 | 76.4 |
| | " | " | 5/16 | 619.7 | 98.2 | 438.5 | 62.7 | " | 5/16 | 667.1 | 105.7 | 653.4 | 81.7 |
| | " | " | 3/8 | 690.1 | 108.3 | 467.1 | 66.7 | " | 3/8 | 747.6 | 117.3 | 696.1 | 87.0 |
| | " | " | 1/2 | 761.9 | 118.4 | 495.7 | 70.8 | " | 1/2 | 829.6 | 128.9 | 738.8 | 92.4 |
| | " | " | 5/8 | 835.2 | 128.5 | 524.3 | 74.9 | " | 5/8 | 913.3 | 140.5 | 781.4 | 97.7 |
| 12" C41 | 30.0 | 14 | 1/4 | 909.8 | 138.6 | 552.9 | 79.0 | 16 | 1/4 | 998.7 | 152.2 | 824.1 | 103.0 |
| | " | " | 5/16 | 985.9 | 148.8 | 581.4 | 83.1 | " | 5/16 | 1085.6 | 163.9 | 866.8 | 108.4 |
| | " | " | 3/8 | 1063.4 | 159.0 | 610.0 | 87.2 | " | 3/8 | 1174.2 | 175.6 | 909.4 | 113.7 |
| | " | " | 1/2 | 1142.4 | 169.3 | 638.6 | 91.2 | " | 1/2 | 1264.5 | 187.3 | 952.1 | 119.0 |
| | " | " | 5/8 | 585.9 | 93.7 | 450.2 | 64.3 | 16 | 5/8 | 623.4 | 99.7 | 675.7 | 84.5 |
| | " | " | 3/4 | 654.9 | 103.7 | 478.8 | 68.4 | " | 3/4 | 702.3 | 111.3 | 718.3 | 89.8 |
| | " | " | 7/8 | 725.3 | 113.8 | 507.3 | 72.5 | " | 7/8 | 782.8 | 122.8 | 761.0 | 95.1 |
| 12" C41 | 35.0 | 14 | 1/4 | 797.1 | 123.8 | 535.9 | 76.6 | 16 | 1/4 | 864.8 | 134.3 | 803.7 | 100.5 |
| | " | " | 5/16 | 870.4 | 133.9 | 564.5 | 80.6 | " | 5/16 | 984.5 | 145.9 | 846.3 | 105.8 |
| | " | " | 3/8 | 945.0 | 144.0 | 593.1 | 84.7 | " | 3/8 | 1033.9 | 157.5 | 889.0 | 111.1 |
| | " | " | 1/2 | 1021.1 | 154.1 | 621.7 | 88.8 | " | 1/2 | 1120.8 | 169.2 | 931.6 | 116.5 |
| | " | " | 5/8 | 1093.6 | 164.3 | 650.3 | 92.9 | " | 5/8 | 1209.4 | 180.9 | 974.3 | 121.8 |
| | " | " | 3/4 | 1177.6 | 174.5 | 678.8 | 97.0 | " | 3/4 | 1299.7 | 192.6 | 1017.0 | 127.1 |
| | " | " | 7/8 | 621.3 | 99.4 | 484.9 | 69.3 | 16 | 7/8 | 658.8 | 105.4 | 733.6 | 91.7 |
| 12" C41 | 40.0 | 14 | 1/4 | 690.3 | 109.4 | 513.4 | 73.4 | 16 | 1/4 | 737.7 | 116.9 | 776.3 | 97.0 |
| | " | " | 5/16 | 760.7 | 119.3 | 542.0 | 77.4 | " | 5/16 | 818.2 | 128.3 | 818.9 | 102.4 |
| | " | " | 3/8 | 832.5 | 129.3 | 570.6 | 81.5 | " | 3/8 | 900.2 | 139.8 | 861.6 | 107.7 |
| | " | " | 1/2 | 905.8 | 139.4 | 599.2 | 85.6 | " | 1/2 | 983.9 | 151.4 | 904.3 | 113.0 |
| | " | " | 5/8 | 980.4 | 149.4 | 627.8 | 89.7 | " | 5/8 | 1069.3 | 162.9 | 946.9 | 118.4 |
| | " | " | 3/4 | 1056.5 | 159.5 | 656.4 | 93.8 | " | 3/4 | 1156.2 | 174.5 | 989.6 | 123.7 |
| | " | " | 7/8 | 1134.0 | 169.6 | 684.9 | 97.9 | " | 7/8 | 1244.8 | 186.1 | 1032.3 | 129.0 |
| 12" C41 | 45.0 | 14 | 1/4 | 1213.0 | 179.7 | 713.5 | 101.9 | 16 | 1/4 | 1335.1 | 197.8 | 1074.9 | 134.4 |
| | " | " | 5/16 | 658.5 | 105.0 | 520.1 | 74.3 | 16 | 5/16 | 694.0 | 111.0 | 792.1 | 99.0 |
| | " | " | 3/8 | 725.5 | 114.9 | 548.7 | 78.4 | " | 3/8 | 772.9 | 122.4 | 834.8 | 104.3 |
| | " | " | 1/2 | 795.9 | 124.9 | 577.2 | 82.5 | " | 1/2 | 853.4 | 133.9 | 877.4 | 109.7 |
| | " | " | 5/8 | 867.7 | 134.8 | 605.8 | 86.6 | " | 5/8 | 935.4 | 145.3 | 920.1 | 115.0 |
| | " | " | 3/4 | 941.0 | 144.8 | 634.4 | 90.6 | " | 3/4 | 1019.1 | 156.8 | 962.8 | 120.3 |
| | " | " | 7/8 | 1015.6 | 154.8 | 663.0 | 94.7 | " | 7/8 | 1104.5 | 168.3 | 1005.4 | 125.7 |
| 12" C41 | 50.0 | 14 | 1/4 | 1091.7 | 164.8 | 691.6 | 98.8 | 16 | 1/4 | 1191.4 | 179.8 | 1048.1 | 131.0 |
| | " | " | 5/16 | 1169.2 | 174.8 | 720.2 | 102.9 | " | 5/16 | 1280.0 | 191.4 | 1090.8 | 136.3 |
| 12" C41 | 55.0 | 14 | 1/4 | 1248.2 | 184.9 | 748.7 | 107.0 | 16 | 1/4 | 1370.3 | 203.0 | 1133.4 | 141.7 |

MOMENTS OF INERTIA AND SECTION MODULI FOR PLATE AND CHAN- NEL COLUMNS.



| Depth of Channel and Section Number. | Weight per Foot. | SERIES A. | | | | | | SERIES B. | | | | | |
|--------------------------------------|------------------|---------------------|---------------|--------------------|------------------|--------------------|------------------|---------------------|---------------|--------------------|------------------|--------------------|------------------|
| | | Width of Plate. | | Axis 1-1. | | Axis 2-2. | | Width of Plate. | | Axis 1-1. | | Axis 2-2. | |
| | | Thickness of Plate. | | Moment of Inertia. | Section Modulus. | Moment of Inertia. | Section Modulus. | Thickness of Plate. | | Moment of Inertia. | Section Modulus. | Moment of Inertia. | Section Modulus. |
| | | In. | In. | | | | | In. | In. | | | | |
| | Lbs. | In. | In. | In. ⁴ | In. ³ | In. ⁴ | In. ³ | In. | In. | In. ⁴ | In. ³ | In. ⁴ | In. ³ |
| 15" C53 | 33.0 | 17 | $\frac{3}{8}$ | 1378.9 | 175.1 | 953.4 | 112.2 | 20 | $\frac{3}{8}$ | 1511.8 | 192.0 | 1525.9 | 152.6 |
| | " | " | $\frac{1}{2}$ | 1512.0 | 190.5 | 1004.7 | 118.2 | " | $\frac{1}{2}$ | 1668.1 | 210.2 | 1609.2 | 160.9 |
| | " | " | $\frac{5}{8}$ | 1646.6 | 205.8 | 1055.7 | 124.2 | " | $\frac{5}{8}$ | 1826.9 | 228.4 | 1692.5 | 169.3 |
| | " | " | $\frac{3}{4}$ | 1783.4 | 221.2 | 1106.8 | 130.2 | " | $\frac{3}{4}$ | 1988.1 | 246.6 | 1775.9 | 177.6 |
| | " | " | $\frac{7}{8}$ | 1922.9 | 236.7 | 1158.1 | 136.2 | " | $\frac{7}{8}$ | 2151.9 | 264.9 | 1859.2 | 185.9 |
| | " | " | $\frac{1}{4}$ | 2064.6 | 252.2 | 1209.4 | 142.3 | " | $\frac{1}{4}$ | 2318.2 | 283.1 | 1942.5 | 194.3 |
| 15" C58 | " | " | $\frac{3}{4}$ | 2207.8 | 267.6 | 1260.4 | 148.3 | " | $\frac{3}{4}$ | 2487.1 | 301.5 | 2025.9 | 202.6 |
| | 35.0 | 17 | $\frac{3}{8}$ | 1393.5 | 177.0 | 971.7 | 114.3 | 20 | $\frac{3}{8}$ | 1526.4 | 193.8 | 1557.3 | 155.7 |
| | " | " | $\frac{1}{2}$ | 1526.6 | 192.3 | 1023.0 | 120.4 | " | $\frac{1}{2}$ | 1682.7 | 212.0 | 1640.7 | 164.1 |
| | " | " | $\frac{5}{8}$ | 1661.2 | 207.7 | 1074.1 | 126.4 | " | $\frac{5}{8}$ | 1841.5 | 230.2 | 1724.0 | 172.4 |
| | " | " | $\frac{3}{4}$ | 1798.0 | 223.0 | 1125.1 | 132.4 | " | $\frac{3}{4}$ | 2002.7 | 248.4 | 1807.3 | 180.7 |
| | " | " | $\frac{7}{8}$ | 1937.5 | 238.5 | 1176.4 | 138.4 | " | $\frac{7}{8}$ | 2166.5 | 266.6 | 1890.7 | 189.1 |
| 15" C58 | " | " | $\frac{1}{4}$ | 2079.2 | 254.0 | 1227.7 | 144.4 | " | $\frac{1}{4}$ | 2332.8 | 284.9 | 1974.0 | 197.4 |
| | " | " | $\frac{3}{4}$ | 2222.4 | 269.4 | 1278.8 | 150.4 | " | $\frac{3}{4}$ | 2501.7 | 303.2 | 2057.3 | 205.7 |
| | 40.0 | 17 | $\frac{3}{8}$ | 1448.7 | 184.0 | 1039.9 | 122.3 | 20 | $\frac{3}{8}$ | 1581.6 | 200.8 | 1674.6 | 167.5 |
| | " | " | $\frac{1}{2}$ | 1581.8 | 199.3 | 1091.2 | 128.4 | " | $\frac{1}{2}$ | 1737.9 | 219.0 | 1757.9 | 175.8 |
| | " | " | $\frac{5}{8}$ | 1716.4 | 214.6 | 1142.3 | 134.4 | " | $\frac{5}{8}$ | 1896.7 | 237.1 | 1841.2 | 184.1 |
| | " | " | $\frac{3}{4}$ | 1853.2 | 229.9 | 1193.3 | 140.4 | " | $\frac{3}{4}$ | 2057.9 | 255.3 | 1924.6 | 192.5 |
| 15" C58 | " | " | $\frac{7}{8}$ | 1992.7 | 245.3 | 1244.6 | 146.4 | " | $\frac{7}{8}$ | 2221.7 | 273.4 | 2007.9 | 200.8 |
| | " | " | $\frac{1}{4}$ | 2134.4 | 260.7 | 1295.9 | 152.5 | " | $\frac{1}{4}$ | 2388.0 | 291.7 | 2091.2 | 209.1 |
| | " | " | $\frac{3}{4}$ | 2277.6 | 276.1 | 1347.0 | 158.5 | " | $\frac{3}{4}$ | 2556.9 | 309.9 | 2174.6 | 217.5 |
| | 45.0 | 17 | $\frac{3}{8}$ | 1503.9 | 191.0 | 1105.4 | 130.1 | 20 | $\frac{3}{8}$ | 1636.8 | 207.9 | 1788.6 | 178.9 |
| | " | " | $\frac{1}{2}$ | 1637.0 | 206.2 | 1156.8 | 136.1 | " | $\frac{1}{2}$ | 1793.1 | 225.9 | 1871.9 | 187.2 |
| | " | " | $\frac{5}{8}$ | 1771.6 | 221.5 | 1207.9 | 142.1 | " | $\frac{5}{8}$ | 1951.9 | 244.0 | 1955.3 | 195.5 |
| 15" C58 | " | " | $\frac{3}{4}$ | 1908.4 | 236.7 | 1258.9 | 148.1 | " | $\frac{3}{4}$ | 2113.1 | 262.1 | 2038.6 | 203.9 |
| | " | " | $\frac{7}{8}$ | 2047.9 | 252.0 | 1310.2 | 154.2 | " | $\frac{7}{8}$ | 2276.9 | 280.2 | 2121.9 | 212.2 |
| | " | " | $\frac{1}{4}$ | 2189.6 | 267.4 | 1361.5 | 160.2 | " | $\frac{1}{4}$ | 2443.2 | 298.4 | 2205.3 | 220.5 |
| | " | " | $\frac{3}{4}$ | 2332.8 | 282.8 | 1412.6 | 166.2 | " | $\frac{3}{4}$ | 2612.1 | 316.6 | 2288.6 | 228.9 |
| | 50.0 | 17 | $\frac{3}{8}$ | 1559.1 | 198.0 | 1165.3 | 137.1 | 20 | $\frac{3}{8}$ | 1692.0 | 214.9 | 1894.9 | 189.5 |
| | " | " | $\frac{1}{2}$ | 1692.2 | 213.2 | 1216.6 | 143.1 | " | $\frac{1}{2}$ | 1848.3 | 232.9 | 1978.2 | 197.8 |
| 15" C58 | " | " | $\frac{5}{8}$ | 1826.8 | 228.4 | 1267.7 | 149.1 | " | $\frac{5}{8}$ | 2007.1 | 250.9 | 2061.5 | 206.2 |
| | " | " | $\frac{3}{4}$ | 1963.6 | 243.5 | 1318.7 | 155.1 | " | $\frac{3}{4}$ | 2168.3 | 268.9 | 2144.9 | 214.5 |
| | " | " | $\frac{7}{8}$ | 2103.1 | 258.8 | 1370.0 | 161.2 | " | $\frac{7}{8}$ | 2332.1 | 287.0 | 2228.2 | 222.8 |
| | " | " | $\frac{1}{4}$ | 2244.8 | 274.2 | 1421.3 | 167.2 | " | $\frac{1}{4}$ | 2498.4 | 305.2 | 2311.5 | 231.2 |
| | " | " | $\frac{3}{4}$ | 2388.0 | 289.5 | 1472.4 | 173.2 | " | $\frac{3}{4}$ | 2667.3 | 323.3 | 2394.9 | 239.5 |
| | 55.0 | 17 | $\frac{3}{8}$ | 1614.1 | 205.0 | 1223.4 | 143.9 | 20 | $\frac{3}{8}$ | 1747.0 | 221.9 | 1998.8 | 199.9 |
| 15" C58 | " | " | $\frac{1}{2}$ | 1747.2 | 220.1 | 1274.7 | 150.0 | " | $\frac{1}{2}$ | 1903.3 | 239.8 | 2082.1 | 208.2 |
| | " | " | $\frac{5}{8}$ | 1881.8 | 235.2 | 1325.7 | 156.0 | " | $\frac{5}{8}$ | 2062.1 | 257.8 | 2165.5 | 216.6 |
| | " | " | $\frac{3}{4}$ | 2018.6 | 250.4 | 1376.8 | 162.0 | " | $\frac{3}{4}$ | 2223.3 | 275.8 | 2248.8 | 224.9 |
| | " | " | $\frac{7}{8}$ | 2158.1 | 265.6 | 1428.1 | 168.0 | " | $\frac{7}{8}$ | 2387.1 | 293.8 | 2332.1 | 233.2 |
| | " | " | $\frac{1}{4}$ | 2299.8 | 280.9 | 1479.4 | 174.0 | " | $\frac{1}{4}$ | 2553.4 | 311.9 | 2415.5 | 241.6 |
| | " | " | $\frac{3}{4}$ | 2443.0 | 296.1 | 1530.4 | 180.1 | " | $\frac{3}{4}$ | 2722.3 | 330.0 | 2498.8 | 249.9 |

**TYPICAL DETAILS OF PLATE GIRDERS, COLUMN
BASES AND STEEL COLUMNS.**

**SAFE LOADS IN THOUSANDS OF POUNDS
FOR I-BEAMS USED AS COLUMNS
WITH SQUARE ENDS.**

Based on Gordon's Formula, $P = \frac{50\,000}{1 + \frac{(12 L)^2}{36\,000 r^2}}$ Safety factor 4.

| Depth of Beam and Section Number. | Weight per Foot. | Area of Section. | Least Radius of Gyration. | Length in Feet. | | | | | | |
|-----------------------------------|------------------|------------------|---------------------------|-----------------|-----|-----|-----|-----|-----|-----|
| | Pounds. | Sq. Ins. | Inch. | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| 3" B 5 | 5.5 | 1.63 | .53 | 19 | 18 | 17 | 15 | 13 | 12 | 11 |
| | 6.5 | 1.91 | .52 | 23 | 21 | 19 | 17 | 16 | 14 | 12 |
| | 7.5 | 2.21 | .52 | 26 | 24 | 22 | 20 | 18 | 16 | 14 |
| 4" B 9 | 7.5 | 2.21 | .59 | 26 | 25 | 23 | 21 | 20 | 18 | 16 |
| | 8.5 | 2.50 | .58 | 30 | 28 | 26 | 24 | 22 | 20 | 18 |
| | 9.5 | 2.79 | .58 | 33 | 31 | 29 | 27 | 24 | 22 | 20 |
| | 10.5 | 3.09 | .57 | 37 | 35 | 32 | 29 | 27 | 24 | 22 |
| 5" B 13 | 9.75 | 2.87 | .65 | 35 | 33 | 31 | 29 | 27 | 24 | 22 |
| | 12.25 | 3.60 | .63 | 43 | 41 | 39 | 36 | 33 | 30 | 27 |
| | 14.75 | 4.34 | .63 | 52 | 50 | 47 | 43 | 40 | 36 | 33 |
| 6" B 17 | 12.25 | 3.61 | .72 | 44 | 42 | 40 | 38 | 35 | 33 | 30 |
| | 14.75 | 4.34 | .69 | 52 | 51 | 48 | 45 | 42 | 39 | 35 |
| | 17.25 | 5.07 | .68 | 61 | 59 | 56 | 52 | 48 | 44 | 41 |
| 7" B 21 | 15.0 | 4.42 | .78 | 54 | 52 | 50 | 47 | 45 | 42 | 39 |
| | 17.5 | 5.15 | .76 | 63 | 61 | 58 | 55 | 52 | 48 | 45 |
| | 20.0 | 5.88 | .74 | 71 | 69 | 66 | 62 | 58 | 54 | 50 |
| 8" B 25 | 18.00 | 5.33 | .84 | 65 | 63 | 61 | 58 | 55 | 52 | 49 |
| | 20.25 | 5.96 | .82 | 73 | 71 | 68 | 65 | 61 | 58 | 54 |
| | 22.75 | 6.69 | .81 | 82 | 79 | 76 | 72 | 69 | 65 | 60 |
| | 25.25 | 7.43 | .80 | 91 | 88 | 84 | 80 | 76 | 71 | 66 |
| 9" B 29 | 21.0 | 6.31 | .90 | 77 | 76 | 73 | 70 | 67 | 63 | 60 |
| | 25.0 | 7.35 | .88 | 90 | 88 | 85 | 81 | 78 | 73 | 69 |
| | 30.0 | 8.82 | .85 | 108 | 105 | 101 | 97 | 92 | 87 | 81 |
| | 35.0 | 10.29 | .84 | 126 | 122 | 118 | 112 | 107 | 101 | 95 |
| 10" B 33 | 25.0 | 7.37 | .97 | 91 | 89 | 86 | 83 | 80 | 76 | 73 |
| | 30.0 | 8.82 | .93 | 108 | 106 | 103 | 99 | 94 | 90 | 85 |
| | 35.0 | 10.29 | .91 | 126 | 123 | 119 | 115 | 110 | 104 | 98 |
| | 40.0 | 11.76 | .90 | 144 | 141 | 136 | 131 | 125 | 118 | 112 |
| 12" B 41 | 31.5 | 9.26 | 1.01 | 114 | 112 | 109 | 105 | 102 | 97 | 93 |
| | 35.0 | 10.29 | .99 | 127 | 124 | 121 | 117 | 112 | 107 | 102 |
| | 40.0 | 11.76 | .96 | 144 | 142 | 137 | 133 | 127 | 121 | 115 |
| 12" B 105 | 40.0 | 11.84 | 1.08 | 146 | 144 | 140 | 136 | 132 | 127 | 121 |
| | 45.0 | 13.24 | 1.06 | 163 | 160 | 156 | 152 | 146 | 141 | 135 |
| | 50.0 | 14.71 | 1.05 | 181 | 178 | 174 | 168 | 163 | 156 | 149 |
| | 55.0 | 16.18 | 1.04 | 199 | 196 | 191 | 185 | 178 | 171 | 163 |

**SAFE LOADS IN THOUSANDS OF POUNDS
FOR I-BEAMS USED AS COLUMNS
WITH SQUARE ENDS.**

Based on Gordon's Formula, $P = \frac{50\,000}{1 + \frac{(12\,L)^2}{36\,000\,r^2}}$ Safety factor 4.

| Length in Feet. | | | | | | | | | Weight per Foot. | Depth of Beam and Section Number. |
|-----------------|-----|-----|-----|-----|-----|-----|-----|----|------------------------|---|
| 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | Pounds. | |
| 9 | | | | | | | | | 5.5 | 3" B 5 |
| 11 | | | | | | | | | 6.5 | |
| 13 | | | | | | | | | 7.5 | |
| 14 | 13 | | | | | | | | 7.5 | 4" B 9 |
| 16 | 14 | | | | | | | | 8.5 | |
| 18 | 16 | | | | | | | | 9.5 | |
| 19 | 17 | | | | | | | | 10.5 | 5" B 13 |
| 20 | 18 | 17 | | | | | | | 9.75 | |
| 25 | 22 | 20 | | | | | | | 12.25 | |
| 30 | 27 | 24 | | | | | | | 14.75 | 6" B 17 |
| 28 | 25 | 23 | 21 | | | | | | 12.25 | |
| 32 | 29 | 27 | 25 | | | | | | 14.75 | |
| 37 | 34 | 31 | 28 | | | | | | 17.25 | 7" B 21 |
| 36 | 33 | 31 | 28 | 26 | | | | | 15.0 | |
| 41 | 38 | 35 | 32 | 30 | | | | | 17.5 | |
| 46 | 43 | 39 | 36 | 33 | | | | | 20.0 | 8" B 25 |
| 46 | 43 | 40 | 37 | 34 | 31 | | | | 18.00 | |
| 50 | 47 | 43 | 40 | 37 | 34 | | | | 20.25 | |
| 56 | 52 | 48 | 45 | 41 | 38 | | | | 22.75 | 9" B 29 |
| 61 | 57 | 53 | 49 | 45 | 42 | | | | 25.25 | |
| 56 | 53 | 49 | 46 | 43 | 40 | 37 | | | 21.0 | |
| 65 | 60 | 57 | 53 | 49 | 46 | 43 | | | 25.0 | 10" B 33 |
| 76 | 71 | 66 | 61 | 57 | 53 | 49 | | | 30.0 | |
| 88 | 82 | 76 | 71 | 66 | 61 | 56 | | | 35.0 | |
| 68 | 65 | 61 | 57 | 54 | 50 | 47 | 44 | | 25.0 | 12" B 41 |
| 80 | 75 | 71 | 66 | 62 | 58 | 54 | 50 | | 30.0 | |
| 92 | 87 | 81 | 76 | 71 | 66 | 62 | 57 | | 35.0 | |
| 105 | 98 | 92 | 86 | 80 | 74 | 69 | 65 | | 40.0 | 12" B 105 |
| 88 | 83 | 78 | 74 | 69 | 65 | 61 | 58 | 54 | 31.5 | |
| 97 | 91 | 86 | 81 | 76 | 72 | 67 | 63 | 59 | 35.0 | |
| 109 | 103 | 96 | 90 | 85 | 79 | 74 | 69 | 65 | 40.0 | |
| 116 | 110 | 105 | 99 | 94 | 88 | 83 | 79 | 75 | 40.0 | |
| 128 | 122 | 116 | 110 | 103 | 98 | 92 | 87 | 82 | 45.0 | |
| 142 | 135 | 128 | 121 | 114 | 108 | 101 | 96 | 90 | 50.0 | |
| 155 | 148 | 140 | 132 | 124 | 117 | 111 | 104 | 98 | 55.0 | |

**SAFE LOADS IN THOUSANDS OF POUNDS
FOR I-BEAMS USED AS COLUMNS
WITH SQUARE ENDS.**

Based on Gordon's Formula, $P = \frac{50\,000}{1 + \frac{(12\,L)^2}{36\,000\,r^2}}$ Safety factor 4.

| Depth of Beam and Section | Weight per Foot. | Area of Section. | Least Radius of Gyration. | Length in Feet. | | | | | | | |
|------------------------------------|------------------------|------------------------|------------------------------------|-----------------|-----|-----|-----|-----|-----|-----|-----|
| | | | | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 15" B 53 | 42.0 | 12.48 | 1.08 | 154 | 151 | 148 | 144 | 139 | 133 | 128 | 122 |
| | 45.0 | 13.24 | 1.07 | 163 | 160 | 157 | 152 | 147 | 142 | 135 | 129 |
| | 50.0 | 14.71 | 1.04 | 181 | 178 | 174 | 168 | 162 | 156 | 149 | 141 |
| | 55.0 | 16.18 | 1.03 | 199 | 196 | 191 | 185 | 178 | 171 | 163 | 155 |
| 15" B 109 | 60.0 | 17.65 | 1.01 | 217 | 213 | 207 | 201 | 194 | 185 | 177 | 167 |
| | 60.0 | 17.67 | 1.21 | 218 | 215 | 212 | 207 | 201 | 195 | 188 | 181 |
| | 65.0 | 19.12 | 1.20 | 236 | 233 | 229 | 223 | 217 | 211 | 203 | 195 |
| | 70.0 | 20.59 | 1.19 | 254 | 251 | 246 | 240 | 234 | 226 | 218 | 209 |
| 15" B 113 | 75.0 | 22.06 | 1.18 | 273 | 269 | 264 | 258 | 250 | 242 | 233 | 224 |
| | 80.0 | 23.53 | 1.17 | 291 | 286 | 281 | 274 | 266 | 257 | 248 | 238 |
| | 80.0 | 23.57 | 1.32 | 292 | 289 | 284 | 279 | 273 | 265 | 256 | 249 |
| | 85.0 | 25.00 | 1.32 | 309 | 306 | 302 | 295 | 289 | 281 | 272 | 264 |
| 18" B 65 | 90.0 | 26.47 | 1.32 | 328 | 324 | 319 | 313 | 306 | 297 | 288 | 279 |
| | 95.0 | 27.94 | 1.31 | 346 | 342 | 336 | 330 | 322 | 314 | 304 | 293 |
| | 100.0 | 29.41 | 1.31 | 364 | 360 | 354 | 348 | 339 | 330 | 320 | 309 |
| | 55.0 | 15.93 | 1.15 | 197 | 194 | 190 | 185 | 180 | 173 | 166 | 160 |
| 20" B 73 | 60.0 | 17.65 | 1.13 | 218 | 214 | 210 | 205 | 198 | 191 | 184 | 176 |
| | 65.0 | 19.12 | 1.11 | 236 | 232 | 227 | 221 | 214 | 206 | 198 | 189 |
| | 70.0 | 20.59 | 1.09 | 254 | 250 | 244 | 237 | 230 | 221 | 212 | 202 |
| | 65.0 | 19.08 | 1.21 | 236 | 233 | 229 | 223 | 217 | 210 | 203 | 196 |
| 20" B 121 | 70.0 | 20.59 | 1.19 | 254 | 251 | 246 | 240 | 234 | 226 | 218 | 209 |
| | 75.0 | 22.06 | 1.17 | 273 | 268 | 264 | 257 | 250 | 241 | 233 | 223 |
| | 80.0 | 23.73 | 1.39 | 294 | 291 | 287 | 282 | 276 | 270 | 261 | 254 |
| | 85.0 | 25.00 | 1.37 | 309 | 307 | 302 | 297 | 290 | 283 | 275 | 266 |
| 24" B 89 | 90.0 | 26.47 | 1.36 | 328 | 325 | 320 | 314 | 307 | 300 | 290 | 282 |
| | 95.0 | 27.94 | 1.35 | 346 | 343 | 337 | 331 | 324 | 315 | 307 | 296 |
| | 100.0 | 29.41 | 1.34 | 364 | 361 | 355 | 349 | 340 | 332 | 321 | 312 |
| | 80.0 | 23.32 | 1.36 | 289 | 286 | 282 | 276 | 271 | 264 | 256 | 248 |
| 24" B 127 | 85.0 | 25.00 | 1.33 | 309 | 306 | 302 | 295 | 289 | 281 | 273 | 264 |
| | 90.0 | 26.47 | 1.31 | 328 | 324 | 319 | 313 | 305 | 297 | 288 | 278 |
| | 95.0 | 27.94 | 1.30 | 346 | 342 | 336 | 330 | 322 | 313 | 303 | 293 |
| | 100.0 | 29.41 | 1.28 | 364 | 360 | 354 | 347 | 338 | 328 | 317 | 307 |
| 24" B 127 | 105.0 | 30.98 | 1.60 | 385 | 382 | 378 | 373 | 367 | 360 | 352 | 344 |
| | 110.0 | 32.48 | 1.58 | 403 | 400 | 396 | 390 | 384 | 376 | 368 | 359 |
| | 115.0 | 33.98 | 1.57 | 422 | 419 | 414 | 408 | 401 | 393 | 385 | 375 |

**SAFE LOADS IN THOUSANDS OF POUNDS
FOR I-BEAMS USED AS COLUMNS
WITH SQUARE ENDS.**

Based on Gordon's Formula, $P = \frac{50\,000}{1 + \frac{(12\,L)^2}{36\,000\,r^2}}$ Safety factor 4.

| Length in Feet. | | | | | | | | | | Weight per Foot. | Depth of Beam and Section. Number. |
|-----------------|-----|-----|-----|-----|-----|-----|-----|-----|-------|------------------------|--|
| 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | Pounds. | |
| 116 | 110 | 105 | 99 | 93 | 88 | 83 | 79 | 74 | | 42.0 | 15" B 53 |
| 123 | 116 | 110 | 104 | 98 | 93 | 87 | 82 | 78 | | 45.0 | |
| 134 | 127 | 120 | 113 | 106 | 101 | 94 | 89 | 84 | | 50.0 | |
| 147 | 139 | 131 | 124 | 116 | 109 | 103 | 97 | 91 | | 55.0 | |
| 153 | 150 | 141 | 132 | 124 | 117 | 110 | 104 | 97 | | 60.0 | |
| 173 | 166 | 159 | 152 | 144 | 137 | 130 | 124 | 117 | 111 | 60.0 | 15" B 109 |
| 187 | 179 | 171 | 163 | 154 | 147 | 140 | 132 | 126 | 120 | 65.0 | |
| 201 | 192 | 183 | 174 | 165 | 157 | 150 | 142 | 135 | 127 | 70.0 | |
| 214 | 205 | 195 | 186 | 176 | 168 | 158 | 151 | 142 | 135 | 75.0 | |
| 228 | 217 | 206 | 197 | 187 | 178 | 168 | 160 | 151 | 143 | 80.0 | |
| 239 | 231 | 221 | 213 | 203 | 194 | 186 | 177 | 169 | 161 | 80.0 | 15" B 113 |
| 254 | 245 | 235 | 226 | 216 | 206 | 197 | 188 | 180 | 171 | 85.0 | |
| 269 | 259 | 249 | 239 | 228 | 218 | 209 | 199 | 190 | 181 | 90.0 | |
| 284 | 272 | 261 | 251 | 240 | 228 | 219 | 208 | 199 | 190 | 95.0 | |
| 299 | 287 | 275 | 264 | 252 | 240 | 230 | 219 | 210 | 200 | 100.0 | |
| 153 | 145 | 139 | 132 | 125 | 119 | 112 | 106 | 100 | 95 | 55.0 | 18" B 65 |
| 168 | 160 | 152 | 144 | 137 | 129 | 122 | 116 | 110 | 104 | 60.0 | |
| 181 | 172 | 163 | 154 | 146 | 138 | 131 | 123 | 117 | 110 | 65.0 | |
| 192 | 183 | 173 | 164 | 155 | 146 | 138 | 130 | 123 | 116 | 70.0 | |
| 187 | 179 | 171 | 164 | 155 | 148 | 141 | 134 | 126 | 120 | 65.0 | 20" B 78 |
| 201 | 192 | 183 | 174 | 165 | 157 | 150 | 142 | 135 | 127 | 70.0 | |
| 214 | 204 | 194 | 185 | 175 | 167 | 158 | 150 | 142 | 135 | 75.0 | |
| 246 | 237 | 229 | 219 | 211 | 202 | 194 | 186 | 177 | 169 | 80.0 | 20" B 121 |
| 258 | 249 | 239 | 230 | 221 | 212 | 202 | 194 | 185 | 176 | 85.0 | |
| 271 | 262 | 253 | 241 | 232 | 223 | 213 | 204 | 195 | 185 | 90.0 | |
| 286 | 277 | 265 | 255 | 244 | 234 | 223 | 214 | 205 | 195 | 95.0 | |
| 300 | 290 | 278 | 267 | 257 | 245 | 235 | 223 | 214 | 203 | 100.0 | |
| 239 | 231 | 223 | 213 | 205 | 196 | 187 | 179 | 172 | 163 | 80.0 | 24" B 89 |
| 255 | 245 | 236 | 226 | 217 | 207 | 198 | 189 | 181 | 172 | 85.0 | |
| 269 | 258 | 247 | 238 | 227 | 216 | 207 | 197 | 189 | 180 | 90.0 | |
| 282 | 271 | 261 | 249 | 239 | 228 | 218 | 207 | 198 | 188 | 95.0 | |
| 296 | 284 | 272 | 260 | 249 | 238 | 226 | 215 | 205 | 196 | 100.0 | |
| 335 | 326 | 316 | 306 | 296 | 286 | 277 | 266 | 257 | 247 | 105.0 | 24" B 127 |
| 350 | 340 | 330 | 319 | 309 | 298 | 288 | 278 | 267 | 257 | 110.0 | |
| 365 | 355 | 344 | 333 | 322 | 311 | 300 | 289 | 278 | 268 | 115.0 | |

SAFE LOADS IN THOUSANDS OF POUNDS FOR PLATE AND ANGLE COLUMNS, SQUARE ENDS.

CALCULATED FOR LEAST RADIUS OF GYRATION, AXIS 1-1.

Based on Gordon's Formula, $P = \frac{50\,000}{1 + \frac{(12 L)^2}{36\,000 r^2}}$

Safety factor 4.

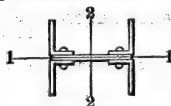


| Size of Angles. | Size of Plate. | Weight of Column. | Area of Column Section. | Least Radius of Gyration Axis 1-1. | Radius of Gyration Axis 2-2. | Length in Feet. | | |
|---------------------------|----------------|-------------------|-------------------------|------------------------------------|------------------------------|-----------------|-----|-----|
| Inches. | Inches. | Lbs. per Ft. | Sq. Ins. | Inches. | Inches. | 2 | 4 | 6 |
| 3 x 2½ x ¼ | 6 x ¼ | 23.1 | 6.74 | 1.24 | 2.41 | 84 | 81 | 77 |
| " " ⅜ | " " ⅜ | 28.8 | 8.36 | 1.27 | 2.39 | 103 | 100 | 96 |
| " " ½ | " " ½ | 34.1 | 9.93 | 1.30 | 2.37 | 123 | 120 | 114 |
| " " ⅝ | " " ⅝ | 39.3 | 11.51 | 1.33 | 2.35 | 142 | 139 | 133 |
| " " ¾ | " " ¾ | 44.2 | 13.00 | 1.36 | 2.33 | 161 | 157 | 151 |
| " " ⅞ | " " ⅞ | 49.5 | 14.50 | 1.39 | 2.31 | 180 | 175 | 169 |
| 3½ x 2½ x ¼ | 7 x ¼ | 25.6 | 7.51 | 1.46 | 2.88 | 93 | 91 | 88 |
| " " ⅜ | " " ⅜ | 31.8 | 9.31 | 1.49 | 2.86 | 115 | 113 | 109 |
| " " ½ | " " ½ | 37.7 | 11.07 | 1.52 | 2.84 | 137 | 135 | 130 |
| " " ⅝ | " " ⅝ | 43.6 | 12.78 | 1.55 | 2.82 | 159 | 156 | 151 |
| " " ¾ | " " ¾ | 49.5 | 14.50 | 1.58 | 2.80 | 180 | 177 | 171 |
| " " ⅞ | " " ⅞ | 55.0 | 16.18 | 1.61 | 2.78 | 201 | 197 | 192 |
| 4 x 3 x ⅜ | 8 x ⅜ | 37.3 | 10.86 | 1.67 | 3.25 | | 133 | 129 |
| " " ½ | " " ½ | 44.2 | 12.92 | 1.70 | 3.23 | | 158 | 154 |
| " " ⅝ | " " ⅝ | 51.1 | 14.98 | 1.73 | 3.21 | | 183 | 179 |
| " " ¾ | " " ¾ | 58.0 | 17.00 | 1.76 | 3.18 | | 208 | 203 |
| " " ⅞ | " " ⅞ | 64.9 | 18.98 | 1.79 | 3.16 | | 233 | 227 |
| " " 1 | " " 1 | 71.4 | 20.92 | 1.82 | 3.14 | | 257 | 251 |
| " " 1 ⅛ | " " 1 ⅛ | 77.9 | 22.86 | 1.85 | 3.12 | | 281 | 274 |
| " " 1 ¼ | " " 1 ¼ | 84.4 | 24.76 | 1.89 | 3.10 | | 304 | 297 |
| " " 1 ½ | " " 1 ½ | 90.5 | 26.62 | 1.92 | 3.08 | | 327 | 320 |
| " " 1 ⅞ | " " 1 ⅞ | 97.0 | 28.44 | 1.95 | 3.06 | | 350 | 343 |
| 5 x 3½ x ⅜ | 10 x ⅜ | 45.4 | 13.37 | 2.08 | 4.10 | | 165 | 162 |
| " " ½ | " " ½ | 54.4 | 15.95 | 2.10 | 4.08 | | 196 | 193 |
| " " ⅝ | " " ⅝ | 62.9 | 18.50 | 2.13 | 4.06 | | 228 | 224 |
| " " ¾ | " " ¾ | 71.4 | 21.00 | 2.16 | 4.04 | | 259 | 255 |
| " " ⅞ | " " ⅞ | 79.9 | 23.51 | 2.19 | 4.02 | | 290 | 285 |
| " " 1 | " " 1 | 88.5 | 25.93 | 2.22 | 4.00 | | 320 | 315 |
| " " 1 ⅛ | " " 1 ⅛ | 96.6 | 28.36 | 2.25 | 3.98 | | 350 | 345 |
| " " 1 ¼ | " " 1 ¼ | 104.7 | 30.74 | 2.29 | 3.96 | | 380 | 374 |
| " " 1 ½ | " " 1 ½ | 112.8 | 33.13 | 2.32 | 3.93 | | 409 | 403 |
| " " 1 ⅞ | " " 1 ⅞ | 120.6 | 35.43 | 2.35 | 3.91 | | 438 | 432 |
| " " 2 | " " 2 | 128.7 | 37.74 | 2.38 | 3.89 | | 466 | 460 |
| 6 x 3½ x ⅜ | 12 x ⅜ | 62.1 | 18.18 | 2.56 | 5.01 | | 225 | 222 |
| " " ½ | " " ½ | 71.9 | 21.13 | 2.59 | 4.99 | | 261 | 258 |
| " " ⅝ | " " ⅝ | 81.6 | 24.00 | 2.62 | 4.97 | | 297 | 294 |
| " " ¾ | " " ¾ | 91.4 | 26.87 | 2.65 | 4.95 | | 333 | 329 |
| " " ⅞ | " " ⅞ | 101.1 | 29.70 | 2.68 | 4.93 | | 368 | 364 |
| " " 1 | " " 1 | 110.5 | 32.49 | 2.71 | 4.91 | | 402 | 398 |
| " " 1 ⅛ | " " 1 ⅛ | 120.2 | 35.24 | 2.74 | 4.88 | | 437 | 432 |
| " " 1 ¼ | " " 1 ¼ | 129.2 | 37.99 | 2.77 | 4.86 | | 471 | 466 |
| " " 1 ½ | " " 1 ½ | 138.5 | 40.70 | 2.80 | 4.84 | | 505 | 499 |
| " " 1 ⅞ | " " 1 ⅞ | 147.5 | 43.37 | 2.83 | 4.82 | | 538 | 532 |
| " " 2 | " " 2 | 156.4 | 46.00 | 2.86 | 4.80 | | 571 | 565 |

**SAFE LOADS IN THOUSANDS OF POUNDS FOR
PLATE AND ANGLE COLUMNS. SQUARE ENDS.
CALCULATED FOR LEAST RADIUS OF GYRATION,
AXIS 1-1.**

Based on Gordon's Formula, $P = \frac{50\,000}{1 + \frac{(12 L)^2}{36\,000 r^2}}$

Safety factor 4.



Length in Feet.

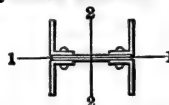
| 8 | 10 | 12 | 14 | 16 | 18 | 20 | 22 | 24 | 26 | 28 | 30 | 32 | 34 |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| 72 | 67 | 61 | 56 | 51 | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| 90 | 84 | 77 | 70 | 64 | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| 108 | 100 | 93 | 85 | 77 | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| 125 | 117 | 108 | 99 | 91 | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| 143 | 134 | 124 | 114 | 105 | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| 160 | 150 | 140 | 129 | 119 | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| 84 | 79 | 74 | 69 | 63 | 58 | 54 | ... | ... | ... | ... | ... | ... | ... |
| 104 | 99 | 92 | 86 | 80 | 73 | 68 | ... | ... | ... | ... | ... | ... | ... |
| 125 | 118 | 111 | 103 | 96 | 89 | 82 | ... | ... | ... | ... | ... | ... | ... |
| 145 | 137 | 129 | 121 | 112 | 104 | 96 | ... | ... | ... | ... | ... | ... | ... |
| 164 | 156 | 147 | 138 | 129 | 119 | 111 | ... | ... | ... | ... | ... | ... | ... |
| 184 | 175 | 166 | 155 | 145 | 135 | 125 | ... | ... | ... | ... | ... | ... | ... |
| 124 | 119 | 113 | 106 | 99 | 93 | 86 | 80 | 74 | ... | ... | ... | ... | ... |
| 149 | 142 | 135 | 127 | 119 | 112 | 104 | 97 | 90 | ... | ... | ... | ... | ... |
| 172 | 165 | 157 | 148 | 139 | 131 | 122 | 114 | 106 | ... | ... | ... | ... | ... |
| 196 | 188 | 179 | 170 | 160 | 150 | 140 | 131 | 122 | ... | ... | ... | ... | ... |
| 220 | 211 | 201 | 191 | 180 | 169 | 158 | 148 | 138 | ... | ... | ... | ... | ... |
| 243 | 234 | 223 | 212 | 200 | 188 | 177 | 165 | 155 | ... | ... | ... | ... | ... |
| 266 | 256 | 245 | 233 | 220 | 208 | 195 | 183 | 171 | ... | ... | ... | ... | ... |
| 289 | 278 | 266 | 254 | 240 | 227 | 213 | 200 | 188 | ... | ... | ... | ... | ... |
| 311 | 300 | 288 | 274 | 260 | 246 | 232 | 218 | 205 | ... | ... | ... | ... | ... |
| 333 | 322 | 309 | 295 | 280 | 265 | 250 | 236 | 222 | ... | ... | ... | ... | ... |
| 158 | 153 | 147 | 141 | 135 | 128 | 122 | 115 | 109 | 103 | 97 | ... | ... | ... |
| 188 | 183 | 176 | 169 | 162 | 154 | 146 | 139 | 131 | 124 | 117 | ... | ... | ... |
| 219 | 212 | 205 | 197 | 189 | 180 | 171 | 162 | 153 | 145 | 137 | ... | ... | ... |
| 249 | 242 | 234 | 225 | 215 | 206 | 196 | 186 | 176 | 166 | 157 | ... | ... | ... |
| 279 | 271 | 262 | 252 | 242 | 231 | 220 | 209 | 198 | 188 | 178 | ... | ... | ... |
| 308 | 300 | 290 | 280 | 269 | 257 | 245 | 233 | 221 | 210 | 198 | ... | ... | ... |
| 337 | 329 | 318 | 307 | 295 | 282 | 270 | 257 | 244 | 231 | 219 | ... | ... | ... |
| 366 | 357 | 346 | 334 | 321 | 308 | 294 | 280 | 267 | 253 | 240 | ... | ... | ... |
| 395 | 385 | 374 | 361 | 348 | 333 | 319 | 304 | 290 | 275 | 261 | ... | ... | ... |
| 423 | 413 | 401 | 388 | 374 | 359 | 343 | 328 | 313 | 297 | 283 | ... | ... | ... |
| 451 | 441 | 428 | 414 | 400 | 384 | 368 | 352 | 336 | 320 | 304 | ... | ... | ... |
| 210 | 214 | 209 | 203 | 197 | 190 | 183 | 176 | 168 | 161 | 154 | 147 | 140 | 133 |
| 254 | 249 | 243 | 236 | 229 | 221 | 213 | 205 | 196 | 188 | 180 | 172 | 164 | 156 |
| 289 | 283 | 277 | 269 | 261 | 252 | 243 | 234 | 225 | 215 | 206 | 197 | 188 | 179 |
| 324 | 318 | 310 | 302 | 293 | 283 | 273 | 263 | 253 | 242 | 232 | 222 | 212 | 202 |
| 358 | 352 | 344 | 335 | 325 | 314 | 303 | 292 | 281 | 269 | 258 | 247 | 236 | 226 |
| 392 | 385 | 376 | 367 | 356 | 345 | 333 | 321 | 309 | 297 | 284 | 272 | 261 | 249 |
| 426 | 418 | 409 | 399 | 388 | 376 | 363 | 350 | 337 | 324 | 311 | 298 | 285 | 273 |
| 459 | 451 | 442 | 431 | 419 | 406 | 393 | 379 | 365 | 351 | 337 | 323 | 310 | 296 |
| 493 | 484 | 474 | 462 | 450 | 437 | 423 | 408 | 393 | 378 | 363 | 349 | 334 | 320 |
| 525 | 516 | 506 | 494 | 481 | 467 | 452 | 437 | 421 | 405 | 390 | 374 | 359 | 344 |
| 558 | 548 | 537 | 525 | 511 | 497 | 481 | 465 | 449 | 432 | 416 | 400 | 384 | 368 |

**SAFE LOADS IN THOUSANDS OF POUNDS FOR
PLATE AND ANGLE COLUMNS. SQUARE ENDS.**

CALCULATED FOR LEAST RADIUS OF GYRATION, AXIS 1-1.

Based on Gordon's Formula, $P = \frac{50\,000}{1 + \frac{(12\,L)^2}{36\,000\,r^2}}$

Safety factor 4.



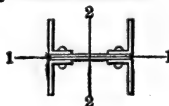
| Size of Angles. | Size of Plate. | Weight of Column. | Area of Column Section. | Least Radius of Gyration Axis 1-1. | Radius of Gyration Axis 2-2. | Length in Feet. | | |
|---------------------------|----------------|-------------------|-------------------------|------------------------------------|------------------------------|-----------------|-----|-----|
| Inches. | Inches. | Lbs. per Ft. | Sq. Ins. | Inches. | Inches. | 2 | 4 | 6 |
| 3 x 2½ x ¼ | 8 x ¼ | 24.8 | 7.24 | 1.19 | 3.25 | 90 | 87 | 82 |
| " " ⅜ | " " ⅜ | 30.9 | 8.98 | 1.22 | 3.23 | 111 | 108 | 102 |
| " " ½ | " " ½ | 36.6 | 10.68 | 1.25 | 3.21 | 132 | 128 | 122 |
| " " ⅝ | " " ⅝ | 42.3 | 12.38 | 1.28 | 3.19 | 153 | 149 | 142 |
| " " ¾ | " " ¾ | 47.6 | 14.00 | 1.31 | 3.17 | 173 | 169 | 161 |
| " " ⅞ | " " ⅞ | 53.3 | 15.62 | 1.34 | 3.15 | 193 | 188 | 181 |
| 3½ x 2½ x ¼ | 8 x ¼ | 26.4 | 7.76 | 1.44 | 3.31 | 96 | 94 | 91 |
| " " ⅜ | " " ⅜ | 32.9 | 9.62 | 1.47 | 3.28 | 119 | 117 | 113 |
| " " ½ | " " ½ | 39.0 | 11.44 | 1.50 | 3.26 | 142 | 139 | 134 |
| " " ⅝ | " " ⅝ | 45.1 | 13.22 | 1.53 | 3.24 | 164 | 161 | 156 |
| " " ¾ | " " ¾ | 51.2 | 15.00 | 1.56 | 3.22 | 186 | 183 | 177 |
| " " ⅞ | " " ⅞ | 56.9 | 16.74 | 1.59 | 3.20 | 208 | 204 | 198 |
| 4 x 3 x ⅜ | 10 x ⅜ | 39.4 | 11.49 | 1.62 | 4.09 | | 140 | 136 |
| " " ½ | " " ½ | 46.8 | 13.67 | 1.65 | 4.07 | | 167 | 163 |
| " " ⅝ | " " ⅝ | 54.1 | 15.86 | 1.68 | 4.04 | | 194 | 189 |
| " " ¾ | " " ¾ | 61.4 | 18.00 | 1.71 | 4.02 | | 220 | 214 |
| " " ⅞ | " " ⅞ | 68.7 | 20.11 | 1.74 | 4.00 | | 246 | 240 |
| " " 1 | " " 1 | 75.7 | 22.17 | 1.77 | 3.98 | | 272 | 265 |
| " " 1¼ | " " 1¼ | 82.6 | 24.24 | 1.80 | 3.96 | | 297 | 290 |
| " " 1½ | " " 1½ | 89.5 | 26.26 | 1.83 | 3.94 | | 322 | 315 |
| " " 1¾ | " " 1¾ | 96.0 | 28.25 | 1.86 | 3.92 | | 347 | 339 |
| " " 2 | " " 2 | 103.0 | 30.19 | 1.90 | 3.90 | | 371 | 363 |
| 5 x 3½ x ⅜ | 12 x ⅜ | 47.6 | 13.99 | 2.03 | 4.95 | | 172 | 169 |
| " " ½ | " " ½ | 56.9 | 16.70 | 2.06 | 4.92 | | 206 | 202 |
| " " ⅝ | " " ⅝ | 65.9 | 19.37 | 2.08 | 4.90 | | 238 | 234 |
| " " ¾ | " " ¾ | 74.8 | 22.00 | 2.11 | 4.88 | | 271 | 266 |
| " " ⅞ | " " ⅞ | 83.8 | 24.63 | 2.14 | 4.86 | | 303 | 298 |
| " " 1 | " " 1 | 92.7 | 27.18 | 2.17 | 4.84 | | 335 | 330 |
| " " 1¼ | " " 1¼ | 101.3 | 29.73 | 2.20 | 4.82 | | 367 | 361 |
| " " 1½ | " " 1½ | 109.8 | 32.24 | 2.23 | 4.80 | | 398 | 392 |
| " " 1¾ | " " 1¾ | 118.4 | 34.75 | 2.26 | 4.78 | | 429 | 422 |
| " " 2 | " " 2 | 126.5 | 37.18 | 2.29 | 4.76 | | 459 | 452 |
| " " 2¼ | " " 2¼ | 135.1 | 39.61 | 2.33 | 4.74 | | 489 | 482 |
| 6 x 3½ x ⅜ | 14 x ⅜ | 64.7 | 18.93 | 2.51 | 5.85 | | 234 | 231 |
| " " ½ | " " ½ | 74.8 | 22.01 | 2.54 | 5.83 | | 272 | 269 |
| " " ⅝ | " " ⅝ | 85.0 | 25.00 | 2.57 | 5.81 | | 309 | 306 |
| " " ¾ | " " ¾ | 95.2 | 28.00 | 2.59 | 5.79 | | 347 | 343 |
| " " ⅞ | " " ⅞ | 105.3 | 30.95 | 2.62 | 5.77 | | 383 | 379 |
| " " 1 | " " 1 | 115.1 | 33.87 | 2.65 | 5.74 | | 419 | 415 |
| " " 1¼ | " " 1¼ | 125.3 | 36.74 | 2.68 | 5.72 | | 455 | 450 |
| " " 1½ | " " 1½ | 134.7 | 39.62 | 2.71 | 5.70 | | 491 | 486 |
| " " 1¾ | " " 1¾ | 144.5 | 42.45 | 2.74 | 5.68 | | 526 | 521 |
| " " 2 | " " 2 | 153.8 | 45.25 | 2.77 | 5.66 | | 561 | 555 |
| " " 2¼ | " " 2¼ | 163.2 | 48.00 | 2.81 | 5.64 | | 595 | 589 |

SAFE LOADS IN THOUSANDS OF POUNDS FOR PLATE AND ANGLE COLUMNS. SQUARE ENDS.

CALCULATED FOR LEAST RADIUS OF GYRATION, AXIS 1-1.

Based on Gordon's Formula, $P = \frac{50\,000}{1 + \frac{(12\,L)^2}{36\,000\,r^2}}$

Safety factor 4.



Length in Feet.

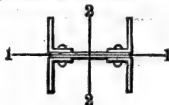
| 8 | 10 | 12 | 14 | 16 | 18 | 20 | 22 | 24 | 26 | 28 | 30 | 32 | 34 |
|-----|-----|-----|-----|-----|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 77 | 71 | 65 | 58 | 53 | | | | | | | | | |
| 96 | 89 | 81 | 74 | 67 | | | | | | | | | |
| 115 | 106 | 98 | 89 | 81 | | | | | | | | | |
| 134 | 124 | 114 | 105 | 95 | | | | | | | | | |
| 152 | 142 | 131 | 120 | 110 | | | | | | | | | |
| 171 | 160 | 148 | 136 | 124 | | | | | | | | | |
| 86 | 81 | 76 | 70 | 65 | 60 | 55 | | | | | | | |
| 107 | 101 | 95 | 88 | 81 | 75 | 69 | | | | | | | |
| 128 | 121 | 114 | 106 | 98 | 91 | 83 | | | | | | | |
| 149 | 141 | 133 | 124 | 115 | 106 | 98 | | | | | | | |
| 170 | 161 | 151 | 142 | 132 | 122 | 113 | | | | | | | |
| 190 | 180 | 170 | 159 | 149 | 138 | 128 | | | | | | | |
| 131 | 125 | 118 | 111 | 103 | 96 | 89 | 83 | 77 | | | | | |
| 156 | 149 | 141 | 133 | 124 | 116 | 108 | 100 | 93 | | | | | |
| 182 | 174 | 165 | 155 | 145 | 136 | 127 | 118 | 109 | | | | | |
| 207 | 198 | 188 | 177 | 167 | 156 | 145 | 135 | 126 | | | | | |
| 232 | 222 | 211 | 200 | 188 | 176 | 164 | 153 | 143 | | | | | |
| 256 | 246 | 234 | 222 | 209 | 196 | 184 | 171 | 160 | | | | | |
| 281 | 270 | 257 | 244 | 230 | 216 | 203 | 190 | 177 | | | | | |
| 305 | 293 | 280 | 266 | 251 | 237 | 222 | 208 | 195 | | | | | |
| 329 | 317 | 303 | 288 | 273 | 257 | 242 | 227 | 212 | | | | | |
| 352 | 340 | 325 | 310 | 294 | 277 | 261 | 245 | 230 | | | | | |
| 165 | 159 | 153 | 147 | 140 | 133 | 126 | 119 | 112 | 105 | 99 | | | |
| 197 | 191 | 184 | 176 | 168 | 160 | 151 | 143 | 135 | 127 | 120 | | | |
| 229 | 222 | 214 | 205 | 196 | 186 | 177 | 167 | 158 | 149 | 141 | | | |
| 260 | 252 | 244 | 234 | 224 | 213 | 202 | 192 | 181 | 171 | 162 | | | |
| 291 | 283 | 273 | 263 | 251 | 240 | 228 | 216 | 205 | 194 | 183 | | | |
| 322 | 313 | 303 | 291 | 279 | 267 | 254 | 241 | 228 | 216 | 204 | | | |
| 353 | 343 | 332 | 320 | 307 | 293 | 279 | 266 | 252 | 239 | 226 | | | |
| 383 | 373 | 361 | 348 | 334 | 320 | 305 | 290 | 276 | 261 | 247 | | | |
| 413 | 403 | 390 | 376 | 362 | 346 | 331 | 315 | 299 | 284 | 269 | | | |
| 443 | 432 | 419 | 405 | 389 | 373 | 357 | 340 | 323 | 307 | 291 | | | |
| 473 | 461 | 447 | 432 | 416 | 399 | 382 | 365 | 347 | 330 | 313 | | | |
| 228 | 223 | 217 | 211 | 204 | 196 | 189 | 181 | 173 | 166 | 158 | 151 | 143 | 136 |
| 264 | 259 | 252 | 245 | 237 | 229 | 220 | 211 | 202 | 194 | 185 | 176 | 168 | 160 |
| 301 | 295 | 287 | 279 | 270 | 261 | 251 | 241 | 231 | 221 | 212 | 202 | 193 | 184 |
| 337 | 330 | 322 | 313 | 304 | 293 | 283 | 272 | 261 | 250 | 239 | 228 | 217 | 207 |
| 373 | 366 | 357 | 347 | 337 | 325 | 314 | 302 | 290 | 278 | 266 | 254 | 242 | 231 |
| 408 | 400 | 391 | 381 | 369 | 357 | 345 | 332 | 319 | 306 | 293 | 280 | 268 | 255 |
| 444 | 435 | 425 | 414 | 402 | 389 | 376 | 362 | 348 | 334 | 320 | 306 | 293 | 280 |
| 478 | 470 | 459 | 447 | 435 | 421 | 407 | 392 | 377 | 362 | 347 | 333 | 318 | 304 |
| 513 | 504 | 493 | 480 | 467 | 453 | 438 | 422 | 406 | 390 | 375 | 359 | 344 | 329 |
| 547 | 538 | 526 | 513 | 499 | 484 | 468 | 452 | 435 | 419 | 402 | 385 | 369 | 353 |
| 581 | 571 | 559 | 546 | 531 | 515 | 499 | 482 | 464 | 447 | 429 | 412 | 395 | 378 |

**SAFE LOADS IN THOUSANDS OF POUNDS FOR
PLATE AND ANGLE COLUMNS. SQUARE ENDS.**

CALCULATED FOR LEAST RADIUS OF GYRATION, AXIS 1-1.

Based on Gordon's Formula, $P = \frac{50\,000}{1 + \frac{(12\,L)^2}{36\,000\,r^2}}$

Safety factor 4.



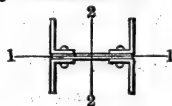
| Size of Angles. | Size of Plate. | Weight of Column. | Area of Column Section. | Least Radius of Gyration Axis 1-1. | Radius of Gyration Axis 2-2. | Length in Feet. | | |
|---------------------------|----------------|-------------------|-------------------------|------------------------------------|------------------------------|-----------------|-----|-----|
| Inches. | Inches. | Lbs. per Ft. | Sq. Ins. | Inches. | Inches. | 2 | 4 | 6 |
| 3 x 2½ x ¼ | 10 x ¼ | 26.5 | 7.74 | 1.16 | 4.07 | 06 | 02 | 87 |
| " " ⅜ | " " ⅜ | 33.0 | 9.61 | 1.18 | 4.05 | 119 | 115 | 109 |
| " " ⅝ | " " ⅝ | 39.2 | 11.43 | 1.21 | 4.03 | 141 | 137 | 130 |
| " " ⅞ | " " ⅞ | 45.3 | 13.26 | 1.24 | 4.01 | 164 | 159 | 151 |
| " " 1½ | " " 1½ | 51.0 | 15.00 | 1.27 | 3.99 | 186 | 180 | 172 |
| " " 1⅞ | " " 1⅞ | 57.1 | 16.75 | 1.30 | 3.96 | 207 | 202 | 193 |
| 3½ x 2½ x ¼ | 10 x ¼ | 28.1 | 8.28 | 1.39 | 4.13 | 102 | 100 | 96 |
| " " ⅜ | " " ⅜ | 35.0 | 10.25 | 1.42 | 4.11 | 127 | 124 | 119 |
| " " ⅝ | " " ⅝ | 41.6 | 12.19 | 1.45 | 4.09 | 151 | 148 | 143 |
| " " ⅞ | " " ⅞ | 48.1 | 14.10 | 1.48 | 4.07 | 175 | 171 | 165 |
| " " 1½ | " " 1½ | 54.6 | 16.00 | 1.51 | 4.05 | 199 | 195 | 188 |
| " " 1⅞ | " " 1⅞ | 60.7 | 17.87 | 1.54 | 4.03 | 222 | 217 | 210 |
| 4 x 3 x ⅜ | 12 x ⅜ | 41.6 | 12.11 | 1.58 | 4.91 | | 148 | 143 |
| " " ⅝ | " " ⅝ | 49.3 | 14.42 | 1.61 | 4.89 | | 176 | 171 |
| " " ⅞ | " " ⅞ | 57.1 | 16.73 | 1.64 | 4.87 | | 204 | 198 |
| " " 1½ | " " 1½ | 64.8 | 19.00 | 1.66 | 4.85 | | 232 | 226 |
| " " 1⅞ | " " 1⅞ | 72.6 | 21.23 | 1.69 | 4.83 | | 260 | 253 |
| " " 2 | " " 2 | 79.9 | 23.42 | 1.72 | 4.81 | | 287 | 279 |
| " " 2½ | " " 2½ | 87.3 | 25.61 | 1.75 | 4.79 | | 314 | 306 |
| " " 3 | " " 3 | 94.6 | 27.76 | 1.78 | 4.77 | | 340 | 332 |
| " " 3½ | " " 3½ | 101.6 | 29.87 | 1.81 | 4.74 | | 366 | 358 |
| " " 4 | " " 4 | 108.9 | 31.94 | 1.84 | 4.72 | | 392 | 383 |
| 5 x 3½ x ⅜ | 14 x ⅜ | 49.7 | 14.62 | 1.98 | 5.77 | | 180 | 176 |
| " " ⅝ | " " ⅝ | 59.5 | 17.45 | 2.01 | 5.75 | | 215 | 211 |
| " " ⅞ | " " ⅞ | 68.8 | 20.25 | 2.04 | 5.73 | | 249 | 245 |
| " " 1½ | " " 1½ | 78.2 | 23.00 | 2.07 | 5.71 | | 283 | 278 |
| " " 1⅞ | " " 1⅞ | 87.6 | 25.76 | 2.09 | 5.69 | | 317 | 312 |
| " " 2 | " " 2 | 96.9 | 28.43 | 2.12 | 5.67 | | 351 | 345 |
| " " 2½ | " " 2½ | 105.9 | 31.11 | 2.15 | 5.64 | | 381 | 377 |
| " " 3 | " " 3 | 114.9 | 33.74 | 2.18 | 5.62 | | 416 | 410 |
| " " 3½ | " " 3½ | 123.9 | 36.38 | 2.21 | 5.60 | | 449 | 442 |
| " " 4 | " " 4 | 132.5 | 38.93 | 2.24 | 5.58 | | 481 | 473 |
| " " 4½ | " " 4½ | 141.4 | 41.49 | 2.27 | 5.56 | | 512 | 505 |
| 6 x 3½ x ⅜ | 16 x ⅜ | 67.2 | 19.68 | 2.46 | 6.68 | | 244 | 240 |
| " " ⅝ | " " ⅝ | 77.8 | 22.88 | 2.49 | 6.66 | | 283 | 279 |
| " " 1½ | " " 1½ | 88.4 | 26.00 | 2.52 | 6.64 | | 322 | 318 |
| " " 1⅞ | " " 1⅞ | 99.0 | 29.12 | 2.54 | 6.61 | | 360 | 356 |
| " " 2 | " " 2 | 109.6 | 32.20 | 2.57 | 6.59 | | 399 | 394 |
| " " 2½ | " " 2½ | 119.8 | 35.24 | 2.60 | 6.57 | | 436 | 431 |
| " " 3 | " " 3 | 130.4 | 38.24 | 2.63 | 6.55 | | 474 | 468 |
| " " 3½ | " " 3½ | 140.2 | 41.24 | 2.66 | 6.53 | | 511 | 505 |
| " " 4 | " " 4 | 150.4 | 44.20 | 2.69 | 6.51 | | 548 | 542 |
| " " 4½ | " " 4½ | 160.2 | 47.12 | 2.72 | 6.48 | | 584 | 578 |
| " " 5 | " " 5 | 170.0 | 50.00 | 2.75 | 6.46 | | 620 | 613 |

SAFE LOADS IN THOUSANDS OF POUNDS FOR PLATE AND ANGLE COLUMNS. SQUARE ENDS.

CALCULATED FOR LEAST RADIUS OF GYRATION, AXIS 1-1.

Based on Gordon's Formula, $P = \frac{50\,000}{1 + \frac{(12\,L)^2}{36\,000\,r^2}}$

Safety factor 4.



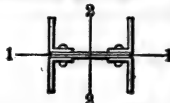
Length in Feet.

| 8 | 10 | 12 | 14 | 16 | 18 | 20 | 22 | 24 | 26 | 28 | 30 | 32 | 34 |
|-----|-----|-----|-----|-----|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 81 | 75 | 68 | 61 | 55 | | | | | | | | | |
| 102 | 93 | 85 | 77 | 69 | | | | | | | | | |
| 122 | 112 | 103 | 93 | 84 | | | | | | | | | |
| 142 | 131 | 120 | 109 | 99 | | | | | | | | | |
| 162 | 150 | 138 | 126 | 114 | | | | | | | | | |
| 182 | 169 | 156 | 143 | 130 | | | | | | | | | |
| 91 | 86 | 80 | 73 | 68 | 62 | 57 | | | | | | | |
| 114 | 107 | 100 | 92 | 85 | 78 | 71 | | | | | | | |
| 136 | 128 | 120 | 111 | 102 | 94 | 86 | | | | | | | |
| 158 | 149 | 140 | 130 | 120 | 111 | 102 | | | | | | | |
| 180 | 170 | 160 | 149 | 138 | 127 | 117 | | | | | | | |
| 201 | 191 | 179 | 168 | 156 | 144 | 133 | | | | | | | |
| 137 | 131 | 123 | 115 | 107 | 100 | 92 | 85 | 79 | | | | | |
| 164 | 156 | 148 | 139 | 129 | 120 | 112 | 103 | 95 | | | | | |
| 191 | 182 | 172 | 162 | 151 | 141 | 131 | 121 | 112 | | | | | |
| 217 | 208 | 197 | 185 | 173 | 162 | 151 | 140 | 130 | | | | | |
| 244 | 233 | 221 | 208 | 196 | 183 | 170 | 158 | 147 | | | | | |
| 270 | 258 | 245 | 232 | 218 | 204 | 190 | 177 | 165 | | | | | |
| 296 | 283 | 270 | 255 | 240 | 225 | 210 | 196 | 183 | | | | | |
| 321 | 308 | 294 | 278 | 262 | 246 | 231 | 216 | 201 | | | | | |
| 346 | 333 | 318 | 301 | 285 | 268 | 251 | 235 | 220 | | | | | |
| 371 | 357 | 341 | 324 | 307 | 289 | 272 | 254 | 238 | | | | | |
| 171 | 166 | 159 | 152 | 145 | 137 | 130 | 122 | 115 | 108 | 102 | | | |
| 205 | 198 | 191 | 183 | 174 | 165 | 156 | 147 | 139 | 131 | 123 | | | |
| 238 | 231 | 222 | 213 | 203 | 193 | 183 | 173 | 163 | 153 | 144 | | | |
| 271 | 263 | 253 | 243 | 232 | 221 | 209 | 198 | 187 | 176 | 166 | | | |
| 304 | 295 | 284 | 273 | 261 | 248 | 236 | 223 | 211 | 199 | 188 | | | |
| 336 | 327 | 315 | 303 | 290 | 276 | 262 | 249 | 235 | 222 | 210 | | | |
| 369 | 358 | 346 | 333 | 319 | 304 | 289 | 274 | 260 | 246 | 232 | | | |
| 400 | 389 | 376 | 362 | 347 | 332 | 316 | 300 | 284 | 269 | 254 | | | |
| 432 | 420 | 407 | 392 | 376 | 359 | 343 | 326 | 309 | 293 | 277 | | | |
| 463 | 451 | 437 | 421 | 404 | 387 | 369 | 351 | 334 | 317 | 300 | | | |
| 494 | 481 | 467 | 450 | 433 | 415 | 396 | 377 | 359 | 340 | 323 | | | |
| 236 | 231 | 225 | 218 | 211 | 203 | 195 | 187 | 178 | 170 | 162 | 154 | 147 | 140 |
| 274 | 268 | 261 | 254 | 245 | 236 | 227 | 218 | 208 | 199 | 190 | 181 | 172 | 164 |
| 312 | 306 | 298 | 289 | 280 | 270 | 259 | 249 | 238 | 228 | 217 | 207 | 197 | 188 |
| 350 | 343 | 334 | 325 | 314 | 303 | 292 | 280 | 268 | 257 | 245 | 234 | 223 | 212 |
| 387 | 370 | 370 | 360 | 348 | 336 | 324 | 311 | 308 | 286 | 273 | 261 | 249 | 237 |
| 424 | 416 | 406 | 395 | 382 | 370 | 356 | 342 | 329 | 315 | 301 | 287 | 274 | 262 |
| 461 | 452 | 441 | 429 | 416 | 403 | 388 | 374 | 359 | 344 | 329 | 314 | 300 | 287 |
| 497 | 488 | 477 | 464 | 450 | 436 | 420 | 405 | 389 | 373 | 357 | 342 | 326 | 312 |
| 533 | 523 | 512 | 498 | 484 | 468 | 452 | 436 | 419 | 402 | 385 | 369 | 353 | 337 |
| 569 | 559 | 546 | 532 | 517 | 501 | 484 | 467 | 449 | 431 | 414 | 396 | 379 | 362 |
| 605 | 594 | 581 | 566 | 550 | 534 | 516 | 498 | 479 | 460 | 442 | 423 | 405 | 388 |

**SAFE LOADS IN THOUSANDS OF POUNDS FOR
PLATE AND ANGLE COLUMNS. SQUARE ENDS.
CALCULATED FOR LEAST RADIUS OF GYRATION,
AXIS 1-1.**

Based on Gordon's Formula, $P = \frac{50\,000}{1 + \frac{(12\,L)^2}{36\,000\,r^2}}$

Safety factor 4.



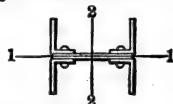
| Size of Angles. | Size of Plate. | Weight of Column. | Area of Column Section. | Least Radius of Gyration Axis 1-1. | Radius of Gyration Axis 2-2. | Length in Feet. | | |
|---------------------------|----------------|-------------------|-------------------------|------------------------------------|------------------------------|-----------------|-----|-----|
| Inches. | Inches. | Lbs. per Ft. | Sq. Ins. | Inches. | Inches. | 2 | 4 | 6 |
| 3 x 2½ x ¼ | 12 x ¼ | 28.2 | 8.24 | 1.12 | 4.87 | 102 | 98 | 92 |
| " " x ⅜ | " " x ⅜ | 35.2 | 10.23 | 1.15 | 4.85 | 126 | 122 | 115 |
| " " x ½ | " " x ½ | 41.7 | 12.18 | 1.17 | 4.83 | 151 | 146 | 138 |
| " " x ⅝ | " " x ⅝ | 48.3 | 14.13 | 1.20 | 4.81 | 174 | 169 | 160 |
| " " x ¾ | " " x ¾ | 54.4 | 16.00 | 1.23 | 4.78 | 198 | 192 | 183 |
| " " x ⅞ | " " x ⅞ | 61.0 | 17.87 | 1.26 | 4.76 | 221 | 215 | 205 |
| 3½ x 2½ x ¼ | 12 x ¼ | 29.8 | 8.76 | 1.35 | 4.94 | 108 | 106 | 101 |
| " " x ⅜ | " " x ⅜ | 37.2 | 10.87 | 1.38 | 4.92 | 135 | 131 | 126 |
| " " x ½ | " " x ½ | 44.1 | 12.94 | 1.41 | 4.90 | 160 | 157 | 151 |
| " " x ⅝ | " " x ⅝ | 51.1 | 14.97 | 1.43 | 4.88 | 186 | 182 | 175 |
| " " x ¾ | " " x ¾ | 58.0 | 17.00 | 1.46 | 4.85 | 211 | 206 | 199 |
| " " x ⅞ | " " x ⅞ | 64.6 | 18.99 | 1.49 | 4.83 | 236 | 231 | 223 |
| 4 x 3 x ⅜ | 14 x ⅜ | 43.7 | 12.74 | 1.54 | 5.72 | | 155 | 150 |
| " " x ½ | " " x ½ | 51.9 | 15.17 | 1.57 | 5.70 | | 185 | 179 |
| " " x ⅝ | " " x ⅝ | 60.0 | 17.61 | 1.60 | 5.68 | | 215 | 208 |
| " " x ¾ | " " x ¾ | 68.2 | 20.00 | 1.62 | 5.66 | | 244 | 237 |
| " " x ⅞ | " " x ⅞ | 76.4 | 22.36 | 1.65 | 5.63 | | 273 | 265 |
| " " x 1 | " " x 1 | 84.1 | 24.67 | 1.68 | 5.61 | | 302 | 294 |
| " " x 1¼ | " " x 1¼ | 91.9 | 26.99 | 1.71 | 5.59 | | 330 | 322 |
| " " x 1½ | " " x 1½ | 99.7 | 29.26 | 1.74 | 5.57 | | 358 | 349 |
| " " x 1¾ | " " x 1¾ | 107.1 | 31.50 | 1.77 | 5.55 | | 386 | 376 |
| " " x 1⅞ | " " x 1⅞ | 114.9 | 33.69 | 1.80 | 5.53 | | 413 | 403 |
| 5 x 3½ x ⅜ | 16 x ⅜ | 51.8 | 15.24 | 1.94 | 6.59 | | 187 | 183 |
| " " x ½ | " " x ½ | 62.0 | 18.20 | 1.97 | 6.57 | | 224 | 219 |
| " " x ⅝ | " " x ⅝ | 71.8 | 21.12 | 2.00 | 6.54 | | 260 | 255 |
| " " x ¾ | " " x ¾ | 81.6 | 24.00 | 2.02 | 6.52 | | 295 | 290 |
| " " x ⅞ | " " x ⅞ | 91.4 | 26.88 | 2.05 | 6.50 | | 331 | 325 |
| " " x 1 | " " x 1 | 101.2 | 29.68 | 2.08 | 6.48 | | 366 | 359 |
| " " x 1¼ | " " x 1¼ | 110.6 | 32.48 | 2.11 | 6.46 | | 400 | 393 |
| " " x 1½ | " " x 1½ | 120.0 | 35.24 | 2.14 | 6.44 | | 435 | 427 |
| " " x 1¾ | " " x 1¾ | 129.4 | 38.00 | 2.17 | 6.41 | | 468 | 461 |
| " " x 1⅞ | " " x 1⅞ | 138.4 | 40.68 | 2.19 | 6.39 | | 502 | 494 |
| " " x 2 | " " x 2 | 147.8 | 43.36 | 2.22 | 6.37 | | 535 | 527 |
| 6 x 3½ x ⅜ | 18 x ⅜ | 69.8 | 20.43 | 2.42 | 7.49 | | 253 | 249 |
| " " x ½ | " " x ½ | 80.8 | 23.76 | 2.44 | 7.47 | | 294 | 290 |
| " " x ⅝ | " " x ⅝ | 91.8 | 27.00 | 2.47 | 7.45 | | 334 | 330 |
| " " x ¾ | " " x ¾ | 102.8 | 30.25 | 2.50 | 7.42 | | 374 | 369 |
| " " x ⅞ | " " x ⅞ | 113.9 | 33.45 | 2.52 | 7.40 | | 414 | 409 |
| " " x 1 | " " x 1 | 124.5 | 36.62 | 2.55 | 7.38 | | 453 | 448 |
| " " x 1¼ | " " x 1¼ | 135.5 | 39.74 | 2.58 | 7.36 | | 492 | 486 |
| " " x 1½ | " " x 1½ | 145.7 | 42.87 | 2.61 | 7.34 | | 531 | 525 |
| " " x 1¾ | " " x 1¾ | 156.4 | 45.95 | 2.64 | 7.32 | | 569 | 563 |
| " " x 1⅞ | " " x 1⅞ | 166.6 | 49.00 | 2.67 | 7.29 | | 607 | 600 |
| " " x 2 | " " x 2 | 176.8 | 52.00 | 2.70 | 7.27 | | 644 | 637 |

SAFE LOADS IN THOUSANDS OF POUNDS FOR PLATE AND ANGLE COLUMNS. SQUARE ENDS.

CALCULATED FOR LEAST RADIUS OF GYRATION, AXIS 1-1.

Based on Gordon's Formula, $P = \frac{50\,000}{1 + \frac{(12\,L)^2}{36\,000\,r^2}}$

Safety factor 4.



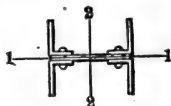
Length in Feet.

| 8 | 10 | 12 | 14 | 16 | 18 | 20 | 22 | 24 | 26 | 28 | 30 | 32 | 34 |
|-----|-----|-----|-----|-----|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 86 | 78 | 71 | 63 | 57 | | | | | | | | | |
| 107 | 98 | 89 | 80 | 72 | | | | | | | | | |
| 128 | 118 | 107 | 97 | 87 | | | | | | | | | |
| 150 | 138 | 126 | 114 | 103 | | | | | | | | | |
| 171 | 158 | 146 | 131 | 119 | | | | | | | | | |
| 192 | 178 | 164 | 149 | 135 | | | | | | | | | |
| 96 | 90 | 83 | 77 | 70 | 64 | 58 | | | | | | | |
| 120 | 112 | 104 | 96 | 88 | 81 | 74 | | | | | | | |
| 143 | 135 | 125 | 116 | 107 | 98 | 89 | | | | | | | |
| 167 | 157 | 146 | 136 | 125 | 115 | 105 | | | | | | | |
| 190 | 179 | 167 | 156 | 144 | 132 | 122 | | | | | | | |
| 213 | 201 | 188 | 175 | 162 | 150 | 138 | | | | | | | |
| 144 | 136 | 128 | 120 | 111 | 103 | 95 | 88 | 81 | | | | | |
| 172 | 163 | 154 | 144 | 134 | 124 | 115 | 106 | 98 | | | | | |
| 200 | 190 | 180 | 168 | 157 | 146 | 135 | 125 | 116 | | | | | |
| 228 | 217 | 205 | 193 | 180 | 168 | 156 | 144 | 133 | | | | | |
| 255 | 244 | 231 | 217 | 203 | 189 | 176 | 163 | 151 | | | | | |
| 283 | 270 | 256 | 241 | 226 | 211 | 197 | 183 | 170 | | | | | |
| 310 | 297 | 282 | 266 | 250 | 234 | 218 | 203 | 188 | | | | | |
| 337 | 323 | 307 | 290 | 273 | 256 | 239 | 223 | 207 | | | | | |
| 364 | 349 | 332 | 315 | 296 | 278 | 260 | 243 | 226 | | | | | |
| 390 | 375 | 357 | 339 | 320 | 301 | 282 | 263 | 246 | | | | | |
| 178 | 172 | 165 | 158 | 150 | 142 | 134 | 126 | 118 | 111 | 104 | | | |
| 213 | 206 | 198 | 189 | 180 | 170 | 161 | 152 | 143 | 134 | 126 | | | |
| 248 | 240 | 231 | 220 | 210 | 199 | 188 | 178 | 167 | 157 | 148 | | | |
| 282 | 273 | 263 | 252 | 240 | 228 | 216 | 204 | 192 | 181 | 170 | | | |
| 316 | 307 | 295 | 283 | 270 | 257 | 243 | 230 | 217 | 204 | 192 | | | |
| 350 | 340 | 327 | 314 | 300 | 286 | 271 | 256 | 242 | 228 | 215 | | | |
| 384 | 372 | 359 | 345 | 330 | 314 | 298 | 283 | 267 | 252 | 238 | | | |
| 417 | 405 | 391 | 376 | 360 | 343 | 326 | 309 | 293 | 277 | 261 | | | |
| 450 | 437 | 423 | 407 | 390 | 372 | 354 | 336 | 318 | 301 | 284 | | | |
| 483 | 470 | 454 | 437 | 419 | 401 | 382 | 363 | 344 | 326 | 308 | | | |
| 515 | 501 | 485 | 468 | 449 | 430 | 410 | 390 | 370 | 350 | 332 | | | |
| 245 | 239 | 233 | 225 | 217 | 209 | 201 | 192 | 183 | 175 | 166 | 158 | 150 | 143 |
| 285 | 278 | 271 | 262 | 253 | 244 | 234 | 224 | 214 | 204 | 194 | 185 | 176 | 167 |
| 324 | 317 | 308 | 299 | 289 | 278 | 267 | 256 | 245 | 234 | 223 | 212 | 202 | 192 |
| 363 | 355 | 346 | 336 | 325 | 313 | 301 | 288 | 276 | 264 | 251 | 240 | 228 | 217 |
| 402 | 393 | 383 | 372 | 360 | 347 | 334 | 321 | 307 | 293 | 280 | 267 | 254 | 242 |
| 440 | 431 | 420 | 408 | 395 | 382 | 367 | 353 | 338 | 323 | 309 | 295 | 281 | 268 |
| 478 | 469 | 457 | 445 | 431 | 416 | 401 | 385 | 369 | 353 | 338 | 323 | 308 | 293 |
| 516 | 506 | 494 | 480 | 466 | 450 | 434 | 417 | 400 | 383 | 367 | 350 | 334 | 319 |
| 554 | 543 | 530 | 516 | 501 | 484 | 467 | 449 | 431 | 414 | 396 | 378 | 362 | 345 |
| 591 | 580 | 567 | 552 | 535 | 518 | 500 | 481 | 463 | 444 | 425 | 407 | 389 | 371 |
| 628 | 616 | 602 | 587 | 570 | 552 | 533 | 513 | 494 | 474 | 454 | 435 | 416 | 397 |

SAFE LOADS IN THOUSANDS OF POUNDS FOR PLATE AND ANGLE COLUMNS. SQUARE ENDS.

CALCULATED FOR LEAST RADIUS OF GYRATION, AXIS 1-1.

Based on Gordon's Formula, $P = \frac{50\,000}{1 + \frac{(12 L)^2}{36\,000 r^2}}$.
Safety factor 4.



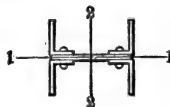
| Size of Angles. | Size of Plate. | Weight of Column. | Area of Column Section. | Least Radius of Gyration Axis 1-1. | Radius of Gyration Axis 2-2. | Length in Feet. | | |
|-----------------|----------------|-------------------|-------------------------|------------------------------------|------------------------------|-----------------|-----|-----|
| Inches. | Inches. | Lbs. per Ft. | Sq. Ins. | Inches. | Inches. | 6 | 8 | 10 |
| 7 x 3½ x ½ | 14 x ½ | 80.8 | 23.73 | 3.05 | 5.92 | 292 | 289 | 285 |
| " " ½ | " " ½ | 91.8 | 27.00 | 3.08 | 5.90 | 332 | 329 | 324 |
| " " ¾ | " " ¾ | 103.2 | 30.24 | 3.11 | 5.87 | 372 | 368 | 363 |
| " " 1 | " " 1 | 113.7 | 33.43 | 3.13 | 5.85 | 412 | 407 | 402 |
| " " 1 ¼ | " " 1 ¼ | 124.7 | 36.63 | 3.17 | 5.83 | 451 | 446 | 440 |
| " " 1 ½ | " " 1 ½ | 135.3 | 39.74 | 3.20 | 5.81 | 490 | 485 | 478 |
| " " 1 ¾ | " " 1 ¾ | 145.9 | 42.86 | 3.23 | 5.79 | 528 | 523 | 516 |
| " " 2 | " " 2 | 156.5 | 45.93 | 3.26 | 5.76 | 567 | 561 | 553 |
| " " 2 ¼ | " " 2 ¼ | 166.6 | 49.01 | 3.29 | 5.74 | 604 | 598 | 591 |
| " " 2 ½ | " " 2 ½ | 176.8 | 52.00 | 3.32 | 5.72 | 642 | 635 | 627 |
| 7 x 3½ x ½ | 16 x ½ | 83.8 | 24.60 | 3.00 | 6.75 | 303 | 299 | 294 |
| " " ½ | " " ½ | 95.2 | 28.00 | 3.02 | 6.73 | 345 | 340 | 335 |
| " " ¾ | " " ¾ | 107.0 | 31.36 | 3.06 | 6.71 | 386 | 382 | 376 |
| " " 1 | " " 1 | 118.0 | 34.68 | 3.08 | 6.69 | 427 | 422 | 416 |
| " " 1 ¼ | " " 1 ¼ | 129.4 | 38.00 | 3.11 | 6.67 | 468 | 463 | 456 |
| " " 1 ½ | " " 1 ½ | 140.4 | 41.24 | 3.14 | 6.64 | 508 | 503 | 496 |
| " " 1 ¾ | " " 1 ¾ | 151.4 | 44.48 | 3.17 | 6.62 | 548 | 542 | 535 |
| " " 2 | " " 2 | 162.4 | 47.68 | 3.20 | 6.60 | 588 | 582 | 574 |
| " " 2 ¼ | " " 2 ¼ | 173.0 | 50.88 | 3.23 | 6.58 | 627 | 621 | 612 |
| " " 2 ½ | " " 2 ½ | 183.6 | 54.00 | 3.26 | 6.56 | 666 | 659 | 651 |
| 7 x 3½ x ½ | 18 x ½ | 86.8 | 25.48 | 2.94 | 7.58 | 313 | 309 | 305 |
| " " ½ | " " ½ | 98.6 | 29.00 | 2.97 | 7.55 | 357 | 352 | 347 |
| " " ¾ | " " ¾ | 110.8 | 32.49 | 3.00 | 7.53 | 400 | 395 | 389 |
| " " 1 | " " 1 | 122.3 | 35.93 | 3.02 | 7.51 | 442 | 437 | 430 |
| " " 1 ¼ | " " 1 ¼ | 134.1 | 39.38 | 3.06 | 7.49 | 485 | 479 | 472 |
| " " 1 ½ | " " 1 ½ | 145.5 | 42.74 | 3.08 | 7.47 | 526 | 520 | 513 |
| " " 1 ¾ | " " 1 ¾ | 156.9 | 46.11 | 3.11 | 7.44 | 568 | 562 | 554 |
| " " 2 | " " 2 | 168.4 | 49.43 | 3.14 | 7.42 | 609 | 602 | 594 |
| " " 2 ¼ | " " 2 ¼ | 179.4 | 52.76 | 3.17 | 7.40 | 650 | 643 | 634 |
| " " 2 ½ | " " 2 ½ | 190.4 | 56.00 | 3.20 | 7.38 | 690 | 683 | 674 |
| 7 x 3½ x ½ | 20 x ½ | 89.8 | 26.35 | 2.89 | 8.39 | 324 | 320 | 314 |
| " " ½ | " " ½ | 102.0 | 30.00 | 2.92 | 8.37 | 369 | 364 | 358 |
| " " ¾ | " " ¾ | 114.7 | 33.61 | 2.95 | 8.34 | 413 | 408 | 402 |
| " " 1 | " " 1 | 126.5 | 37.18 | 2.97 | 8.32 | 457 | 452 | 445 |
| " " 1 ¼ | " " 1 ¼ | 138.7 | 40.75 | 3.00 | 8.30 | 501 | 495 | 488 |
| " " 1 ½ | " " 1 ½ | 150.6 | 44.24 | 3.03 | 8.28 | 545 | 538 | 530 |
| " " 1 ¾ | " " 1 ¾ | 162.5 | 47.73 | 3.06 | 8.25 | 588 | 581 | 572 |
| " " 2 | " " 2 | 174.3 | 51.18 | 3.09 | 8.23 | 630 | 623 | 614 |
| " " 2 ¼ | " " 2 ¼ | 185.8 | 54.63 | 3.12 | 8.21 | 673 | 665 | 656 |
| " " 2 ½ | " " 2 ½ | 197.2 | 58.00 | 3.15 | 8.19 | 715 | 707 | 697 |

SAFE LOADS IN THOUSANDS OF POUNDS FOR PLATE AND ANGLE COLUMNS. SQUARE ENDS.

CALCULATED FOR LEAST RADIUS OF GYRATION, AXIS 1-1.

Based on Gordon's Formula, $P = \frac{50\,000}{1 + \frac{(12 L)^2}{36\,000 r^2}}$

Safety factor 4.



Length in Feet.

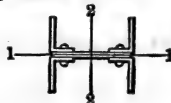
| 12 | 14 | 16 | 18 | 20 | 22 | 24 | 26 | 28 | 30 | 32 | 34 | 36 | 38 | 40 |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|------|
| 279 | 274 | 267 | 260 | 253 | 246 | 238 | 230 | 222 | 214 | 206 | 198 | 191 | 183 | 176 |
| 318 | 312 | 305 | 297 | 289 | 280 | 271 | 263 | 254 | 245 | 236 | 227 | 218 | 210 | 201 |
| 357 | 350 | 342 | 333 | 324 | 315 | 305 | 295 | 286 | 276 | 266 | 256 | 246 | 237 | 228 |
| 395 | 387 | 379 | 369 | 359 | 349 | 339 | 328 | 317 | 306 | 295 | 284 | 274 | 263 | 253 |
| 433 | 424 | 415 | 405 | 395 | 384 | 372 | 360 | 349 | 337 | 325 | 313 | 302 | 290 | 279 |
| 470 | 462 | 452 | 441 | 430 | 418 | 406 | 393 | 380 | 368 | 355 | 342 | 330 | 318 | 306 |
| 508 | 498 | 488 | 477 | 465 | 452 | 439 | 425 | 412 | 398 | 385 | 371 | 358 | 345 | 332 |
| 545 | 535 | 524 | 512 | 499 | 486 | 472 | 458 | 443 | 429 | 415 | 400 | 386 | 372 | 358 |
| 581 | 571 | 559 | 547 | 534 | 520 | 505 | 490 | 475 | 460 | 444 | 429 | 414 | 399 | 385 |
| 618 | 607 | 595 | 582 | 568 | 553 | 538 | 522 | 506 | 490 | 474 | 458 | 442 | 427 | 412 |
| 289 | 283 | 276 | 269 | 261 | 253 | 245 | 236 | 228 | 220 | 211 | 203 | 195 | 187 | 180 |
| 329 | 322 | 315 | 307 | 298 | 289 | 280 | 270 | 261 | 251 | 242 | 232 | 223 | 214 | 206 |
| 369 | 362 | 353 | 344 | 335 | 325 | 314 | 304 | 293 | 283 | 272 | 262 | 252 | 242 | 233 |
| 409 | 400 | 391 | 381 | 371 | 360 | 349 | 337 | 326 | 314 | 303 | 291 | 280 | 269 | 259 |
| 448 | 439 | 429 | 419 | 407 | 396 | 383 | 371 | 359 | 346 | 334 | 321 | 309 | 297 | 286 |
| 487 | 478 | 467 | 456 | 444 | 431 | 418 | 405 | 391 | 378 | 364 | 351 | 338 | 325 | 313 |
| 526 | 516 | 505 | 493 | 480 | 466 | 452 | 438 | 424 | 409 | 395 | 381 | 367 | 353 | 340 |
| 564 | 554 | 542 | 529 | 516 | 501 | 487 | 472 | 456 | 441 | 426 | 411 | 396 | 381 | 367 |
| 603 | 591 | 579 | 566 | 551 | 536 | 521 | 505 | 489 | 473 | 457 | 441 | 425 | 409 | 394 |
| 640 | 629 | 616 | 602 | 587 | 571 | 555 | 538 | 521 | 504 | 487 | 471 | 454 | 437 | 421 |
| 299 | 292 | 285 | 277 | 269 | 260 | 252 | 243 | 234 | 225 | 216 | 208 | 199 | 191 | |
| 340 | 333 | 325 | 316 | 307 | 297 | 287 | 277 | 267 | 257 | 248 | 238 | 228 | 219 | |
| 382 | 374 | 365 | 355 | 345 | 334 | 323 | 312 | 301 | 290 | 279 | 268 | 258 | 247 | |
| 423 | 414 | 404 | 393 | 382 | 371 | 359 | 347 | 335 | 322 | 310 | 298 | 287 | 275 | |
| 463 | 454 | 443 | 432 | 420 | 407 | 395 | 382 | 368 | 355 | 342 | 329 | 316 | 304 | |
| 504 | 494 | 483 | 470 | 457 | 444 | 430 | 416 | 402 | 388 | 374 | 360 | 346 | 333 | |
| 544 | 533 | 521 | 508 | 495 | 481 | 466 | 451 | 436 | 420 | 405 | 390 | 376 | 361 | |
| 584 | 573 | 560 | 546 | 532 | 517 | 501 | 485 | 469 | 453 | 437 | 421 | 405 | 390 | |
| 624 | 612 | 598 | 584 | 569 | 553 | 536 | 520 | 503 | 486 | 469 | 452 | 435 | 419 | |
| 663 | 650 | 636 | 622 | 606 | 589 | 572 | 554 | 536 | 518 | 500 | 483 | 465 | 448 | |
| 308 | 301 | 294 | 285 | 277 | 268 | 258 | 249 | 240 | 230 | 221 | 212 | 204 | 195 | |
| 351 | 343 | 335 | 326 | 316 | 306 | 295 | 285 | 274 | 264 | 253 | 243 | 233 | 224 | |
| 394 | 385 | 376 | 366 | 355 | 344 | 332 | 321 | 309 | 297 | 286 | 274 | 263 | 253 | |
| 436 | 427 | 417 | 405 | 394 | 381 | 369 | 356 | 343 | 330 | 318 | 305 | 293 | 281 | |
| 479 | 468 | 457 | 445 | 432 | 419 | 406 | 392 | 378 | 364 | 350 | 337 | 323 | 310 | |
| 521 | 510 | 498 | 485 | 471 | 457 | 442 | 427 | 412 | 397 | 383 | 368 | 354 | 340 | |
| 562 | 551 | 538 | 524 | 510 | 495 | 479 | 463 | 447 | 431 | 415 | 400 | 384 | 369 | |
| 603 | 591 | 578 | 563 | 548 | 532 | 515 | 499 | 482 | 465 | 448 | 431 | 415 | 399 | |
| 644 | 632 | 618 | 602 | 586 | 569 | 552 | 534 | 516 | 498 | 480 | 463 | 445 | 428 | |
| 685 | 672 | 657 | 641 | 624 | 607 | 588 | 570 | 551 | 532 | 513 | 494 | 476 | 458 | |

SAFE LOADS IN THOUSANDS OF POUNDS FOR PLATE AND ANGLE COLUMNS. SQUARE ENDS.

CALCULATED FOR RADIUS OF GYRATION,
AXIS 2-2.

Based on Gordon's Formula, $P = \frac{50\,000}{1 + \frac{(12\,L)^2}{36\,000\,r^2}}$

Safety factor 4.

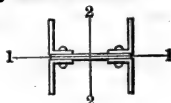


| Size of Angles. | Size of Plate. | Weight of Column. | Area of Column Section. | Least Radius of Gyration Axis 1-1. | Radius of Gyration Axis 2-2. | Length in Feet. | | |
|-----------------|----------------|-------------------|-------------------------|------------------------------------|------------------------------|-----------------|-------|-----|
| Inches. | Inches. | Lbs. per Ft. | Sq. Ins. | Inches | Inches. | 4 | 6 | 8 |
| 3 x 2½ x ¼ | 6 x ¼ | 23.1 | 6.74 | 1.24 | 2.41 | 83 | 82 | 81 |
| " " ⅜ | " ⅜ | 28.8 | 8.36 | 1.27 | 2.39 | 103 | 102 | 100 |
| " " ½ | " ½ | 34.1 | 9.93 | 1.30 | 2.37 | 123 | 121 | 119 |
| " " ⅝ | " ⅝ | 39.3 | 11.51 | 1.33 | 2.35 | 142 | 140 | 137 |
| " " ¾ | " ¾ | 44.2 | 13.00 | 1.36 | 2.33 | 161 | 158 | 155 |
| " " ⅞ | " ⅞ | 49.5 | 14.50 | 1.39 | 2.31 | 179 | 176 | 173 |
| 3½ x 2½ x ¼ | 7 x ¼ | 25.6 | 7.51 | 1.46 | 2.88 | 93 | 92 | 91 |
| " " ⅜ | " ⅜ | 31.8 | 9.31 | 1.49 | 2.86 | 115 | 114 | 113 |
| " " ½ | " ½ | 37.7 | 11.07 | 1.52 | 2.84 | 137 | 136 | 134 |
| " " ⅝ | " ⅝ | 43.6 | 12.78 | 1.55 | 2.82 | 159 | 157 | 155 |
| " " ¾ | " ¾ | 49.5 | 14.50 | 1.58 | 2.80 | 180 | 178 | 176 |
| " " ⅞ | " ⅞ | 55.0 | 16.18 | 1.61 | 2.78 | 200 | 198 | 196 |
| 4 x 3 x ⅜ | 8 x ⅜ | 37.3 | 10.86 | 1.67 | 3.25 | | 134 | 133 |
| " " ½ | " ½ | 44.2 | 12.92 | 1.70 | 3.23 | | 160 | 158 |
| " " ⅝ | " ⅝ | 51.1 | 14.98 | 1.73 | 3.21 | | 185 | 183 |
| " " ¾ | " ¾ | 58.0 | 17.00 | 1.76 | 3.18 | | 210 | 207 |
| " " ⅞ | " ⅞ | 64.9 | 18.98 | 1.79 | 3.16 | | 234 | 231 |
| " " 1 | " 1 | 71.4 | 20.92 | 1.82 | 3.14 | | 258 | 255 |
| " " 1¼ | " 1¼ | 77.9 | 22.86 | 1.85 | 3.12 | | 282 | 278 |
| " " 1½ | " 1½ | 84.4 | 24.76 | 1.89 | 3.10 | | 305 | 301 |
| " " 1¾ | " 1¾ | 90.5 | 26.62 | 1.92 | 3.08 | | 328 | 324 |
| " " 2 | " 2 | 97.0 | 28.44 | 1.95 | 3.06 | | 350 | 346 |
| 5 x 3½ x ⅜ | 10 x ⅜ | 45.4 | 13.37 | 2.08 | 4.10 | | 166 | 165 |
| " " ½ | " ½ | 54.4 | 15.95 | 2.10 | 4.08 | | 198 | 196 |
| " " ⅝ | " ⅝ | 62.9 | 18.50 | 2.13 | 4.06 | | 229 | 228 |
| " " ¾ | " ¾ | 71.4 | 21.00 | 2.16 | 4.04 | | 260 | 258 |
| " " ⅞ | " ⅞ | 79.9 | 23.51 | 2.19 | 4.02 | | 291 | 289 |
| " " 1 | " 1 | 88.5 | 25.93 | 2.22 | 4.00 | | 321 | 319 |
| " " 1¼ | " 1¼ | 96.6 | 28.36 | 2.25 | 3.98 | | 351 | 349 |
| " " 1½ | " 1½ | 104.7 | 30.74 | 2.29 | 3.96 | | 381 | 378 |
| " " 1¾ | " 1¾ | 112.8 | 33.13 | 2.32 | 3.93 | | 410 | 407 |
| " " 2 | " 2 | 120.6 | 35.43 | 2.35 | 3.91 | | 439 | 436 |
| " " 2¼ | " 2¼ | 128.7 | 37.74 | 2.38 | 3.89 | | 467 | 464 |
| 6 x 3½ x ⅜ | 12 x ⅜ | 62.1 | 18.18 | 2.56 | 5.01 | | | 225 |
| " " ½ | " ½ | 71.9 | 21.13 | 2.59 | 4.99 | | | 261 |
| " " ⅝ | " ⅝ | 81.6 | 24.00 | 2.62 | 4.97 | | | 297 |
| " " ¾ | " ¾ | 91.4 | 26.87 | 2.65 | 4.95 | | | 332 |
| " " ⅞ | " ⅞ | 101.1 | 29.70 | 2.68 | 4.93 | | | 367 |
| " " 1 | " 1 | 110.5 | 32.49 | 2.71 | 4.91 | | | 402 |
| " " 1¼ | " 1¼ | 120.2 | 35.24 | 2.74 | 4.88 | | | 436 |
| " " 1½ | " 1½ | 129.2 | 37.99 | 2.77 | 4.86 | | | 470 |
| " " 1¾ | " 1¾ | 138.5 | 40.70 | 2.80 | 4.84 | | | 503 |
| " " 2 | " 2 | 147.5 | 43.37 | 2.83 | 4.82 | | | 536 |
| " " 2¼ | " 2¼ | 156.4 | 46.00 | 2.86 | 4.80 | | | 569 |

SAFE LOADS IN THOUSANDS OF POUNDS FOR PLATE AND ANGLE COLUMNS. SQUARE ENDS.

CALCULATED FOR RADIUS OF GYRATION,
AXIS 2-2.

Based on Gordon's Formula, $P = \frac{50\,000}{1 + \frac{(12\,L)^2}{36\,000\,r^2}}$
Safety factor 4.

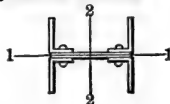


Length in Feet.

| 10 | 12 | 14 | 16 | 18 | 20 | 22 | 24 | 26 | 28 | 30 | 32 | 34 | 36 | 38 | 40 |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-------|-------|-------|-------|-------|
| 79 | 77 | 74 | 72 | 69 | 66 | 63 | 60 | 58 | 55 | 52 | | | | | |
| 98 | 95 | 92 | 89 | 85 | 82 | 78 | 75 | 71 | 68 | 64 | | | | | |
| 116 | 113 | 109 | 105 | 101 | 97 | 92 | 88 | 84 | 80 | 76 | | | | | |
| 134 | 130 | 126 | 121 | 116 | 111 | 106 | 101 | 96 | 92 | 87 | | | | | |
| 151 | 147 | 142 | 137 | 131 | 126 | 120 | 114 | 108 | 103 | 98 | | | | | |
| 169 | 163 | 158 | 152 | 146 | 139 | 133 | 127 | 120 | 114 | 108 | | | | | |
| 89 | 88 | 86 | 83 | 81 | 79 | 76 | 73 | 71 | 68 | 65 | 63 | 60 | 58 | | |
| 111 | 109 | 106 | 103 | 100 | 97 | 94 | 91 | 87 | 84 | 81 | 77 | 74 | 71 | | |
| 132 | 129 | 126 | 123 | 119 | 115 | 112 | 108 | 104 | 100 | 96 | 92 | 88 | 84 | | |
| 152 | 149 | 146 | 142 | 137 | 133 | 129 | 124 | 119 | 115 | 110 | 106 | 101 | 97 | | |
| 172 | 169 | 165 | 160 | 156 | 151 | 145 | 140 | 135 | 129 | 124 | 119 | 114 | 109 | | |
| 192 | 188 | 183 | 178 | 173 | 167 | 162 | 156 | 150 | 144 | 138 | 132 | 126 | 121 | | |
| 131 | 129 | 126 | 124 | 121 | 118 | 115 | 111 | 108 | 105 | 101 | 98 | 94 | 91 | 88 | 85 |
| 156 | 153 | 150 | 147 | 144 | 140 | 136 | 132 | 128 | 124 | 120 | 116 | 112 | 108 | 104 | 100 |
| 180 | 177 | 174 | 170 | 166 | 162 | 158 | 153 | 148 | 143 | 139 | 134 | 129 | 124 | 120 | 115 |
| 204 | 201 | 197 | 193 | 188 | 184 | 178 | 173 | 168 | 162 | 157 | 151 | 146 | 141 | 135 | 130 |
| 228 | 224 | 220 | 215 | 210 | 205 | 199 | 193 | 187 | 181 | 175 | 168 | 162 | 156 | 150 | 145 |
| 252 | 247 | 243 | 237 | 231 | 225 | 219 | 212 | 206 | 199 | 192 | 185 | 178 | 172 | 165 | 159 |
| 274 | 270 | 264 | 259 | 252 | 245 | 238 | 231 | 224 | 216 | 209 | 201 | 194 | 187 | 179 | 173 |
| 297 | 292 | 286 | 280 | 273 | 265 | 258 | 250 | 242 | 233 | 225 | 217 | 209 | 201 | 193 | 186 |
| 319 | 314 | 307 | 300 | 293 | 285 | 276 | 268 | 259 | 250 | 241 | 232 | 224 | 215 | 207 | 199 |
| 341 | 335 | 328 | 321 | 312 | 304 | 295 | 285 | 276 | 266 | 257 | 248 | 238 | 229 | 220 | 211 |
| 163 | 161 | 160 | 157 | 155 | 153 | 150 | 147 | 144 | 141 | 138 | 134 | 131 | 128 | 124 | 121 |
| 195 | 193 | 190 | 188 | 185 | 182 | 179 | 175 | 171 | 168 | 164 | 160 | 156 | 152 | 148 | 144 |
| 226 | 223 | 221 | 218 | 214 | 211 | 207 | 203 | 199 | 194 | 190 | 185 | 181 | 176 | 171 | 166 |
| 256 | 254 | 250 | 247 | 243 | 239 | 235 | 230 | 225 | 220 | 215 | 210 | 205 | 199 | 194 | 189 |
| 287 | 284 | 280 | 276 | 272 | 267 | 262 | 257 | 251 | 246 | 240 | 234 | 228 | 222 | 216 | 210 |
| 316 | 313 | 309 | 305 | 300 | 295 | 289 | 283 | 277 | 271 | 265 | 258 | 251 | 245 | 238 | 232 |
| 346 | 342 | 338 | 333 | 328 | 322 | 316 | 309 | 303 | 296 | 289 | 282 | 274 | 267 | 260 | 252 |
| 375 | 371 | 366 | 361 | 355 | 349 | 342 | 335 | 328 | 320 | 312 | 305 | 297 | 289 | 281 | 273 |
| 403 | 399 | 394 | 388 | 382 | 375 | 368 | 360 | 352 | 344 | 336 | 327 | 319 | 310 | 301 | 293 |
| 432 | 427 | 421 | 415 | 408 | 401 | 393 | 385 | 377 | 368 | 359 | 350 | 340 | 331 | 322 | 313 |
| 460 | 454 | 449 | 442 | 435 | 427 | 418 | 410 | 400 | 391 | 381 | 371 | 362 | 352 | 342 | 332 |
| 224 | 222 | 221 | 218 | 216 | 214 | 211 | 208 | 205 | 202 | 199 | 196 | 192 | 189 | 185 | 181 |
| 260 | 258 | 256 | 253 | 251 | 248 | 245 | 242 | 238 | 234 | 231 | 227 | 223 | 218 | 214 | 210 |
| 295 | 293 | 291 | 288 | 285 | 282 | 278 | 274 | 270 | 266 | 262 | 257 | 253 | 248 | 243 | 238 |
| 330 | 328 | 325 | 322 | 319 | 315 | 311 | 307 | 302 | 298 | 293 | 288 | 282 | 277 | 272 | 266 |
| 365 | 363 | 360 | 356 | 352 | 348 | 344 | 339 | 334 | 329 | 323 | 318 | 312 | 306 | 300 | 294 |
| 399 | 397 | 393 | 389 | 385 | 381 | 376 | 371 | 365 | 359 | 353 | 347 | 341 | 334 | 327 | 321 |
| 433 | 430 | 427 | 422 | 418 | 413 | 408 | 402 | 396 | 389 | 383 | 376 | 369 | 362 | 355 | 347 |
| 467 | 463 | 460 | 455 | 450 | 445 | 439 | 433 | 426 | 419 | 412 | 405 | 397 | 389 | 382 | 374 |
| 500 | 496 | 492 | 487 | 482 | 476 | 470 | 463 | 456 | 449 | 441 | 433 | 425 | 417 | 408 | 400 |
| 533 | 529 | 524 | 519 | 513 | 507 | 500 | 493 | 486 | 478 | 469 | 461 | 452 | 443 | 434 | 425 |
| 565 | 561 | 556 | 551 | 544 | 538 | 530 | 523 | 515 | 506 | 497 | 488 | 479 | 469 | 460 | 450 |

**SAFE LOADS IN THOUSANDS OF POUNDS FOR
PLATE AND ANGLE COLUMNS. SQUARE ENDS.
CALCULATED FOR RADIUS OF GYRATION,
AXIS 2-2.**

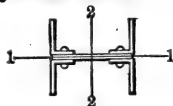
Based on Gordon's Formula, $P = \frac{50\,000}{1 + \frac{(12\,L)^2}{36\,000\,r^2}}$
Safety factor 4.



| Size of Angles. | Size of Plate. | Weight of Column. | Area of Column Section. | Least Radius of Gyration Axis 1-1. | Radius of Gyration Axis 2-2. | Length in Feet. | | |
|--------------------|----------------|-------------------|-------------------------|------------------------------------|------------------------------|-----------------|-------|-------|
| Inches. | Inches. | Lbs. per Ft. | Sq. Ins. | Inches. | Inches. | 4 | 6 | 8 |
| 3 x 2½ x ¼ | 8 x ¼ | 24.8 | 7.24 | 1.19 | 3.25 | 90 | 89 | 88 |
| " " ⅜ | " ⅜ | 30.9 | 8.98 | 1.22 | 3.23 | 112 | 111 | 110 |
| " " ½ | " ½ | 36.6 | 10.68 | 1.25 | 3.21 | 133 | 132 | 130 |
| " " ⅝ | " ⅝ | 42.3 | 12.38 | 1.28 | 3.19 | 154 | 152 | 151 |
| " " ¾ | " ¾ | 47.6 | 14.00 | 1.31 | 3.17 | 174 | 173 | 171 |
| " " ⅞ | " ⅞ | 53.3 | 15.62 | 1.34 | 3.15 | 194 | 192 | 190 |
| 3½ x 2½ x ¼ | 8 x ¼ | 26.4 | 7.76 | 1.44 | 3.31 | | 96 | 95 |
| " " ⅜ | " ⅜ | 32.9 | 9.62 | 1.47 | 3.28 | | 119 | 117 |
| " " ½ | " ½ | 39.0 | 11.44 | 1.50 | 3.26 | | 141 | 140 |
| " " ⅝ | " ⅝ | 45.1 | 13.22 | 1.53 | 3.24 | | 163 | 161 |
| " " ¾ | " ¾ | 51.2 | 15.00 | 1.56 | 3.22 | | 185 | 183 |
| " " ⅞ | " ⅞ | 56.9 | 16.74 | 1.59 | 3.20 | | 206 | 204 |
| 4 x 3 x ⅜ | 10 x ⅜ | 39.4 | 11.49 | 1.62 | 4.09 | | 142 | 141 |
| " " ½ | " ½ | 46.8 | 13.67 | 1.65 | 4.07 | | 170 | 169 |
| " " ⅝ | " ⅝ | 54.1 | 15.86 | 1.68 | 4.04 | | 197 | 195 |
| " " ¾ | " ¾ | 61.4 | 18.00 | 1.71 | 4.02 | | 223 | 222 |
| " " ⅞ | " ⅞ | 68.7 | 20.11 | 1.74 | 4.00 | | 249 | 247 |
| " " 1 | " 1 | 75.7 | 22.17 | 1.77 | 3.98 | | 275 | 273 |
| " " 1¼ | " 1¼ | 82.6 | 24.24 | 1.80 | 3.96 | | 300 | 298 |
| " " 1½ | " 1½ | 89.5 | 26.26 | 1.83 | 3.94 | | 325 | 323 |
| " " 1¾ | " 1¾ | 96.0 | 28.25 | 1.86 | 3.92 | | 350 | 347 |
| " " 2 | " 2 | 103.0 | 30.19 | 1.90 | 3.90 | | 374 | 371 |
| 5 x 3½ x ⅜ | 12 x ⅜ | 47.6 | 13.99 | 2.03 | 4.95 | | | 173 |
| " " ½ | " ½ | 56.9 | 16.70 | 2.06 | 4.92 | | | 206 |
| " " ⅝ | " ⅝ | 65.9 | 19.37 | 2.08 | 4.90 | | | 239 |
| " " ¾ | " ¾ | 74.8 | 22.00 | 2.11 | 4.88 | | | 272 |
| " " ⅞ | " ⅞ | 83.8 | 24.63 | 2.14 | 4.86 | | | 304 |
| " " 1 | " 1 | 92.7 | 27.18 | 2.17 | 4.84 | | | 336 |
| " " 1¼ | " 1¼ | 101.3 | 29.73 | 2.20 | 4.82 | | | 368 |
| " " 1½ | " 1½ | 109.8 | 32.24 | 2.23 | 4.80 | | | 399 |
| " " 1¾ | " 1¾ | 118.4 | 34.75 | 2.26 | 4.78 | | | 429 |
| " " 2 | " 2 | 126.5 | 37.18 | 2.29 | 4.76 | | | 460 |
| " " 2¼ | " 2¼ | 135.1 | 39.61 | 2.33 | 4.74 | | | 490 |
| 6 x 3½ x ⅜ | 14 x ⅜ | 64.7 | 18.93 | 2.51 | 5.85 | | | |
| " " ½ | " ½ | 74.8 | 22.01 | 2.54 | 5.83 | | | |
| " " ⅝ | " ⅝ | 85.0 | 25.00 | 2.57 | 5.81 | | | |
| " " ¾ | " ¾ | 95.2 | 28.00 | 2.59 | 5.79 | | | |
| " " ⅞ | " ⅞ | 105.3 | 30.95 | 2.62 | 5.77 | | | |
| " " 1 | " 1 | 115.1 | 33.87 | 2.65 | 5.74 | | | |
| " " 1¼ | " 1¼ | 125.3 | 36.74 | 2.68 | 5.72 | | | |
| " " 1½ | " 1½ | 134.7 | 39.62 | 2.71 | 5.70 | | | |
| " " 1¾ | " 1¾ | 144.5 | 42.45 | 2.74 | 5.68 | | | |
| " " 2 | " 2 | 153.8 | 45.25 | 2.77 | 5.66 | | | |
| " " 2¼ | " 2¼ | 163.2 | 48.00 | 2.81 | 5.64 | | | |

**SAFE LOADS IN THOUSANDS OF POUNDS FOR
PLATE AND ANGLE COLUMNS. SQUARE ENDS.**
CALCULATED FOR RADIUS OF GYRATION,
AXIS 2-2.

Based on Gordon's Formula, $P = \frac{50\,000}{1 + \frac{(12\,L)^2}{36\,000\,r^2}}$
Safety factor 4.



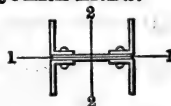
Length in Feet.

| 10 | 12 | 14 | 16 | 18 | 20 | 22 | 24 | 26 | 28 | 30 | 32 | 34 | 36 | 38 | 40 |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| 87 | 86 | 84 | 83 | 81 | 79 | 77 | 74 | 72 | 70 | 68 | 65 | 63 | 61 | 59 | 56 |
| 108 | 106 | 104 | 102 | 100 | 97 | 95 | 92 | 89 | 86 | 83 | 81 | 78 | 75 | 72 | 70 |
| 129 | 127 | 124 | 122 | 119 | 116 | 112 | 109 | 106 | 102 | 99 | 96 | 92 | 89 | 86 | 82 |
| 149 | 146 | 143 | 140 | 137 | 133 | 130 | 126 | 122 | 118 | 114 | 110 | 106 | 102 | 99 | 95 |
| 168 | 166 | 162 | 159 | 155 | 151 | 147 | 142 | 138 | 133 | 129 | 124 | 120 | 115 | 111 | 107 |
| 188 | 184 | 181 | 177 | 173 | 168 | 163 | 158 | 153 | 148 | 143 | 138 | 133 | 128 | 123 | 119 |
| 93 | 92 | 90 | 89 | 87 | 85 | 82 | 80 | 78 | 75 | 73 | 70 | 68 | 66 | 63 | 61 |
| 116 | 114 | 112 | 110 | 108 | 105 | 102 | 99 | 96 | 93 | 90 | 87 | 84 | 81 | 78 | 75 |
| 138 | 136 | 133 | 130 | 127 | 124 | 121 | 118 | 114 | 110 | 107 | 103 | 100 | 96 | 93 | 89 |
| 159 | 157 | 154 | 151 | 147 | 144 | 140 | 136 | 132 | 127 | 123 | 119 | 115 | 111 | 107 | 103 |
| 181 | 178 | 174 | 171 | 167 | 162 | 158 | 153 | 149 | 144 | 139 | 134 | 130 | 125 | 120 | 116 |
| 201 | 198 | 194 | 190 | 186 | 181 | 176 | 171 | 165 | 160 | 155 | 149 | 144 | 139 | 134 | 129 |
| 140 | 139 | 137 | 135 | 133 | 131 | 129 | 126 | 124 | 121 | 118 | 115 | 112 | 110 | 107 | 104 |
| 167 | 165 | 163 | 161 | 159 | 156 | 153 | 150 | 147 | 144 | 141 | 137 | 134 | 130 | 127 | 123 |
| 194 | 192 | 189 | 187 | 184 | 181 | 177 | 174 | 170 | 166 | 162 | 159 | 155 | 151 | 147 | 143 |
| 220 | 217 | 215 | 212 | 208 | 205 | 201 | 197 | 193 | 189 | 184 | 180 | 175 | 170 | 166 | 161 |
| 245 | 243 | 240 | 236 | 233 | 229 | 224 | 220 | 215 | 210 | 205 | 200 | 195 | 190 | 185 | 180 |
| 271 | 268 | 264 | 261 | 256 | 252 | 247 | 242 | 237 | 232 | 226 | 220 | 215 | 209 | 203 | 198 |
| 295 | 292 | 289 | 284 | 280 | 275 | 270 | 264 | 258 | 253 | 246 | 240 | 234 | 228 | 222 | 215 |
| 320 | 316 | 312 | 308 | 303 | 298 | 292 | 286 | 280 | 273 | 266 | 260 | 253 | 246 | 239 | 232 |
| 344 | 340 | 336 | 331 | 326 | 320 | 314 | 307 | 300 | 293 | 286 | 279 | 271 | 264 | 257 | 249 |
| 368 | 364 | 359 | 354 | 348 | 342 | 335 | 328 | 320 | 313 | 305 | 297 | 289 | 282 | 274 | 266 |
| 172 | 171 | 169 | 168 | 166 | 164 | 162 | 160 | 157 | 155 | 152 | 150 | 147 | 144 | 141 | 139 |
| 205 | 204 | 202 | 200 | 198 | 196 | 193 | 191 | 188 | 185 | 182 | 178 | 175 | 172 | 168 | 165 |
| 238 | 236 | 234 | 232 | 230 | 227 | 224 | 221 | 218 | 214 | 210 | 207 | 203 | 199 | 195 | 191 |
| 270 | 269 | 266 | 264 | 261 | 258 | 254 | 251 | 247 | 243 | 239 | 235 | 230 | 226 | 221 | 217 |
| 303 | 300 | 298 | 295 | 292 | 288 | 284 | 280 | 276 | 272 | 267 | 262 | 257 | 252 | 247 | 242 |
| 334 | 332 | 329 | 326 | 322 | 318 | 314 | 309 | 305 | 300 | 295 | 289 | 284 | 278 | 273 | 267 |
| 365 | 363 | 359 | 356 | 352 | 348 | 343 | 338 | 333 | 327 | 322 | 316 | 310 | 304 | 298 | 291 |
| 396 | 393 | 390 | 386 | 382 | 377 | 372 | 366 | 361 | 355 | 349 | 342 | 336 | 329 | 322 | 315 |
| 427 | 423 | 420 | 415 | 411 | 406 | 400 | 394 | 388 | 382 | 375 | 368 | 361 | 354 | 346 | 339 |
| 457 | 453 | 449 | 445 | 440 | 434 | 428 | 422 | 415 | 408 | 401 | 394 | 386 | 378 | 370 | 362 |
| 486 | 483 | 478 | 474 | 468 | 462 | 456 | 449 | 442 | 434 | 427 | 419 | 410 | 402 | 394 | 385 |
| 234 | 233 | 231 | 230 | 228 | 226 | 224 | 222 | 219 | 217 | 214 | 211 | 209 | 206 | 203 | 199 |
| 272 | 270 | 269 | 267 | 265 | 263 | 260 | 257 | 255 | 252 | 249 | 245 | 242 | 239 | 235 | 231 |
| 309 | 307 | 305 | 303 | 301 | 298 | 296 | 293 | 289 | 286 | 282 | 279 | 275 | 271 | 267 | 263 |
| 346 | 344 | 342 | 340 | 337 | 334 | 331 | 327 | 324 | 320 | 316 | 312 | 307 | 303 | 298 | 294 |
| 382 | 380 | 378 | 375 | 372 | 369 | 365 | 362 | 358 | 353 | 349 | 344 | 340 | 335 | 330 | 324 |
| 418 | 416 | 413 | 411 | 407 | 404 | 400 | 396 | 391 | 387 | 382 | 377 | 371 | 366 | 360 | 355 |
| 454 | 451 | 449 | 445 | 442 | 438 | 434 | 429 | 424 | 419 | 414 | 408 | 403 | 397 | 391 | 384 |
| 489 | 487 | 483 | 480 | 476 | 472 | 467 | 462 | 457 | 452 | 446 | 440 | 433 | 427 | 420 | 414 |
| 524 | 521 | 518 | 514 | 510 | 505 | 500 | 495 | 490 | 484 | 477 | 471 | 464 | 457 | 450 | 443 |
| 559 | 556 | 552 | 548 | 544 | 539 | 533 | 528 | 521 | 515 | 508 | 501 | 494 | 487 | 479 | 471 |
| 593 | 589 | 586 | 581 | 577 | 571 | 566 | 559 | 553 | 546 | 539 | 532 | 524 | 516 | 508 | 500 |

**SAFE LOADS IN THOUSANDS OF POUNDS FOR
PLATE AND ANGLE COLUMNS. SQUARE ENDS.
CALCULATED FOR RADIUS OF GYRATION,
AXIS 2-2.**

Based on Gordon's Formula, $P = \frac{50,000}{1 + \frac{(12 L)^2}{36,000 r^2}}$

Safety factor 4.



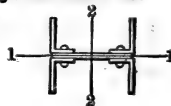
| Size of Angles. | Size of Plate. | Weight of Column. | Area of Column Section. | Least Radius of Gyration Axis 1-1. | Radius of Gyration Axis 2-2. | Length in Feet. | | |
|--------------------|----------------|-------------------|-------------------------|------------------------------------|------------------------------|-----------------|-------|-------|
| Inches. | Inches. | Lbs. per Ft. | Sq. Ins. | Inches. | Inches. | 6 | 8 | 10 |
| 3 x 2½ x ¼ | 10 x ¼ | 25.5 | 7.74 | 1.16 | 4.07 | 96 | 95 | 95 |
| " " x ⅜ | " " x ⅜ | 33.0 | 9.61 | 1.18 | 4.05 | 119 | 118 | 117 |
| " " x ½ | " " x ½ | 39.2 | 11.43 | 1.21 | 4.03 | 142 | 141 | 140 |
| " " x ⅝ | " " x ⅝ | 45.3 | 13.26 | 1.24 | 4.01 | 164 | 163 | 161 |
| " " x ¾ | " " x ¾ | 51.0 | 15.00 | 1.27 | 3.99 | 186 | 185 | 183 |
| " " x ⅞ | " " x ⅞ | 57.1 | 16.75 | 1.30 | 3.96 | 207 | 206 | 204 |
| 3½ x 2½ x ¼ | 10 x ¼ | 28.1 | 8.26 | 1.39 | 4.13 | 102 | 102 | 101 |
| " " x ⅜ | " " x ⅜ | 35.0 | 10.25 | 1.42 | 4.11 | 127 | 126 | 125 |
| " " x ½ | " " x ½ | 41.6 | 12.19 | 1.45 | 4.09 | 151 | 150 | 149 |
| " " x ⅝ | " " x ⅝ | 48.1 | 14.10 | 1.48 | 4.07 | 175 | 174 | 172 |
| " " x ¾ | " " x ¾ | 54.6 | 16.00 | 1.51 | 4.05 | 198 | 197 | 195 |
| " " x ⅞ | " " x ⅞ | 60.7 | 17.87 | 1.54 | 4.03 | 221 | 220 | 218 |
| 4 x 3 x ⅜ | 12 x ⅜ | 41.6 | 12.11 | 1.58 | 4.91 | | 150 | 149 |
| " " x ½ | " " x ½ | 49.3 | 14.42 | 1.61 | 4.89 | | 179 | 178 |
| " " x ⅝ | " " x ⅝ | 57.1 | 16.73 | 1.64 | 4.87 | | 207 | 206 |
| " " x ¾ | " " x ¾ | 64.8 | 19.00 | 1.66 | 4.85 | | 235 | 234 |
| " " x ⅞ | " " x ⅞ | 72.6 | 21.23 | 1.69 | 4.83 | | 262 | 261 |
| " " x 1 | " " x 1 | 79.9 | 23.42 | 1.72 | 4.81 | | 290 | 288 |
| " " x 1¼ | " " x 1¼ | 87.3 | 25.61 | 1.75 | 4.79 | | 317 | 315 |
| " " x 1½ | " " x 1½ | 94.6 | 27.76 | 1.78 | 4.77 | | 343 | 341 |
| " " x 1¾ | " " x 1¾ | 101.6 | 29.87 | 1.81 | 4.74 | | 369 | 367 |
| " " x 1⅞ | " " x 1⅞ | 108.9 | 31.94 | 1.84 | 4.72 | | 395 | 392 |
| 5 x 3½ x ⅜ | 14 x ⅜ | 49.7 | 14.62 | 1.98 | 5.77 | | | 180 |
| " " x ½ | " " x ½ | 59.5 | 17.45 | 2.01 | 5.75 | | | 215 |
| " " x ⅝ | " " x ⅝ | 68.8 | 20.25 | 2.04 | 5.73 | | | 250 |
| " " x ¾ | " " x ¾ | 78.2 | 23.00 | 2.07 | 5.71 | | | 284 |
| " " x ⅞ | " " x ⅞ | 87.6 | 25.76 | 2.09 | 5.69 | | | 318 |
| " " x 1 | " " x 1 | 96.9 | 28.43 | 2.12 | 5.67 | | | 351 |
| " " x 1¼ | " " x 1¼ | 105.9 | 31.11 | 2.15 | 5.64 | | | 384 |
| " " x 1½ | " " x 1½ | 114.9 | 33.74 | 2.18 | 5.62 | | | 417 |
| " " x 1¾ | " " x 1¾ | 123.9 | 36.38 | 2.21 | 5.60 | | | 449 |
| " " x 1⅞ | " " x 1⅞ | 132.5 | 38.93 | 2.24 | 5.58 | | | 481 |
| " " x 2 | " " x 2 | 141.4 | 41.49 | 2.27 | 5.56 | | | 512 |
| 6 x 3½ x ¾ | 16 x ¾ | 67.2 | 19.68 | 2.46 | 6.68 | | | |
| " " x 1 | " " x 1 | 77.8 | 22.88 | 2.49 | 6.66 | | | |
| " " x 1¼ | " " x 1¼ | 88.4 | 26.00 | 2.52 | 6.64 | | | |
| " " x 1½ | " " x 1½ | 99.0 | 29.12 | 2.54 | 6.61 | | | |
| " " x 1¾ | " " x 1¾ | 109.6 | 32.20 | 2.57 | 6.59 | | | |
| " " x 1⅞ | " " x 1⅞ | 119.8 | 35.24 | 2.60 | 6.57 | | | |
| " " x 2 | " " x 2 | 130.4 | 38.24 | 2.63 | 6.55 | | | |
| " " x 2¼ | " " x 2¼ | 140.2 | 41.24 | 2.66 | 6.53 | | | |
| " " x 2½ | " " x 2½ | 150.4 | 44.20 | 2.69 | 6.51 | | | |
| " " x 2¾ | " " x 2¾ | 160.2 | 47.12 | 2.72 | 6.48 | | | |
| " " x 3 | " " x 3 | 170.0 | 50.00 | 2.75 | 6.46 | | | |

SAFE LOADS IN THOUSANDS OF POUNDS FOR PLATE AND ANGLE COLUMNS. SQUARE ENDS.

CALCULATED FOR RADIUS OF GYRATION,
AXIS 2-2.

Based on Gordon's Formula, $P = \frac{50\,000}{1 + \frac{(12L)^2}{36\,000r^2}}$

Safety factor 4.

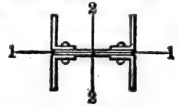


Length in Feet.

| 12 | 14 | 16 | 18 | 20 | 22 | 24 | 26 | 28 | 30 | 32 | 34 | 36 | 38 | 40 |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| 94 | 92 | 91 | 90 | 88 | 87 | 85 | 83 | 81 | 80 | 78 | 76 | 74 | 72 | 70 |
| 116 | 115 | 113 | 111 | 109 | 107 | 105 | 103 | 101 | 98 | 96 | 94 | 91 | 89 | 86 |
| 138 | 136 | 135 | 132 | 130 | 128 | 125 | 123 | 120 | 117 | 114 | 111 | 108 | 105 | 103 |
| 160 | 158 | 156 | 153 | 150 | 148 | 145 | 142 | 138 | 135 | 132 | 128 | 125 | 122 | 118 |
| 181 | 179 | 176 | 173 | 170 | 167 | 164 | 160 | 157 | 153 | 149 | 145 | 141 | 138 | 134 |
| 202 | 199 | 196 | 193 | 190 | 186 | 183 | 179 | 174 | 170 | 166 | 162 | 157 | 153 | 149 |
| 100 | 99 | 97 | 96 | 94 | 93 | 91 | 89 | 87 | 85 | 83 | 81 | 79 | 77 | 75 |
| 124 | 122 | 121 | 119 | 117 | 115 | 113 | 110 | 108 | 106 | 103 | 101 | 98 | 95 | 93 |
| 147 | 146 | 144 | 141 | 139 | 137 | 134 | 131 | 128 | 125 | 122 | 119 | 116 | 113 | 110 |
| 170 | 168 | 166 | 164 | 161 | 158 | 155 | 152 | 148 | 145 | 141 | 138 | 134 | 131 | 127 |
| 193 | 191 | 188 | 185 | 182 | 179 | 175 | 172 | 168 | 164 | 160 | 156 | 152 | 148 | 144 |
| 216 | 213 | 210 | 207 | 203 | 199 | 195 | 191 | 187 | 183 | 178 | 174 | 169 | 165 | 160 |
| 148 | 147 | 145 | 144 | 142 | 140 | 138 | 136 | 134 | 132 | 129 | 127 | 125 | 122 | 120 |
| 176 | 175 | 173 | 171 | 169 | 167 | 165 | 162 | 160 | 157 | 154 | 151 | 148 | 145 | 142 |
| 204 | 202 | 200 | 198 | 196 | 193 | 191 | 188 | 185 | 182 | 178 | 175 | 172 | 168 | 165 |
| 232 | 230 | 228 | 225 | 222 | 219 | 216 | 213 | 210 | 206 | 202 | 198 | 195 | 191 | 187 |
| 259 | 257 | 254 | 251 | 248 | 245 | 242 | 238 | 234 | 230 | 226 | 221 | 217 | 213 | 208 |
| 286 | 283 | 281 | 277 | 274 | 270 | 266 | 262 | 258 | 254 | 249 | 244 | 239 | 234 | 229 |
| 312 | 310 | 306 | 303 | 299 | 295 | 291 | 286 | 282 | 277 | 272 | 266 | 261 | 256 | 250 |
| 338 | 335 | 332 | 328 | 324 | 320 | 315 | 310 | 305 | 299 | 294 | 288 | 282 | 277 | 271 |
| 364 | 361 | 357 | 353 | 348 | 344 | 339 | 333 | 328 | 322 | 316 | 310 | 303 | 297 | 291 |
| 389 | 386 | 382 | 377 | 373 | 367 | 362 | 356 | 350 | 344 | 337 | 331 | 324 | 317 | 310 |
| 180 | 178 | 177 | 176 | 174 | 173 | 171 | 169 | 167 | 165 | 163 | 160 | 158 | 156 | 153 |
| 214 | 213 | 211 | 210 | 208 | 206 | 204 | 202 | 199 | 197 | 194 | 191 | 188 | 186 | 183 |
| 249 | 247 | 245 | 243 | 241 | 239 | 236 | 234 | 231 | 228 | 225 | 222 | 218 | 215 | 212 |
| 283 | 281 | 279 | 277 | 274 | 271 | 269 | 265 | 262 | 259 | 255 | 252 | 248 | 244 | 240 |
| 316 | 314 | 312 | 309 | 307 | 304 | 300 | 297 | 293 | 290 | 286 | 281 | 277 | 273 | 269 |
| 349 | 347 | 345 | 342 | 339 | 335 | 332 | 328 | 324 | 320 | 315 | 311 | 306 | 301 | 296 |
| 382 | 380 | 377 | 374 | 370 | 367 | 363 | 358 | 354 | 349 | 345 | 340 | 334 | 329 | 324 |
| 414 | 412 | 409 | 405 | 402 | 398 | 393 | 389 | 384 | 379 | 373 | 368 | 362 | 357 | 351 |
| 446 | 443 | 440 | 436 | 432 | 428 | 423 | 418 | 413 | 408 | 402 | 396 | 390 | 384 | 378 |
| 478 | 475 | 471 | 467 | 463 | 458 | 453 | 448 | 442 | 436 | 430 | 424 | 417 | 411 | 404 |
| 509 | 506 | 502 | 498 | 493 | 488 | 483 | 477 | 471 | 465 | 458 | 451 | 444 | 437 | 430 |
| 243 | 242 | 241 | 239 | 238 | 236 | 234 | 232 | 230 | 228 | 225 | 223 | 221 | 218 | 215 |
| 282 | 281 | 279 | 278 | 276 | 274 | 272 | 269 | 267 | 264 | 262 | 259 | 256 | 253 | 250 |
| 321 | 319 | 318 | 316 | 314 | 311 | 309 | 306 | 303 | 300 | 297 | 294 | 291 | 287 | 284 |
| 359 | 357 | 356 | 353 | 351 | 348 | 346 | 343 | 340 | 336 | 333 | 329 | 325 | 321 | 317 |
| 397 | 395 | 393 | 391 | 388 | 385 | 382 | 379 | 375 | 372 | 368 | 364 | 359 | 355 | 351 |
| 435 | 433 | 430 | 428 | 425 | 421 | 418 | 414 | 411 | 406 | 402 | 398 | 393 | 388 | 384 |
| 472 | 470 | 467 | 464 | 461 | 457 | 454 | 450 | 446 | 441 | 436 | 432 | 427 | 421 | 416 |
| 509 | 506 | 503 | 500 | 497 | 493 | 489 | 485 | 480 | 475 | 470 | 465 | 459 | 454 | 448 |
| 545 | 542 | 539 | 536 | 532 | 528 | 524 | 519 | 514 | 509 | 504 | 498 | 492 | 486 | 480 |
| 581 | 578 | 575 | 571 | 567 | 563 | 558 | 553 | 548 | 542 | 537 | 531 | 524 | 518 | 511 |
| 617 | 613 | 610 | 606 | 602 | 597 | 592 | 587 | 581 | 575 | 569 | 563 | 556 | 549 | 542 |

**SAFE LOADS IN THOUSANDS OF POUNDS FOR
PLATE AND ANGLE COLUMNS. SQUARE ENDS.**
**CALCULATED FOR RADIUS OF GYRATION,
AXIS 2-2.**

Based on Gordon's Formula, $P = \frac{50\,000}{1 + \frac{(12\,L)^2}{36\,000\,r^2}}$
Safety factor 4.

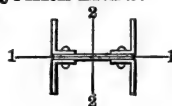


| Size of Angles. | Size of Plate. | Weight of Column. | Area of Column Section. | Least Radius of Gyrations Axis 1-1. | Radius of Gyrations Axis 2-2. | Length in Feet. | | |
|---------------------------|----------------------|-------------------------|----------------------------------|--|-------------------------------------|--------------------|-------|-------|
| Inches. | Inches. | Lbs. per Ft. | Sq. Ins. | Inches. | Inches. | 6 | 8 | 10 |
| 3 x 2½ x ¼ | 12 x ¼ | 28.2 | 8.24 | 1.12 | 4.87 | 103 | 102 | 101 |
| " " ⅜ | " " ⅜ | 35.2 | 10.23 | 1.15 | 4.85 | 127 | 126 | 126 |
| " " ½ | " " ½ | 41.7 | 12.18 | 1.17 | 4.83 | 151 | 151 | 150 |
| " " ⅝ | " " ⅝ | 48.3 | 14.13 | 1.20 | 4.81 | 175 | 174 | 173 |
| " " ¾ | " " ¾ | 54.4 | 16.00 | 1.23 | 4.78 | 199 | 198 | 197 |
| " " ⅞ | " " ⅞ | 61.0 | 17.87 | 1.26 | 4.76 | 222 | 221 | 219 |
| 3½ x 2½ x ¼ | 12 x ¼ | 29.8 | 8.76 | 1.35 | 4.94 | | 108 | 108 |
| " " ⅜ | " " ⅜ | 37.2 | 10.87 | 1.38 | 4.92 | | 134 | 134 |
| " " ½ | " " ½ | 44.1 | 12.94 | 1.41 | 4.90 | | 160 | 159 |
| " " ⅝ | " " ⅝ | 51.1 | 14.97 | 1.43 | 4.88 | | 185 | 184 |
| " " ¾ | " " ¾ | 58.0 | 17.00 | 1.46 | 4.85 | | 210 | 209 |
| " " ⅞ | " " ⅞ | 64.6 | 18.99 | 1.49 | 4.83 | | 235 | 233 |
| 4 - 3 x ⅜ | 14 x ⅜ | 43.7 | 12.74 | 1.54 | 5.72 | | 158 | 157 |
| " " ½ | " " ½ | 51.9 | 15.17 | 1.57 | 5.70 | | 188 | 188 |
| " " ¾ | " " ¾ | 60.0 | 17.61 | 1.60 | 5.68 | | 218 | 217 |
| " " ⅝ | " " ⅝ | 68.2 | 20.00 | 1.62 | 5.66 | | 248 | 247 |
| " " ¾ | " " ¾ | 76.4 | 22.36 | 1.65 | 5.63 | | 277 | 276 |
| " " ⅞ | " " ⅞ | 84.1 | 24.67 | 1.68 | 5.61 | | 306 | 305 |
| " " 1 | " " 1 | 91.9 | 26.99 | 1.71 | 5.59 | | 335 | 333 |
| " " 1¼ | " " 1¼ | 99.7 | 29.26 | 1.74 | 5.57 | | 363 | 361 |
| " " 1½ | " " 1½ | 107.1 | 31.50 | 1.77 | 5.55 | | 390 | 389 |
| " " 1¾ | " " 1¾ | 114.9 | 33.69 | 1.80 | 5.53 | | 418 | 416 |
| 5 x 3½ x ⅜ | 16 x ⅜ | 51.8 | 15.24 | 1.94 | 6.59 | | | 189 |
| " " ½ | " " ½ | 62.0 | 18.20 | 1.97 | 6.57 | | | 225 |
| " " ¾ | " " ¾ | 71.8 | 21.12 | 2.00 | 6.54 | | | 261 |
| " " ⅝ | " " ⅝ | 81.6 | 24.00 | 2.02 | 6.52 | | | 297 |
| " " ¾ | " " ¾ | 91.4 | 26.88 | 2.05 | 6.50 | | | 333 |
| " " ⅞ | " " ⅞ | 101.2 | 29.68 | 2.08 | 6.48 | | | 368 |
| " " 1 | " " 1 | 110.6 | 32.48 | 2.11 | 6.46 | | | 402 |
| " " 1¼ | " " 1¼ | 120.0 | 35.24 | 2.14 | 6.44 | | | 436 |
| " " 1½ | " " 1½ | 129.4 | 38.00 | 2.17 | 6.41 | | | 470 |
| " " 1¾ | " " 1¾ | 138.4 | 40.68 | 2.19 | 6.39 | | | 504 |
| " " 2 | " " 2 | 147.8 | 43.36 | 2.22 | 6.37 | | | 537 |
| 6 x 3½ x ¾ | 18 x ¾ | 69.8 | 20.43 | 2.42 | 7.49 | | | |
| " " 1 | " " 1 | 80.8 | 23.76 | 2.44 | 7.47 | | | |
| " " 1¼ | " " 1¼ | 91.8 | 27.00 | 2.47 | 7.45 | | | |
| " " 1½ | " " 1½ | 102.8 | 30.25 | 2.50 | 7.42 | | | |
| " " 1¾ | " " 1¾ | 113.9 | 33.45 | 2.52 | 7.40 | | | |
| " " 2 | " " 2 | 124.5 | 36.62 | 2.55 | 7.38 | | | |
| " " 2¼ | " " 2¼ | 135.5 | 39.74 | 2.58 | 7.36 | | | |
| " " 2½ | " " 2½ | 145.7 | 42.87 | 2.61 | 7.34 | | | |
| " " 2¾ | " " 2¾ | 156.4 | 45.95 | 2.64 | 7.32 | | | |
| " " 3 | " " 3 | 166.6 | 49.00 | 2.67 | 7.29 | | | |
| " " 3½ | " " 3½ | 176.8 | 52.00 | 2.70 | 7.27 | | | |

SAFE LOADS IN THOUSANDS OF POUNDS FOR PLATE AND ANGLE COLUMNS. SQUARE ENDS.

CALCULATED FOR RADIUS OF GYRATION,
AXIS 2-2.

Based on Gordon's Formula, $P = \frac{50\,000}{1 + \frac{(L)^2}{36\,000r^2}}$
Safety factor 4.



Length in Feet.

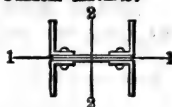
| 12 | 14 | 16 | 18 | 20 | 22 | 24 | 26 | 28 | 30 | 32 | 34 | 36 | 38 | 40 |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| 101 | 100 | 99 | 98 | 97 | 95 | 94 | 93 | 91 | 90 | 88 | 86 | 85 | 83 | 81 |
| 125 | 124 | 123 | 121 | 120 | 118 | 116 | 115 | 113 | 111 | 109 | 107 | 105 | 103 | 101 |
| 149 | 147 | 146 | 144 | 143 | 141 | 139 | 137 | 134 | 132 | 130 | 127 | 125 | 122 | 120 |
| 172 | 171 | 169 | 167 | 165 | 163 | 160 | 158 | 155 | 153 | 150 | 147 | 144 | 141 | 138 |
| 195 | 193 | 191 | 189 | 187 | 184 | 182 | 179 | 176 | 173 | 170 | 166 | 163 | 160 | 156 |
| 218 | 216 | 214 | 211 | 209 | 206 | 203 | 199 | 196 | 193 | 189 | 185 | 182 | 178 | 174 |
| 107 | 106 | 105 | 104 | 103 | 101 | 100 | 98 | 97 | 95 | 94 | 92 | 90 | 88 | 87 |
| 133 | 131 | 130 | 129 | 127 | 126 | 124 | 122 | 120 | 118 | 116 | 114 | 112 | 110 | 107 |
| 158 | 157 | 155 | 153 | 152 | 150 | 148 | 145 | 143 | 141 | 138 | 136 | 133 | 130 | 128 |
| 183 | 181 | 180 | 178 | 175 | 173 | 171 | 168 | 165 | 163 | 160 | 157 | 154 | 151 | 148 |
| 207 | 206 | 204 | 201 | 199 | 196 | 194 | 191 | 188 | 184 | 181 | 178 | 174 | 171 | 167 |
| 232 | 230 | 227 | 225 | 222 | 219 | 216 | 213 | 209 | 206 | 202 | 198 | 194 | 190 | 186 |
| 156 | 156 | 154 | 153 | 152 | 150 | 149 | 147 | 145 | 143 | 142 | 140 | 137 | 135 | 133 |
| 187 | 185 | 184 | 183 | 181 | 179 | 177 | 175 | 173 | 171 | 169 | 166 | 164 | 161 | 159 |
| 216 | 215 | 213 | 212 | 210 | 208 | 205 | 203 | 201 | 198 | 195 | 193 | 190 | 187 | 184 |
| 246 | 244 | 242 | 240 | 238 | 236 | 233 | 231 | 228 | 225 | 222 | 218 | 215 | 212 | 208 |
| 275 | 273 | 271 | 269 | 266 | 263 | 261 | 258 | 254 | 251 | 248 | 244 | 240 | 236 | 233 |
| 303 | 301 | 299 | 296 | 294 | 291 | 288 | 284 | 281 | 277 | 273 | 269 | 265 | 261 | 257 |
| 331 | 329 | 327 | 324 | 321 | 318 | 314 | 311 | 307 | 303 | 298 | 294 | 289 | 285 | 280 |
| 359 | 357 | 354 | 351 | 348 | 344 | 340 | 336 | 332 | 328 | 323 | 318 | 313 | 308 | 303 |
| 386 | 384 | 381 | 378 | 374 | 370 | 366 | 362 | 357 | 352 | 347 | 342 | 337 | 331 | 326 |
| 413 | 411 | 407 | 404 | 400 | 396 | 392 | 387 | 382 | 377 | 371 | 366 | 360 | 354 | 348 |
| 188 | 187 | 186 | 185 | 184 | 182 | 181 | 179 | 178 | 176 | 174 | 172 | 170 | 168 | 166 |
| 224 | 223 | 222 | 221 | 219 | 218 | 216 | 214 | 212 | 210 | 208 | 205 | 203 | 201 | 198 |
| 260 | 259 | 258 | 256 | 254 | 252 | 250 | 248 | 246 | 243 | 241 | 238 | 235 | 233 | 230 |
| 296 | 295 | 293 | 291 | 289 | 287 | 285 | 282 | 279 | 277 | 274 | 271 | 267 | 264 | 261 |
| 331 | 330 | 328 | 326 | 324 | 321 | 318 | 316 | 313 | 309 | 306 | 303 | 299 | 295 | 292 |
| 366 | 364 | 362 | 360 | 357 | 355 | 352 | 349 | 345 | 342 | 338 | 334 | 330 | 326 | 322 |
| 400 | 399 | 396 | 394 | 391 | 388 | 385 | 381 | 378 | 374 | 370 | 365 | 361 | 357 | 352 |
| 435 | 432 | 430 | 427 | 424 | 421 | 417 | 414 | 410 | 405 | 401 | 396 | 392 | 387 | 382 |
| 468 | 466 | 463 | 460 | 457 | 453 | 450 | 445 | 441 | 437 | 432 | 427 | 422 | 416 | 411 |
| 502 | 499 | 496 | 493 | 489 | 486 | 481 | 477 | 472 | 467 | 462 | 457 | 451 | 446 | 440 |
| 534 | 532 | 529 | 525 | 521 | 517 | 513 | 508 | 503 | 498 | 492 | 487 | 481 | 475 | 468 |
| 253 | 252 | 251 | 250 | 248 | 247 | 245 | 244 | 242 | 240 | 238 | 236 | 234 | 232 | 229 |
| 294 | 293 | 291 | 290 | 288 | 287 | 285 | 283 | 281 | 279 | 276 | 274 | 272 | 269 | 266 |
| 334 | 333 | 331 | 330 | 328 | 326 | 324 | 322 | 319 | 317 | 314 | 312 | 309 | 306 | 303 |
| 374 | 373 | 371 | 369 | 367 | 365 | 363 | 360 | 358 | 355 | 352 | 349 | 346 | 342 | 339 |
| 414 | 412 | 410 | 408 | 406 | 404 | 401 | 398 | 395 | 392 | 389 | 385 | 382 | 378 | 374 |
| 453 | 451 | 449 | 447 | 445 | 442 | 439 | 436 | 433 | 429 | 426 | 422 | 418 | 414 | 410 |
| 492 | 490 | 488 | 485 | 483 | 480 | 477 | 473 | 470 | 466 | 462 | 458 | 453 | 449 | 444 |
| 530 | 528 | 526 | 523 | 520 | 517 | 514 | 510 | 506 | 502 | 498 | 493 | 489 | 484 | 479 |
| 568 | 566 | 563 | 561 | 558 | 554 | 551 | 547 | 542 | 538 | 533 | 529 | 524 | 518 | 513 |
| 606 | 603 | 601 | 598 | 595 | 591 | 587 | 583 | 578 | 574 | 569 | 563 | 558 | 552 | 547 |
| 643 | 641 | 638 | 634 | 631 | 627 | 623 | 618 | 614 | 609 | 603 | 598 | 592 | 586 | 580 |

SAFE LOADS IN THOUSANDS OF POUNDS FOR PLATE AND ANGLE COLUMNS. SQUARE ENDS.

CALCULATED FOR RADIUS OF GYRATION,
AXIS 2-2.

Based on Gordon's Formula, $P = \frac{50\,000}{1 + \frac{(12 L)^2}{36\,000 r^2}}$

Safety factor 4.



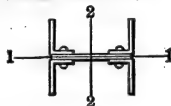
| Size of Angles. | Size of Plate. | Weight of Column. | Area of Column Section. | Least Radius of Gyration Axis 1-1. | Radius of Gyration Axis 2-2. | Length in Feet. | |
|-------------------|----------------|-------------------|-------------------------|------------------------------------|------------------------------|-----------------|------|
| Inches. | Inches. | Lbs. per Ft. | Sq. Ins. | Inches. | Inches. | 10 | 12 |
| 7 x 3½ x ⅞ | 14 x ⅞ | 80.8 | 23.73 | 3.05 | 5.92 | 293 | 292 |
| " " ⅞ | " " ⅞ | 91.8 | 27.00 | 3.08 | 5.90 | 334 | 332 |
| " " ⅞ | " " ⅞ | 103.2 | 30.24 | 3.11 | 5.87 | 374 | 372 |
| " " ⅞ | " " ⅞ | 113.7 | 33.43 | 3.13 | 5.85 | 413 | 411 |
| " " ⅞ | " " ⅞ | 124.7 | 36.63 | 3.17 | 5.83 | 452 | 450 |
| " " ⅞ | " " ⅞ | 135.3 | 39.74 | 3.20 | 5.81 | 491 | 489 |
| " " ⅞ | " " ⅞ | 145.9 | 42.86 | 3.23 | 5.79 | 529 | 527 |
| " " ⅞ | " " ⅞ | 156.5 | 45.93 | 3.26 | 5.76 | 567 | 564 |
| " " ⅞ | " " ⅞ | 166.6 | 49.01 | 3.29 | 5.74 | 605 | 602 |
| " " 1 | " " 1 | 176.8 | 52.00 | 3.32 | 5.72 | 642 | 639 |
| 7 x 3½ x ⅞ | 16 x ⅞ | 83.8 | 24.60 | 3.00 | 6.75 | | 304 |
| " " ⅞ | " " ⅞ | 95.2 | 28.00 | 3.02 | 6.73 | | 346 |
| " " ⅞ | " " ⅞ | 107.0 | 31.36 | 3.06 | 6.71 | | 387 |
| " " ⅞ | " " ⅞ | 118.0 | 34.68 | 3.08 | 6.69 | | 428 |
| " " ⅞ | " " ⅞ | 129.4 | 38.00 | 3.11 | 6.67 | | 469 |
| " " ⅞ | " " ⅞ | 140.4 | 41.24 | 3.14 | 6.64 | | 509 |
| " " ⅞ | " " ⅞ | 151.4 | 44.48 | 3.17 | 6.62 | | 549 |
| " " ⅞ | " " ⅞ | 162.4 | 47.68 | 3.20 | 6.60 | | 588 |
| " " ⅞ | " " ⅞ | 173.0 | 50.88 | 3.23 | 6.58 | | 627 |
| " " 1 | " " 1 | 183.6 | 54.00 | 3.26 | 6.56 | | 666 |
| 7 x 3½ x ⅞ | 18 x ⅞ | 86.8 | 25.48 | 2.94 | 7.58 | | 315 |
| " " ⅞ | " " ⅞ | 98.6 | 29.00 | 2.97 | 7.55 | | 359 |
| " " ⅞ | " " ⅞ | 110.8 | 32.49 | 3.00 | 7.53 | | 402 |
| " " ⅞ | " " ⅞ | 122.3 | 35.93 | 3.02 | 7.51 | | 445 |
| " " ⅞ | " " ⅞ | 134.1 | 39.38 | 3.06 | 7.49 | | 487 |
| " " ⅞ | " " ⅞ | 145.5 | 42.74 | 3.08 | 7.47 | | 529 |
| " " ⅞ | " " ⅞ | 156.9 | 46.11 | 3.11 | 7.44 | | 570 |
| " " ⅞ | " " ⅞ | 168.4 | 49.43 | 3.14 | 7.42 | | 612 |
| " " ⅞ | " " ⅞ | 179.4 | 52.76 | 3.17 | 7.40 | | 652 |
| " " 1 | " " 1 | 190.4 | 56.00 | 3.20 | 7.38 | | 693 |
| 7 x 3½ x ⅞ | 20 x ⅞ | 89.8 | 26.35 | 2.89 | 8.39 | | |
| " " ⅞ | " " ⅞ | 102.0 | 30.00 | 2.92 | 8.37 | | |
| " " ⅞ | " " ⅞ | 114.7 | 33.61 | 2.95 | 8.34 | | |
| " " ⅞ | " " ⅞ | 126.5 | 37.18 | 2.97 | 8.32 | | |
| " " ⅞ | " " ⅞ | 138.7 | 40.75 | 3.00 | 8.30 | | |
| " " ⅞ | " " ⅞ | 150.6 | 44.24 | 3.03 | 8.28 | | |
| " " ⅞ | " " ⅞ | 162.5 | 47.73 | 3.06 | 8.25 | | |
| " " ⅞ | " " ⅞ | 174.3 | 51.18 | 3.09 | 8.23 | | |
| " " ⅞ | " " ⅞ | 185.8 | 54.63 | 3.12 | 8.21 | | |
| " " 1 | " " 1 | 197.2 | 58.00 | 3.15 | 8.19 | | |

SAFE LOADS IN THOUSANDS OF POUNDS FOR PLATE AND ANGLE COLUMNS. SQUARE ENDS.

CALCULATED FOR RADIUS OF GYRATION,
AXIS 2-2.

Based on Gordon's Formula, $P = \frac{50\,000}{1 + \frac{(12\,L)^2}{36\,000\,r^2}}$

Safety factor 4.



Length in Feet.

| 14 | 16 | 18 | 20 | 22 | 24 | 26 | 28 | 30 | 32 | 34 | 36 | 38 | 40 |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| 290 | 288 | 286 | 284 | 281 | 278 | 275 | 272 | 269 | 266 | 262 | 258 | 255 | 251 |
| 330 | 328 | 325 | 323 | 320 | 317 | 313 | 310 | 306 | 302 | 298 | 294 | 289 | 285 |
| 370 | 367 | 364 | 361 | 358 | 354 | 351 | 347 | 342 | 338 | 333 | 329 | 324 | 319 |
| 409 | 406 | 403 | 399 | 396 | 392 | 387 | 383 | 378 | 373 | 368 | 363 | 358 | 352 |
| 447 | 444 | 441 | 437 | 433 | 429 | 424 | 419 | 414 | 408 | 403 | 397 | 391 | 385 |
| 486 | 482 | 478 | 474 | 470 | 465 | 460 | 455 | 449 | 443 | 437 | 431 | 424 | 418 |
| 523 | 520 | 516 | 511 | 506 | 501 | 496 | 490 | 484 | 477 | 471 | 464 | 457 | 450 |
| 561 | 557 | 553 | 548 | 543 | 537 | 531 | 525 | 518 | 511 | 504 | 497 | 489 | 482 |
| 598 | 594 | 589 | 584 | 578 | 572 | 566 | 559 | 552 | 545 | 537 | 529 | 521 | 513 |
| 635 | 630 | 625 | 620 | 614 | 607 | 600 | 593 | 586 | 578 | 570 | 561 | 553 | 544 |
| | | | | | | | | | | | | | |
| 302 | 301 | 299 | 297 | 295 | 293 | 290 | 288 | 285 | 282 | 279 | 276 | 273 | 270 |
| 344 | 342 | 340 | 338 | 336 | 333 | 330 | 327 | 324 | 321 | 318 | 314 | 310 | 307 |
| 385 | 383 | 381 | 379 | 376 | 373 | 370 | 366 | 363 | 359 | 355 | 352 | 347 | 343 |
| 426 | 424 | 421 | 419 | 416 | 412 | 409 | 405 | 401 | 397 | 393 | 389 | 384 | 379 |
| 467 | 464 | 461 | 458 | 455 | 451 | 448 | 443 | 439 | 435 | 430 | 425 | 420 | 415 |
| 507 | 504 | 501 | 498 | 494 | 490 | 486 | 481 | 477 | 472 | 467 | 461 | 456 | 450 |
| 546 | 543 | 540 | 536 | 532 | 528 | 524 | 519 | 514 | 509 | 503 | 497 | 491 | 485 |
| 586 | 582 | 579 | 575 | 571 | 566 | 561 | 556 | 551 | 545 | 539 | 533 | 526 | 520 |
| 624 | 621 | 617 | 613 | 609 | 604 | 598 | 593 | 587 | 581 | 574 | 568 | 561 | 554 |
| 663 | 659 | 655 | 651 | 646 | 641 | 635 | 629 | 623 | 616 | 609 | 602 | 595 | 588 |
| | | | | | | | | | | | | | |
| 314 | 313 | 312 | 310 | 308 | 306 | 304 | 302 | 300 | 297 | 295 | 292 | 290 | 287 |
| 358 | 356 | 354 | 353 | 351 | 348 | 346 | 344 | 341 | 338 | 335 | 332 | 329 | 326 |
| 401 | 399 | 397 | 395 | 393 | 390 | 388 | 385 | 382 | 379 | 376 | 372 | 369 | 365 |
| 443 | 441 | 439 | 437 | 434 | 432 | 429 | 426 | 422 | 419 | 415 | 411 | 408 | 403 |
| 485 | 483 | 481 | 478 | 476 | 473 | 469 | 466 | 462 | 459 | 455 | 450 | 446 | 442 |
| 527 | 525 | 522 | 519 | 516 | 513 | 510 | 506 | 502 | 498 | 493 | 489 | 484 | 479 |
| 568 | 566 | 563 | 560 | 557 | 553 | 550 | 546 | 541 | 537 | 532 | 527 | 522 | 517 |
| 609 | 607 | 604 | 601 | 597 | 593 | 589 | 585 | 580 | 575 | 570 | 565 | 559 | 554 |
| 650 | 647 | 644 | 641 | 637 | 633 | 628 | 624 | 619 | 613 | 608 | 602 | 596 | 590 |
| 690 | 687 | 684 | 680 | 676 | 672 | 667 | 662 | 657 | 651 | 645 | 639 | 633 | 626 |
| | | | | | | | | | | | | | |
| 326 | 325 | 324 | 322 | 321 | 319 | 317 | 315 | 313 | 311 | 309 | 307 | 305 | 302 |
| 371 | 370 | 368 | 367 | 365 | 363 | 361 | 359 | 357 | 354 | 352 | 349 | 346 | 344 |
| 415 | 414 | 412 | 411 | 409 | 407 | 404 | 402 | 399 | 397 | 394 | 391 | 388 | 385 |
| 460 | 458 | 456 | 454 | 452 | 450 | 447 | 445 | 442 | 439 | 436 | 432 | 429 | 426 |
| 503 | 502 | 500 | 498 | 495 | 493 | 490 | 487 | 484 | 481 | 477 | 473 | 470 | 466 |
| 547 | 545 | 543 | 541 | 538 | 535 | 532 | 529 | 526 | 522 | 518 | 514 | 510 | 506 |
| 590 | 588 | 585 | 583 | 580 | 577 | 574 | 570 | 567 | 563 | 559 | 554 | 550 | 545 |
| 633 | 630 | 628 | 625 | 622 | 619 | 615 | 612 | 608 | 603 | 599 | 594 | 590 | 585 |
| 675 | 672 | 670 | 667 | 664 | 660 | 656 | 652 | 648 | 644 | 639 | 634 | 629 | 623 |
| 717 | 714 | 711 | 708 | 705 | 701 | 697 | 693 | 688 | 683 | 678 | 673 | 667 | 662 |

SAFE LOADS IN THOUSANDS OF POUNDS FOR LATTICED CHANNEL COLUMNS. SQUARE ENDS.

Based on Gordon's Formula $P = \frac{50\,000}{1 + \frac{(12 L)^2}{36\,000 r^2}}$ Safety factor 4.



| Depth of Channel. | Weight of each Channel. | Area of Column Section. | Least Radius of Gyration. | Length in Feet. | | | | | |
|-------------------------|-------------------------------|-------------------------------|---------------------------------|-----------------|------|-----|-----|-----|-----|
| | | | | 4 | 6 | 8 | 10 | 12 | 14 |
| Inches. | Lbs. per Foot. | Sq. Ins. | Inches. | | | | | | |
| 6 | 8.0 | 4.76 | 2.34 | 59 | 58 | 57 | 55 | 54 | 52 |
| " | 10.5 | 6.18 | 2.21 | 76 | 75 | 73 | 71 | 69 | 67 |
| " | 13.0 | 7.64 | 2.13 | 94 | 93 | 90 | 88 | 85 | 81 |
| " | 15.5 | 9.12 | 2.06 | 112 | 110 | 107 | 104 | 100 | 96 |
| 7 | 9.75 | 5.70 | 2.72 | 71 | 70 | 69 | 68 | 66 | 65 |
| " | 12.25 | 7.20 | 2.59 | 89 | 88 | 87 | 85 | 83 | 81 |
| " | 14.75 | 8.68 | 2.50 | 107 | 106 | 104 | 102 | 99 | 96 |
| " | 17.25 | 10.14 | 2.44 | 125 | 124 | 121 | 119 | 116 | 112 |
| " | 19.75 | 11.62 | 2.39 | 144 | 142 | 139 | 136 | 132 | 128 |
| 8 | 11.25 | 6.70 | 3.11 | 83 | 83 | 82 | 80 | 79 | 77 |
| " | 13.75 | 8.08 | 2.99 | 100 | 99 | 98 | 97 | 95 | 93 |
| " | 16.25 | 9.56 | 2.89 | 119 | 117 | 116 | 114 | 112 | 109 |
| " | 18.75 | 11.02 | 2.82 | 137 | 135 | 134 | 131 | 128 | 125 |
| " | 21.25 | 12.50 | 2.77 | 155 | 153 | 151 | 149 | 145 | 142 |
| 9 | 13.25 | 7.78 | 3.45 | | 96 | 95 | 94 | 93 | 91 |
| " | 15.00 | 8.82 | 3.37 | | 109 | 108 | 107 | 105 | 103 |
| " | 20.00 | 11.76 | 3.20 | | 145 | 143 | 142 | 139 | 137 |
| " | 25.00 | 14.70 | 3.08 | | 181 | 179 | 177 | 173 | 170 |
| 10 | 15.0 | 8.92 | 3.84 | | 110 | 110 | 109 | 107 | 106 |
| " | 20.0 | 11.76 | 3.66 | | 146 | 144 | 143 | 141 | 139 |
| " | 25.0 | 14.70 | 3.52 | | 182 | 180 | 178 | 176 | 173 |
| " | 30.0 | 17.64 | 3.41 | | 218 | 216 | 213 | 210 | 207 |
| " | 35.0 | 20.58 | 3.31 | | 254 | 251 | 248 | 245 | 240 |
| 12 | 20.5 | 12.06 | 4.61 | | | 149 | 148 | 147 | 146 |
| " | 25.0 | 14.70 | 4.43 | | | 181 | 180 | 179 | 177 |
| " | 30.0 | 17.64 | 4.28 | | | 217 | 216 | 214 | 211 |
| " | 35.0 | 20.58 | 4.17 | | | 254 | 251 | 249 | 246 |
| " | 40.0 | 23.52 | 4.09 | | | 289 | 287 | 284 | 281 |
| 15 | 33.0 | 19.80 | 5.59 | | | 246 | 244 | 243 | 241 |
| " | 35.0 | 20.58 | 5.56 | | | 255 | 254 | 252 | 251 |
| " | 40.0 | 23.52 | 5.44 | | | 291 | 290 | 288 | 286 |
| " | 45.0 | 26.48 | 5.32 | | | 328 | 326 | 324 | 322 |
| " | 50.0 | 29.42 | 5.23 | | | 364 | 363 | 360 | 357 |
| " | 55.0 | 32.36 | 5.16 | | | 400 | 399 | 396 | 393 |

For detail dimensions see page 230

SAFE LOADS IN THOUSANDS OF POUNDS FOR LATTICED CHANNEL COLUMNS. SQUARE ENDS.

Based on Gordon's Formula $P = \frac{50\,000}{1 + \frac{(12 L)^2}{36\,000 r^2}}$ Safety factor 4.



| Length in Feet. | | | | | | | | Weight of each Channel. | Depth of Channels. |
|-----------------|-----|-----|-----|-----|------|------|------|-------------------------------|--------------------------|
| 16 | 18 | 20 | 22 | 24 | 26 | 28 | 30 | Lbs. per Foot. | Inches. |
| 50 | 48 | 46 | 44 | 42 | | | | 8.0 | 6 |
| 64 | 61 | 58 | 55 | 52 | | | | 10.5 | " |
| 78 | 74 | 71 | 67 | 63 | | | | 13.0 | " |
| 92 | 88 | 83 | 78 | 74 | | | | 15.5 | " |
| 63 | 61 | 58 | 56 | 54 | 52 | | | 9.75 | 7 |
| 78 | 76 | 73 | 70 | 67 | 64 | | | 12.25 | " |
| 93 | 90 | 86 | 83 | 79 | 76 | | | 14.75 | " |
| 108 | 104 | 100 | 96 | 92 | 87 | | | 17.25 | " |
| 123 | 119 | 113 | 108 | 104 | 98 | | | 19.75 | " |
| 76 | 74 | 72 | 70 | 68 | 65 | 63 | 61 | 11.25 | 8 |
| 90 | 88 | 86 | 83 | 80 | 78 | 75 | 72 | 13.75 | " |
| 107 | 104 | 100 | 97 | 94 | 90 | 87 | 83 | 16.25 | " |
| 122 | 118 | 115 | 111 | 107 | 103 | 99 | 95 | 18.75 | " |
| 138 | 134 | 129 | 124 | 120 | 115 | 111 | 106 | 21.25 | " |
| 90 | 88 | 86 | 84 | 82 | 80 | 77 | 75 | 13.25 | 9 |
| 101 | 99 | 97 | 94 | 92 | 90 | 87 | 84 | 15.00 | " |
| 134 | 131 | 127 | 124 | 120 | 116 | 113 | 109 | 20.00 | " |
| 166 | 162 | 157 | 153 | 149 | 143 | 139 | 134 | 25.00 | " |
| 104 | 102 | 101 | 99 | 97 | 95 | 93 | 90 | 15.0 | 10 |
| 136 | 134 | 131 | 128 | 125 | 122 | 119 | 116 | 20.0 | " |
| 170 | 166 | 163 | 159 | 155 | 151 | 146 | 143 | 25.0 | " |
| 203 | 198 | 194 | 189 | 185 | 179 | 174 | 168 | 30.0 | " |
| 236 | 230 | 225 | 219 | 213 | 207 | 201 | 194 | 35.0 | " |
| 144 | 142 | 140 | 138 | 136 | 134 | 131 | 129 | 20.5 | 12 |
| 175 | 172 | 170 | 167 | 165 | 161 | 159 | 155 | 25.0 | " |
| 209 | 206 | 203 | 200 | 196 | 192 | 187 | 184 | 30.0 | " |
| 243 | 240 | 236 | 231 | 227 | 223 | 218 | 213 | 35.0 | " |
| 277 | 273 | 268 | 263 | 258 | 253 | 248 | 243 | 40.0 | " |
| 240 | 238 | 235 | 233 | 230 | 228 | 225 | 222 | 33.0 | 15 |
| 249 | 247 | 245 | 242 | 240 | 236 | 234 | 230 | 35.0 | " |
| 284 | 282 | 279 | 276 | 273 | 269 | 266 | 262 | 40.0 | " |
| 319 | 316 | 313 | 310 | 306 | 302 | 298 | 294 | 45.0 | " |
| 354 | 352 | 348 | 344 | 339 | 334 | 329 | 325 | 50.0 | " |
| 390 | 386 | 381 | 377 | 372 | 368 | 362 | 357 | 55.0 | " |

For detail dimensions see page 230

SAFE LOADS IN THOUSANDS OF POUNDS FOR LATTICED CHANNEL COLUMNS. SQUARE ENDS.

Based on Gordon's Formula $P = \frac{50\,000}{1 + \frac{(12L)^2}{36\,000r^2}}$ Safety factor 4.



| Depth of Channels. | Weight of each Channel. | Area of Column Section. | Least Radius of Gyration. | Length in Feet. | | | | |
|--------------------------|-------------------------------|-------------------------------|---------------------------------|-----------------|-----|-------|-------|-------|
| | | | | 32 | 34 | 36 | 38 | 40 |
| Inches. | Lbs. per Foot. | Sq. Ins. | Inches. | | | | | |
| 9 | 13.25 | 7.78 | 3.45 | 73 | 71 | | | |
| " | 15.00 | 8.82 | 3.37 | 81 | 79 | | | |
| " | 20.00 | 11.76 | 3.20 | 106 | 101 | | | |
| " | 25.00 | 14.70 | 3.08 | 129 | 124 | | | |
| 10 | 15.0 | 8.92 | 3.84 | 87 | 85 | 83 | | |
| " | 20.0 | 11.76 | 3.66 | 113 | 109 | 106 | | |
| " | 25.0 | 14.70 | 3.52 | 138 | 134 | 130 | | |
| " | 30.0 | 17.64 | 3.41 | 163 | 158 | 153 | | |
| " | 35.0 | 20.58 | 3.31 | 188 | 183 | 176 | | |
| 12 | 20.5 | 12.06 | 4.61 | 127 | 124 | 121 | 119 | 116 |
| " | 25.0 | 14.70 | 4.43 | 152 | 149 | 146 | 142 | 139 |
| " | 30.0 | 17.64 | 4.28 | 180 | 176 | 172 | 167 | 164 |
| " | 35.0 | 20.58 | 4.17 | 208 | 203 | 199 | 193 | 188 |
| " | 40.0 | 23.52 | 4.09 | 236 | 231 | 224 | 218 | 212 |
| 15 | 33.0 | 19.80 | 5.59 | 219 | 215 | 213 | 209 | 206 |
| " | 35.0 | 20.58 | 5.56 | 228 | 224 | 220 | 217 | 213 |
| " | 40.0 | 23.52 | 5.44 | 258 | 254 | 250 | 246 | 241 |
| " | 45.0 | 26.48 | 5.32 | 289 | 284 | 279 | 275 | 270 |
| " | 50.0 | 29.42 | 5.23 | 320 | 315 | 309 | 303 | 299 |
| " | 55.0 | 32.36 | 5.16 | 351 | 344 | 338 | 332 | 325 |

For detail dimensions see page 230.

SAFE LOADS IN THOUSANDS OF POUNDS FOR LATTICED CHANNEL COLUMNS. SQUARE ENDS.

Based on Gordon's Formula $P = \frac{50\,000}{1 + \frac{(12 L)^2}{36\,000 r^2}}$ Safety factor 4.



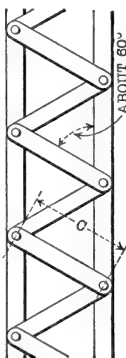
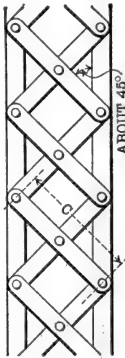
| Length in Feet. | | | | | | | Weight of each Channel. | Depth of Channels. |
|-----------------|-------|-------|-------|-------|-------|-------|-------------------------------|--------------------------|
| 42 | 44 | 46 | 48 | 50 | 52 | 54 | Lbs. per Foot. | Inches. |
| | | | | | | | 13.25 | 9 |
| | | | | | | | 15.00 | " |
| | | | | | | | 20.00 | " |
| | | | | | | | 25.00 | " |
| | | | | | | | 15.0 | 10 |
| | | | | | | | 20.0 | " |
| | | | | | | | 25.0 | " |
| | | | | | | | 30.0 | " |
| | | | | | | | 35.0 | " |
| 113 | 111 | 108 | | | | | 20.5 | 12 |
| 135 | 132 | 128 | | | | | 25.0 | " |
| 159 | 155 | 151 | | | | | 30.0 | " |
| 183 | 178 | 173 | | | | | 35.0 | " |
| 206 | 200 | 196 | | | | | 40.0 | " |
| 202 | 199 | 195 | 192 | 188 | 184 | 181 | 33.0 | 15 |
| 210 | 206 | 203 | 199 | 194 | 191 | 187 | 35.0 | " |
| 238 | 233 | 228 | 224 | 220 | 215 | 211 | 40.0 | " |
| 265 | 260 | 255 | 250 | 245 | 239 | 234 | 45.0 | " |
| 293 | 287 | 281 | 275 | 269 | 264 | 258 | 50.0 | " |
| 319 | 314 | 307 | 301 | 294 | 287 | 281 | 55.0 | " |

For detail dimensions see page 230.

SIZE OF SINGLE LATTICE BARS TO BE USED WITH LATTICED CHANNEL COLUMNS.

| Depth of Channels. | Dimensions of Lattice Bars. | | Weight of Lattice Bars per Foot. | Center of Hole to End of Bar. (a) | Distance Center to Center of Rivets. (d) | |
|--------------------|-----------------------------|------------|----------------------------------|-----------------------------------|--|----------|
| | W | Thickness. | | | Maximum. | Minimum. |
| Inches. | Inches. | Inch. | Pounds. | Inch. | Inches. | Inches. |
| 6 | 1¾ | ¼ | 1.49 | 1⅝ | 10 | 6⅝ |
| 7 | 2 | ¼ | 1.70 | 1¾ | 10 | 7⅝ |
| 8 | 2 | ⅝ | 2.12 | 1¾ | 12½ | 8¼ |
| 9 | 2¼ | ⅝ | 2.39 | 1¾ | 12½ | 9½ |
| 10 | 2¼ | ⅝ | 2.87 | 1¾ | 15 | 10¼ |
| 12 | 2¼ | ⅝ | 2.87 | 1¾ | 15 | 13 |
| 15 | 2½ | ⅝ | 3.72 | 1½ | 17½ | 15⅝ |

MAXIMUM LENGTHS OF LATTICE BARS BETWEEN FLANGE RIVET CENTERS FOR DIFFERENT BAR THICKNESSES.

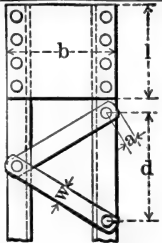
|  | Thickness of Lattice Bar. | Maximum Length (C) | |
|--|---------------------------|--------------------|-----------------|
| | | Single Lattice. | Double Lattice. |
| | Inch. | Inches. | Inches. |
|  | ¼ | 10 | 15 |
| | ⅝ | 12½ | 18¾ |
| | ⅜ | 15 | 22½ |
| | ⅞ | 17½ | 26¼ |
| | ½ | 20 | 30 |
| | ⅞ | 22½ | 33¾ |
| | ⅝ | 25 | 37½ |

Latticing should be so proportioned to resist a shearing stress, 2% of direct stress.

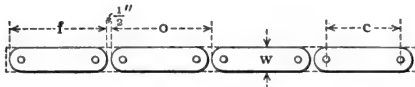
Inclination of lattice bars to axis of member should not be less than 45 degrees Where distance between lines of flange rivets exceeds 15 inches, if single rivet bars be used, lattice should be double.

Pitch of lattice rivets along flange divided by least radius of gyration of the member between connections should be less than corresponding ratio of the member as a whole.

SIZE OF STAY PLATES TO BE USED WITH LATTICE CHANNEL COLUMNS.

| Minimum size of Stay Plates at Ends of Columns. | | | Weight of Minimum Stay Plate. | Diameter of Rivets. |  |
|---|------------|---------|-------------------------------|---------------------|---|
| b | Thickness. | l | | | |
| Inches. | Inch. | Inches. | Pounds. | Inch. | |
| 7½ | ¼ | 5¾ | 3.06 | 5/8 | |
| 8½ | ¼ | 6¾ | 4.07 | 5/8, ¾ | |
| 9½ | ¼ | 7½ | 5.12 | 5/8, ¾ | |
| 10¾ | ¼ | 8½ | 6.07 | 5/8, ¾ | |
| 11½ | ¼ | 9¼ | 7.54 | 5/8, ¾ | |
| 13½ | ¼ | 11¼ | 10.86 | 5/8, ¾ | |
| 16¼ | ⅝ | 13¼ | 19.07 | ¾, 7/8 | |

DISTANCES TO BE ADDED TO LENGTHS OF LATTICE BARS BETWEEN FLANGE RIVET CENTERS TO GIVE FULL LENGTHS.



| Width of Bar. w | Add to Length c | | | | | | | |
|--------------------|------------------------|-------|-------|-------|-----------------------|-------|-------|-------|
| | For Finished Length f. | | | | For Ordered Length o. | | | |
| | Rivet Diameter. | | | | Rivet Diameter. | | | |
| | 1/2 | 5/8 | 3/4 | 7/8 | 1/2 | 5/8 | 3/4 | 7/8 |
| Ins. | Ins. | Ins. | Ins. | Ins. | Ins. | Ins. | Ins. | Ins. |
| 1½ | 2 | 2¼ | | | 2½ | 2¾ | 3 | 3½ |
| 1¾ | | 2½ | 2½ | | | 3 | 3 | 3½ |
| 2 | | 2½ | 2½ | | | 3 | 3 | 3½ |
| 2¼ | | | 3 | 3 | | | 3½ | 3½ |
| 2½ | | | 3 | 3 | | | 3½ | 3½ |
| 2¾ | | | 3½ | 3½ | | | 4 | 4 |
| 3 | | | | | | | | |

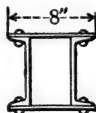
Length of end stay plates should be not less than distance between lines of flange rivets.

Length of intermediate stay plates should be not less than one-half same distance.

Thickness of stay plates should be not less than 1/50 same distance.

SAFE LOADS IN THOUSANDS OF POUNDS FOR 6" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula $P = \frac{50\,000}{1 + \frac{(12 L)^2}{36\,000 r^2}}$. Safety factor 4.



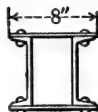
SERIES A.

| Weight of each Channel. | Thickness of Plates. | Weight of Column. | Area of Column Section. | Least Radius of Gyrations. | Length in Feet. | | | |
|-------------------------------|----------------------------|-------------------------|-------------------------------|----------------------------------|-----------------|-----|-----|-----|
| Lbs. per Foot. | Inch. | Lbs. per Ft. | Sq. Ins. | Inches. | 4 | 6 | 8 | 10 |
| 8 | $\frac{1}{4}$ | 29.6 | 8.76 | 2.35 | 108 | 107 | 105 | 102 |
| " | $\frac{5}{16}$ | 33.0 | 9.76 | 2.35 | 121 | 119 | 117 | 114 |
| " | $\frac{3}{8}$ | 36.4 | 10.76 | 2.34 | 133 | 131 | 129 | 125 |
| " | $\frac{7}{16}$ | 39.8 | 11.76 | 2.34 | 145 | 143 | 141 | 137 |
| " | $\frac{1}{2}$ | 43.2 | 12.76 | 2.34 | 158 | 155 | 152 | 149 |
| " | $\frac{5}{8}$ | 46.6 | 13.76 | 2.34 | 170 | 167 | 164 | 160 |
| " | $\frac{3}{4}$ | 50.0 | 14.76 | 2.33 | 182 | 180 | 176 | 172 |
| 10.5 | $\frac{1}{4}$ | 34.6 | 10.18 | 2.27 | 126 | 124 | 121 | 118 |
| " | $\frac{5}{16}$ | 38.0 | 11.18 | 2.27 | 138 | 136 | 133 | 130 |
| " | $\frac{3}{8}$ | 41.4 | 12.18 | 2.28 | 150 | 148 | 145 | 141 |
| " | $\frac{7}{16}$ | 44.8 | 13.18 | 2.28 | 163 | 160 | 157 | 153 |
| " | $\frac{1}{2}$ | 48.2 | 14.18 | 2.28 | 175 | 173 | 169 | 165 |
| " | $\frac{5}{8}$ | 51.6 | 15.18 | 2.28 | 187 | 185 | 181 | 176 |
| " | $\frac{3}{4}$ | 55.0 | 16.18 | 2.28 | 200 | 197 | 193 | 188 |
| 13 | $\frac{1}{4}$ | 39.6 | 11.64 | 2.20 | 144 | 141 | 138 | 135 |
| " | $\frac{5}{16}$ | 43.0 | 12.64 | 2.21 | 156 | 154 | 150 | 146 |
| " | $\frac{3}{8}$ | 46.4 | 13.64 | 2.22 | 168 | 166 | 162 | 158 |
| " | $\frac{7}{16}$ | 49.8 | 14.64 | 2.23 | 181 | 178 | 174 | 169 |
| " | $\frac{1}{2}$ | 53.2 | 15.64 | 2.23 | 193 | 190 | 186 | 181 |
| " | $\frac{5}{8}$ | 56.6 | 16.64 | 2.24 | 205 | 202 | 198 | 192 |
| " | $\frac{3}{4}$ | 60.0 | 17.64 | 2.24 | 218 | 214 | 210 | 204 |
| 15.5 | $\frac{1}{4}$ | 44.6 | 13.12 | 2.14 | 162 | 159 | 155 | 151 |
| " | $\frac{5}{16}$ | 48.0 | 14.12 | 2.15 | 174 | 171 | 167 | 162 |
| " | $\frac{3}{8}$ | 51.4 | 15.12 | 2.16 | 186 | 183 | 179 | 174 |
| " | $\frac{7}{16}$ | 54.8 | 16.12 | 2.17 | 199 | 195 | 191 | 186 |
| " | $\frac{1}{2}$ | 58.2 | 17.12 | 2.18 | 211 | 207 | 203 | 197 |
| " | $\frac{5}{8}$ | 61.6 | 18.12 | 2.19 | 224 | 220 | 215 | 209 |
| " | $\frac{3}{4}$ | 65.0 | 19.12 | 2.19 | 236 | 232 | 227 | 220 |

For detail dimensions see page 232

**SAFE LOADS IN THOUSANDS OF POUNDS FOR
6" CHANNEL AND PLATE COLUMNS.
SQUARE ENDS.**

Based on Gordon's Formula $P = \frac{50\,000}{1 + \frac{(12\,L)^2}{36\,000\,r^2}}$ Safety factor 4.



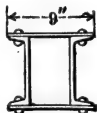
SERIES A.

| Length in Feet. | | | | | | | Thickness of Plates. | Weight of each Channel. |
|-----------------|-----|-----|-----|-----|-----|-----|----------------------------|-------------------------------|
| 12 | 14 | 16 | 18 | 20 | 22 | 24 | Inch. | Lbs. per Foot. |
| 99 | 96 | 92 | 89 | 85 | 81 | 77 | $\frac{1}{4}$ | 8 |
| 111 | 107 | 103 | 99 | 95 | 90 | 86 | $\frac{1}{8}$ | " |
| 122 | 118 | 114 | 109 | 104 | 99 | 94 | $\frac{3}{8}$ | " |
| 133 | 128 | 124 | 119 | 114 | 109 | 103 | $\frac{1}{2}$ | " |
| 144 | 139 | 135 | 129 | 124 | 118 | 112 | $\frac{1}{2}$ | " |
| 156 | 150 | 145 | 139 | 133 | 127 | 121 | $\frac{1}{8}$ | " |
| 166 | 161 | 155 | 149 | 142 | 136 | 130 | $\frac{3}{8}$ | " |
| 114 | 110 | 106 | 102 | 97 | 92 | 88 | $\frac{1}{4}$ | 10.5 |
| 126 | 121 | 117 | 112 | 107 | 102 | 96 | $\frac{1}{8}$ | " |
| 137 | 133 | 127 | 122 | 116 | 111 | 106 | $\frac{3}{8}$ | " |
| 148 | 143 | 138 | 132 | 126 | 120 | 114 | $\frac{1}{2}$ | " |
| 159 | 154 | 148 | 142 | 135 | 130 | 123 | $\frac{1}{2}$ | " |
| 171 | 165 | 159 | 152 | 144 | 139 | 132 | $\frac{1}{8}$ | " |
| 182 | 176 | 169 | 162 | 154 | 148 | 140 | $\frac{3}{8}$ | " |
| 130 | 125 | 120 | 115 | 109 | 104 | 99 | $\frac{1}{4}$ | 13 |
| 141 | 136 | 131 | 125 | 119 | 113 | 107 | $\frac{1}{8}$ | " |
| 153 | 147 | 141 | 135 | 129 | 122 | 116 | $\frac{3}{8}$ | " |
| 164 | 158 | 152 | 145 | 138 | 131 | 125 | $\frac{1}{2}$ | " |
| 175 | 169 | 162 | 155 | 148 | 140 | 133 | $\frac{1}{2}$ | " |
| 186 | 179 | 173 | 166 | 158 | 150 | 143 | $\frac{1}{8}$ | " |
| 197 | 190 | 183 | 176 | 167 | 159 | 151 | $\frac{3}{8}$ | " |
| 146 | 140 | 134 | 128 | 122 | 115 | 109 | $\frac{1}{4}$ | 15.5 |
| 157 | 151 | 145 | 138 | 131 | 125 | 118 | $\frac{1}{8}$ | " |
| 170 | 162 | 155 | 148 | 140 | 133 | 127 | $\frac{3}{8}$ | " |
| 180 | 172 | 165 | 158 | 150 | 143 | 135 | $\frac{1}{2}$ | " |
| 191 | 184 | 176 | 168 | 160 | 152 | 144 | $\frac{1}{2}$ | " |
| 202 | 195 | 187 | 178 | 170 | 162 | 153 | $\frac{1}{8}$ | " |
| 213 | 205 | 197 | 188 | 180 | 171 | 161 | $\frac{3}{8}$ | " |

For detail dimensions see page 232

SAFE LOADS IN THOUSANDS OF POUNDS FOR 7" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula $P = \frac{50\,000}{1 + \frac{(12\,L)^2}{36\,000\,r^2}}$ Safety factor 4.

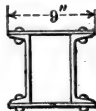


SERIES A.

| Weight of each Channel. | Thickness of Plates. | Weight of Column. | Area of Column Section. | Least Radius of Gyration. | Length in Feet. | | | |
|-------------------------|----------------------|-------------------|-------------------------|---------------------------|-----------------|-----|-----|-----|
| Lbs. per Foot. | Inch. | Lbs. per Ft. | Sq. Ins. | Inches. | 4 | 6 | 8 | 10 |
| 9.75 | $\frac{1}{4}$ | 34.8 | 10.20 | 2.63 | 126 | 125 | 123 | 121 |
| " | $\frac{5}{16}$ | 38.6 | 11.32 | 2.63 | 140 | 139 | 137 | 134 |
| " | $\frac{3}{8}$ | 42.5 | 12.45 | 2.62 | 154 | 152 | 150 | 147 |
| " | $\frac{7}{16}$ | 46.3 | 13.58 | 2.62 | 168 | 166 | 163 | 160 |
| " | $\frac{1}{2}$ | 50.1 | 14.70 | 2.62 | 182 | 180 | 177 | 174 |
| " | $\frac{5}{8}$ | 53.9 | 15.82 | 2.62 | 196 | 194 | 190 | 187 |
| " | $\frac{3}{4}$ | 57.8 | 16.95 | 2.62 | 210 | 207 | 204 | 200 |
| 12.25 | $\frac{1}{4}$ | 39.8 | 11.70 | 2.55 | 145 | 143 | 141 | 138 |
| " | $\frac{5}{16}$ | 43.6 | 12.82 | 2.56 | 159 | 157 | 154 | 151 |
| " | $\frac{3}{8}$ | 47.5 | 13.95 | 2.56 | 173 | 171 | 168 | 164 |
| " | $\frac{7}{16}$ | 51.3 | 15.08 | 2.56 | 187 | 185 | 182 | 178 |
| " | $\frac{1}{2}$ | 55.1 | 16.20 | 2.57 | 200 | 198 | 195 | 191 |
| " | $\frac{5}{8}$ | 58.9 | 17.32 | 2.57 | 214 | 212 | 208 | 204 |
| " | $\frac{3}{4}$ | 62.8 | 18.45 | 2.57 | 228 | 226 | 222 | 217 |
| 14.75 | $\frac{1}{4}$ | 44.8 | 13.18 | 2.49 | 163 | 161 | 158 | 155 |
| " | $\frac{5}{16}$ | 48.6 | 14.30 | 2.50 | 177 | 175 | 172 | 168 |
| " | $\frac{3}{8}$ | 52.5 | 15.43 | 2.50 | 191 | 189 | 185 | 181 |
| " | $\frac{7}{16}$ | 56.3 | 16.56 | 2.51 | 205 | 202 | 199 | 195 |
| " | $\frac{1}{2}$ | 60.1 | 17.68 | 2.52 | 219 | 216 | 212 | 208 |
| " | $\frac{5}{8}$ | 63.9 | 18.80 | 2.52 | 233 | 230 | 226 | 221 |
| " | $\frac{3}{4}$ | 67.8 | 19.93 | 2.53 | 247 | 244 | 239 | 234 |
| 17.25 | $\frac{1}{4}$ | 49.8 | 14.64 | 2.42 | 181 | 178 | 175 | 171 |
| " | $\frac{5}{16}$ | 53.6 | 15.76 | 2.43 | 195 | 192 | 189 | 185 |
| " | $\frac{3}{8}$ | 57.5 | 16.89 | 2.45 | 209 | 206 | 202 | 198 |
| " | $\frac{7}{16}$ | 61.3 | 18.02 | 2.46 | 223 | 220 | 216 | 211 |
| " | $\frac{1}{2}$ | 65.1 | 19.14 | 2.46 | 237 | 234 | 229 | 224 |
| " | $\frac{5}{8}$ | 68.9 | 20.26 | 2.47 | 251 | 248 | 243 | 238 |
| " | $\frac{3}{4}$ | 72.8 | 21.39 | 2.48 | 265 | 261 | 257 | 251 |
| 19.75 | $\frac{1}{4}$ | 54.8 | 16.12 | 2.37 | 199 | 197 | 193 | 188 |
| " | $\frac{5}{16}$ | 58.6 | 17.24 | 2.38 | 213 | 210 | 206 | 201 |
| " | $\frac{3}{8}$ | 62.5 | 18.37 | 2.40 | 227 | 224 | 220 | 214 |
| " | $\frac{7}{16}$ | 66.3 | 19.50 | 2.41 | 241 | 238 | 234 | 228 |
| " | $\frac{1}{2}$ | 70.1 | 20.62 | 2.42 | 255 | 251 | 247 | 242 |
| " | $\frac{5}{8}$ | 73.9 | 21.74 | 2.43 | 269 | 265 | 260 | 255 |
| " | $\frac{3}{4}$ | 77.8 | 22.87 | 2.44 | 283 | 279 | 274 | 268 |

SAFE LOADS IN THOUSANDS OF POUNDS FOR 7" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula $P = \frac{50\,000}{1 + \frac{(12\,L)^2}{36\,000\,r^2}}$ Safety factor 4.



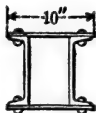
SERIES A.

| Length in Feet. | | | | | | | | Thickness of Plates. | Weight of each Channel. |
|-----------------|-----|-----|-----|-----|-----|-----|-----|----------------------------|-------------------------------|
| 12 | 14 | 16 | 18 | 20 | 22 | 24 | 26 | Inch. | Lbs. per Ft. |
| 118 | 115 | 111 | 108 | 104 | 99 | 96 | 92 | $\frac{1}{4}$ | 9.75 |
| 130 | 127 | 123 | 119 | 115 | 110 | 106 | 102 | $\frac{5}{16}$ | " |
| 143 | 140 | 135 | 131 | 126 | 121 | 116 | 112 | $\frac{3}{8}$ | " |
| 156 | 153 | 148 | 143 | 138 | 132 | 127 | 122 | $\frac{1}{2}$ | " |
| 169 | 165 | 160 | 154 | 149 | 143 | 137 | 132 | $\frac{5}{8}$ | " |
| 182 | 178 | 172 | 166 | 161 | 154 | 148 | 142 | $\frac{3}{4}$ | " |
| 195 | 190 | 184 | 178 | 172 | 165 | 158 | 152 | $\frac{7}{8}$ | " |
| 134 | 130 | 126 | 122 | 118 | 113 | 108 | 103 | $\frac{1}{4}$ | 12.25 |
| 147 | 143 | 139 | 134 | 129 | 124 | 118 | 113 | $\frac{5}{16}$ | " |
| 160 | 156 | 151 | 146 | 140 | 135 | 129 | 123 | $\frac{3}{8}$ | " |
| 173 | 168 | 163 | 158 | 152 | 145 | 139 | 133 | $\frac{1}{2}$ | " |
| 186 | 181 | 176 | 169 | 163 | 156 | 150 | 144 | $\frac{5}{8}$ | " |
| 199 | 194 | 188 | 181 | 174 | 167 | 161 | 154 | $\frac{3}{4}$ | " |
| 212 | 207 | 200 | 193 | 185 | 178 | 171 | 164 | $\frac{7}{8}$ | " |
| 151 | 146 | 142 | 136 | 131 | 126 | 120 | 115 | $\frac{1}{4}$ | 14.75 |
| 164 | 159 | 154 | 148 | 142 | 136 | 131 | 125 | $\frac{5}{16}$ | " |
| 177 | 171 | 166 | 160 | 154 | 147 | 141 | 135 | $\frac{3}{8}$ | " |
| 190 | 184 | 178 | 171 | 165 | 158 | 151 | 144 | $\frac{1}{2}$ | " |
| 202 | 196 | 191 | 184 | 177 | 170 | 162 | 155 | $\frac{5}{8}$ | " |
| 215 | 209 | 203 | 196 | 188 | 180 | 173 | 165 | $\frac{3}{4}$ | " |
| 229 | 222 | 215 | 207 | 199 | 191 | 183 | 175 | $\frac{7}{8}$ | " |
| 166 | 161 | 156 | 150 | 143 | 137 | 131 | 126 | $\frac{1}{4}$ | 17.25 |
| 180 | 174 | 168 | 162 | 155 | 148 | 142 | 135 | $\frac{5}{16}$ | " |
| 193 | 187 | 181 | 174 | 166 | 159 | 153 | 146 | $\frac{3}{8}$ | " |
| 206 | 199 | 193 | 186 | 178 | 171 | 163 | 155 | $\frac{1}{2}$ | " |
| 218 | 212 | 205 | 197 | 190 | 182 | 173 | 165 | $\frac{5}{8}$ | " |
| 231 | 224 | 217 | 209 | 201 | 192 | 184 | 176 | $\frac{3}{4}$ | " |
| 245 | 238 | 229 | 220 | 212 | 203 | 194 | 186 | $\frac{7}{8}$ | " |
| 183 | 177 | 170 | 164 | 157 | 150 | 143 | 136 | $\frac{1}{4}$ | 19.75 |
| 196 | 189 | 183 | 175 | 168 | 161 | 153 | 146 | $\frac{5}{16}$ | " |
| 209 | 202 | 195 | 187 | 180 | 172 | 164 | 157 | $\frac{3}{8}$ | " |
| 222 | 215 | 208 | 199 | 191 | 183 | 174 | 166 | $\frac{1}{2}$ | " |
| 234 | 227 | 220 | 211 | 202 | 194 | 185 | 177 | $\frac{5}{8}$ | " |
| 248 | 240 | 231 | 223 | 214 | 204 | 195 | 186 | $\frac{3}{4}$ | " |
| 261 | 253 | 243 | 235 | 225 | 216 | 207 | 196 | $\frac{7}{8}$ | " |

For detail dimensions see page 232

SAFE LOADS IN THOUSANDS OF POUNDS FOR 8" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula $P = \frac{50\,000}{1 + \frac{(12 L)^2}{36\,000 r^2}}$. Safety factor 4.



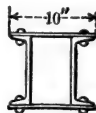
SERIES A.

| Weight of each Channel. | Thickness of Plates. | Weight of Column. | Area of Column Section. | Least Radius of Gyration. | Length in Feet. | | | | |
|-------------------------|----------------------|-------------------|-------------------------|---------------------------|-----------------|-----|-----|-----|-----|
| Lbs. per Foot. | Inch. | Lbs. per Ft. | Sq. Ina. | Inches. | 4 | 6 | 8 | 10 | 12 |
| 11.25 | 1/4 | 39.5 | 11.70 | 2.98 | 145 | 144 | 142 | 140 | 137 |
| " | 1/8 | 43.7 | 12.95 | 2.97 | 161 | 159 | 157 | 155 | 152 |
| " | 3/16 | 48.0 | 14.20 | 2.97 | 176 | 175 | 172 | 170 | 167 |
| " | 1/2 | 52.3 | 15.45 | 2.96 | 192 | 190 | 188 | 185 | 181 |
| " | 5/8 | 56.5 | 16.70 | 2.95 | 207 | 205 | 203 | 200 | 196 |
| " | 3/4 | 60.8 | 17.95 | 2.95 | 223 | 221 | 219 | 214 | 210 |
| " | 7/8 | 65.0 | 19.20 | 2.95 | 238 | 236 | 233 | 229 | 225 |
| 13.75 | 1/4 | 44.5 | 13.08 | 2.92 | 162 | 161 | 159 | 156 | 153 |
| " | 1/8 | 48.7 | 14.33 | 2.92 | 178 | 176 | 174 | 171 | 168 |
| " | 3/16 | 53.0 | 15.58 | 2.92 | 193 | 191 | 189 | 186 | 182 |
| " | 1/2 | 57.3 | 16.83 | 2.91 | 209 | 207 | 204 | 201 | 197 |
| " | 5/8 | 61.5 | 18.08 | 2.91 | 224 | 222 | 220 | 216 | 212 |
| " | 3/4 | 65.8 | 19.33 | 2.91 | 240 | 237 | 235 | 231 | 226 |
| " | 7/8 | 70.0 | 20.58 | 2.91 | 255 | 253 | 250 | 246 | 241 |
| 16.25 | 1/4 | 49.5 | 14.56 | 2.86 | 181 | 179 | 176 | 173 | 170 |
| " | 1/8 | 53.7 | 15.81 | 2.87 | 196 | 194 | 192 | 188 | 185 |
| " | 3/16 | 58.0 | 17.06 | 2.87 | 212 | 210 | 207 | 203 | 199 |
| " | 1/2 | 62.3 | 18.31 | 2.87 | 227 | 225 | 222 | 218 | 214 |
| " | 5/8 | 66.5 | 19.56 | 2.87 | 243 | 240 | 237 | 233 | 228 |
| " | 3/4 | 70.8 | 20.81 | 2.87 | 258 | 256 | 252 | 248 | 243 |
| " | 7/8 | 75.0 | 22.06 | 2.87 | 274 | 271 | 267 | 263 | 258 |
| 18.75 | 1/4 | 54.5 | 16.02 | 2.81 | 199 | 197 | 194 | 190 | 186 |
| " | 1/8 | 58.7 | 17.27 | 2.81 | 214 | 212 | 209 | 205 | 201 |
| " | 3/16 | 63.0 | 18.52 | 2.82 | 230 | 227 | 224 | 221 | 216 |
| " | 1/2 | 67.3 | 19.77 | 2.82 | 245 | 243 | 240 | 236 | 230 |
| " | 5/8 | 71.5 | 21.02 | 2.83 | 261 | 258 | 255 | 250 | 245 |
| " | 3/4 | 75.8 | 22.27 | 2.83 | 276 | 274 | 270 | 265 | 260 |
| " | 7/8 | 80.0 | 23.52 | 2.83 | 292 | 289 | 285 | 280 | 275 |
| 21.25 | 1/4 | 59.5 | 17.50 | 2.76 | 217 | 215 | 212 | 208 | 204 |
| " | 1/8 | 63.7 | 18.75 | 2.77 | 233 | 230 | 227 | 223 | 218 |
| " | 3/16 | 68.0 | 20.00 | 2.77 | 248 | 245 | 242 | 238 | 233 |
| " | 1/2 | 72.3 | 21.25 | 2.78 | 264 | 261 | 257 | 253 | 247 |
| " | 5/8 | 76.5 | 22.50 | 2.79 | 279 | 276 | 272 | 267 | 262 |
| " | 3/4 | 80.8 | 23.75 | 2.79 | 295 | 291 | 287 | 282 | 276 |
| " | 7/8 | 85.0 | 25.00 | 2.80 | 310 | 307 | 302 | 297 | 291 |

For detail dimensions see page 232

SAFE LOADS IN THOUSANDS OF POUNDS FOR 8" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula $P = \frac{50\,000}{1 + \frac{(12L)^2}{36\,000 r^2}}$ Safety factor 4.



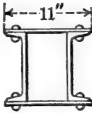
SERIES A.

| Length in Feet. | | | | | | | | | Thickness of Plates. | Weight of each Channel. |
|-----------------|-----|-----|-----|-----|-----|-----|-----|-----|----------------------------|-------------------------------|
| 14 | 16 | 18 | 20 | 22 | 24 | 26 | 28 | 30 | Inch. | Lbs. per Foot. |
| 134 | 131 | 128 | 124 | 120 | 116 | 112 | 108 | 104 | $\frac{1}{4}$ | 11.25 |
| 149 | 145 | 141 | 137 | 133 | 128 | 124 | 120 | 115 | $\frac{1}{8}$ | " |
| 163 | 159 | 154 | 150 | 146 | 141 | 136 | 131 | 126 | $\frac{3}{8}$ | " |
| 177 | 173 | 168 | 163 | 158 | 153 | 147 | 142 | 137 | $\frac{1}{2}$ | " |
| 192 | 187 | 182 | 176 | 170 | 165 | 159 | 153 | 147 | $\frac{1}{2}$ | " |
| 206 | 201 | 195 | 189 | 183 | 178 | 171 | 165 | 158 | $\frac{1}{2}$ | " |
| 221 | 215 | 209 | 203 | 196 | 190 | 183 | 177 | 169 | $\frac{3}{8}$ | " |
| | | | | | | | | | | |
| 150 | 146 | 142 | 138 | 133 | 129 | 124 | 119 | 115 | $\frac{1}{4}$ | 13.75 |
| 164 | 160 | 155 | 151 | 146 | 141 | 136 | 131 | 126 | $\frac{1}{8}$ | " |
| 178 | 174 | 169 | 164 | 159 | 153 | 148 | 142 | 137 | $\frac{3}{8}$ | " |
| 193 | 188 | 182 | 177 | 171 | 166 | 160 | 153 | 148 | $\frac{1}{2}$ | " |
| 207 | 202 | 196 | 190 | 184 | 178 | 172 | 164 | 159 | $\frac{1}{2}$ | " |
| 221 | 216 | 209 | 203 | 196 | 190 | 183 | 176 | 170 | $\frac{1}{2}$ | " |
| 236 | 229 | 223 | 216 | 209 | 203 | 195 | 187 | 181 | $\frac{3}{8}$ | " |
| | | | | | | | | | | |
| 166 | 162 | 157 | 152 | 147 | 142 | 137 | 131 | 126 | $\frac{1}{4}$ | 16.25 |
| 180 | 176 | 171 | 165 | 160 | 154 | 148 | 143 | 137 | $\frac{1}{8}$ | " |
| 195 | 189 | 184 | 178 | 172 | 166 | 160 | 154 | 148 | $\frac{3}{8}$ | " |
| 209 | 203 | 198 | 191 | 185 | 178 | 172 | 165 | 159 | $\frac{1}{2}$ | " |
| 223 | 217 | 211 | 204 | 198 | 191 | 184 | 177 | 170 | $\frac{1}{2}$ | " |
| 237 | 231 | 224 | 217 | 210 | 203 | 195 | 188 | 181 | $\frac{1}{2}$ | " |
| 252 | 245 | 238 | 231 | 223 | 215 | 207 | 199 | 191 | $\frac{3}{8}$ | " |
| | | | | | | | | | | |
| 182 | 177 | 172 | 167 | 161 | 155 | 149 | 143 | 137 | $\frac{1}{4}$ | 18.75 |
| 196 | 191 | 185 | 180 | 174 | 167 | 160 | 154 | 148 | $\frac{1}{8}$ | " |
| 210 | 205 | 199 | 193 | 186 | 180 | 173 | 166 | 160 | $\frac{3}{8}$ | " |
| 225 | 219 | 212 | 206 | 199 | 192 | 185 | 178 | 171 | $\frac{1}{2}$ | " |
| 240 | 233 | 226 | 219 | 211 | 204 | 196 | 189 | 181 | $\frac{1}{2}$ | " |
| 254 | 246 | 239 | 232 | 224 | 216 | 208 | 200 | 192 | $\frac{1}{2}$ | " |
| 268 | 260 | 253 | 245 | 236 | 228 | 220 | 211 | 203 | $\frac{3}{8}$ | " |
| | | | | | | | | | | |
| 198 | 193 | 187 | 181 | 174 | 168 | 162 | 155 | 148 | $\frac{1}{4}$ | 21.25 |
| 212 | 207 | 200 | 194 | 187 | 180 | 173 | 166 | 159 | $\frac{1}{8}$ | " |
| 226 | 220 | 214 | 207 | 200 | 192 | 185 | 178 | 170 | $\frac{3}{8}$ | " |
| 241 | 234 | 227 | 220 | 213 | 205 | 196 | 189 | 181 | $\frac{1}{2}$ | " |
| 256 | 249 | 241 | 233 | 225 | 217 | 209 | 201 | 192 | $\frac{1}{2}$ | " |
| 270 | 263 | 254 | 246 | 238 | 229 | 221 | 212 | 202 | $\frac{1}{2}$ | " |
| 284 | 277 | 268 | 260 | 250 | 241 | 232 | 223 | 214 | $\frac{3}{8}$ | " |

For detail dimensions see page 232

**SAFE LOADS IN THOUSANDS OF POUNDS FOR
9" CHANNEL AND PLATE COLUMNS.
SQUARE ENDS.**

Based on Gordon's Formula $P = \frac{50\,000}{1 + \frac{(12L)^2}{36\,000\,r^2}}$ Safety factor 4.



SERIES A.

| Weight of each Channel. | Thick- ness of Plates. | Weight of Column. | Area of Column Section. | Least Radius of Gyration. | Length in Feet. | | | | | |
|-------------------------------|------------------------------|-------------------------|-------------------------------|---------------------------------|-----------------|-----|-----|-----|-----|-----|
| | | | | | 6 | 8 | 10 | 12 | 14 | 16 |
| Lbs. per Ft. | Inch. | Lbs. per Ft. | Sq. Ins. | Inches. | | | | | | |
| 13.25 | $\frac{1}{4}$ | 45.2 | 13.28 | 3.34 | 164 | 162 | 160 | 158 | 155 | 152 |
| " | $\frac{5}{16}$ | 49.9 | 14.66 | 3.32 | 181 | 179 | 177 | 174 | 171 | 168 |
| " | $\frac{3}{8}$ | 54.6 | 16.03 | 3.31 | 198 | 196 | 193 | 191 | 187 | 183 |
| " | $\frac{7}{16}$ | 59.2 | 17.40 | 3.30 | 215 | 213 | 210 | 207 | 203 | 199 |
| " | $\frac{1}{2}$ | 63.9 | 18.78 | 3.29 | 232 | 229 | 227 | 223 | 219 | 214 |
| " | $\frac{9}{16}$ | 68.5 | 20.16 | 3.28 | 249 | 246 | 243 | 239 | 235 | 230 |
| " | $\frac{5}{8}$ | 73.3 | 21.53 | 3.28 | 266 | 263 | 260 | 255 | 251 | 246 |
| 15 | $\frac{1}{4}$ | 48.7 | 14.32 | 3.29 | 177 | 175 | 173 | 170 | 167 | 163 |
| " | $\frac{5}{16}$ | 53.4 | 15.70 | 3.28 | 194 | 192 | 189 | 186 | 183 | 179 |
| " | $\frac{3}{8}$ | 58.1 | 17.07 | 3.28 | 211 | 209 | 206 | 202 | 199 | 195 |
| " | $\frac{7}{16}$ | 62.7 | 18.44 | 3.27 | 228 | 225 | 222 | 219 | 215 | 210 |
| " | $\frac{1}{2}$ | 67.4 | 19.82 | 3.26 | 245 | 242 | 239 | 235 | 231 | 226 |
| " | $\frac{9}{16}$ | 72.0 | 21.20 | 3.26 | 262 | 259 | 255 | 251 | 247 | 242 |
| " | $\frac{5}{8}$ | 76.8 | 22.57 | 3.25 | 279 | 275 | 272 | 267 | 263 | 257 |
| 20 | $\frac{1}{4}$ | 58.7 | 17.26 | 3.19 | 213 | 210 | 208 | 204 | 200 | 196 |
| " | $\frac{5}{16}$ | 63.4 | 18.64 | 3.19 | 230 | 227 | 224 | 220 | 216 | 212 |
| " | $\frac{3}{8}$ | 68.1 | 20.01 | 3.19 | 247 | 244 | 241 | 236 | 232 | 227 |
| " | $\frac{7}{16}$ | 72.7 | 21.38 | 3.19 | 263 | 261 | 257 | 253 | 248 | 243 |
| " | $\frac{1}{2}$ | 77.4 | 22.76 | 3.19 | 280 | 278 | 274 | 269 | 264 | 259 |
| " | $\frac{9}{16}$ | 82.0 | 24.14 | 3.19 | 297 | 294 | 291 | 285 | 280 | 274 |
| " | $\frac{5}{8}$ | 86.8 | 25.51 | 3.18 | 314 | 311 | 307 | 301 | 296 | 290 |
| 25 | $\frac{1}{4}$ | 68.7 | 20.20 | 3.10 | 249 | 246 | 243 | 238 | 234 | 228 |
| " | $\frac{5}{16}$ | 73.4 | 21.58 | 3.11 | 266 | 263 | 259 | 254 | 250 | 244 |
| " | $\frac{3}{8}$ | 78.1 | 22.95 | 3.11 | 283 | 279 | 276 | 270 | 265 | 260 |
| " | $\frac{7}{16}$ | 82.7 | 24.32 | 3.12 | 300 | 296 | 292 | 287 | 281 | 275 |
| " | $\frac{1}{2}$ | 87.4 | 25.70 | 3.12 | 317 | 313 | 309 | 304 | 297 | 291 |
| " | $\frac{9}{16}$ | 92.0 | 27.08 | 3.12 | 334 | 330 | 325 | 320 | 313 | 307 |
| " | $\frac{5}{8}$ | 96.8 | 28.45 | 3.12 | 351 | 346 | 342 | 336 | 329 | 322 |

For detail dimensions see page 232

SAFE LOADS IN THOUSANDS OF POUNDS FOR 9" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula $P = \frac{50\,000}{1 + \frac{(12 L)^2}{36\,000 r^2}}$ Safety factor 4.



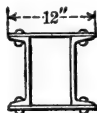
SERIES A.

| Length in Feet. | | | | | | | | | Thickness of Plates. | Weight of each Channel. |
|-----------------|-----|-----|-----|-----|-----|-----|-----|-----|----------------------------|-------------------------------|
| 18 | 20 | 22 | 24 | 26 | 28 | 30 | 32 | 34 | Inch. | Lbs. per Foot. |
| 149 | 145 | 141 | 137 | 134 | 129 | 125 | 121 | 117 | $\frac{1}{4}$ | 13.25 |
| 164 | 160 | 156 | 152 | 147 | 143 | 138 | 134 | 129 | $\frac{5}{16}$ | " |
| 179 | 175 | 171 | 165 | 160 | 155 | 150 | 146 | 141 | $\frac{3}{8}$ | " |
| 194 | 189 | 184 | 179 | 174 | 169 | 163 | 158 | 153 | $\frac{7}{16}$ | " |
| 209 | 204 | 199 | 194 | 188 | 182 | 176 | 171 | 165 | $\frac{1}{2}$ | " |
| 225 | 219 | 214 | 208 | 202 | 195 | 189 | 182 | 176 | $\frac{5}{8}$ | " |
| 240 | 234 | 228 | 222 | 215 | 209 | 202 | 194 | 188 | $\frac{3}{4}$ | " |
| 160 | 156 | 152 | 148 | 143 | 139 | 134 | 130 | 126 | $\frac{1}{4}$ | 15 |
| 175 | 171 | 166 | 162 | 157 | 152 | 147 | 142 | 137 | $\frac{5}{16}$ | " |
| 190 | 186 | 181 | 176 | 171 | 166 | 160 | 154 | 149 | $\frac{3}{8}$ | " |
| 206 | 201 | 195 | 190 | 184 | 178 | 172 | 167 | 161 | $\frac{7}{16}$ | " |
| 221 | 216 | 210 | 203 | 197 | 191 | 185 | 179 | 173 | $\frac{1}{2}$ | " |
| 236 | 231 | 225 | 217 | 211 | 204 | 198 | 191 | 185 | $\frac{5}{8}$ | " |
| 252 | 245 | 238 | 231 | 225 | 218 | 211 | 204 | 196 | $\frac{3}{4}$ | " |
| 192 | 186 | 181 | 176 | 170 | 165 | 159 | 154 | 148 | $\frac{1}{4}$ | 20 |
| 207 | 201 | 196 | 190 | 184 | 178 | 172 | 166 | 160 | $\frac{5}{16}$ | " |
| 222 | 216 | 210 | 204 | 197 | 191 | 185 | 179 | 172 | $\frac{3}{8}$ | " |
| 237 | 231 | 224 | 218 | 211 | 204 | 197 | 191 | 183 | $\frac{7}{16}$ | " |
| 253 | 246 | 239 | 232 | 224 | 217 | 210 | 203 | 195 | $\frac{1}{2}$ | " |
| 268 | 260 | 253 | 246 | 238 | 230 | 223 | 216 | 207 | $\frac{5}{8}$ | " |
| 282 | 275 | 268 | 260 | 251 | 243 | 236 | 226 | 219 | $\frac{3}{4}$ | " |
| 223 | 216 | 210 | 204 | 197 | 191 | 183 | 177 | 170 | $\frac{1}{4}$ | 25 |
| 238 | 232 | 224 | 218 | 210 | 204 | 197 | 189 | 183 | $\frac{5}{16}$ | " |
| 253 | 246 | 239 | 232 | 224 | 217 | 210 | 201 | 194 | $\frac{3}{8}$ | " |
| 268 | 261 | 253 | 246 | 238 | 230 | 222 | 213 | 206 | $\frac{7}{16}$ | " |
| 283 | 276 | 267 | 260 | 252 | 243 | 235 | 226 | 218 | $\frac{1}{2}$ | " |
| 298 | 291 | 282 | 274 | 265 | 256 | 247 | 238 | 229 | $\frac{5}{8}$ | " |
| 313 | 306 | 296 | 287 | 279 | 269 | 260 | 250 | 241 | $\frac{3}{4}$ | " |

For detail dimensions see page 232

SAFE LOADS IN THOUSANDS OF POUNDS FOR 10" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula $P = \frac{50\,000}{1 + \frac{(12L)^2}{36\,000r^2}}$ Safety factor 4.



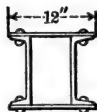
SERIES A.

| Weight of each Channel. | Thick-ness of Plates. | Weight of Column. | Area of Column Section. | Least Radius of Gyration. | Length in Feet. | | | | | |
|-------------------------|-----------------------|-------------------|-------------------------|---------------------------|-----------------|-----|-----|-----|-----|-----|
| | | | | | 6 | 8 | 10 | 12 | 14 | 16 |
| Lbs. per Ft. | Inch. | Lbs. per Ft. | Sq. Ins. | Inches. | | | | | | |
| 15 | $\frac{1}{4}$ | 50.4 | 14.92 | 3.62 | 184 | 183 | 181 | 179 | 176 | 173 |
| " | $\frac{5}{16}$ | 55.5 | 16.42 | 3.61 | 203 | 201 | 199 | 197 | 193 | 191 |
| " | $\frac{3}{8}$ | 60.6 | 17.92 | 3.59 | 221 | 220 | 217 | 215 | 211 | 207 |
| " | $\frac{7}{16}$ | 65.7 | 19.42 | 3.58 | 240 | 238 | 235 | 232 | 229 | 225 |
| " | $\frac{1}{2}$ | 70.8 | 20.92 | 3.58 | 259 | 257 | 254 | 250 | 247 | 242 |
| " | $\frac{5}{8}$ | 75.9 | 22.42 | 3.57 | 277 | 275 | 272 | 268 | 264 | 259 |
| " | $\frac{3}{4}$ | 81.0 | 23.92 | 3.56 | 296 | 293 | 290 | 286 | 282 | 277 |
| 20 | $\frac{1}{4}$ | 60.4 | 17.76 | 3.52 | 219 | 217 | 215 | 212 | 209 | 205 |
| " | $\frac{5}{16}$ | 65.5 | 19.26 | 3.52 | 238 | 236 | 233 | 230 | 226 | 223 |
| " | $\frac{3}{8}$ | 70.6 | 20.76 | 3.51 | 257 | 254 | 252 | 248 | 244 | 239 |
| " | $\frac{7}{16}$ | 75.7 | 22.26 | 3.51 | 275 | 272 | 270 | 266 | 262 | 257 |
| " | $\frac{1}{2}$ | 80.8 | 23.76 | 3.51 | 294 | 291 | 288 | 284 | 279 | 274 |
| " | $\frac{5}{8}$ | 85.9 | 25.26 | 3.50 | 312 | 309 | 305 | 302 | 297 | 291 |
| " | $\frac{3}{4}$ | 91.0 | 26.76 | 3.50 | 331 | 328 | 324 | 320 | 314 | 308 |
| 25 | $\frac{1}{4}$ | 70.4 | 20.70 | 3.42 | 255 | 253 | 250 | 247 | 242 | 238 |
| " | $\frac{5}{16}$ | 75.5 | 22.20 | 3.43 | 274 | 272 | 268 | 265 | 260 | 255 |
| " | $\frac{3}{8}$ | 80.6 | 23.70 | 3.43 | 293 | 290 | 287 | 282 | 278 | 272 |
| " | $\frac{7}{16}$ | 85.7 | 25.20 | 3.43 | 311 | 308 | 305 | 300 | 295 | 289 |
| " | $\frac{1}{2}$ | 90.8 | 26.70 | 3.43 | 330 | 327 | 323 | 318 | 313 | 307 |
| " | $\frac{5}{8}$ | 95.9 | 28.20 | 3.44 | 348 | 345 | 341 | 336 | 330 | 324 |
| " | $\frac{3}{4}$ | 101.0 | 29.70 | 3.44 | 367 | 364 | 359 | 355 | 348 | 341 |
| 30 | $\frac{1}{4}$ | 80.4 | 23.64 | 3.33 | 292 | 289 | 285 | 281 | 276 | 271 |
| " | $\frac{5}{16}$ | 85.5 | 25.14 | 3.34 | 310 | 307 | 303 | 299 | 294 | 288 |
| " | $\frac{3}{8}$ | 90.6 | 26.64 | 3.35 | 329 | 325 | 321 | 317 | 311 | 305 |
| " | $\frac{7}{16}$ | 95.7 | 28.14 | 3.36 | 347 | 344 | 340 | 334 | 329 | 322 |
| " | $\frac{1}{2}$ | 100.8 | 29.64 | 3.36 | 366 | 362 | 358 | 352 | 346 | 339 |
| " | $\frac{5}{8}$ | 105.9 | 31.14 | 3.37 | 384 | 380 | 376 | 370 | 364 | 358 |
| " | $\frac{3}{4}$ | 111.0 | 32.64 | 3.37 | 403 | 399 | 394 | 388 | 381 | 375 |
| 35 | $\frac{1}{4}$ | 90.4 | 26.58 | 3.26 | 328 | 324 | 320 | 315 | 309 | 303 |
| " | $\frac{5}{16}$ | 95.5 | 28.08 | 3.27 | 347 | 343 | 338 | 333 | 327 | 320 |
| " | $\frac{3}{8}$ | 100.6 | 29.58 | 3.28 | 365 | 361 | 357 | 351 | 344 | 337 |
| " | $\frac{7}{16}$ | 105.7 | 31.08 | 3.29 | 384 | 380 | 375 | 369 | 362 | 354 |
| " | $\frac{1}{2}$ | 110.8 | 32.58 | 3.29 | 402 | 398 | 393 | 387 | 379 | 372 |
| " | $\frac{5}{8}$ | 115.9 | 34.08 | 3.30 | 421 | 416 | 411 | 405 | 398 | 390 |
| " | $\frac{3}{4}$ | 121.0 | 35.58 | 3.31 | 439 | 435 | 429 | 423 | 415 | 407 |

For detail dimensions see page 233

SAFE LOADS IN THOUSANDS OF POUNDS FOR 10" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula $P = \frac{50\,000}{1 + \frac{(12 L)^2}{36\,000 r^2}}$ Safety factor 4.

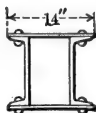


SERIES A.

| Length in Feet. | | | | | | | | | | Thick- ness of Plates. | Weight of each Channel. |
|-----------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|------------------------------|-------------------------------|
| 18 | 20 | 22 | 24 | 26 | 28 | 30 | 32 | 34 | 36 | Inch. | Lbs. per Ft. |
| 170 | 166 | 162 | 159 | 154 | 151 | 146 | 142 | 138 | 134 | 1/4 | 15 |
| 187 | 183 | 179 | 175 | 170 | 165 | 161 | 156 | 152 | 147 | 5/16 | " |
| 204 | 199 | 195 | 190 | 186 | 180 | 175 | 170 | 165 | 160 | 3/8 | " |
| 221 | 216 | 211 | 206 | 200 | 195 | 189 | 184 | 178 | 172 | 1/2 | " |
| 238 | 232 | 228 | 222 | 216 | 210 | 204 | 199 | 192 | 186 | 5/8 | " |
| 255 | 249 | 243 | 238 | 231 | 225 | 219 | 212 | 206 | 199 | 3/4 | " |
| 271 | 266 | 259 | 253 | 246 | 239 | 233 | 226 | 218 | 212 | 7/8 | " |
| | | | | | | | | | | | |
| 201 | 196 | 192 | 187 | 182 | 177 | 172 | 167 | 161 | 157 | 1/4 | 20 |
| 218 | 213 | 208 | 203 | 197 | 192 | 187 | 181 | 175 | 170 | 5/16 | " |
| 235 | 230 | 224 | 219 | 213 | 207 | 201 | 195 | 189 | 182 | 3/8 | " |
| 252 | 246 | 240 | 235 | 228 | 222 | 216 | 209 | 202 | 195 | 1/2 | " |
| 269 | 263 | 256 | 251 | 244 | 236 | 230 | 223 | 216 | 209 | 5/8 | " |
| 286 | 279 | 272 | 265 | 259 | 251 | 244 | 237 | 229 | 222 | 3/4 | " |
| 303 | 296 | 289 | 281 | 274 | 266 | 258 | 251 | 243 | 235 | 7/8 | " |
| | | | | | | | | | | | |
| 233 | 228 | 222 | 216 | 210 | 204 | 198 | 191 | 186 | 180 | 1/4 | 25 |
| 250 | 245 | 238 | 232 | 225 | 219 | 213 | 206 | 199 | 193 | 5/16 | " |
| 267 | 261 | 255 | 248 | 241 | 233 | 227 | 220 | 213 | 206 | 3/8 | " |
| 284 | 278 | 271 | 263 | 256 | 248 | 242 | 234 | 226 | 219 | 1/2 | " |
| 301 | 294 | 287 | 279 | 271 | 263 | 256 | 248 | 240 | 232 | 5/8 | " |
| 318 | 311 | 303 | 295 | 286 | 279 | 271 | 262 | 253 | 245 | 3/4 | " |
| 335 | 327 | 319 | 310 | 302 | 294 | 285 | 276 | 267 | 258 | 7/8 | " |
| | | | | | | | | | | | |
| 265 | 258 | 252 | 245 | 238 | 230 | 223 | 216 | 209 | 201 | 1/4 | 30 |
| 281 | 275 | 268 | 260 | 253 | 245 | 237 | 230 | 222 | 214 | 5/16 | " |
| 298 | 291 | 284 | 276 | 268 | 260 | 252 | 243 | 237 | 228 | 3/8 | " |
| 315 | 307 | 301 | 293 | 284 | 276 | 267 | 258 | 250 | 241 | 1/2 | " |
| 332 | 324 | 317 | 308 | 299 | 290 | 281 | 272 | 263 | 254 | 5/8 | " |
| 350 | 342 | 333 | 324 | 315 | 305 | 296 | 286 | 276 | 267 | 3/4 | " |
| 357 | 358 | 349 | 339 | 330 | 320 | 310 | 300 | 290 | 280 | 7/8 | " |
| | | | | | | | | | | | |
| 296 | 289 | 282 | 273 | 265 | 256 | 248 | 240 | 232 | 224 | 1/4 | 35 |
| 313 | 306 | 298 | 289 | 279 | 271 | 262 | 254 | 245 | 237 | 5/16 | " |
| 330 | 322 | 313 | 305 | 296 | 287 | 278 | 267 | 258 | 249 | 3/8 | " |
| 347 | 338 | 329 | 320 | 311 | 301 | 292 | 282 | 273 | 263 | 1/2 | " |
| 363 | 354 | 345 | 336 | 326 | 316 | 306 | 296 | 286 | 276 | 5/8 | " |
| 380 | 371 | 361 | 351 | 341 | 330 | 320 | 310 | 299 | 289 | 3/4 | " |
| 398 | 389 | 379 | 367 | 356 | 345 | 334 | 323 | 312 | 301 | 7/8 | " |

SAFE LOADS IN THOUSANDS OF POUNDS FOR 12" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula $P = \frac{50\,000}{1 + \frac{(12L)^2}{36\,000r^2}}$ Safety factor 4.



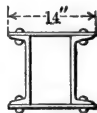
SERIES A.

| Weight of each Channel. | Thick-ness of Plates. | Weight of Column. | Area of Column Section. | Least Radius of Gyration | Length in Feet. | | | | | | | |
|-------------------------|-----------------------|-------------------|-------------------------|--------------------------|-----------------|-----|-----|-----|-----|-----|-----|-----|
| | | | | | 8 | 10 | 12 | 14 | 16 | 18 | 20 | 22 |
| Lbs. per Ft. | Inch. | Lbs. per Ft. | Sq. Ins. | Inches. | | | | | | | | |
| 20.5 | $\frac{1}{4}$ | 64.8 | 19.06 | 4.41 | 235 | 233 | 232 | 229 | 227 | 223 | 220 | 217 |
| " | $\frac{5}{16}$ | 70.8 | 20.81 | 4.38 | 257 | 255 | 253 | 250 | 247 | 244 | 240 | 236 |
| " | $\frac{3}{8}$ | 76.7 | 22.56 | 4.36 | 278 | 276 | 273 | 271 | 267 | 264 | 260 | 256 |
| " | $\frac{7}{16}$ | 82.7 | 24.31 | 4.34 | 300 | 298 | 295 | 292 | 288 | 285 | 280 | 275 |
| " | $\frac{1}{2}$ | 88.6 | 26.06 | 4.32 | 321 | 319 | 316 | 313 | 309 | 304 | 300 | 295 |
| " | $\frac{9}{16}$ | 94.6 | 27.81 | 4.30 | 343 | 340 | 337 | 333 | 330 | 325 | 319 | 315 |
| " | $\frac{5}{8}$ | 100.5 | 29.56 | 4.28 | 364 | 362 | 358 | 354 | 350 | 345 | 339 | 335 |
| 25 | $\frac{1}{4}$ | 73.8 | 21.70 | 4.35 | 268 | 266 | 263 | 261 | 257 | 254 | 250 | 246 |
| " | $\frac{5}{16}$ | 79.8 | 23.45 | 4.32 | 289 | 287 | 284 | 282 | 278 | 274 | 270 | 266 |
| " | $\frac{3}{8}$ | 85.7 | 25.20 | 4.31 | 311 | 308 | 305 | 303 | 299 | 294 | 290 | 285 |
| " | $\frac{7}{16}$ | 91.7 | 26.95 | 4.29 | 332 | 330 | 327 | 323 | 319 | 315 | 310 | 305 |
| " | $\frac{1}{2}$ | 97.6 | 28.70 | 4.27 | 354 | 351 | 348 | 344 | 340 | 335 | 330 | 324 |
| " | $\frac{9}{16}$ | 103.6 | 30.45 | 4.26 | 375 | 373 | 369 | 365 | 360 | 356 | 350 | 343 |
| " | $\frac{5}{8}$ | 109.5 | 32.20 | 4.25 | 397 | 393 | 390 | 386 | 381 | 376 | 370 | 363 |
| 30 | $\frac{1}{4}$ | 83.8 | 24.64 | 4.27 | 304 | 302 | 299 | 295 | 292 | 288 | 283 | 278 |
| " | $\frac{5}{16}$ | 89.8 | 26.39 | 4.26 | 325 | 323 | 320 | 316 | 312 | 308 | 303 | 298 |
| " | $\frac{3}{8}$ | 95.7 | 28.14 | 4.25 | 347 | 344 | 341 | 337 | 333 | 329 | 323 | 317 |
| " | $\frac{7}{16}$ | 101.7 | 29.89 | 4.23 | 368 | 365 | 362 | 358 | 353 | 348 | 343 | 337 |
| " | $\frac{1}{2}$ | 107.6 | 31.64 | 4.22 | 390 | 387 | 383 | 379 | 374 | 368 | 363 | 357 |
| " | $\frac{9}{16}$ | 113.6 | 33.39 | 4.21 | 411 | 408 | 404 | 400 | 395 | 389 | 382 | 377 |
| " | $\frac{5}{8}$ | 119.5 | 35.14 | 4.21 | 433 | 429 | 425 | 421 | 415 | 409 | 402 | 396 |
| 35 | $\frac{1}{4}$ | 93.8 | 27.58 | 4.19 | 340 | 337 | 334 | 330 | 326 | 321 | 316 | 310 |
| " | $\frac{5}{16}$ | 99.8 | 29.33 | 4.18 | 361 | 358 | 355 | 351 | 347 | 341 | 336 | 330 |
| " | $\frac{3}{8}$ | 105.7 | 31.08 | 4.18 | 383 | 380 | 376 | 372 | 367 | 362 | 356 | 349 |
| " | $\frac{7}{16}$ | 111.7 | 32.83 | 4.17 | 405 | 401 | 397 | 392 | 388 | 382 | 376 | 369 |
| " | $\frac{1}{2}$ | 117.6 | 34.58 | 4.16 | 426 | 422 | 418 | 413 | 409 | 402 | 396 | 389 |
| " | $\frac{9}{16}$ | 123.6 | 36.33 | 4.16 | 448 | 444 | 439 | 434 | 429 | 423 | 416 | 408 |
| " | $\frac{5}{8}$ | 129.5 | 38.08 | 4.15 | 469 | 465 | 461 | 455 | 449 | 443 | 436 | 428 |
| 40 | $\frac{1}{4}$ | 103.8 | 30.52 | 4.13 | 376 | 373 | 369 | 365 | 360 | 354 | 349 | 343 |
| " | $\frac{5}{16}$ | 109.8 | 32.27 | 4.12 | 398 | 394 | 390 | 386 | 380 | 374 | 368 | 363 |
| " | $\frac{3}{8}$ | 115.7 | 34.02 | 4.12 | 419 | 416 | 411 | 406 | 401 | 395 | 388 | 382 |
| " | $\frac{7}{16}$ | 121.7 | 35.77 | 4.12 | 441 | 437 | 433 | 427 | 421 | 415 | 408 | 402 |
| " | $\frac{1}{2}$ | 127.6 | 37.52 | 4.11 | 462 | 458 | 454 | 448 | 442 | 435 | 428 | 420 |
| " | $\frac{9}{16}$ | 133.6 | 39.27 | 4.11 | 484 | 480 | 475 | 469 | 463 | 456 | 448 | 440 |
| " | $\frac{5}{8}$ | 139.5 | 41.02 | 4.11 | 505 | 501 | 496 | 490 | 483 | 476 | 468 | 459 |

For detail dimensions see page 233

SAFE LOADS IN THOUSANDS OF POUNDS FOR 12" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula $P = \frac{50\,000}{1 + \frac{(12\,L)^2}{36\,000\,r^2}}$ Safety factor 4.



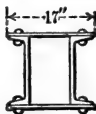
SERIES A.

| Length in Feet. | | | | | | | | | | | Thick- ness of Plates. | Weight of each Channel. |
|-----------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|------------------------------|-------------------------------|
| 24 | 26 | 28 | 30 | 32 | 34 | 36 | 38 | 40 | 42 | 44 | Inch. | Lbs. per Ft. |
| 213 | 209 | 206 | 201 | 196 | 193 | 188 | 184 | 179 | 175 | 170 | $\frac{1}{4}$ | 20.5 |
| 232 | 228 | 223 | 220 | 214 | 209 | 205 | 200 | 195 | 190 | 186 | $\frac{5}{16}$ | " |
| 252 | 246 | 242 | 237 | 232 | 227 | 221 | 216 | 211 | 206 | 200 | $\frac{3}{8}$ | " |
| 271 | 266 | 260 | 255 | 249 | 244 | 238 | 232 | 227 | 223 | 216 | $\frac{7}{16}$ | " |
| 289 | 285 | 279 | 274 | 267 | 261 | 255 | 249 | 242 | 237 | 230 | $\frac{1}{2}$ | " |
| 309 | 304 | 297 | 291 | 285 | 278 | 271 | 265 | 258 | 251 | 245 | $\frac{5}{8}$ | " |
| 328 | 322 | 316 | 309 | 302 | 296 | 288 | 281 | 274 | 267 | 259 | $\frac{3}{4}$ | " |
| 242 | 237 | 233 | 228 | 223 | 218 | 213 | 208 | 203 | 197 | 193 | $\frac{1}{4}$ | 25 |
| 260 | 256 | 251 | 246 | 240 | 235 | 230 | 224 | 218 | 213 | 207 | $\frac{5}{16}$ | " |
| 280 | 275 | 269 | 263 | 258 | 252 | 246 | 241 | 234 | 229 | 222 | $\frac{3}{8}$ | " |
| 299 | 293 | 288 | 282 | 275 | 270 | 263 | 256 | 250 | 243 | 237 | $\frac{7}{16}$ | " |
| 319 | 312 | 306 | 300 | 293 | 286 | 280 | 272 | 265 | 259 | 252 | $\frac{1}{2}$ | " |
| 338 | 331 | 324 | 318 | 311 | 303 | 295 | 289 | 281 | 273 | 267 | $\frac{5}{8}$ | " |
| 358 | 350 | 343 | 335 | 329 | 320 | 312 | 306 | 297 | 289 | 281 | $\frac{3}{4}$ | " |
| 274 | 268 | 262 | 257 | 251 | 245 | 240 | 234 | 228 | 223 | 216 | $\frac{1}{4}$ | 30 |
| 293 | 287 | 281 | 276 | 269 | 263 | 256 | 250 | 244 | 237 | 232 | $\frac{5}{16}$ | " |
| 313 | 306 | 300 | 293 | 287 | 280 | 273 | 267 | 260 | 253 | 246 | $\frac{3}{8}$ | " |
| 331 | 325 | 318 | 311 | 304 | 297 | 290 | 282 | 275 | 268 | 261 | $\frac{7}{16}$ | " |
| 350 | 343 | 337 | 329 | 321 | 313 | 307 | 299 | 291 | 282 | 276 | $\frac{1}{2}$ | " |
| 369 | 362 | 354 | 347 | 339 | 331 | 322 | 315 | 307 | 298 | 290 | $\frac{5}{8}$ | " |
| 389 | 381 | 372 | 365 | 357 | 348 | 339 | 332 | 323 | 314 | 305 | $\frac{3}{4}$ | " |
| 305 | 299 | 292 | 286 | 280 | 273 | 266 | 259 | 253 | 246 | 239 | $\frac{1}{4}$ | 35 |
| 324 | 318 | 311 | 304 | 296 | 290 | 283 | 275 | 268 | 262 | 254 | $\frac{5}{16}$ | " |
| 344 | 337 | 329 | 322 | 314 | 308 | 300 | 292 | 284 | 277 | 270 | $\frac{3}{8}$ | " |
| 362 | 356 | 348 | 340 | 332 | 323 | 317 | 308 | 300 | 291 | 283 | $\frac{7}{16}$ | " |
| 381 | 375 | 366 | 358 | 349 | 341 | 332 | 325 | 316 | 307 | 298 | $\frac{1}{2}$ | " |
| 400 | 394 | 385 | 376 | 367 | 358 | 349 | 341 | 332 | 323 | 313 | $\frac{5}{8}$ | " |
| 420 | 411 | 404 | 394 | 385 | 375 | 365 | 356 | 348 | 338 | 328 | $\frac{3}{4}$ | " |
| 336 | 329 | 322 | 314 | 308 | 301 | 293 | 285 | 277 | 269 | 262 | $\frac{1}{4}$ | 40 |
| 356 | 348 | 340 | 333 | 324 | 316 | 310 | 301 | 293 | 285 | 277 | $\frac{5}{16}$ | " |
| 375 | 367 | 359 | 351 | 342 | 333 | 326 | 318 | 309 | 300 | 292 | $\frac{3}{8}$ | " |
| 394 | 386 | 377 | 369 | 360 | 351 | 343 | 334 | 325 | 316 | 307 | $\frac{7}{16}$ | " |
| 413 | 405 | 396 | 387 | 377 | 368 | 358 | 350 | 341 | 331 | 322 | $\frac{1}{2}$ | " |
| 433 | 424 | 412 | 405 | 395 | 385 | 375 | 367 | 357 | 347 | 337 | $\frac{5}{8}$ | " |
| 452 | 442 | 433 | 423 | 412 | 402 | 391 | 383 | 373 | 362 | 352 | $\frac{3}{4}$ | " |

For detail dimensions see page 233

SAFE LOADS IN THOUSANDS OF POUNDS FOR 15" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula $P = \frac{50\,000}{1 + \frac{(12 L)^2}{36\,000 r^2}}$ Safety factor 4.



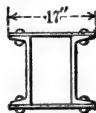
SERIES A.

| Weight of each Channel. | Thick- ness of Plates. | Weight of Column. | Area of Column Section. | Least Radius of Gyration. | Length in Feet. | | | | | | | | | |
|-------------------------------|------------------------------|-------------------------|-------------------------------|---------------------------------|-----------------|-----|-----|-----|-----|-----|-----|-----|-----|--|
| | | | | | 12 | 14 | 16 | 18 | 20 | 22 | 24 | 26 | 28 | |
| Lbs. per Ft. | Inch. | Lbs. per Ft. | Sq. Ins. | Inches. | 12 | 14 | 16 | 18 | 20 | 22 | 24 | 26 | 28 | |
| 33 | $\frac{3}{8}$ | 109.4 | 32.55 | 5.41 | 399 | 396 | 393 | 390 | 386 | 381 | 378 | 373 | 367 | |
| " | $\frac{1}{2}$ | 116.6 | 34.68 | 5.38 | 425 | 422 | 418 | 415 | 411 | 406 | 401 | 397 | 391 | |
| " | $\frac{5}{16}$ | 123.8 | 36.80 | 5.36 | 451 | 448 | 444 | 440 | 436 | 431 | 426 | 420 | 415 | |
| " | $\frac{3}{4}$ | 131.0 | 38.92 | 5.33 | 476 | 474 | 470 | 465 | 460 | 456 | 450 | 444 | 437 | |
| " | $\frac{7}{8}$ | 138.2 | 41.05 | 5.31 | 502 | 500 | 495 | 490 | 485 | 481 | 475 | 468 | 461 | |
| " | $\frac{1}{2}$ | 145.4 | 43.18 | 5.29 | 529 | 526 | 521 | 516 | 510 | 504 | 499 | 492 | 485 | |
| " | $\frac{3}{4}$ | 152.7 | 45.30 | 5.24 | 555 | 550 | 545 | 541 | 535 | 529 | 522 | 515 | 509 | |
| 35 | $\frac{3}{8}$ | 113.4 | 33.33 | 5.40 | 409 | 406 | 402 | 399 | 395 | 390 | 387 | 381 | 376 | |
| " | $\frac{1}{2}$ | 120.6 | 35.46 | 5.37 | 435 | 432 | 428 | 424 | 420 | 415 | 410 | 406 | 400 | |
| " | $\frac{5}{16}$ | 127.8 | 37.58 | 5.35 | 461 | 457 | 453 | 449 | 445 | 440 | 435 | 429 | 424 | |
| " | $\frac{3}{4}$ | 135.0 | 39.70 | 5.32 | 486 | 483 | 479 | 474 | 469 | 465 | 459 | 453 | 446 | |
| " | $\frac{7}{8}$ | 142.2 | 41.83 | 5.30 | 512 | 509 | 505 | 500 | 494 | 488 | 484 | 477 | 470 | |
| " | $\frac{1}{2}$ | 149.4 | 43.96 | 5.28 | 538 | 534 | 530 | 525 | 520 | 513 | 508 | 501 | 494 | |
| " | $\frac{3}{4}$ | 156.7 | 46.08 | 5.27 | 564 | 560 | 556 | 551 | 545 | 538 | 531 | 525 | 518 | |
| 40 | $\frac{3}{8}$ | 123.4 | 36.27 | 5.35 | 445 | 441 | 438 | 433 | 430 | 425 | 419 | 414 | 409 | |
| " | $\frac{1}{2}$ | 130.6 | 38.40 | 5.33 | 470 | 467 | 463 | 459 | 454 | 450 | 444 | 438 | 432 | |
| " | $\frac{5}{16}$ | 137.8 | 40.52 | 5.31 | 496 | 493 | 489 | 484 | 479 | 475 | 469 | 462 | 455 | |
| " | $\frac{3}{4}$ | 145.0 | 42.64 | 5.29 | 522 | 519 | 514 | 509 | 504 | 498 | 493 | 486 | 479 | |
| " | $\frac{7}{8}$ | 152.2 | 44.77 | 5.27 | 548 | 544 | 540 | 535 | 529 | 523 | 516 | 511 | 503 | |
| " | $\frac{1}{2}$ | 159.4 | 46.90 | 5.26 | 574 | 570 | 566 | 560 | 554 | 548 | 540 | 535 | 527 | |
| " | $\frac{3}{4}$ | 166.7 | 49.02 | 5.24 | 600 | 595 | 590 | 586 | 579 | 572 | 565 | 557 | 551 | |
| 45 | $\frac{3}{8}$ | 133.4 | 39.23 | 5.31 | 480 | 477 | 473 | 469 | 464 | 459 | 454 | 447 | 441 | |
| " | $\frac{1}{2}$ | 140.6 | 41.36 | 5.29 | 506 | 503 | 499 | 494 | 489 | 483 | 478 | 472 | 465 | |
| " | $\frac{5}{16}$ | 147.8 | 43.48 | 5.27 | 532 | 528 | 525 | 519 | 514 | 508 | 501 | 496 | 489 | |
| " | $\frac{3}{4}$ | 155.0 | 45.60 | 5.25 | 558 | 554 | 550 | 545 | 539 | 532 | 525 | 518 | 512 | |
| " | $\frac{7}{8}$ | 162.2 | 47.73 | 5.24 | 584 | 580 | 575 | 570 | 564 | 557 | 550 | 542 | 536 | |
| " | $\frac{1}{2}$ | 169.4 | 49.86 | 5.23 | 610 | 606 | 600 | 596 | 589 | 582 | 575 | 567 | 558 | |
| " | $\frac{3}{4}$ | 176.7 | 51.98 | 5.21 | 636 | 631 | 626 | 619 | 614 | 607 | 599 | 591 | 582 | |
| 50 | $\frac{3}{8}$ | 143.4 | 42.17 | 5.26 | 516 | 512 | 509 | 504 | 498 | 492 | 486 | 481 | 474 | |
| " | $\frac{1}{2}$ | 150.6 | 44.30 | 5.24 | 542 | 538 | 533 | 529 | 524 | 517 | 511 | 503 | 498 | |
| " | $\frac{5}{16}$ | 157.8 | 46.42 | 5.23 | 568 | 564 | 559 | 555 | 549 | 542 | 535 | 528 | 520 | |
| " | $\frac{3}{4}$ | 165.0 | 48.54 | 5.21 | 594 | 590 | 584 | 578 | 574 | 567 | 559 | 552 | 543 | |
| " | $\frac{7}{8}$ | 172.2 | 50.67 | 5.20 | 620 | 615 | 610 | 604 | 599 | 592 | 584 | 576 | 567 | |
| " | $\frac{1}{2}$ | 179.4 | 52.80 | 5.19 | 646 | 641 | 636 | 629 | 622 | 616 | 608 | 600 | 591 | |
| " | $\frac{3}{4}$ | 186.7 | 54.92 | 5.18 | 672 | 667 | 661 | 654 | 647 | 641 | 633 | 624 | 615 | |
| 55 | $\frac{3}{8}$ | 153.4 | 45.11 | 5.21 | 552 | 548 | 543 | 538 | 533 | 527 | 520 | 513 | 505 | |
| " | $\frac{1}{2}$ | 160.6 | 47.24 | 5.19 | 578 | 574 | 569 | 563 | 557 | 552 | 544 | 537 | 529 | |
| " | $\frac{5}{16}$ | 167.8 | 49.36 | 5.18 | 604 | 600 | 594 | 588 | 582 | 576 | 569 | 561 | 553 | |
| " | $\frac{3}{4}$ | 175.0 | 51.48 | 5.17 | 630 | 625 | 620 | 613 | 607 | 599 | 593 | 585 | 576 | |
| " | $\frac{7}{8}$ | 182.2 | 53.61 | 5.16 | 656 | 651 | 645 | 639 | 632 | 624 | 616 | 609 | 600 | |
| " | $\frac{1}{2}$ | 189.4 | 55.74 | 5.15 | 682 | 677 | 671 | 664 | 657 | 649 | 640 | 633 | 624 | |
| " | $\frac{3}{4}$ | 196.7 | 57.86 | 5.14 | 708 | 703 | 696 | 689 | 682 | 673 | 665 | 655 | 648 | |

For detail dimensions see page 233

SAFE LOADS IN THOUSANDS OF POUNDS FOR 15" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula $P = \frac{50\,000}{1 + \frac{(12 L)^2}{36\,000 r^2}}$ Safety factor 4.



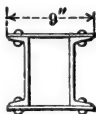
SERIES A.

| Length in Feet. | | | | | | | | | | | | Thick- ness of Plates. | Weight of each Channel. |
|-----------------|------|------|------|------|------|------|------|------|------|------|------|------------------------------|-------------------------------|
| 30 | 32 | 34 | 36 | 38 | 40 | 42 | 44 | 46 | 48 | 50 | 52 | Inch. | Lbs. per Ft. |
| 363 | 357 | 351 | 345 | 340 | 334 | 327 | 322 | 316 | 309 | 304 | 297 | 3/8 | 33 |
| 385 | 381 | 374 | 368 | 361 | 356 | 349 | 342 | 335 | 329 | 322 | 315 | 1/2 | " |
| 409 | 402 | 397 | 390 | 383 | 376 | 370 | 362 | 355 | 347 | 342 | 334 | 5/8 | " |
| 432 | 425 | 418 | 411 | 405 | 397 | 389 | 381 | 375 | 367 | 359 | 351 | 7/8 | " |
| 456 | 449 | 441 | 433 | 425 | 419 | 411 | 402 | 394 | 388 | 379 | 371 | 1 1/8 | " |
| 478 | 472 | 464 | 456 | 447 | 438 | 432 | 423 | 414 | 405 | 397 | 390 | 1 1/4 | " |
| 501 | 493 | 484 | 476 | 467 | 460 | 451 | 442 | 432 | 423 | 416 | 407 | 1 3/4 | " |
| 570 | 566 | 560 | 553 | 548 | 542 | 535 | 530 | 523 | 516 | 510 | 504 | 1 7/8 | 35 |
| 594 | 587 | 583 | 576 | 569 | 564 | 557 | 549 | 542 | 537 | 529 | 522 | 2 | " |
| 617 | 611 | 604 | 598 | 591 | 583 | 576 | 570 | 562 | 555 | 549 | 541 | 2 1/8 | " |
| 641 | 634 | 626 | 619 | 613 | 605 | 597 | 589 | 583 | 575 | 567 | 559 | 2 1/4 | " |
| 663 | 657 | 649 | 641 | 633 | 627 | 618 | 610 | 601 | 593 | 586 | 578 | 2 3/8 | " |
| 686 | 678 | 672 | 664 | 655 | 646 | 637 | 631 | 622 | 613 | 604 | 597 | 2 1/2 | " |
| 709 | 701 | 693 | 686 | 677 | 668 | 659 | 652 | 642 | 633 | 623 | 614 | 2 5/8 | " |
| 780 | 776 | 769 | 762 | 753 | 744 | 735 | 726 | 716 | 706 | 696 | 686 | 3 | 40 |
| 803 | 796 | 788 | 780 | 771 | 762 | 753 | 744 | 734 | 724 | 714 | 704 | 3 1/8 | " |
| 827 | 820 | 812 | 803 | 794 | 784 | 774 | 764 | 754 | 743 | 733 | 722 | 3 1/4 | " |
| 850 | 843 | 835 | 826 | 816 | 806 | 796 | 785 | 774 | 763 | 752 | 741 | 3 3/8 | " |
| 872 | 866 | 858 | 848 | 838 | 827 | 816 | 805 | 794 | 782 | 771 | 759 | 3 1/2 | " |
| 895 | 887 | 879 | 869 | 858 | 847 | 835 | 824 | 812 | 800 | 788 | 776 | 3 5/8 | " |
| 919 | 910 | 902 | 891 | 880 | 868 | 856 | 844 | 832 | 819 | 807 | 794 | 4 | " |
| 942 | 933 | 924 | 913 | 901 | 889 | 876 | 864 | 851 | 838 | 825 | 812 | 4 1/8 | " |
| 1013 | 1009 | 1001 | 991 | 980 | 968 | 956 | 943 | 930 | 917 | 903 | 890 | 4 1/4 | 45 |
| 1036 | 1029 | 1021 | 1010 | 1000 | 988 | 976 | 963 | 950 | 936 | 923 | 909 | 4 3/8 | " |
| 1058 | 1052 | 1044 | 1033 | 1022 | 1010 | 998 | 985 | 972 | 958 | 944 | 930 | 4 1/2 | " |
| 1081 | 1074 | 1066 | 1055 | 1044 | 1032 | 1020 | 1007 | 994 | 979 | 965 | 951 | 4 3/4 | " |
| 1104 | 1097 | 1089 | 1077 | 1066 | 1054 | 1042 | 1029 | 1016 | 1001 | 987 | 972 | 4 7/8 | " |
| 1127 | 1120 | 1112 | 1101 | 1090 | 1078 | 1066 | 1053 | 1040 | 1025 | 1011 | 996 | 5 | " |
| 1198 | 1194 | 1186 | 1174 | 1163 | 1151 | 1139 | 1126 | 1113 | 1098 | 1083 | 1068 | 5 1/8 | 50 |
| 1221 | 1214 | 1206 | 1195 | 1184 | 1172 | 1160 | 1147 | 1134 | 1119 | 1104 | 1089 | 5 1/4 | " |
| 1244 | 1237 | 1229 | 1218 | 1207 | 1195 | 1183 | 1169 | 1156 | 1141 | 1126 | 1111 | 5 1/2 | " |
| 1267 | 1260 | 1252 | 1241 | 1230 | 1218 | 1206 | 1192 | 1179 | 1164 | 1149 | 1134 | 5 3/8 | " |
| 1290 | 1283 | 1275 | 1264 | 1253 | 1241 | 1229 | 1215 | 1202 | 1187 | 1172 | 1157 | 5 1/2 | " |
| 1313 | 1306 | 1298 | 1287 | 1276 | 1264 | 1252 | 1238 | 1225 | 1209 | 1194 | 1179 | 5 5/8 | " |
| 1336 | 1329 | 1321 | 1310 | 1299 | 1287 | 1275 | 1261 | 1248 | 1232 | 1217 | 1202 | 5 3/4 | " |
| 1407 | 1403 | 1395 | 1384 | 1373 | 1361 | 1349 | 1335 | 1322 | 1306 | 1291 | 1276 | 6 | 55 |
| 1430 | 1423 | 1415 | 1404 | 1393 | 1381 | 1369 | 1355 | 1342 | 1326 | 1311 | 1296 | 6 1/8 | " |
| 1453 | 1446 | 1438 | 1427 | 1416 | 1404 | 1392 | 1378 | 1365 | 1349 | 1334 | 1319 | 6 1/4 | " |
| 1476 | 1469 | 1461 | 1450 | 1439 | 1427 | 1415 | 1401 | 1388 | 1372 | 1357 | 1342 | 6 1/2 | " |
| 1499 | 1492 | 1484 | 1473 | 1462 | 1450 | 1438 | 1424 | 1411 | 1395 | 1380 | 1365 | 6 3/8 | " |
| 1522 | 1515 | 1507 | 1496 | 1485 | 1473 | 1461 | 1447 | 1434 | 1418 | 1403 | 1388 | 6 1/2 | " |
| 1545 | 1538 | 1530 | 1519 | 1508 | 1496 | 1484 | 1470 | 1457 | 1441 | 1426 | 1411 | 6 5/8 | " |
| 1568 | 1561 | 1553 | 1542 | 1531 | 1519 | 1507 | 1493 | 1480 | 1464 | 1449 | 1434 | 6 3/4 | " |
| 1591 | 1584 | 1576 | 1565 | 1554 | 1542 | 1530 | 1516 | 1503 | 1487 | 1472 | 1457 | 6 7/8 | " |
| 1614 | 1607 | 1599 | 1588 | 1577 | 1565 | 1553 | 1539 | 1526 | 1510 | 1495 | 1480 | 7 | " |
| 1638 | 1631 | 1623 | 1612 | 1601 | 1589 | 1577 | 1563 | 1550 | 1534 | 1519 | 1504 | 7 1/8 | " |

For detail dimensions see page 233

SAFE LOADS IN THOUSANDS OF POUNDS FOR 6" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula $P = \frac{50\,000}{1 + \frac{(12 L)^2}{36\,000 r^2}}$ Safety factor 4.



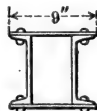
SERIES B.

| Weight of each Channel. | Thickness of Plates. | Weight of Column. | Area of Column Section. | Least Radius of Gyration. | Length in Feet. | | | | |
|-------------------------------|----------------------------|-------------------------|-------------------------------|---------------------------------|-----------------|-----|-----|-----|-----|
| Lbs. per Foot. | Inch. | Lbs. per Ft. | Sq. Ins. | Inches. | 4 | 6 | 8 | 10 | 12 |
| 8 | $\frac{1}{4}$ | 31.3 | 9.26 | 2.74 | 115 | 114 | 112 | 110 | 107 |
| " | $\frac{5}{16}$ | 35.1 | 10.39 | 2.73 | 129 | 127 | 126 | 123 | 121 |
| " | $\frac{3}{8}$ | 39.0 | 11.51 | 2.71 | 142 | 141 | 139 | 136 | 134 |
| " | $\frac{7}{16}$ | 42.8 | 12.64 | 2.70 | 156 | 155 | 153 | 150 | 147 |
| " | $\frac{1}{2}$ | 46.6 | 13.76 | 2.70 | 170 | 169 | 166 | 163 | 160 |
| " | $\frac{5}{8}$ | 50.4 | 14.89 | 2.69 | 184 | 183 | 180 | 176 | 172 |
| " | $\frac{3}{4}$ | 54.3 | 16.01 | 2.68 | 198 | 196 | 193 | 190 | 185 |
| 10.5 | $\frac{1}{4}$ | 36.3 | 10.68 | 2.68 | 132 | 131 | 129 | 126 | 123 |
| " | $\frac{5}{16}$ | 40.1 | 11.81 | 2.67 | 146 | 145 | 142 | 140 | 137 |
| " | $\frac{3}{8}$ | 44.0 | 12.93 | 2.66 | 160 | 158 | 156 | 153 | 150 |
| " | $\frac{7}{16}$ | 47.8 | 14.06 | 2.66 | 174 | 172 | 170 | 166 | 163 |
| " | $\frac{1}{2}$ | 51.6 | 15.18 | 2.65 | 188 | 186 | 183 | 179 | 176 |
| " | $\frac{5}{8}$ | 55.4 | 16.31 | 2.65 | 202 | 200 | 197 | 193 | 189 |
| " | $\frac{3}{4}$ | 59.3 | 17.43 | 2.65 | 216 | 213 | 210 | 206 | 202 |
| 13 | $\frac{1}{4}$ | 41.3 | 12.14 | 2.54 | 150 | 148 | 146 | 143 | 139 |
| " | $\frac{5}{16}$ | 45.1 | 13.27 | 2.62 | 164 | 162 | 160 | 157 | 153 |
| " | $\frac{3}{8}$ | 49.0 | 14.39 | 2.62 | 178 | 176 | 173 | 170 | 164 |
| " | $\frac{7}{16}$ | 52.8 | 15.52 | 2.62 | 192 | 190 | 187 | 183 | 179 |
| " | $\frac{1}{2}$ | 56.6 | 16.64 | 2.61 | 206 | 204 | 200 | 197 | 192 |
| " | $\frac{5}{8}$ | 60.4 | 17.77 | 2.61 | 220 | 218 | 214 | 210 | 205 |
| " | $\frac{3}{4}$ | 64.3 | 18.89 | 2.61 | 234 | 231 | 227 | 223 | 218 |
| 15.5 | $\frac{1}{4}$ | 46.3 | 13.62 | 2.47 | 169 | 166 | 164 | 160 | 155 |
| " | $\frac{5}{16}$ | 50.1 | 14.75 | 2.54 | 183 | 180 | 178 | 174 | 169 |
| " | $\frac{3}{8}$ | 54.0 | 15.87 | 2.57 | 196 | 194 | 191 | 187 | 182 |
| " | $\frac{7}{16}$ | 57.8 | 17.00 | 2.57 | 210 | 208 | 205 | 200 | 195 |
| " | $\frac{1}{2}$ | 61.6 | 18.12 | 2.57 | 224 | 222 | 218 | 214 | 208 |
| " | $\frac{5}{8}$ | 65.4 | 19.25 | 2.57 | 238 | 236 | 232 | 227 | 221 |
| " | $\frac{3}{4}$ | 69.3 | 20.37 | 2.57 | 252 | 249 | 245 | 240 | 234 |

For detail dimensions see page 234

SAFE LOADS IN THOUSANDS OF POUNDS FOR 6" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula $P = \frac{50\,000}{1 + \frac{(12\,L)^2}{36\,000\,r^2}}$ Safety factor 4.



SERIES B.

| Length in Feet. | | | | | | | | Thickness of Plates. | Weight of each Channel. |
|-----------------|-----|-----|-----|-----|-----|-----|-----|----------------------------|-------------------------------|
| 14 | 16 | 18 | 20 | 22 | 24 | 26 | 28 | Inch. | Lbs. per Ft. |
| 105 | 102 | 99 | 95 | 92 | 88 | 85 | 82 | $\frac{1}{4}$ | 8 |
| 118 | 114 | 111 | 107 | 103 | 99 | 95 | 91 | $\frac{5}{16}$ | " |
| 130 | 126 | 123 | 118 | 114 | 109 | 105 | 101 | $\frac{3}{8}$ | " |
| 143 | 139 | 134 | 130 | 125 | 120 | 115 | 110 | $\frac{7}{16}$ | " |
| 155 | 151 | 146 | 141 | 136 | 131 | 126 | 120 | $\frac{1}{2}$ | " |
| 168 | 163 | 158 | 153 | 147 | 141 | 135 | 130 | $\frac{5}{8}$ | " |
| 181 | 175 | 170 | 163 | 158 | 151 | 145 | 140 | $\frac{3}{4}$ | " |
| 120 | 116 | 113 | 108 | 105 | 100 | 96 | 92 | $\frac{1}{4}$ | 10.5 |
| 133 | 129 | 125 | 121 | 116 | 111 | 107 | 102 | $\frac{5}{16}$ | " |
| 145 | 141 | 136 | 132 | 127 | 122 | 117 | 112 | $\frac{3}{8}$ | " |
| 158 | 154 | 148 | 143 | 138 | 133 | 127 | 122 | $\frac{7}{16}$ | " |
| 171 | 166 | 160 | 155 | 149 | 143 | 137 | 131 | $\frac{1}{2}$ | " |
| 183 | 178 | 172 | 166 | 160 | 153 | 147 | 141 | $\frac{5}{8}$ | " |
| 196 | 190 | 184 | 178 | 171 | 164 | 157 | 151 | $\frac{3}{4}$ | " |
| 135 | 131 | 126 | 121 | 116 | 112 | 107 | 102 | $\frac{1}{4}$ | 13 |
| 149 | 144 | 139 | 135 | 129 | 124 | 119 | 114 | $\frac{5}{16}$ | " |
| 162 | 157 | 151 | 146 | 134 | 134 | 129 | 123 | $\frac{3}{8}$ | " |
| 174 | 169 | 163 | 158 | 151 | 145 | 139 | 133 | $\frac{7}{16}$ | " |
| 186 | 181 | 175 | 168 | 162 | 155 | 149 | 143 | $\frac{1}{2}$ | " |
| 199 | 193 | 187 | 180 | 173 | 166 | 159 | 152 | $\frac{5}{8}$ | " |
| 211 | 206 | 198 | 191 | 184 | 176 | 169 | 162 | $\frac{3}{4}$ | " |
| 151 | 146 | 140 | 135 | 129 | 124 | 118 | 113 | $\frac{1}{4}$ | 15.5 |
| 164 | 159 | 153 | 148 | 142 | 136 | 130 | 124 | $\frac{5}{16}$ | " |
| 178 | 172 | 166 | 160 | 153 | 147 | 141 | 134 | $\frac{3}{8}$ | " |
| 190 | 184 | 178 | 171 | 164 | 158 | 151 | 144 | $\frac{7}{16}$ | " |
| 203 | 196 | 189 | 182 | 175 | 168 | 161 | 154 | $\frac{1}{2}$ | " |
| 215 | 209 | 201 | 194 | 186 | 179 | 171 | 163 | $\frac{5}{8}$ | " |
| 228 | 221 | 213 | 205 | 196 | 189 | 181 | 173 | $\frac{3}{4}$ | " |

For detail dimensions see page 234

SAFE LOADS IN THOUSANDS OF POUNDS FOR 7" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula $P = \frac{50\,000}{1 + \frac{(12 L)^2}{36\,000 r^2}}$ Safety factor 4.



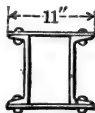
SERIES B.

| Weight of each Channel. | Thick-ness of Plates. | Weight of Column. | Area of Column Section. | Least Radius of Gyration. | Length in Feet. | | | | | |
|-------------------------|-----------------------|-------------------|-------------------------|---------------------------|-----------------|-----|-----|-----|-----|-----|
| Lbs. per Ft. | Inch. | Lbs. per Ft. | Sq. Ina. | Inches. | 6 | 8 | 10 | 12 | 14 | 16 |
| 9.75 | $\frac{1}{4}$ | 38.2 | 11.20 | 3.20 | 138 | 137 | 135 | 132 | 130 | 127 |
| " | $\frac{3}{8}$ | 42.9 | 12.58 | 3.27 | 155 | 154 | 151 | 149 | 146 | 143 |
| " | $\frac{1}{2}$ | 47.6 | 13.95 | 3.33 | 172 | 170 | 168 | 166 | 163 | 160 |
| " | $\frac{5}{8}$ | 52.2 | 15.32 | 3.35 | 189 | 187 | 185 | 182 | 179 | 175 |
| " | $\frac{3}{4}$ | 56.9 | 16.70 | 3.34 | 206 | 204 | 202 | 198 | 195 | 191 |
| " | $\frac{7}{8}$ | 61.5 | 18.08 | 3.33 | 223 | 221 | 218 | 215 | 211 | 207 |
| " | $\frac{1}{2}$ | 66.3 | 19.45 | 3.32 | 240 | 238 | 235 | 231 | 227 | 223 |
| 12.25 | $\frac{1}{4}$ | 43.2 | 12.70 | 3.08 | 156 | 155 | 153 | 150 | 147 | 143 |
| " | $\frac{3}{8}$ | 47.9 | 14.08 | 3.16 | 173 | 172 | 169 | 166 | 163 | 159 |
| " | $\frac{1}{2}$ | 52.6 | 15.45 | 3.22 | 190 | 188 | 186 | 183 | 180 | 176 |
| " | $\frac{5}{8}$ | 57.2 | 16.82 | 3.29 | 208 | 206 | 203 | 200 | 196 | 192 |
| " | $\frac{3}{4}$ | 61.9 | 18.20 | 3.31 | 225 | 222 | 220 | 216 | 213 | 208 |
| " | $\frac{7}{8}$ | 66.5 | 19.58 | 3.30 | 242 | 239 | 236 | 233 | 229 | 224 |
| " | $\frac{1}{2}$ | 71.3 | 20.95 | 3.29 | 259 | 256 | 253 | 249 | 244 | 239 |
| 14.75 | $\frac{1}{4}$ | 48.2 | 14.18 | 2.99 | 174 | 172 | 170 | 167 | 163 | 159 |
| " | $\frac{3}{8}$ | 52.9 | 15.56 | 3.07 | 191 | 189 | 186 | 183 | 179 | 176 |
| " | $\frac{1}{2}$ | 57.6 | 16.93 | 3.14 | 209 | 206 | 203 | 200 | 196 | 192 |
| " | $\frac{5}{8}$ | 62.2 | 18.30 | 3.20 | 225 | 223 | 220 | 216 | 212 | 208 |
| " | $\frac{3}{4}$ | 66.9 | 19.68 | 3.26 | 243 | 240 | 237 | 233 | 229 | 224 |
| " | $\frac{7}{8}$ | 71.5 | 21.06 | 3.27 | 260 | 257 | 253 | 250 | 245 | 240 |
| " | $\frac{1}{2}$ | 76.3 | 22.43 | 3.27 | 277 | 274 | 270 | 266 | 261 | 256 |
| 17.25 | $\frac{1}{4}$ | 53.2 | 15.64 | 2.91 | 192 | 190 | 187 | 183 | 179 | 174 |
| " | $\frac{3}{8}$ | 57.9 | 17.02 | 2.99 | 209 | 207 | 204 | 200 | 195 | 191 |
| " | $\frac{1}{2}$ | 62.6 | 18.39 | 3.06 | 226 | 224 | 220 | 217 | 212 | 207 |
| " | $\frac{5}{8}$ | 67.2 | 19.76 | 3.13 | 243 | 240 | 237 | 234 | 228 | 224 |
| " | $\frac{3}{4}$ | 71.9 | 21.14 | 3.19 | 260 | 258 | 254 | 250 | 245 | 240 |
| " | $\frac{7}{8}$ | 76.5 | 22.52 | 3.24 | 277 | 275 | 271 | 267 | 262 | 257 |
| " | $\frac{1}{2}$ | 81.3 | 23.89 | 3.24 | 294 | 291 | 288 | 283 | 278 | 272 |
| 19.75 | $\frac{1}{4}$ | 58.2 | 17.12 | 2.85 | 210 | 207 | 204 | 200 | 195 | 190 |
| " | $\frac{3}{8}$ | 62.9 | 18.50 | 2.93 | 228 | 225 | 221 | 217 | 212 | 206 |
| " | $\frac{1}{2}$ | 67.6 | 19.87 | 3.00 | 244 | 241 | 238 | 233 | 228 | 223 |
| " | $\frac{5}{8}$ | 72.2 | 21.24 | 3.07 | 261 | 259 | 254 | 250 | 245 | 240 |
| " | $\frac{3}{4}$ | 76.9 | 22.62 | 3.13 | 279 | 275 | 272 | 267 | 262 | 256 |
| " | $\frac{7}{8}$ | 81.5 | 24.00 | 3.19 | 296 | 293 | 289 | 284 | 278 | 273 |
| " | $\frac{1}{2}$ | 86.3 | 25.37 | 3.21 | 313 | 309 | 305 | 301 | 294 | 288 |

For detail dimensions see page 234

SAFE LOADS IN THOUSANDS OF POUNDS FOR 7" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula $P = \frac{50\,000}{1 + \frac{(12 L)^2}{36\,000 r^2}}$ Safety factor 4.



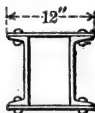
SERIES B.

| Length in Feet. | | | | | | | | | Thickness of Plates. | Weight of each Channel. |
|-----------------|-----|-----|-----|-----|-----|-----|-----|-----|----------------------------|-------------------------------|
| 18 | 20 | 22 | 24 | 26 | 28 | 30 | 32 | 34 | Inch. | Lbs. per Ft. |
| 124 | 121 | 118 | 114 | 111 | 107 | 103 | 100 | 97 | $\frac{1}{4}$ | 9.75 |
| 140 | 137 | 133 | 130 | 125 | 121 | 117 | 114 | 110 | $\frac{1}{8}$ | " |
| 156 | 152 | 148 | 144 | 140 | 136 | 132 | 127 | 123 | $\frac{3}{8}$ | " |
| 171 | 167 | 163 | 159 | 154 | 149 | 145 | 140 | 136 | $\frac{1}{2}$ | " |
| 187 | 182 | 178 | 173 | 168 | 163 | 158 | 153 | 147 | $\frac{5}{8}$ | " |
| 202 | 198 | 192 | 187 | 182 | 173 | 171 | 165 | 160 | $\frac{1}{2}$ | " |
| 218 | 213 | 207 | 201 | 196 | 190 | 184 | 178 | 172 | $\frac{3}{8}$ | " |
| 140 | 136 | 132 | 128 | 124 | 119 | 115 | 111 | 107 | $\frac{1}{4}$ | 12.25 |
| 156 | 152 | 147 | 143 | 139 | 134 | 129 | 125 | 120 | $\frac{1}{8}$ | " |
| 172 | 167 | 163 | 158 | 153 | 148 | 143 | 139 | 133 | $\frac{3}{8}$ | " |
| 188 | 183 | 178 | 173 | 168 | 163 | 158 | 153 | 148 | $\frac{1}{2}$ | " |
| 204 | 199 | 194 | 188 | 182 | 176 | 171 | 165 | 160 | $\frac{1}{2}$ | " |
| 218 | 213 | 207 | 202 | 196 | 190 | 184 | 178 | 172 | $\frac{1}{2}$ | " |
| 234 | 228 | 222 | 216 | 210 | 203 | 197 | 190 | 184 | $\frac{3}{8}$ | " |
| 155 | 150 | 145 | 141 | 136 | 131 | 127 | 122 | 117 | $\frac{1}{4}$ | 14.75 |
| 171 | 166 | 161 | 156 | 151 | 146 | 141 | 136 | 130 | $\frac{1}{8}$ | " |
| 187 | 182 | 177 | 172 | 166 | 161 | 155 | 149 | 144 | $\frac{3}{8}$ | " |
| 203 | 198 | 192 | 187 | 181 | 175 | 169 | 163 | 158 | $\frac{1}{2}$ | " |
| 219 | 214 | 209 | 202 | 196 | 190 | 184 | 178 | 172 | $\frac{1}{2}$ | " |
| 235 | 229 | 223 | 217 | 210 | 203 | 197 | 190 | 184 | $\frac{1}{2}$ | " |
| 250 | 244 | 238 | 231 | 223 | 216 | 209 | 203 | 196 | $\frac{3}{8}$ | " |
| 169 | 164 | 159 | 154 | 148 | 143 | 137 | 132 | 128 | $\frac{1}{4}$ | 17.25 |
| 186 | 180 | 175 | 169 | 163 | 157 | 152 | 146 | 140 | $\frac{1}{8}$ | " |
| 202 | 197 | 190 | 185 | 178 | 172 | 166 | 160 | 154 | $\frac{3}{8}$ | " |
| 218 | 212 | 206 | 200 | 194 | 188 | 180 | 174 | 167 | $\frac{1}{2}$ | " |
| 235 | 228 | 222 | 216 | 208 | 202 | 195 | 189 | 181 | $\frac{1}{2}$ | " |
| 250 | 244 | 238 | 231 | 224 | 217 | 209 | 202 | 195 | $\frac{1}{2}$ | " |
| 265 | 259 | 252 | 245 | 238 | 230 | 222 | 215 | 207 | $\frac{3}{8}$ | " |
| 185 | 179 | 173 | 167 | 161 | 155 | 149 | 143 | 137 | $\frac{1}{4}$ | 19.75 |
| 201 | 195 | 189 | 182 | 176 | 169 | 163 | 157 | 150 | $\frac{1}{8}$ | " |
| 217 | 211 | 205 | 198 | 191 | 185 | 177 | 170 | 164 | $\frac{3}{8}$ | " |
| 233 | 227 | 220 | 214 | 206 | 199 | 192 | 185 | 178 | $\frac{1}{2}$ | " |
| 249 | 243 | 236 | 229 | 222 | 215 | 207 | 200 | 192 | $\frac{1}{2}$ | " |
| 267 | 259 | 252 | 245 | 236 | 229 | 222 | 214 | 206 | $\frac{1}{2}$ | " |
| 282 | 275 | 266 | 259 | 251 | 243 | 236 | 227 | 219 | $\frac{3}{8}$ | " |

For detail dimensions see page 234

SAFE LOADS IN THOUSANDS OF POUNDS FOR 8" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula $P = \frac{50\,000}{1 + \frac{(12\,L)^2}{36\,000\,r^2}}$. Safety factor 4.



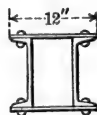
SERIES B.

| Weight of each Channel. Lbs. per Ft. | Thick- ness of Plates. | Weight of Column. Lbs. per Ft. | Area of Column Section. Sq. Ins. | Least Radius of Gyration. Inches. | Length in Feet. | | | | | | |
|---|------------------------------|---|---|--|-----------------|-----|-----|-----|-----|-----|-----|
| | Inch. | | | | 6 | 8 | 10 | 12 | 14 | 16 | 18 |
| 11.25 | $\frac{1}{4}$ | 42.9 | 12.70 | 3.62 | 157 | 156 | 154 | 152 | 150 | 147 | 144 |
| " | $\frac{3}{8}$ | 48.0 | 14.20 | 3.70 | 176 | 174 | 172 | 171 | 168 | 165 | 162 |
| " | $\frac{1}{2}$ | 53.1 | 15.70 | 3.72 | 194 | 193 | 191 | 189 | 186 | 183 | 180 |
| " | $\frac{5}{8}$ | 58.2 | 17.20 | 3.70 | 213 | 211 | 209 | 207 | 203 | 200 | 196 |
| " | $\frac{3}{4}$ | 63.3 | 18.70 | 3.68 | 231 | 229 | 227 | 224 | 221 | 218 | 213 |
| " | $\frac{7}{8}$ | 68.4 | 20.20 | 3.66 | 250 | 248 | 245 | 242 | 239 | 234 | 230 |
| " | $\frac{1}{8}$ | 73.5 | 21.70 | 3.65 | 268 | 266 | 264 | 260 | 256 | 252 | 247 |
| 13.75 | $\frac{1}{4}$ | 47.9 | 14.08 | 3.52 | 174 | 172 | 171 | 168 | 165 | 163 | 159 |
| " | $\frac{3}{8}$ | 53.0 | 15.58 | 3.60 | 193 | 191 | 189 | 187 | 184 | 181 | 177 |
| " | $\frac{1}{2}$ | 58.1 | 17.08 | 3.67 | 211 | 209 | 207 | 205 | 202 | 198 | 195 |
| " | $\frac{5}{8}$ | 63.2 | 18.58 | 3.67 | 230 | 228 | 226 | 223 | 220 | 216 | 212 |
| " | $\frac{3}{4}$ | 68.3 | 20.08 | 3.66 | 248 | 246 | 244 | 241 | 237 | 233 | 229 |
| " | $\frac{7}{8}$ | 73.4 | 21.58 | 3.64 | 267 | 265 | 262 | 258 | 255 | 250 | 246 |
| " | $\frac{1}{8}$ | 78.5 | 23.08 | 3.63 | 285 | 283 | 280 | 276 | 272 | 268 | 263 |
| 16.25 | $\frac{1}{4}$ | 52.9 | 15.56 | 3.42 | 192 | 190 | 188 | 185 | 182 | 179 | 175 |
| " | $\frac{3}{8}$ | 58.0 | 17.06 | 3.50 | 211 | 209 | 206 | 204 | 200 | 197 | 193 |
| " | $\frac{1}{2}$ | 63.1 | 18.56 | 3.58 | 229 | 228 | 225 | 222 | 219 | 215 | 211 |
| " | $\frac{5}{8}$ | 68.2 | 20.06 | 3.64 | 248 | 246 | 244 | 240 | 237 | 233 | 229 |
| " | $\frac{3}{4}$ | 73.3 | 21.56 | 3.63 | 266 | 264 | 261 | 253 | 254 | 250 | 245 |
| " | $\frac{7}{8}$ | 78.4 | 23.06 | 3.62 | 285 | 283 | 279 | 276 | 272 | 268 | 262 |
| " | $\frac{1}{8}$ | 83.5 | 24.56 | 3.61 | 303 | 301 | 298 | 294 | 289 | 285 | 279 |
| 18.75 | $\frac{1}{4}$ | 57.9 | 17.02 | 3.34 | 210 | 208 | 205 | 202 | 199 | 195 | 191 |
| " | $\frac{3}{8}$ | 63.0 | 18.52 | 3.42 | 229 | 227 | 224 | 221 | 217 | 213 | 208 |
| " | $\frac{1}{2}$ | 68.1 | 20.02 | 3.50 | 247 | 245 | 242 | 239 | 235 | 231 | 227 |
| " | $\frac{5}{8}$ | 73.2 | 21.52 | 3.57 | 266 | 264 | 261 | 257 | 254 | 249 | 245 |
| " | $\frac{3}{4}$ | 78.3 | 23.02 | 3.61 | 284 | 282 | 279 | 276 | 271 | 267 | 262 |
| " | $\frac{7}{8}$ | 83.4 | 24.52 | 3.60 | 303 | 301 | 297 | 294 | 289 | 284 | 279 |
| " | $\frac{1}{8}$ | 88.5 | 26.02 | 3.59 | 322 | 319 | 315 | 312 | 307 | 301 | 296 |
| 21.25 | $\frac{1}{4}$ | 62.9 | 18.50 | 3.27 | 228 | 226 | 223 | 219 | 215 | 211 | 206 |
| " | $\frac{3}{8}$ | 68.0 | 20.00 | 3.36 | 247 | 244 | 241 | 238 | 234 | 229 | 224 |
| " | $\frac{1}{2}$ | 73.1 | 21.50 | 3.43 | 266 | 263 | 260 | 256 | 252 | 247 | 243 |
| " | $\frac{5}{8}$ | 78.2 | 23.00 | 3.51 | 284 | 282 | 279 | 275 | 270 | 265 | 260 |
| " | $\frac{3}{4}$ | 83.3 | 24.50 | 3.57 | 303 | 300 | 297 | 293 | 289 | 283 | 278 |
| " | $\frac{7}{8}$ | 88.4 | 26.00 | 3.57 | 321 | 319 | 315 | 311 | 306 | 301 | 295 |
| " | $\frac{1}{8}$ | 93.5 | 27.50 | 3.57 | 340 | 337 | 333 | 329 | 324 | 318 | 313 |

For detail dimensions see page 234

SAFE LOADS IN THOUSANDS OF POUNDS FOR 8" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula $P = \frac{50\,000}{1 + \frac{(12\,L)^2}{36\,000\,r^2}}$ Safety factor 4.



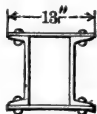
SERIES B.

| Length in Feet. | | | | | | | | | | Thick- ness of Plates. | Weight of each Channel. |
|-----------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|------------------------------|-------------------------------|
| 20 | 22 | 24 | 26 | 28 | 30 | 32 | 34 | 36 | 38 | Inch. | Lbs. per Ft. |
| 142 | 138 | 135 | 131 | 128 | 124 | 121 | 117 | 114 | 110 | $\frac{1}{4}$ | 11.25 |
| 159 | 156 | 152 | 148 | 144 | 141 | 137 | 133 | 129 | 125 | $\frac{1}{8}$ | " |
| 176 | 172 | 168 | 164 | 160 | 155 | 151 | 147 | 143 | 139 | $\frac{3}{8}$ | " |
| 193 | 189 | 184 | 180 | 175 | 170 | 166 | 161 | 156 | 151 | $\frac{1}{2}$ | " |
| 209 | 204 | 200 | 194 | 190 | 184 | 179 | 175 | 169 | 164 | $\frac{5}{8}$ | " |
| 225 | 221 | 215 | 210 | 204 | 199 | 194 | 188 | 182 | 176 | $\frac{1}{2}$ | " |
| 242 | 237 | 231 | 226 | 219 | 214 | 207 | 202 | 195 | 189 | $\frac{3}{8}$ | " |
| 156 | 152 | 149 | 144 | 140 | 137 | 132 | 128 | 124 | 120 | $\frac{1}{4}$ | 13.75 |
| 173 | 170 | 165 | 161 | 157 | 153 | 148 | 144 | 139 | 134 | $\frac{1}{8}$ | " |
| 191 | 187 | 183 | 178 | 173 | 168 | 164 | 159 | 154 | 149 | $\frac{3}{8}$ | " |
| 208 | 203 | 199 | 193 | 187 | 183 | 178 | 173 | 168 | 162 | $\frac{1}{2}$ | " |
| 224 | 219 | 214 | 209 | 203 | 198 | 193 | 186 | 181 | 175 | $\frac{5}{8}$ | " |
| 241 | 236 | 230 | 224 | 218 | 213 | 206 | 200 | 194 | 188 | $\frac{1}{2}$ | " |
| 257 | 251 | 246 | 239 | 233 | 226 | 220 | 213 | 207 | 200 | $\frac{3}{8}$ | " |
| 171 | 167 | 163 | 158 | 153 | 149 | 144 | 140 | 135 | 130 | $\frac{1}{4}$ | 16.25 |
| 189 | 184 | 179 | 175 | 170 | 165 | 160 | 155 | 150 | 145 | $\frac{1}{8}$ | " |
| 206 | 202 | 197 | 191 | 187 | 181 | 176 | 170 | 165 | 160 | $\frac{3}{8}$ | " |
| 224 | 219 | 214 | 209 | 203 | 198 | 191 | 186 | 180 | 175 | $\frac{1}{2}$ | " |
| 240 | 235 | 230 | 223 | 218 | 211 | 206 | 199 | 194 | 187 | $\frac{5}{8}$ | " |
| 257 | 251 | 245 | 239 | 233 | 226 | 220 | 213 | 207 | 200 | $\frac{1}{2}$ | " |
| 274 | 267 | 261 | 254 | 247 | 241 | 233 | 227 | 219 | 213 | $\frac{3}{8}$ | " |
| 186 | 181 | 176 | 171 | 166 | 161 | 155 | 150 | 145 | 140 | $\frac{1}{4}$ | 18.75 |
| 204 | 199 | 194 | 188 | 182 | 177 | 171 | 166 | 161 | 155 | $\frac{1}{8}$ | " |
| 221 | 216 | 210 | 205 | 199 | 193 | 188 | 182 | 176 | 170 | $\frac{3}{8}$ | " |
| 239 | 233 | 228 | 222 | 216 | 210 | 203 | 198 | 191 | 186 | $\frac{1}{2}$ | " |
| 257 | 250 | 245 | 238 | 231 | 226 | 219 | 213 | 206 | 200 | $\frac{5}{8}$ | " |
| 272 | 267 | 260 | 254 | 247 | 240 | 233 | 226 | 219 | 212 | $\frac{1}{2}$ | " |
| 289 | 283 | 276 | 269 | 262 | 254 | 247 | 239 | 232 | 224 | $\frac{3}{8}$ | " |
| 201 | 196 | 191 | 184 | 178 | 173 | 167 | 161 | 156 | 150 | $\frac{1}{4}$ | 21.25 |
| 219 | 214 | 208 | 202 | 196 | 190 | 184 | 178 | 172 | 165 | $\frac{1}{8}$ | " |
| 237 | 231 | 225 | 218 | 212 | 206 | 200 | 193 | 187 | 180 | $\frac{3}{8}$ | " |
| 254 | 248 | 243 | 236 | 229 | 223 | 216 | 209 | 202 | 196 | $\frac{1}{2}$ | " |
| 272 | 265 | 260 | 252 | 246 | 239 | 231 | 225 | 218 | 211 | $\frac{5}{8}$ | " |
| 289 | 282 | 276 | 268 | 261 | 253 | 245 | 239 | 231 | 224 | $\frac{1}{2}$ | " |
| 305 | 298 | 291 | 283 | 276 | 268 | 260 | 253 | 244 | 237 | $\frac{3}{8}$ | " |

For detail dimensions see page 234

SAFE LOADS IN THOUSANDS OF POUNDS FOR 9" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula $P = \frac{50\,000}{1 + \frac{(12 L)^2}{36\,000 r^2}}$ Safety factor 4.



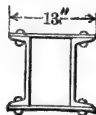
SERIES B.

| Weight of each Channel. | Thick- ness of Plates. | Weight of Column. | Area of Column Section. | Least Radius of Gyration. | Length in Feet. | | | | | | | |
|-------------------------------|------------------------------|-------------------------|-------------------------------|---------------------------------|-----------------|-----|-----|-----|-----|-----|-----|-----|
| | | | | | 6 | 8 | 10 | 12 | 14 | 16 | 18 | 20 |
| Lbs. per Ft. | Inch. | Lbs. per Ft. | Sq. Ins. | Inches. | | | | | | | | |
| 13.25 | $\frac{1}{4}$ | 48.6 | 14.28 | 4.05 | 177 | 176 | 174 | 172 | 170 | 168 | 166 | 163 |
| " | $\frac{5}{16}$ | 54.1 | 15.90 | 4.10 | 197 | 196 | 194 | 192 | 190 | 187 | 184 | 181 |
| " | $\frac{3}{8}$ | 59.7 | 17.53 | 4.07 | 217 | 216 | 214 | 212 | 209 | 207 | 203 | 200 |
| " | $\frac{1}{2}$ | 65.2 | 19.16 | 4.04 | 237 | 236 | 234 | 231 | 228 | 225 | 222 | 218 |
| " | $\frac{5}{8}$ | 70.7 | 20.78 | 4.02 | 257 | 256 | 253 | 251 | 248 | 244 | 240 | 236 |
| " | $\frac{3}{4}$ | 76.2 | 22.40 | 4.00 | 277 | 276 | 273 | 270 | 267 | 263 | 259 | 255 |
| " | $\frac{7}{8}$ | 81.7 | 24.03 | 3.99 | 297 | 296 | 293 | 290 | 286 | 282 | 278 | 273 |
| 15.0 | $\frac{1}{4}$ | 52.1 | 15.32 | 3.97 | 190 | 188 | 187 | 185 | 183 | 180 | 177 | 174 |
| " | $\frac{5}{16}$ | 57.6 | 16.94 | 4.05 | 210 | 208 | 207 | 204 | 202 | 199 | 197 | 193 |
| " | $\frac{3}{8}$ | 63.2 | 18.57 | 4.05 | 230 | 228 | 226 | 224 | 221 | 218 | 215 | 212 |
| " | $\frac{1}{2}$ | 68.7 | 20.20 | 4.03 | 250 | 249 | 246 | 244 | 241 | 237 | 234 | 230 |
| " | $\frac{5}{8}$ | 74.2 | 21.82 | 4.01 | 270 | 268 | 266 | 263 | 260 | 256 | 252 | 248 |
| " | $\frac{3}{4}$ | 79.7 | 23.44 | 3.99 | 290 | 288 | 286 | 283 | 279 | 275 | 271 | 266 |
| " | $\frac{7}{8}$ | 85.2 | 25.07 | 3.97 | 310 | 308 | 306 | 302 | 299 | 295 | 290 | 285 |
| 20.0 | $\frac{1}{4}$ | 62.1 | 18.26 | 3.78 | 226 | 224 | 222 | 219 | 216 | 213 | 209 | 205 |
| " | $\frac{5}{16}$ | 67.6 | 19.88 | 3.87 | 246 | 244 | 242 | 239 | 236 | 233 | 228 | 224 |
| " | $\frac{3}{8}$ | 73.2 | 21.51 | 3.95 | 266 | 264 | 262 | 260 | 256 | 252 | 248 | 244 |
| " | $\frac{1}{2}$ | 78.7 | 23.14 | 3.98 | 286 | 285 | 282 | 279 | 276 | 272 | 268 | 263 |
| " | $\frac{5}{8}$ | 84.2 | 24.76 | 3.96 | 306 | 305 | 302 | 299 | 295 | 291 | 286 | 280 |
| " | $\frac{3}{4}$ | 89.7 | 26.39 | 3.95 | 327 | 325 | 322 | 318 | 314 | 309 | 304 | 299 |
| " | $\frac{7}{8}$ | 95.2 | 28.01 | 3.94 | 347 | 345 | 342 | 338 | 333 | 328 | 323 | 317 |
| 25.0 | $\frac{1}{4}$ | 72.1 | 21.20 | 3.64 | 262 | 260 | 257 | 254 | 251 | 246 | 242 | 236 |
| " | $\frac{5}{16}$ | 77.6 | 22.82 | 3.73 | 282 | 280 | 277 | 274 | 270 | 266 | 261 | 255 |
| " | $\frac{3}{8}$ | 83.2 | 24.45 | 3.81 | 303 | 300 | 298 | 294 | 290 | 285 | 281 | 276 |
| " | $\frac{1}{2}$ | 88.7 | 26.08 | 3.89 | 323 | 320 | 317 | 314 | 310 | 305 | 301 | 295 |
| " | $\frac{5}{8}$ | 94.2 | 27.70 | 3.92 | 343 | 341 | 337 | 333 | 329 | 324 | 319 | 314 |
| " | $\frac{3}{4}$ | 99.7 | 29.32 | 3.91 | 363 | 361 | 357 | 353 | 348 | 343 | 338 | 332 |
| " | $\frac{7}{8}$ | 105.2 | 30.95 | 3.90 | 383 | 380 | 377 | 373 | 368 | 362 | 357 | 350 |

For detail dimensions see page 234

SAFE LOADS IN THOUSANDS OF POUNDS FOR 9" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula $P = \frac{50\,000}{1 + \frac{(12 L)^2}{36\,000 r^2}}$ Safety factor 4.



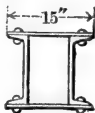
SERIES B.

| Length in Feet. | | | | | | | | | | | Thickness of Plates. | Weight of each Channel. |
|-----------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|----------------------------|-------------------------------|
| 22 | 24 | 26 | 28 | 30 | 32 | 34 | 36 | 38 | 40 | 42 | Inch. | Lbs. per Ft. |
| 160 | 157 | 153 | 150 | 146 | 143 | 139 | 136 | 132 | 128 | 125 | $\frac{1}{4}$ | 13.25 |
| 178 | 174 | 172 | 168 | 164 | 160 | 156 | 152 | 148 | 144 | 140 | $\frac{5}{16}$ | " |
| 196 | 192 | 188 | 184 | 180 | 175 | 171 | 167 | 163 | 158 | 154 | $\frac{3}{8}$ | " |
| 214 | 210 | 206 | 201 | 196 | 192 | 187 | 182 | 177 | 172 | 167 | $\frac{7}{16}$ | " |
| 232 | 227 | 222 | 217 | 212 | 207 | 202 | 196 | 191 | 186 | 181 | $\frac{1}{2}$ | " |
| 250 | 245 | 240 | 234 | 229 | 223 | 217 | 211 | 206 | 200 | 194 | $\frac{5}{8}$ | " |
| 268 | 263 | 257 | 251 | 245 | 239 | 233 | 227 | 221 | 215 | 208 | $\frac{3}{4}$ | " |
| 171 | 167 | 164 | 159 | 156 | 152 | 148 | 144 | 140 | 136 | 132 | $\frac{1}{4}$ | 15.0 |
| 190 | 186 | 182 | 178 | 174 | 169 | 165 | 161 | 156 | 152 | 148 | $\frac{5}{16}$ | " |
| 208 | 204 | 199 | 195 | 190 | 186 | 181 | 176 | 172 | 167 | 162 | $\frac{3}{8}$ | " |
| 225 | 221 | 216 | 212 | 207 | 202 | 197 | 192 | 187 | 181 | 176 | $\frac{7}{16}$ | " |
| 243 | 238 | 233 | 228 | 223 | 217 | 212 | 206 | 200 | 195 | 189 | $\frac{1}{2}$ | " |
| 261 | 256 | 251 | 245 | 239 | 233 | 227 | 221 | 215 | 209 | 203 | $\frac{5}{8}$ | " |
| 280 | 274 | 268 | 261 | 255 | 248 | 242 | 235 | 229 | 223 | 216 | $\frac{3}{4}$ | " |
| 201 | 197 | 192 | 187 | 183 | 177 | 172 | 168 | 162 | 158 | 153 | $\frac{1}{4}$ | 20.0 |
| 220 | 215 | 211 | 206 | 200 | 195 | 190 | 185 | 180 | 174 | 168 | $\frac{5}{16}$ | " |
| 239 | 234 | 229 | 224 | 218 | 213 | 207 | 202 | 196 | 191 | 186 | $\frac{3}{8}$ | " |
| 258 | 253 | 247 | 242 | 236 | 230 | 224 | 218 | 213 | 205 | 200 | $\frac{7}{16}$ | " |
| 275 | 269 | 264 | 258 | 251 | 245 | 239 | 232 | 226 | 220 | 214 | $\frac{1}{2}$ | " |
| 293 | 287 | 281 | 274 | 268 | 261 | 255 | 248 | 241 | 234 | 228 | $\frac{5}{8}$ | " |
| 311 | 305 | 298 | 291 | 284 | 277 | 270 | 263 | 256 | 247 | 240 | $\frac{3}{4}$ | " |
| 232 | 226 | 221 | 214 | 209 | 202 | 197 | 190 | 185 | 179 | 173 | $\frac{1}{4}$ | 25.0 |
| 250 | 245 | 238 | 233 | 227 | 220 | 214 | 207 | 201 | 196 | 189 | $\frac{5}{16}$ | " |
| 269 | 264 | 258 | 252 | 245 | 238 | 232 | 226 | 218 | 212 | 206 | $\frac{3}{8}$ | " |
| 288 | 283 | 276 | 270 | 264 | 257 | 250 | 242 | 236 | 229 | 222 | $\frac{7}{16}$ | " |
| 308 | 301 | 295 | 288 | 280 | 273 | 266 | 259 | 252 | 245 | 238 | $\frac{1}{2}$ | " |
| 326 | 319 | 312 | 304 | 296 | 289 | 281 | 274 | 266 | 260 | 251 | $\frac{5}{8}$ | " |
| 344 | 335 | 328 | 320 | 313 | 309 | 297 | 289 | 281 | 273 | 264 | $\frac{3}{4}$ | " |

For detail dimensions see page 234

SAFE LOADS IN THOUSANDS OF POUNDS FOR 10" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula $P = \frac{50\,000}{1 + \frac{(12\,L)^2}{36\,000\,r^2}}$ Safety factor 4.



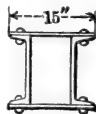
SERIES B.

| Weight of each Channel. | Thick- ness of Plates. | Weight of Column. | Area of Column Section. | Least Radius of Gyration. | Length in Feet. | | | | | | | | | |
|-------------------------------|------------------------------|-------------------------|-------------------------------|---------------------------------|-----------------|-------|--------------|----------|---------|-----|-----|-----|-----|----|
| | | | | | Lbs. per Ft. | Inch. | Lbs. per Ft. | Sq. Ins. | Inches. | 8 | 10 | 12 | 14 | 16 |
| 15 | $\frac{1}{4}$ | 55.5 | 16.42 | 4.49 | 203 | 201 | 199 | 198 | 195 | 193 | 190 | 187 | 185 | |
| " | $\frac{5}{16}$ | 61.9 | 18.30 | 4.58 | 226 | 224 | 223 | 220 | 218 | 216 | 212 | 209 | 206 | |
| " | $\frac{3}{8}$ | 68.3 | 20.17 | 4.65 | 249 | 247 | 245 | 243 | 241 | 238 | 235 | 232 | 228 | |
| " | $\frac{7}{16}$ | 74.6 | 22.05 | 4.70 | 272 | 271 | 268 | 266 | 263 | 261 | 257 | 253 | 250 | |
| " | $\frac{1}{2}$ | 81.0 | 23.92 | 4.67 | 296 | 294 | 291 | 289 | 286 | 282 | 278 | 275 | 271 | |
| " | $\frac{9}{16}$ | 87.4 | 25.80 | 4.65 | 319 | 316 | 314 | 311 | 308 | 304 | 300 | 296 | 291 | |
| " | $\frac{5}{8}$ | 93.8 | 27.67 | 4.63 | 342 | 339 | 337 | 334 | 330 | 326 | 322 | 317 | 312 | |
| 20 | $\frac{1}{4}$ | 65.5 | 19.26 | 4.29 | 237 | 236 | 233 | 231 | 228 | 225 | 221 | 218 | 214 | |
| " | $\frac{5}{16}$ | 71.9 | 21.14 | 4.39 | 261 | 259 | 257 | 254 | 251 | 248 | 244 | 240 | 236 | |
| " | $\frac{3}{8}$ | 78.3 | 23.01 | 4.47 | 284 | 282 | 279 | 277 | 273 | 270 | 266 | 262 | 258 | |
| " | $\frac{7}{16}$ | 84.6 | 24.80 | 4.55 | 307 | 305 | 303 | 300 | 297 | 292 | 289 | 285 | 280 | |
| " | $\frac{1}{2}$ | 91.0 | 26.76 | 4.62 | 331 | 328 | 326 | 323 | 319 | 315 | 311 | 306 | 302 | |
| " | $\frac{9}{16}$ | 97.4 | 28.64 | 4.63 | 354 | 351 | 349 | 346 | 341 | 337 | 333 | 328 | 323 | |
| " | $\frac{5}{8}$ | 103.8 | 30.51 | 4.61 | 377 | 374 | 371 | 368 | 364 | 359 | 355 | 349 | 344 | |
| 25 | $\frac{1}{4}$ | 75.5 | 22.20 | 4.13 | 274 | 271 | 268 | 265 | 262 | 258 | 254 | 249 | 245 | |
| " | $\frac{5}{16}$ | 81.9 | 24.08 | 4.23 | 297 | 294 | 292 | 288 | 285 | 280 | 277 | 272 | 266 | |
| " | $\frac{3}{8}$ | 88.3 | 25.95 | 4.32 | 320 | 318 | 315 | 312 | 308 | 303 | 299 | 294 | 288 | |
| " | $\frac{7}{16}$ | 94.6 | 27.83 | 4.40 | 343 | 341 | 333 | 334 | 331 | 326 | 322 | 316 | 310 | |
| " | $\frac{1}{2}$ | 101.0 | 29.70 | 4.48 | 367 | 364 | 361 | 357 | 353 | 349 | 343 | 339 | 332 | |
| " | $\frac{9}{16}$ | 107.4 | 31.58 | 4.55 | 390 | 387 | 384 | 380 | 376 | 371 | 366 | 361 | 355 | |
| " | $\frac{5}{8}$ | 113.8 | 33.45 | 4.58 | 413 | 410 | 407 | 403 | 399 | 394 | 388 | 383 | 377 | |
| 30 | $\frac{1}{4}$ | 85.5 | 25.14 | 4.01 | 309 | 307 | 303 | 300 | 295 | 291 | 286 | 280 | 275 | |
| " | $\frac{5}{16}$ | 91.9 | 27.02 | 4.11 | 333 | 330 | 327 | 323 | 318 | 313 | 308 | 302 | 298 | |
| " | $\frac{3}{8}$ | 98.3 | 28.89 | 4.20 | 356 | 353 | 349 | 346 | 341 | 336 | 331 | 326 | 320 | |
| " | $\frac{7}{16}$ | 104.6 | 30.77 | 4.28 | 379 | 377 | 373 | 369 | 365 | 359 | 353 | 348 | 342 | |
| " | $\frac{1}{2}$ | 111.0 | 32.64 | 4.36 | 403 | 400 | 396 | 392 | 387 | 382 | 376 | 371 | 364 | |
| " | $\frac{9}{16}$ | 117.4 | 34.52 | 4.43 | 426 | 423 | 419 | 415 | 410 | 404 | 399 | 392 | 386 | |
| " | $\frac{5}{8}$ | 123.8 | 36.39 | 4.50 | 449 | 446 | 442 | 438 | 432 | 428 | 422 | 415 | 409 | |
| 35 | $\frac{1}{4}$ | 95.5 | 28.08 | 3.90 | 345 | 342 | 338 | 334 | 329 | 324 | 318 | 312 | 304 | |
| " | $\frac{5}{16}$ | 101.9 | 29.96 | 4.00 | 369 | 365 | 361 | 357 | 352 | 346 | 340 | 334 | 327 | |
| " | $\frac{3}{8}$ | 108.3 | 31.83 | 4.10 | 392 | 389 | 385 | 380 | 375 | 369 | 363 | 356 | 349 | |
| " | $\frac{7}{16}$ | 114.6 | 33.71 | 4.18 | 415 | 412 | 408 | 404 | 398 | 392 | 386 | 379 | 373 | |
| " | $\frac{1}{2}$ | 121.0 | 35.58 | 4.26 | 438 | 436 | 431 | 426 | 420 | 415 | 409 | 401 | 395 | |
| " | $\frac{9}{16}$ | 127.4 | 37.46 | 4.33 | 462 | 459 | 454 | 450 | 444 | 437 | 432 | 424 | 418 | |
| " | $\frac{5}{8}$ | 133.8 | 39.33 | 4.40 | 485 | 481 | 478 | 472 | 467 | 461 | 455 | 447 | 439 | |

For detail dimensions see page 235

SAFE LOADS IN THOUSANDS OF POUNDS FOR 10" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula $P = \frac{50\,000}{1 + \frac{(12 L)^2}{36\,000 r^2}}$ Safety factor 4.

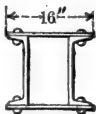


SERIES B.

| Length in Feet. | | | | | | | | | | | | Thick- ness of Plates. | Weight of each Channel. |
|-----------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|------------------------------|-------------------------------|
| 26 | 28 | 30 | 32 | 34 | 36 | 38 | 40 | 42 | 44 | 46 | 48 | Inch. | Lbs. per Ft. |
| 181 | 178 | 174 | 171 | 167 | 163 | 159 | 156 | 152 | 148 | 145 | 141 | 1/4 | 15 |
| 202 | 199 | 195 | 191 | 188 | 183 | 179 | 176 | 171 | 167 | 163 | 159 | 5/16 | " |
| 224 | 220 | 216 | 212 | 208 | 204 | 199 | 195 | 190 | 185 | 181 | 177 | 3/8 | " |
| 246 | 241 | 237 | 233 | 228 | 223 | 218 | 214 | 209 | 204 | 199 | 195 | 1/2 | " |
| 266 | 261 | 257 | 251 | 246 | 242 | 237 | 231 | 226 | 221 | 215 | 210 | 5/8 | " |
| 287 | 282 | 276 | 271 | 266 | 261 | 254 | 249 | 244 | 237 | 232 | 226 | 1 1/8 | " |
| 307 | 302 | 296 | 291 | 285 | 278 | 273 | 267 | 260 | 254 | 248 | 241 | 1 1/4 | " |
| | | | | | | | | | | | | | |
| 210 | 206 | 201 | 197 | 193 | 188 | 183 | 179 | 174 | 169 | 165 | 160 | 1/4 | 20 |
| 232 | 227 | 223 | 218 | 214 | 208 | 203 | 198 | 193 | 189 | 183 | 179 | 5/16 | " |
| 254 | 248 | 244 | 238 | 234 | 228 | 223 | 218 | 213 | 208 | 202 | 197 | 3/8 | " |
| 275 | 270 | 265 | 260 | 254 | 249 | 243 | 238 | 232 | 226 | 221 | 216 | 1/2 | " |
| 297 | 291 | 286 | 281 | 274 | 269 | 264 | 257 | 251 | 246 | 239 | 233 | 5/8 | " |
| 318 | 313 | 306 | 301 | 295 | 288 | 282 | 276 | 269 | 263 | 257 | 250 | 1 1/8 | " |
| 339 | 332 | 326 | 320 | 313 | 307 | 301 | 293 | 286 | 280 | 272 | 266 | 1 1/4 | " |
| | | | | | | | | | | | | | |
| 239 | 234 | 229 | 224 | 219 | 213 | 207 | 202 | 196 | 190 | 186 | 180 | 1/4 | 25 |
| 262 | 256 | 250 | 245 | 240 | 234 | 227 | 221 | 216 | 210 | 204 | 199 | 5/16 | " |
| 284 | 277 | 272 | 266 | 260 | 254 | 248 | 241 | 236 | 229 | 223 | 217 | 3/8 | " |
| 305 | 299 | 294 | 287 | 281 | 274 | 268 | 261 | 256 | 248 | 241 | 236 | 1/2 | " |
| 327 | 322 | 315 | 309 | 302 | 296 | 288 | 282 | 274 | 268 | 261 | 255 | 5/8 | " |
| 349 | 342 | 336 | 330 | 322 | 316 | 308 | 301 | 295 | 287 | 280 | 274 | 1 1/8 | " |
| 370 | 364 | 356 | 350 | 343 | 335 | 328 | 321 | 312 | 305 | 299 | 290 | 1 1/4 | " |
| | | | | | | | | | | | | | |
| 269 | 263 | 257 | 250 | 244 | 237 | 231 | 224 | 218 | 212 | 205 | 199 | 1/4 | 30 |
| 291 | 285 | 278 | 272 | 265 | 258 | 252 | 245 | 239 | 232 | 225 | 218 | 5/16 | " |
| 313 | 306 | 300 | 293 | 286 | 279 | 273 | 265 | 258 | 251 | 243 | 238 | 3/8 | " |
| 335 | 329 | 322 | 314 | 308 | 300 | 292 | 286 | 278 | 270 | 264 | 256 | 1/2 | " |
| 357 | 351 | 342 | 336 | 328 | 320 | 313 | 305 | 298 | 290 | 282 | 275 | 5/8 | " |
| 379 | 372 | 364 | 357 | 349 | 342 | 333 | 326 | 317 | 310 | 301 | 294 | 1 1/8 | " |
| 401 | 394 | 386 | 378 | 370 | 362 | 355 | 345 | 338 | 329 | 321 | 312 | 1 1/4 | " |
| | | | | | | | | | | | | | |
| 298 | 291 | 284 | 277 | 269 | 262 | 255 | 248 | 239 | 282 | 225 | 219 | 1/4 | 35 |
| 320 | 313 | 306 | 298 | 291 | 283 | 275 | 267 | 260 | 252 | 245 | 238 | 5/16 | " |
| 343 | 336 | 328 | 320 | 312 | 304 | 296 | 287 | 281 | 273 | 265 | 257 | 3/8 | " |
| 365 | 357 | 349 | 340 | 334 | 325 | 317 | 309 | 301 | 292 | 284 | 276 | 1/2 | " |
| 387 | 379 | 372 | 363 | 354 | 345 | 338 | 329 | 320 | 312 | 303 | 294 | 5/8 | " |
| 409 | 401 | 393 | 384 | 375 | 367 | 358 | 350 | 340 | 331 | 323 | 314 | 1 1/8 | " |
| 432 | 422 | 415 | 405 | 397 | 387 | 379 | 369 | 361 | 351 | 341 | 333 | 1 1/4 | " |

SAFE LOADS IN THOUSANDS OF POUNDS FOR 12" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula $P = \frac{50\,000}{1 + \frac{(12 L)^2}{36\,000 r^2}}$ Safety factor 4.



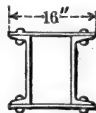
SERIES B.

| Weight of each Channel. | Thick-ness of Plates. | Weight of Column. | Area of Column Section. | Least Radius of Gyration. | Length in Feet. | | | | | | | | | | | |
|-------------------------|-----------------------|-------------------|-------------------------|---------------------------|-----------------|-----|-----|-----|-----|-----|-----|-----|-----|--|--|--|
| Lbs. per Ft. | Inch. | Lbs. per Ft. | Sq. Ins. | Inches. | 8 | 10 | 12 | 14 | 16 | 18 | 20 | 22 | 24 | | | |
| 20.5 | $\frac{1}{4}$ | 68.2 | 20.06 | 5.23 | 248 | 247 | 246 | 244 | 241 | 240 | 237 | 234 | 231 | | | |
| " | $\frac{5}{16}$ | 75.0 | 22.06 | 5.18 | 273 | 272 | 270 | 268 | 266 | 263 | 260 | 258 | 254 | | | |
| " | $\frac{3}{8}$ | 81.8 | 24.06 | 5.14 | 298 | 296 | 295 | 292 | 290 | 287 | 283 | 280 | 276 | | | |
| " | $\frac{7}{16}$ | 88.6 | 26.06 | 5.10 | 322 | 321 | 318 | 317 | 314 | 311 | 307 | 303 | 299 | | | |
| " | $\frac{1}{2}$ | 95.4 | 28.06 | 5.07 | 347 | 345 | 343 | 340 | 337 | 333 | 331 | 327 | 322 | | | |
| " | $\frac{5}{8}$ | 102.2 | 30.06 | 5.04 | 372 | 370 | 367 | 364 | 361 | 357 | 354 | 349 | 344 | | | |
| " | $\frac{3}{4}$ | 109.0 | 32.06 | 5.01 | 397 | 394 | 392 | 389 | 385 | 381 | 377 | 372 | 367 | | | |
| 25 | $\frac{1}{4}$ | 77.2 | 22.70 | 5.09 | 281 | 279 | 277 | 275 | 273 | 270 | 267 | 264 | 261 | | | |
| " | $\frac{5}{16}$ | 84.0 | 24.70 | 5.14 | 306 | 304 | 302 | 300 | 297 | 294 | 291 | 287 | 284 | | | |
| " | $\frac{3}{8}$ | 90.8 | 26.70 | 5.11 | 330 | 328 | 326 | 324 | 321 | 318 | 315 | 311 | 307 | | | |
| " | $\frac{7}{16}$ | 97.6 | 28.70 | 5.07 | 355 | 353 | 351 | 348 | 345 | 341 | 338 | 334 | 330 | | | |
| " | $\frac{1}{2}$ | 104.4 | 30.70 | 5.05 | 380 | 378 | 375 | 372 | 369 | 365 | 361 | 356 | 351 | | | |
| " | $\frac{5}{8}$ | 111.2 | 32.70 | 5.02 | 405 | 402 | 400 | 396 | 393 | 389 | 384 | 379 | 374 | | | |
| " | $\frac{3}{4}$ | 118.0 | 34.70 | 5.00 | 429 | 427 | 424 | 421 | 417 | 412 | 408 | 403 | 397 | | | |
| 30 | $\frac{1}{4}$ | 87.2 | 25.64 | 4.93 | 317 | 315 | 313 | 311 | 308 | 304 | 300 | 296 | 292 | | | |
| " | $\frac{5}{16}$ | 94.0 | 27.64 | 5.04 | 342 | 340 | 338 | 335 | 332 | 328 | 326 | 321 | 316 | | | |
| " | $\frac{3}{8}$ | 100.8 | 29.64 | 5.07 | 367 | 365 | 362 | 359 | 356 | 352 | 349 | 345 | 340 | | | |
| " | $\frac{7}{16}$ | 107.6 | 31.64 | 5.04 | 391 | 389 | 387 | 383 | 380 | 376 | 373 | 367 | 362 | | | |
| " | $\frac{1}{2}$ | 114.4 | 33.64 | 5.02 | 416 | 414 | 411 | 408 | 404 | 400 | 395 | 390 | 385 | | | |
| " | $\frac{5}{8}$ | 121.2 | 35.64 | 4.99 | 441 | 438 | 435 | 432 | 428 | 424 | 419 | 413 | 408 | | | |
| " | $\frac{3}{4}$ | 128.0 | 37.64 | 4.98 | 466 | 463 | 460 | 456 | 452 | 447 | 442 | 437 | 431 | | | |
| 35 | $\frac{1}{4}$ | 97.2 | 28.58 | 4.80 | 353 | 351 | 349 | 346 | 342 | 338 | 334 | 329 | 325 | | | |
| " | $\frac{5}{16}$ | 104.0 | 30.58 | 4.91 | 378 | 376 | 374 | 370 | 366 | 362 | 358 | 354 | 349 | | | |
| " | $\frac{3}{8}$ | 110.8 | 32.58 | 5.01 | 403 | 401 | 398 | 395 | 391 | 387 | 383 | 378 | 373 | | | |
| " | $\frac{7}{16}$ | 117.6 | 34.58 | 4.99 | 428 | 425 | 422 | 419 | 415 | 411 | 406 | 401 | 396 | | | |
| " | $\frac{1}{2}$ | 124.4 | 36.58 | 4.97 | 453 | 450 | 447 | 443 | 439 | 435 | 430 | 424 | 419 | | | |
| " | $\frac{5}{8}$ | 131.2 | 38.58 | 4.95 | 477 | 475 | 471 | 468 | 463 | 458 | 453 | 448 | 442 | | | |
| " | $\frac{3}{4}$ | 138.0 | 40.58 | 4.94 | 502 | 499 | 496 | 492 | 487 | 482 | 477 | 469 | 463 | | | |
| 40 | $\frac{1}{4}$ | 107.2 | 31.52 | 4.69 | 389 | 387 | 384 | 380 | 377 | 373 | 367 | 362 | 357 | | | |
| " | $\frac{5}{16}$ | 114.0 | 33.52 | 4.80 | 414 | 412 | 409 | 405 | 402 | 396 | 391 | 386 | 381 | | | |
| " | $\frac{3}{8}$ | 120.8 | 35.52 | 4.90 | 439 | 437 | 434 | 430 | 425 | 421 | 416 | 411 | 405 | | | |
| " | $\frac{7}{16}$ | 127.6 | 37.52 | 4.95 | 464 | 462 | 458 | 455 | 451 | 446 | 441 | 435 | 429 | | | |
| " | $\frac{1}{2}$ | 134.4 | 39.52 | 4.94 | 489 | 486 | 483 | 479 | 474 | 470 | 464 | 457 | 451 | | | |
| " | $\frac{5}{8}$ | 141.2 | 41.52 | 4.92 | 514 | 511 | 507 | 503 | 497 | 492 | 486 | 480 | 473 | | | |
| " | $\frac{3}{4}$ | 148.0 | 43.52 | 4.91 | 538 | 535 | 532 | 526 | 521 | 516 | 510 | 503 | 496 | | | |

For detail dimensions see page 235

SAFE LOADS IN THOUSANDS OF POUNDS FOR 12" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula $P = \frac{50\,000}{1 + \frac{(12L)^2}{36\,000r^2}}$ Safety factor 4.



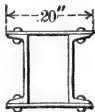
SERIES B.

| Length in Feet. | | | | | | | | | | | | Thick- ness of Plates. | Weight of each Channel. |
|-----------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|------------------------------|-------------------------------|
| 26 | 28 | 30 | 32 | 34 | 36 | 38 | 40 | 42 | 44 | 46 | 48 | Inch. | Lbs. per Ft. |
| 228 | 225 | 222 | 218 | 215 | 211 | 207 | 204 | 200 | 196 | 191 | 187 | $\frac{1}{4}$ | 20.5 |
| 251 | 247 | 243 | 239 | 235 | 231 | 227 | 223 | 218 | 214 | 209 | 205 | $\frac{1}{8}$ | " |
| 272 | 269 | 265 | 261 | 256 | 251 | 247 | 242 | 237 | 232 | 228 | 223 | $\frac{3}{8}$ | " |
| 295 | 291 | 286 | 281 | 276 | 271 | 266 | 262 | 257 | 251 | 246 | 241 | $\frac{1}{2}$ | " |
| 318 | 313 | 308 | 303 | 297 | 292 | 286 | 281 | 275 | 269 | 263 | 258 | $\frac{1}{2}$ | " |
| 339 | 334 | 328 | 324 | 319 | 313 | 307 | 301 | 295 | 288 | 282 | 276 | $\frac{1}{2}$ | " |
| 362 | 356 | 350 | 344 | 338 | 332 | 326 | 319 | 313 | 306 | 299 | 293 | $\frac{5}{8}$ | " |
| 257 | 253 | 249 | 245 | 241 | 236 | 232 | 227 | 222 | 219 | 214 | 210 | $\frac{1}{4}$ | 25 |
| 280 | 276 | 272 | 268 | 263 | 258 | 253 | 248 | 243 | 238 | 234 | 229 | $\frac{1}{8}$ | " |
| 302 | 298 | 293 | 288 | 283 | 279 | 274 | 268 | 263 | 258 | 252 | 247 | $\frac{3}{8}$ | " |
| 325 | 320 | 315 | 310 | 304 | 299 | 293 | 287 | 281 | 275 | 269 | 264 | $\frac{1}{2}$ | " |
| 348 | 342 | 337 | 331 | 325 | 319 | 313 | 307 | 301 | 295 | 288 | 282 | $\frac{1}{2}$ | " |
| 369 | 363 | 357 | 351 | 345 | 339 | 332 | 325 | 319 | 312 | 305 | 299 | $\frac{1}{2}$ | " |
| 391 | 385 | 379 | 373 | 366 | 359 | 352 | 345 | 338 | 331 | 324 | 317 | $\frac{5}{8}$ | " |
| 288 | 284 | 279 | 274 | 269 | 264 | 259 | 254 | 249 | 243 | 238 | 233 | $\frac{1}{4}$ | 30 |
| 312 | 307 | 302 | 298 | 293 | 287 | 282 | 276 | 271 | 265 | 260 | 254 | $\frac{1}{8}$ | " |
| 336 | 330 | 325 | 320 | 314 | 308 | 302 | 296 | 290 | 284 | 278 | 272 | $\frac{3}{8}$ | " |
| 357 | 351 | 346 | 341 | 335 | 329 | 323 | 316 | 310 | 304 | 297 | 291 | $\frac{1}{2}$ | " |
| 379 | 374 | 368 | 361 | 355 | 348 | 342 | 335 | 328 | 321 | 314 | 307 | $\frac{1}{2}$ | " |
| 402 | 396 | 389 | 383 | 376 | 369 | 362 | 355 | 347 | 340 | 333 | 326 | $\frac{1}{2}$ | " |
| 425 | 418 | 411 | 404 | 397 | 390 | 382 | 375 | 367 | 359 | 351 | 344 | $\frac{5}{8}$ | " |
| 320 | 315 | 310 | 303 | 297 | 292 | 286 | 280 | 273 | 267 | 261 | 255 | $\frac{1}{4}$ | 35 |
| 344 | 338 | 333 | 327 | 321 | 315 | 309 | 303 | 295 | 289 | 282 | 276 | $\frac{1}{8}$ | " |
| 368 | 362 | 356 | 350 | 344 | 337 | 331 | 324 | 318 | 311 | 304 | 298 | $\frac{3}{8}$ | " |
| 390 | 384 | 378 | 371 | 365 | 358 | 351 | 344 | 337 | 330 | 323 | 316 | $\frac{1}{2}$ | " |
| 413 | 406 | 400 | 393 | 386 | 379 | 371 | 364 | 355 | 347 | 340 | 332 | $\frac{1}{2}$ | " |
| 434 | 427 | 420 | 413 | 405 | 398 | 390 | 382 | 374 | 366 | 358 | 350 | $\frac{1}{2}$ | " |
| 456 | 449 | 442 | 434 | 426 | 418 | 410 | 402 | 394 | 385 | 377 | 369 | $\frac{5}{8}$ | " |
| 351 | 344 | 339 | 333 | 326 | 318 | 312 | 306 | 298 | 291 | 285 | 278 | $\frac{1}{4}$ | 40 |
| 375 | 369 | 363 | 355 | 349 | 342 | 335 | 328 | 320 | 313 | 306 | 299 | $\frac{1}{8}$ | " |
| 399 | 393 | 386 | 380 | 373 | 366 | 357 | 350 | 343 | 335 | 328 | 321 | $\frac{3}{8}$ | " |
| 422 | 415 | 408 | 401 | 394 | 387 | 379 | 372 | 364 | 356 | 348 | 341 | $\frac{1}{2}$ | " |
| 444 | 437 | 430 | 423 | 415 | 407 | 399 | 391 | 383 | 375 | 367 | 359 | $\frac{1}{2}$ | " |
| 466 | 459 | 452 | 444 | 436 | 428 | 420 | 411 | 403 | 394 | 386 | 375 | $\frac{1}{2}$ | " |
| 489 | 481 | 473 | 465 | 457 | 448 | 440 | 431 | 420 | 411 | 402 | 393 | $\frac{5}{8}$ | " |

For detail dimensions see page 235

SAFE LOADS IN THOUSANDS OF POUNDS FOR 15" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula $P = \frac{50\,000}{1 + \frac{(12 L)^2}{36\,000 r^2}}$ Safety factor 4.



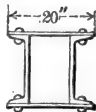
SERIES B.

| Weight of each Channel. | Thick- ness of Plates. | Weight of Column. | Area of Column Section. | Least Radius of Gyrations. | Length in Feet. | | | | | | | | | |
|-------------------------------|------------------------------|-------------------------|-------------------------------|----------------------------------|-----------------|-----|-----|-----|-----|-----|-----|-----|-----|--|
| | | | | | 12 | 14 | 16 | 18 | 20 | 22 | 24 | 26 | 28 | |
| Lbs. per Ft. | Inch. | Lbs. per Ft. | Sq. Ins. | Inches. | 12 | 14 | 16 | 18 | 20 | 22 | 24 | 26 | 28 | |
| 33 | $\frac{3}{8}$ | 117.0 | 34.80 | 6.59 | 429 | 427 | 425 | 423 | 420 | 417 | 414 | 410 | 406 | |
| " | $\frac{7}{16}$ | 125.5 | 37.30 | 6.57 | 460 | 458 | 456 | 453 | 450 | 447 | 442 | 438 | 434 | |
| " | $\frac{1}{2}$ | 134.0 | 39.80 | 6.52 | 491 | 489 | 485 | 482 | 479 | 476 | 472 | 468 | 463 | |
| " | $\frac{5}{8}$ | 142.5 | 42.30 | 6.48 | 521 | 519 | 516 | 513 | 509 | 505 | 501 | 497 | 492 | |
| " | $\frac{3}{4}$ | 151.0 | 44.80 | 6.44 | 552 | 549 | 546 | 543 | 539 | 535 | 531 | 526 | 521 | |
| " | $\frac{7}{8}$ | 159.5 | 47.30 | 6.41 | 583 | 580 | 577 | 573 | 569 | 565 | 561 | 554 | 549 | |
| " | 1 | 168.0 | 49.80 | 6.38 | 614 | 611 | 607 | 604 | 599 | 595 | 589 | 583 | 578 | |
| 35 | $\frac{3}{8}$ | 121.0 | 35.58 | 6.55 | 439 | 437 | 435 | 432 | 428 | 425 | 422 | 418 | 414 | |
| " | $\frac{7}{16}$ | 129.5 | 38.08 | 6.56 | 470 | 468 | 465 | 463 | 459 | 455 | 451 | 447 | 443 | |
| " | $\frac{1}{2}$ | 138.0 | 40.58 | 6.52 | 501 | 498 | 495 | 492 | 488 | 485 | 481 | 477 | 472 | |
| " | $\frac{5}{8}$ | 146.5 | 43.08 | 6.48 | 531 | 528 | 525 | 522 | 519 | 515 | 511 | 506 | 501 | |
| " | $\frac{3}{4}$ | 155.0 | 45.58 | 6.44 | 562 | 559 | 556 | 552 | 549 | 545 | 540 | 535 | 531 | |
| " | $\frac{7}{8}$ | 163.5 | 48.08 | 6.41 | 592 | 590 | 586 | 583 | 579 | 574 | 570 | 563 | 558 | |
| " | 1 | 172.0 | 50.58 | 6.38 | 623 | 620 | 617 | 613 | 609 | 604 | 598 | 592 | 587 | |
| 40 | $\frac{3}{8}$ | 131.0 | 38.52 | 6.41 | 475 | 472 | 470 | 467 | 464 | 460 | 457 | 451 | 447 | |
| " | $\frac{7}{16}$ | 139.5 | 41.02 | 6.51 | 506 | 503 | 500 | 497 | 494 | 490 | 486 | 482 | 477 | |
| " | $\frac{1}{2}$ | 148.0 | 43.52 | 6.50 | 537 | 534 | 531 | 527 | 524 | 520 | 516 | 511 | 507 | |
| " | $\frac{5}{8}$ | 156.5 | 46.02 | 6.47 | 567 | 564 | 561 | 558 | 554 | 550 | 545 | 541 | 536 | |
| " | $\frac{3}{4}$ | 165.0 | 48.52 | 6.43 | 598 | 595 | 592 | 588 | 584 | 580 | 575 | 570 | 563 | |
| " | $\frac{7}{8}$ | 173.5 | 51.02 | 6.40 | 629 | 626 | 622 | 618 | 614 | 610 | 603 | 598 | 592 | |
| " | 1 | 182.0 | 53.52 | 6.37 | 659 | 656 | 653 | 649 | 644 | 638 | 633 | 627 | 621 | |
| 45 | $\frac{3}{8}$ | 141.0 | 41.48 | 6.28 | 511 | 509 | 506 | 502 | 498 | 494 | 490 | 486 | 480 | |
| " | $\frac{7}{16}$ | 149.5 | 43.98 | 6.39 | 542 | 539 | 536 | 533 | 529 | 525 | 520 | 515 | 510 | |
| " | $\frac{1}{2}$ | 158.0 | 46.48 | 6.48 | 573 | 570 | 567 | 563 | 559 | 555 | 551 | 546 | 541 | |
| " | $\frac{5}{8}$ | 166.5 | 48.98 | 6.45 | 604 | 601 | 597 | 594 | 590 | 585 | 580 | 575 | 570 | |
| " | $\frac{3}{4}$ | 175.0 | 51.48 | 6.42 | 634 | 631 | 628 | 624 | 620 | 615 | 610 | 603 | 597 | |
| " | $\frac{7}{8}$ | 183.5 | 53.98 | 6.39 | 665 | 662 | 658 | 654 | 650 | 645 | 638 | 632 | 626 | |
| " | 1 | 192.0 | 56.48 | 6.37 | 696 | 693 | 689 | 685 | 680 | 673 | 667 | 661 | 655 | |
| 50 | $\frac{3}{8}$ | 151.0 | 44.42 | 6.17 | 547 | 544 | 541 | 537 | 533 | 528 | 523 | 519 | 514 | |
| " | $\frac{7}{16}$ | 159.5 | 46.92 | 6.28 | 578 | 575 | 572 | 567 | 563 | 559 | 555 | 550 | 543 | |
| " | $\frac{1}{2}$ | 168.0 | 49.42 | 6.37 | 609 | 606 | 603 | 599 | 595 | 589 | 584 | 579 | 573 | |
| " | $\frac{5}{8}$ | 176.5 | 51.92 | 6.43 | 640 | 636 | 633 | 629 | 625 | 620 | 615 | 610 | 602 | |
| " | $\frac{3}{4}$ | 185.0 | 54.42 | 6.40 | 671 | 667 | 664 | 660 | 655 | 650 | 643 | 637 | 631 | |
| " | $\frac{7}{8}$ | 193.5 | 56.92 | 6.37 | 701 | 698 | 694 | 690 | 685 | 678 | 673 | 667 | 660 | |
| " | 1 | 202.0 | 59.42 | 6.35 | 732 | 729 | 725 | 720 | 715 | 708 | 702 | 696 | 689 | |
| 55 | $\frac{3}{8}$ | 161.0 | 47.36 | 6.07 | 583 | 580 | 576 | 571 | 567 | 563 | 556 | 551 | 546 | |
| " | $\frac{7}{16}$ | 169.5 | 49.86 | 6.18 | 614 | 610 | 607 | 603 | 599 | 593 | 588 | 582 | 577 | |
| " | $\frac{1}{2}$ | 178.0 | 52.36 | 6.28 | 645 | 642 | 639 | 633 | 629 | 624 | 619 | 613 | 605 | |
| " | $\frac{5}{8}$ | 186.5 | 54.86 | 6.37 | 676 | 673 | 669 | 665 | 660 | 654 | 648 | 643 | 636 | |
| " | $\frac{3}{4}$ | 195.0 | 57.36 | 6.38 | 707 | 703 | 700 | 695 | 690 | 685 | 678 | 672 | 665 | |
| " | $\frac{7}{8}$ | 203.5 | 59.86 | 6.35 | 738 | 734 | 730 | 726 | 721 | 713 | 707 | 701 | 694 | |
| " | 1 | 212.0 | 62.36 | 6.33 | 768 | 764 | 760 | 756 | 751 | 743 | 737 | 730 | 724 | |

For detail dimensions see page 235

SAFE LOADS IN THOUSANDS OF POUNDS FOR 15" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula $P = \frac{50\,000}{1 + \frac{(L)^2}{36\,000\,r^2}}$ Safety factor 4.



SERIES B.

| Length in Feet. | | | | | | | | | | | | Thick- ness of Plates. | Weight of each Channel. |
|-----------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|------------------------------|-------------------------------|
| 80 | 82 | 84 | 36 | 38 | 40 | 42 | 44 | 46 | 48 | 50 | 52 | Inch. | Lbs. per Ft. |
| 401 | 397 | 393 | 388 | 383 | 379 | 374 | 369 | 364 | 359 | 353 | 348 | $\frac{3}{8}$ | 33 |
| 430 | 425 | 421 | 416 | 411 | 406 | 401 | 395 | 390 | 384 | 379 | 373 | $\frac{1}{2}$ | " |
| 459 | 454 | 449 | 444 | 439 | 433 | 427 | 422 | 414 | 408 | 402 | 396 | $\frac{1}{2}$ | " |
| 487 | 482 | 477 | 470 | 464 | 458 | 452 | 446 | 440 | 434 | 427 | 421 | $\frac{1}{2}$ | " |
| 515 | 509 | 503 | 498 | 492 | 485 | 479 | 473 | 466 | 457 | 450 | 444 | $\frac{5}{16}$ | " |
| 543 | 538 | 532 | 525 | 519 | 512 | 504 | 497 | 490 | 483 | 476 | 468 | $\frac{1}{2}$ | " |
| 572 | 566 | 560 | 553 | 544 | 537 | 530 | 523 | 516 | 508 | 501 | 491 | $\frac{3}{4}$ | " |
| 410 | 406 | 401 | 397 | 392 | 387 | 382 | 377 | 372 | 367 | 361 | 356 | $\frac{3}{8}$ | 35 |
| 439 | 434 | 430 | 425 | 420 | 414 | 409 | 404 | 398 | 392 | 387 | 381 | $\frac{1}{2}$ | " |
| 468 | 463 | 458 | 452 | 447 | 442 | 436 | 430 | 422 | 416 | 410 | 404 | $\frac{1}{2}$ | " |
| 496 | 491 | 486 | 478 | 473 | 467 | 461 | 454 | 448 | 442 | 435 | 429 | $\frac{5}{16}$ | " |
| 523 | 518 | 512 | 506 | 500 | 494 | 487 | 481 | 474 | 465 | 458 | 451 | $\frac{5}{16}$ | " |
| 552 | 546 | 540 | 534 | 528 | 521 | 512 | 505 | 498 | 491 | 483 | 476 | $\frac{1}{2}$ | " |
| 581 | 575 | 568 | 562 | 553 | 546 | 538 | 531 | 524 | 516 | 509 | 498 | $\frac{3}{4}$ | " |
| 442 | 438 | 433 | 428 | 423 | 417 | 410 | 404 | 399 | 393 | 387 | 381 | $\frac{3}{8}$ | 40 |
| 473 | 468 | 463 | 457 | 452 | 446 | 439 | 433 | 427 | 421 | 414 | 408 | $\frac{1}{2}$ | " |
| 502 | 496 | 491 | 485 | 480 | 471 | 465 | 459 | 453 | 446 | 440 | 433 | $\frac{1}{2}$ | " |
| 530 | 525 | 517 | 511 | 505 | 499 | 492 | 485 | 479 | 472 | 465 | 458 | $\frac{5}{16}$ | " |
| 557 | 551 | 545 | 539 | 532 | 526 | 519 | 512 | 502 | 495 | 488 | 480 | $\frac{5}{16}$ | " |
| 586 | 580 | 573 | 567 | 560 | 553 | 543 | 536 | 528 | 521 | 513 | 505 | $\frac{1}{2}$ | " |
| 615 | 608 | 601 | 592 | 585 | 577 | 570 | 562 | 554 | 546 | 538 | 527 | $\frac{3}{4}$ | " |
| 475 | 470 | 464 | 459 | 451 | 445 | 440 | 433 | 427 | 421 | 413 | 407 | $\frac{3}{8}$ | 45 |
| 505 | 500 | 494 | 488 | 483 | 474 | 468 | 462 | 455 | 449 | 442 | 435 | $\frac{1}{2}$ | " |
| 536 | 530 | 524 | 516 | 510 | 504 | 497 | 490 | 483 | 477 | 470 | 463 | $\frac{1}{2}$ | " |
| 563 | 557 | 550 | 544 | 537 | 531 | 524 | 517 | 509 | 502 | 492 | 485 | $\frac{5}{16}$ | " |
| 591 | 585 | 578 | 572 | 565 | 558 | 550 | 540 | 533 | 525 | 518 | 510 | $\frac{5}{16}$ | " |
| 620 | 613 | 607 | 600 | 592 | 582 | 575 | 567 | 559 | 551 | 543 | 535 | $\frac{1}{2}$ | " |
| 649 | 642 | 635 | 625 | 617 | 609 | 601 | 593 | 585 | 576 | 568 | 556 | $\frac{3}{4}$ | " |
| 507 | 501 | 495 | 489 | 481 | 475 | 469 | 462 | 453 | 447 | 440 | 433 | $\frac{3}{8}$ | 50 |
| 537 | 531 | 525 | 519 | 510 | 504 | 497 | 493 | 483 | 476 | 467 | 460 | $\frac{1}{2}$ | " |
| 568 | 562 | 555 | 547 | 540 | 533 | 526 | 519 | 512 | 504 | 497 | 487 | $\frac{1}{2}$ | " |
| 596 | 590 | 583 | 577 | 570 | 563 | 555 | 548 | 538 | 530 | 522 | 514 | $\frac{5}{16}$ | " |
| 625 | 618 | 612 | 604 | 597 | 590 | 579 | 571 | 563 | 555 | 547 | 539 | $\frac{5}{16}$ | " |
| 654 | 647 | 640 | 630 | 622 | 614 | 606 | 598 | 589 | 581 | 572 | 561 | $\frac{1}{2}$ | " |
| 682 | 675 | 665 | 657 | 649 | 641 | 632 | 623 | 615 | 603 | 594 | 585 | $\frac{3}{4}$ | " |
| 540 | 532 | 526 | 520 | 511 | 504 | 497 | 490 | 481 | 474 | 466 | 457 | $\frac{3}{8}$ | 55 |
| 569 | 562 | 556 | 549 | 542 | 533 | 526 | 519 | 511 | 501 | 494 | 486 | $\frac{1}{2}$ | " |
| 599 | 593 | 586 | 579 | 570 | 562 | 555 | 547 | 540 | 532 | 521 | 513 | $\frac{1}{2}$ | " |
| 630 | 623 | 616 | 607 | 599 | 592 | 584 | 576 | 568 | 560 | 552 | 540 | $\frac{5}{16}$ | " |
| 659 | 652 | 645 | 637 | 627 | 619 | 611 | 602 | 594 | 585 | 577 | 565 | $\frac{5}{16}$ | " |
| 687 | 680 | 670 | 662 | 654 | 646 | 637 | 628 | 620 | 608 | 599 | 590 | $\frac{1}{2}$ | " |
| 716 | 706 | 698 | 690 | 681 | 673 | 664 | 652 | 643 | 633 | 624 | 614 | $\frac{3}{4}$ | " |

For detail dimensions see page 235

SAFE LOADS IN THOUSANDS OF POUNDS FOR HOLLOW ROUND CAST IRON COLUMNS. SQUARE ENDS.

$$\text{Based on Gordon's Formula } P = \frac{10\,000}{1 + \frac{l^2}{800 d^3}}$$

P = safe load in pounds per square inch.

l = length of column in inches.

d = outside diameter of column in inches.

Ultimate compressive strength = 80 000 pounds per square inch. Safety factor 8.

Safe loads for other safety factors than that of the tables may be obtained as

follows:—New safe load = Safe load from table $\times \frac{8}{\text{New factor}}$.

| Outside Diam- eter in Inches. | Thick- ness in Inches. | Length of Column in Feet. | | | | | | | | | | Area of Metal in Sq. Ins. | Weight per Foot in Pounds. |
|--|------------------------------|---------------------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|------------------------------------|-------------------------------------|
| | | 6 | 8 | 10 | 12 | 14 | 16 | 18 | 20 | 22 | 24 | | |
| 6 | $\frac{3}{8}$ | 105 | 94 | 82 | 72 | 62 | 54 | 47 | 41 | 36 | 32 | 12.4 | 38.7 |
| | $\frac{1}{2}$ | 119 | 107 | 94 | 82 | 71 | 62 | 54 | 47 | 41 | 36 | 14.1 | 44.0 |
| 7 | $\frac{3}{8}$ | 130 | 119 | 108 | 96 | 86 | 76 | 67 | 60 | 53 | 47 | 14.7 | 46.0 |
| | $\frac{1}{2}$ | 149 | 136 | 123 | 110 | 98 | 87 | 77 | 68 | 61 | 54 | 16.8 | 52.6 |
| 8 | $\frac{3}{8}$ | 155 | 145 | 133 | 122 | 110 | 99 | 89 | 80 | 72 | 65 | 17.1 | 53.4 |
| | $\frac{1}{2}$ | 178 | 166 | 153 | 139 | 126 | 114 | 104 | 92 | 83 | 75 | 19.6 | 61.2 |
| 9 | 1 | 200 | 186 | 172 | 158 | 142 | 128 | 115 | 103 | 93 | 84 | 22.0 | 68.7 |
| | $\frac{1}{8}$ | 207 | 196 | 183 | 169 | 156 | 142 | 130 | 118 | 108 | 98 | 22.3 | 69.8 |
| 10 | 1 | 233 | 220 | 206 | 190 | 175 | 160 | 146 | 133 | 121 | 110 | 25.1 | 78.5 |
| | $\frac{1}{8}$ | 258 | 244 | 228 | 211 | 194 | 177 | 162 | 147 | 134 | 122 | 27.8 | 87.0 |
| 11 | $\frac{1}{8}$ | 235 | 225 | 212 | 199 | 185 | 172 | 158 | 146 | 134 | 123 | 25.1 | 78.4 |
| | 1 | 265 | 254 | 240 | 224 | 209 | 194 | 178 | 164 | 151 | 139 | 28.3 | 88.4 |
| 12 | $\frac{1}{8}$ | 294 | 281 | 266 | 249 | 232 | 215 | 198 | 182 | 168 | 154 | 31.4 | 98.0 |
| | $\frac{1}{4}$ | 323 | 308 | 291 | 273 | 254 | 235 | 217 | 200 | 184 | 169 | 34.4 | 107.4 |
| 13 | 1 | 298 | 287 | 273 | 259 | 243 | 227 | 212 | 197 | 183 | 169 | 31.4 | 98.2 |
| | $\frac{1}{8}$ | 330 | 319 | 304 | 287 | 270 | 253 | 235 | 219 | 203 | 188 | 34.9 | 109.1 |
| 14 | $\frac{1}{8}$ | 363 | 350 | 333 | 315 | 296 | 277 | 258 | 240 | 223 | 206 | 38.3 | 119.7 |
| | $\frac{1}{2}$ | 395 | 380 | 361 | 342 | 322 | 301 | 280 | 261 | 242 | 224 | 41.6 | 129.9 |
| 15 | $\frac{1}{8}$ | 368 | 356 | 342 | 326 | 309 | 291 | 274 | 256 | 239 | 223 | 38.4 | 120.1 |
| | $\frac{1}{4}$ | 404 | 391 | 375 | 358 | 339 | 320 | 300 | 281 | 263 | 245 | 42.2 | 131.9 |
| 16 | $\frac{1}{4}$ | 439 | 425 | 408 | 389 | 369 | 348 | 327 | 306 | 287 | 267 | 45.9 | 143.4 |
| | $\frac{1}{2}$ | 473 | 458 | 440 | 419 | 397 | 375 | 352 | 330 | 308 | 288 | 49.5 | 154.6 |
| 17 | $\frac{1}{8}$ | 404 | 393 | 379 | 364 | 347 | 330 | 312 | 294 | 277 | 260 | 42.0 | 131.2 |
| | $\frac{1}{4}$ | 444 | 432 | 417 | 400 | 382 | 363 | 343 | 323 | 304 | 286 | 46.1 | 144.2 |
| 18 | $\frac{1}{4}$ | 484 | 470 | 454 | 435 | 415 | 395 | 373 | 352 | 331 | 311 | 50.2 | 156.9 |
| | $\frac{1}{2}$ | 522 | 507 | 490 | 470 | 448 | 426 | 403 | 380 | 358 | 336 | 54.2 | 169.4 |
| 19 | $\frac{1}{4}$ | 485 | 473 | 459 | 442 | 424 | 405 | 386 | 366 | 347 | 327 | 50.1 | 156.5 |
| | $\frac{1}{2}$ | 528 | 515 | 499 | 482 | 462 | 441 | 420 | 399 | 378 | 357 | 54.5 | 170.4 |
| 20 | $\frac{1}{2}$ | 570 | 556 | 540 | 520 | 499 | 477 | 454 | 431 | 408 | 385 | 58.9 | 184.1 |
| | $\frac{3}{8}$ | 612 | 597 | 579 | 558 | 535 | 511 | 487 | 462 | 437 | 413 | 63.2 | 197.4 |
| 21 | $\frac{1}{8}$ | 573 | 560 | 545 | 528 | 509 | 489 | 467 | 446 | 424 | 406 | 58.9 | 183.9 |
| | $\frac{1}{4}$ | 618 | 605 | 589 | 570 | 550 | 528 | 505 | 482 | 459 | 439 | 63.6 | 198.8 |
| 22 | $\frac{1}{4}$ | 664 | 650 | 632 | 612 | 590 | 567 | 542 | 517 | 492 | 471 | 68.3 | 213.4 |
| | $\frac{1}{2}$ | 708 | 694 | 675 | 653 | 630 | 605 | 579 | 552 | 525 | 502 | 72.8 | 227.6 |
| 23 | $\frac{1}{8}$ | 666 | 654 | 638 | 620 | 600 | 579 | 557 | 533 | 510 | 486 | 68.3 | 213.5 |
| | $\frac{1}{4}$ | 716 | 702 | 686 | 666 | 645 | 622 | 598 | 573 | 548 | 522 | 73.4 | 229.3 |
| 24 | $\frac{1}{4}$ | 764 | 750 | 732 | 711 | 689 | 664 | 638 | 611 | 584 | 558 | 78.3 | 244.8 |
| | $\frac{1}{2}$ | 811 | 796 | 777 | 756 | 731 | 705 | 678 | 649 | 621 | 592 | 83.2 | 260.0 |

SAFE LOADS IN THOUSANDS OF POUNDS FOR HOLLOW ROUND CAST IRON COLUMNS. SQUARE ENDS.

$$\text{Based on Gordon's Formula } P = \frac{10\,000}{1 + \frac{l^2}{800 d^3}}$$

P = safe load in pounds per square inch.

l = length of column in inches.

d = outside diameter of column in inches.

Ultimate compressive strength = 80 000 pounds per square inch. Safety factor 8.

Safe loads for other safety factors than that of the tables may be obtained as

follows:—New safe load = Safe load from table $\times \frac{8}{\text{New factor}}$.

| Outside Diam- eter in Inches. | Thick- ness in Inches. | Length of Column in Feet. | | | | | | | | | | Area of Metal in Sq. Ins. | Weight per Foot in Pounds. |
|--|------------------------------|---------------------------|------|------|------|------|------|------|------|------|------|------------------------------------|-------------------------------------|
| | | 14 | 16 | 18 | 20 | 22 | 24 | 26 | 28 | 30 | 32 | | |
| 18 | 1½ | 754 | 732 | 708 | 684 | 659 | 633 | 608 | 596 | 557 | 533 | 83.6 | 261.2 |
| | 1¾ | 806 | 782 | 757 | 732 | 704 | 677 | 650 | 637 | 596 | 569 | 89.3 | 279.2 |
| | 1⅞ | 857 | 832 | 805 | 777 | 749 | 720 | 691 | 677 | 633 | 605 | 95.0 | 296.8 |
| | 2 | 907 | 880 | 852 | 823 | 792 | 762 | 731 | 717 | 670 | 641 | 100.5 | 314.2 |
| 20 | 1¾ | 922 | 900 | 876 | 850 | 824 | 797 | 769 | 742 | 714 | 687 | 100.3 | 313.6 |
| | 1⅞ | 981 | 957 | 932 | 905 | 877 | 848 | 819 | 789 | 760 | 731 | 106.8 | 333.6 |
| | 2 | 1039 | 1014 | 987 | 958 | 929 | 898 | 867 | 836 | 805 | 774 | 113.1 | 353.4 |
| | 2½ | 1097 | 1070 | 1041 | 1011 | 980 | 948 | 915 | 882 | 849 | 817 | 119.3 | 372.9 |
| 22 | 1¾ | 1105 | 1082 | 1058 | 1032 | 1005 | 976 | 947 | 918 | 888 | 859 | 118.5 | 370.5 |
| | 2 | 1171 | 1147 | 1122 | 1094 | 1065 | 1035 | 1004 | 974 | 941 | 910 | 125.7 | 392.7 |
| | 2½ | 1239 | 1213 | 1186 | 1157 | 1126 | 1094 | 1062 | 1029 | 996 | 962 | 132.9 | 415.3 |
| | 2¾ | 1301 | 1275 | 1246 | 1215 | 1183 | 1150 | 1116 | 1081 | 1046 | 1011 | 139.6 | 436.3 |
| 24 | 2 | 1303 | 1280 | 1241 | 1229 | 1201 | 1171 | 1141 | 1110 | 1079 | 1047 | 138.2 | 432.0 |
| | 2½ | 1376 | 1352 | 1311 | 1298 | 1268 | 1238 | 1206 | 1173 | 1140 | 1106 | 146.0 | 456.4 |
| | 2¾ | 1449 | 1423 | 1380 | 1367 | 1335 | 1303 | 1269 | 1235 | 1200 | 1165 | 153.7 | 480.4 |
| | 2⅞ | 1520 | 1494 | 1448 | 1434 | 1402 | 1367 | 1332 | 1296 | 1259 | 1222 | 161.4 | 504.2 |
| 26 | 2½ | 1515 | 1492 | 1467 | 1440 | 1412 | 1382 | 1351 | 1319 | 1286 | 1252 | 159.4 | 498.1 |
| | 2¾ | 1596 | 1572 | 1546 | 1517 | 1487 | 1456 | 1423 | 1389 | 1354 | 1319 | 167.9 | 524.6 |
| | 2⅞ | 1675 | 1650 | 1623 | 1593 | 1562 | 1528 | 1494 | 1458 | 1422 | 1385 | 176.3 | 550.9 |
| | 2⅞ | 1754 | 1728 | 1699 | 1668 | 1635 | 1600 | 1564 | 1527 | 1489 | 1450 | 184.6 | 576.8 |
| 28 | 2¾ | 1742 | 1719 | 1694 | 1667 | 1638 | 1608 | 1576 | 1542 | 1508 | 1474 | 182.0 | 568.8 |
| | 2⅞ | 1829 | 1806 | 1780 | 1751 | 1721 | 1689 | 1655 | 1620 | 1584 | 1548 | 191.2 | 597.5 |
| | 2⅞ | 1917 | 1892 | 1864 | 1834 | 1802 | 1769 | 1734 | 1697 | 1660 | 1622 | 200.3 | 625.9 |
| | 2⅞ | 2002 | 1967 | 1948 | 1917 | 1883 | 1848 | 1811 | 1773 | 1734 | 1694 | 209.3 | 653.9 |
| 30 | 2⅞ | 1982 | 1961 | 1936 | 1909 | 1879 | 1848 | 1816 | 1782 | 1747 | 1711 | 206.1 | 644.1 |
| | 2⅞ | 2078 | 2055 | 2028 | 2000 | 1969 | 1937 | 1903 | 1867 | 1830 | 1793 | 216.0 | 675.0 |
| | 2⅞ | 2172 | 2148 | 2119 | 2090 | 2058 | 2024 | 1989 | 1952 | 1913 | 1874 | 226.8 | 705.5 |
| | 2⅞ | 2265 | 2240 | 2210 | 2180 | 2147 | 2111 | 2074 | 2035 | 1995 | 1954 | 235.4 | 735.7 |
| 32 | 2⅞ | 2239 | 2217 | 2192 | 2165 | 2135 | 2104 | 2071 | 2036 | 2000 | 1963 | 231.7 | 724.0 |
| | 2⅞ | 2341 | 2318 | 2292 | 2264 | 2233 | 2200 | 2165 | 2129 | 2092 | 2053 | 242.2 | 757.0 |
| | 2⅞ | 2442 | 2418 | 2391 | 2361 | 2329 | 2295 | 2259 | 2221 | 2182 | 2141 | 252.7 | 789.7 |
| | 2⅞ | 2542 | 2517 | 2489 | 2458 | 2424 | 2389 | 2351 | 2312 | 2271 | 2229 | 263.1 | 822.1 |
| 34 | 2⅞ | 2511 | 2488 | 2463 | 2436 | 2406 | 2374 | 2341 | 2306 | 2272 | 2232 | 258.7 | 808.6 |
| | 2⅞ | 2620 | 2596 | 2570 | 2542 | 2511 | 2478 | 2441 | 2406 | 2370 | 2329 | 270.0 | 843.7 |
| | 2⅞ | 2728 | 2703 | 2676 | 2646 | 2614 | 2580 | 2544 | 2505 | 2468 | 2425 | 281.1 | 878.5 |
| | 3 | 2835 | 2810 | 2781 | 2750 | 2717 | 2681 | 2643 | 2604 | 2565 | 2520 | 292.2 | 913.0 |
| 36 | 2¾ | 2796 | 2774 | 2749 | 2721 | 2692 | 2660 | 2626 | 2591 | 2553 | 2515 | 287.3 | 897.7 |
| | 2¾ | 2913 | 2889 | 2863 | 2834 | 2803 | 2770 | 2735 | 2698 | 2659 | 2619 | 299.2 | 935.0 |
| | 3 | 3028 | 3003 | 2976 | 2946 | 2904 | 2880 | 2849 | 2805 | 2765 | 2723 | 311.0 | 971.9 |

STRENGTH OF HOLLOW ROUND AND HOLLOW RECTANGULAR CAST IRON COLUMNS.

For various values of $\frac{L}{d}$ in which:—

L = length of column in feet.

d = least outside diameter in inches.

P = ultimate strength in pounds per square inch.

Based on Gordon's Formulæ for Columns with Square Ends.

Hollow Round.

$$P = \frac{80000}{1 + \frac{(12L)^2}{800 d^2}}$$

Hollow Rectangular.

$$P = \frac{80000}{1 + \frac{(12L)^2}{1067 d^2}}$$

| $\frac{L}{d}$ | Ultimate Strength in lbs. per sq. in. | | $\frac{L}{d}$ | Ultimate Strength in lbs. per sq. in. | |
|---------------|--|------------------------|---------------|--|------------------------|
| | Hollow Round. | Hollow Rectangular. | | Hollow Round. | Hollow Rectangular. |
| 1.0 | 67800 | 70487 | 2.5 | 37647 | 43396 |
| 1.1 | 65692 | 68770 | 2.6 | 36088 | 41834 |
| 1.2 | 63532 | 66983 | 2.7 | 34599 | 40326 |
| 1.3 | 61340 | 65142 | 2.8 | 33178 | 38871 |
| 1.4 | 59137 | 63265 | 2.9 | 31817 | 37471 |
| 1.5 | 56940 | 61366 | 3.0 | 30534 | 36123 |
| 1.6 | 54766 | 59458 | 3.1 | 29306 | 34829 |
| 1.7 | 52625 | 57553 | 3.2 | 28137 | 33586 |
| 1.8 | 50531 | 55660 | 3.3 | 27025 | 32393 |
| 1.9 | 48491 | 53792 | 3.4 | 25967 | 31249 |
| 2.0 | 46512 | 51954 | 3.5 | 24961 | 30152 |
| 2.1 | 44598 | 50151 | 3.6 | 24004 | 29101 |
| 2.2 | 42753 | 48391 | 3.7 | 23093 | 28094 |
| 2.3 | 40979 | 46676 | 3.8 | 22227 | 27130 |
| 2.4 | 39277 | 45011 | 3.9 | 21403 | 26206 |

Safe loads for any given hollow round or hollow rectangular columns, corresponding to any suitable factor of safety, can be found from the above table as follows:—

Find from the table the ultimate strength in pounds per square inch corresponding to the given value of $\frac{L}{d}$. Multiply this by the area of the column in square inches and divide the product by the safety factor which will give as a quotient the required safe load in pounds.

EXAMPLE:—Required the safe load for a hollow round cast iron column 16 feet long, 10 inches external diameter with metal 1 inch thick with safety factor of eight. The ratio of $\frac{L}{d}$ in this case is $\frac{16}{10} = 1.6$ and the corresponding ultimate strength from the tables is 54 766 pounds per square inch.

From the table of areas of circles it is found that the net area of the column is 28.3 square inches. The safe load is, therefore, $\frac{54\ 766 \times 28.3}{8} = 193\ 735$ pounds or approximately 97 net tons, which is the required result.

EXPLANATIONS OF TABLES OF SAFE LOADS FOR BEAM BOX-GIRDERS AND PLATE GIRDERS, PAGES 306 TO 326 INCLUSIVE.

For cases in which the loads to be carried exceed the capacities of single rolled beams or ordinary beam girders composed of two or more beams with the usual bolts and separators, it is necessary to use built-up sections.

BEAM BOX-GIRDERS.—A useful and economical section of this kind can be composed of two rolled beams with plates riveted to the top and bottom flanges, making a beam box-girder, for which tables of safe uniformly distributed loads are given on pages 306 to 316 inclusive.

The safe loads given in the tables include the weights of the beam box-girders, and are figured from the moment of inertia or the section modulus after making the necessary deductions for rivet holes, the fibre stress used in the calculations being 15 000 pounds per square inch of net section.

Beam box-girders are particularly useful for supporting wide walls and in other locations up to the limits of their capacity, but they should not be placed where exposed to moisture, as the section is such that access cannot be had to their interior for inspection and painting.

PLATE GIRDERS.—In cases where the widths of beam box-girders would prohibit their use, and for loads greater than their capacities, plate girders composed of plates and angles may be used.

Tables of safe loads uniformly distributed for plate girders from 24" to 48" deep are given on pages 317 to 326 inclusive.

The loads given in the tables include the weights of the girders and are calculated from the moment of inertia or the section modulus after making a proper deduction for rivet holes, the fibre stress used in the calculation being 15 000 pounds per square inch of net section.

Although the tables do not show the stiffener angles for plate girders, care should be taken that these are provided in all cases where necessary to prevent buckling of the web due to the shearing action therein. The stiffeners should be made of angles riveted to the web, fitted tightly between the top and bottom flange angles, and they should be provided, at the end of the girders, of such size and number as to be capable of carrying the total reaction at each end to the supports. Stiffeners should also be provided at intervals along the girder, spaced at suitable distances apart, as determined by the formula and explanations on pages 94 and 95.

Care should also be taken in arranging the rivet spacing for connecting the flange angles to the web, so that sufficient rivets are provided to properly transmit the stresses which act between these two portions of the construction. This will require the rivets to be spaced more closely at the ends than at the center, and the exact spacing at any point along the girder may be obtained by dividing the product of the distance between the center lines of the rivet holes in the two flanges and the resistance of one rivet by the total vertical shear at the given point, thus:

$$p = \frac{r h}{S} \text{ in which}$$

S = the total vertical shear, in pounds, at the point under consideration.

r = the resistance of one rivet, *i. e.*, the bearing value or shearing value, whichever is the smaller, expressed in pounds.

h = the depth of the girder between the upper and lower center lines of rivets, expressed in inches.

p = pitch of rivets in the flange angles, expressed in inches.

The formula above will give the theoretical rivet spacing at any point in the flanges due to the total shear, but in practice the pitch for various portions of the length should be stated for the least possible number of spacing panels containing an even number of spaces, the pitch in each of which should preferably be expressed in even inches or even inches and halves or quarters of an inch, and the usual limits of pitch will vary from 2½" to 6".

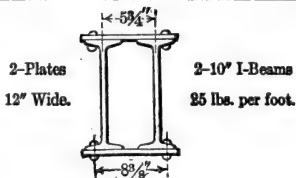
The rivet spacing should also conform to the rules given on page 358, and in cases where loads are applied directly to the flanges, sufficient rivets must be provided to carry these in addition to the rivets necessary for securing the web and flanges together as explained above.

It should also be noted that the safe loads given in the tables are based on the assumption that the girder is supported laterally, otherwise a proper reduction in the allowable safe load must be made, as explained in connection with beams on pages 82 and 83.

The weights of beam box-girders and plate girders in the tables are expressed in pounds per lineal foot, including the rivets necessary to secure the web and flanges together, but the weights do not include any allowance for brackets, stiffeners, connections or other details, as these will vary, subject to the conditions of each case.

SAFE LOADS IN THOUSANDS OF POUNDS UNIFORMLY DISTRIBUTED FOR BEAM BOX GIRDERS.

Safe loads below are figured for fibre stress of 15 000 pounds per square inch, with $\frac{11}{16}$ " rivet holes in both flanges deducted, and include weight of girder.

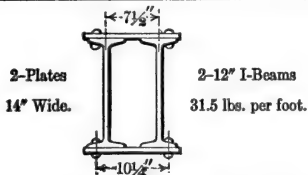


| Distance Center to Center of Bearings in Feet. | Thickness of Plates in Inches. For Thicknesses Greater than $\frac{3}{4}$ " Use Two Plates. | | | | | | | | |
|--|--|----------------|---------------|-----------------|---------------|-----------------|---------------|-----------------|-------|
| | $\frac{1}{2}$ | $\frac{9}{16}$ | $\frac{5}{8}$ | $\frac{11}{16}$ | $\frac{3}{4}$ | $\frac{13}{16}$ | $\frac{7}{8}$ | $\frac{15}{16}$ | 1 |
| 10 | 90 | 96 | 102 | 109 | 115 | 121 | 127 | 134 | 140 |
| 11 | 82 | 87 | 93 | 99 | 104 | 110 | 116 | 121 | 127 |
| 12 | 75 | 80 | 85 | 90 | 96 | 101 | 106 | 111 | 117 |
| 13 | 69 | 74 | 79 | 84 | 88 | 93 | 98 | 103 | 108 |
| 14 | 64 | 69 | 73 | 78 | 82 | 86 | 91 | 95 | 100 |
| 15 | 60 | 64 | 68 | 72 | 77 | 81 | 85 | 89 | 93 |
| 16 | 56 | 60 | 64 | 68 | 72 | 76 | 80 | 83 | 87 |
| 17 | 53 | 57 | 60 | 64 | 68 | 71 | 75 | 79 | 82 |
| 18 | 50 | 53 | 57 | 60 | 64 | 67 | 71 | 74 | 78 |
| 19 | 47 | 51 | 54 | 57 | 60 | 64 | 67 | 70 | 74 |
| 20 | 45 | 48 | 51 | 54 | 57 | 60 | 64 | 67 | 70 |
| 21 | 43 | 46 | 49 | 52 | 55 | 58 | 61 | 64 | 67 |
| 22 | 41 | 44 | 47 | 49 | 52 | 55 | 58 | 61 | 64 |
| 23 | 39 | 42 | 45 | 47 | 50 | 53 | 55 | 58 | 61 |
| 24 | 38 | 40 | 43 | 45 | 48 | 50 | 53 | 56 | 58 |
| 25 | 36 | 38 | 41 | 43 | 46 | 48 | 51 | 53 | 56 |
| 26 | 35 | 37 | 39 | 42 | 44 | 47 | 49 | 51 | 54 |
| 27 | 33 | 36 | 38 | 40 | 43 | 45 | 47 | 49 | 52 |
| 28 | 32 | 34 | 37 | 39 | 41 | 43 | 45 | 48 | 50 |
| 29 | 31 | 33 | 35 | 37 | 40 | 42 | 44 | 46 | 48 |
| 30 | 30 | 32 | 34 | 36 | 38 | 40 | 42 | 45 | 47 |
| 31 | 29 | 31 | 33 | 35 | 37 | 39 | 41 | 43 | 45 |
| 32 | 28 | 30 | 32 | 34 | 36 | 38 | 40 | 42 | 44 |
| 33 | 27 | 29 | 31 | 33 | 35 | 37 | 39 | 40 | 42 |
| 34 | 26 | 28 | 30 | 32 | 34 | 36 | 37 | 39 | 41 |
| Weight per Foot in Pounds. | 94.6 | 99.8 | 104.8 | 110.0 | 115.0 | 120.1 | 125.2 | 130.3 | 135.4 |
| Section Modulus. | 90.1 | 96.3 | 102.4 | 108.6 | 114.8 | 121.0 | 127.2 | 133.5 | 139.8 |
| Coefficient of Deflection. | 0.00000145 | | | 0.00000118 | | | 0.00000098 | | |

For safe loads below the heavy lines, the deflections will be greater than the allowable limit for plastered ceilings = $\frac{1}{160}$ span.

SAFE LOADS IN THOUSANDS OF POUNDS UNIFORMLY DISTRIBUTED FOR BEAM BOX GIRDERS.

Safe loads below are figured for fibre stress of 15 000 pounds per square inch, with $\frac{11}{16}$ " rivet holes in both flanges deducted, and include weight of girder.

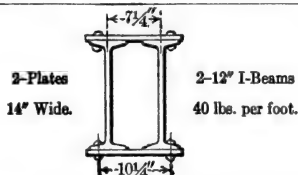


| Distance Center to Center of Bearings in Feet. | Thickness of Plates in Inches. For Thicknesses Greater than $\frac{3}{4}$ " Use Two Plates. | | | | | | | | |
|--|--|----------------|---------------|-----------------|---------------|-----------------|---------------|-----------------|-------|
| | $\frac{1}{2}$ | $\frac{9}{16}$ | $\frac{5}{8}$ | $\frac{11}{16}$ | $\frac{3}{4}$ | $\frac{13}{16}$ | $\frac{7}{8}$ | $\frac{15}{16}$ | 1 |
| 10 | 132 | 141 | 150 | 159 | 167 | 176 | 185 | 194 | 203 |
| 11 | 120 | 128 | 136 | 144 | 152 | 160 | 168 | 177 | 185 |
| 12 | 110 | 117 | 125 | 132 | 140 | 147 | 154 | 162 | 169 |
| 13 | 102 | 108 | 115 | 122 | 129 | 136 | 143 | 149 | 156 |
| 14 | 94 | 101 | 107 | 113 | 120 | 126 | 132 | 139 | 145 |
| 15 | 88 | 94 | 100 | 106 | 112 | 118 | 123 | 129 | 135 |
| 16 | 83 | 88 | 94 | 99 | 105 | 110 | 116 | 121 | 127 |
| 17 | 78 | 83 | 88 | 93 | 98 | 104 | 109 | 114 | 120 |
| 18 | 73 | 78 | 83 | 88 | 93 | 98 | 103 | 108 | 113 |
| 19 | 70 | 74 | 79 | 83 | 88 | 93 | 98 | 102 | 107 |
| 20 | 66 | 70 | 75 | 79 | 84 | 88 | 93 | 97 | 102 |
| 21 | 63 | 67 | 71 | 76 | 80 | 84 | 88 | 92 | 97 |
| 22 | 60 | 64 | 68 | 72 | 76 | 80 | 84 | 88 | 92 |
| 23 | 57 | 61 | 65 | 69 | 73 | 77 | 81 | 84 | 88 |
| 24 | 55 | 59 | 62 | 66 | 70 | 73 | 77 | 81 | 85 |
| 25 | 53 | 56 | 60 | 63 | 67 | 71 | 74 | 78 | 81 |
| 26 | 51 | 54 | 58 | 61 | 64 | 68 | 71 | 75 | 78 |
| 27 | 49 | 52 | 55 | 59 | 62 | 65 | 69 | 72 | 75 |
| 28 | 47 | 50 | 53 | 57 | 60 | 63 | 66 | 69 | 73 |
| 29 | 46 | 49 | 52 | 55 | 58 | 61 | 64 | 67 | 70 |
| 30 | 44 | 47 | 50 | 53 | 56 | 59 | 62 | 65 | 68 |
| 31 | 43 | 45 | 48 | 51 | 54 | 57 | 60 | 63 | 66 |
| 32 | 41 | 44 | 47 | 50 | 52 | 55 | 58 | 61 | 64 |
| 33 | 40 | 43 | 45 | 48 | 51 | 53 | 56 | 59 | 62 |
| 34 | 39 | 41 | 44 | 47 | 49 | 52 | 54 | 57 | 60 |
| Weight per Foot in Pounds. | 114.4 | 120.4 | 126.3 | 132.3 | 138.3 | 144.2 | 150.1 | 156.1 | 162.0 |
| Section Modulus. | 132.1 | 140.9 | 149.7 | 158.5 | 167.4 | 176.3 | 185.3 | 194.2 | 203.2 |
| Coefficient of Deflection. | 0.000000842 | | | 0.000000688 | | | 0.000000577 | | |

For safe loads below the heavy lines, the deflections will be greater than the allowable limit for plastered ceilings = $\frac{1}{360}$ span.

SAFE LOADS IN THOUSANDS OF POUNDS UNIFORMLY DISTRIBUTED FOR BEAM BOX GIRDERS.

Safe loads below are figured for fibre stress of 15 000 pounds per square inch, with $\frac{1}{4}$ " rivet holes in both flanges deducted, and include weight of girder.

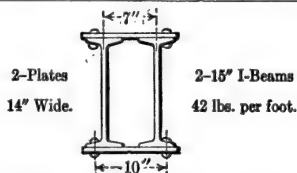


| Distance Center to Center of Bearings in Feet. | Thickness of Plates in Inches. For Thicknesses Greater than $\frac{3}{4}$ " Use Two Plates. | | | | | | | | |
|---|--|----------------|---------------|-----------------|---------------|-----------------|---------------|-----------------|-------|
| | $\frac{1}{2}$ | $\frac{9}{16}$ | $\frac{5}{8}$ | $\frac{11}{16}$ | $\frac{3}{4}$ | $\frac{13}{16}$ | $\frac{7}{8}$ | $\frac{15}{16}$ | 1 |
| 10 | 147 | 155 | 164 | 173 | 181 | 190 | 199 | 208 | 217 |
| 11 | 133 | 141 | 149 | 157 | 165 | 173 | 181 | 189 | 197 |
| 12 | 122 | 129 | 137 | 144 | 151 | 158 | 166 | 173 | 181 |
| 13 | 113 | 119 | 126 | 133 | 140 | 146 | 153 | 160 | 167 |
| 14 | 105 | 111 | 117 | 123 | 130 | 136 | 142 | 148 | 155 |
| 15 | 98 | 104 | 109 | 115 | 121 | 127 | 133 | 139 | 144 |
| 16 | 92 | 97 | 102 | 108 | 113 | 119 | 124 | 130 | 135 |
| 17 | 86 | 91 | 96 | 102 | 107 | 112 | 117 | 122 | 127 |
| 18 | 81 | 86 | 91 | 96 | 101 | 106 | 111 | 115 | 120 |
| 19 | 77 | 82 | 86 | 91 | 95 | 100 | 105 | 109 | 114 |
| 20 | 73 | 78 | 82 | 86 | 91 | 95 | 99 | 104 | 108 |
| 21 | 70 | 74 | 78 | 82 | 86 | 91 | 95 | 99 | 103 |
| 22 | 67 | 71 | 75 | 78 | 82 | 86 | 90 | 94 | 99 |
| 23 | 64 | 68 | 71 | 75 | 79 | 83 | 87 | 90 | 94 |
| 24 | 61 | 65 | 68 | 72 | 76 | 79 | 83 | 87 | 90 |
| 25 | 59 | 62 | 66 | 69 | 73 | 76 | 80 | 83 | 87 |
| 26 | 56 | 60 | 63 | 66 | 70 | 73 | 77 | 80 | 83 |
| 27 | 54 | 58 | 61 | 64 | 67 | 70 | 74 | 77 | 80 |
| 28 | 52 | 55 | 59 | 62 | 65 | 68 | 71 | 74 | 77 |
| 29 | 51 | 54 | 57 | 60 | 63 | 66 | 69 | 72 | 75 |
| 30 | 49 | 52 | 55 | 58 | 60 | 63 | 66 | 69 | 72 |
| 31 | 47 | 50 | 53 | 56 | 59 | 61 | 64 | 67 | 70 |
| 32 | 46 | 49 | 51 | 54 | 57 | 59 | 62 | 65 | 68 |
| 33 | 44 | 47 | 50 | 52 | 55 | 58 | 60 | 63 | 66 |
| 34 | 43 | 46 | 48 | 51 | 53 | 56 | 59 | 61 | 64 |
| Weight per Foot in Pounds. | 131.4 | 137.4 | 143.3 | 149.3 | 155.3 | 161.2 | 167.1 | 173.1 | 179.0 |
| Section Modulus. | 146.6 | 155.3 | 163.9 | 172.7 | 181.4 | 190.2 | 199.0 | 207.8 | 216.7 |
| Coefficient of Deflection. | 0.000000763 | | | 0.000000635 | | | 0.000000539 | | |

For safe loads below the heavy lines, the deflections will be greater than the allowable limit for plastered ceilings = $\frac{1}{360}$ span.

SAFE LOADS IN THOUSANDS OF POUNDS UNIFORMLY DISTRIBUTED FOR BEAM BOX GIRDERS.

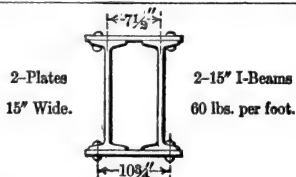
Safe loads below are figured for fibre stress of 15 000 pounds per square inch, with $\frac{11}{16}$ " rivet holes in both flanges deducted, and include weight of girder.



| Distance Center to Center of Bearings in Feet. | Thickness of Plates in Inches. For Thicknesses Greater than $\frac{3}{4}$ " Use Two Plates. | | | | | | | | | | |
|--|--|-----------------|---------------|-----------------|---------------|-----------------|-------------|-----------------|----------------|-----------------|----------------|
| | $\frac{5}{8}$ | $\frac{11}{16}$ | $\frac{3}{4}$ | $\frac{13}{16}$ | $\frac{7}{8}$ | $\frac{15}{16}$ | 1 | $1\frac{1}{16}$ | $1\frac{1}{8}$ | $1\frac{3}{16}$ | $1\frac{1}{2}$ |
| 10 | 212 | 223 | 234 | 245 | 256 | 267 | 278 | 289 | 300 | 312 | 323 |
| 11 | 193 | 203 | 213 | 223 | 233 | 243 | 253 | 263 | 273 | 283 | 293 |
| 12 | 177 | 186 | 195 | 204 | 213 | 223 | 232 | 241 | 250 | 260 | 269 |
| 13 | 163 | 172 | 180 | 188 | 197 | 205 | 214 | 223 | 231 | 240 | 248 |
| 14 | 151 | 159 | 167 | 175 | 183 | 191 | 199 | 207 | 215 | 223 | 231 |
| 15 | 141 | 149 | 156 | 163 | 171 | 178 | 185 | 193 | 200 | 208 | 215 |
| 16 | 133 | 139 | 146 | 153 | 160 | 167 | 174 | 181 | 188 | 195 | 202 |
| 17 | 125 | 131 | 138 | 144 | 151 | 157 | 164 | 170 | 177 | 183 | 190 |
| 18 | 118 | 124 | 130 | 136 | 142 | 148 | 155 | 161 | 167 | 173 | 179 |
| 19 | 112 | 117 | 123 | 129 | 135 | 141 | 146 | 152 | 158 | 164 | 170 |
| 20 | 106 | 112 | 117 | 122 | 128 | 134 | 139 | 145 | 150 | 156 | 161 |
| 21 | 101 | 106 | 111 | 117 | 122 | 127 | 132 | 138 | 143 | 148 | 154 |
| 22 | 96 | 101 | 106 | 111 | 116 | 121 | 126 | 131 | 137 | 142 | 147 |
| 23 | 92 | 97 | 102 | 107 | 111 | 116 | 121 | 126 | 131 | 135 | 140 |
| 24 | 88 | 93 | 98 | 102 | 107 | 111 | 116 | 121 | 125 | 130 | 135 |
| 25 | 85 | 89 | 94 | 98 | 102 | 107 | 111 | 116 | 120 | 125 | 129 |
| 26 | 82 | 86 | 90 | 94 | 98 | 103 | 107 | 111 | 116 | 120 | 124 |
| 27 | 79 | 83 | 87 | 91 | 95 | 99 | 103 | 107 | 111 | 115 | 120 |
| 28 | 76 | 80 | 84 | 88 | 91 | 95 | 99 | 103 | 107 | 111 | 115 |
| 29 | 73 | 77 | 81 | 84 | 88 | 92 | 96 | 100 | 104 | 107 | 111 |
| 30 | 71 | 74 | 78 | 82 | 85 | 89 | 93 | 96 | 100 | 104 | 108 |
| 31 | 68 | 72 | 75 | 79 | 83 | 86 | 90 | 93 | 97 | 101 | 104 |
| 32 | 66 | 70 | 73 | 77 | 80 | 83 | 87 | 90 | 94 | 97 | 101 |
| 33 | 64 | 68 | 71 | 74 | 78 | 81 | 84 | 88 | 91 | 94 | 98 |
| 34 | 62 | 66 | 69 | 72 | 75 | 79 | 82 | 85 | 88 | 92 | 95 |
| Weight per Foot in Pounds. | 147.3 | 153.3 | 159.3 | 165.2 | 171.1 | 177.1 | 183.0 | 189.0 | 194.9 | 200.9 | 206.8 |
| Section Modulus. | 212.1 | 223.0 | 234.0 | 245.0 | 256.0 | 267.1 | 278.2 | 289.3 | 300.5 | 311.6 | 322.8 |
| Coefficient of Deflection. | 0.000000426 | | | 0.000000362 | | | 0.000000314 | | | 0.000000281 | |

SAFE LOADS IN THOUSANDS OF POUNDS UNIFORMLY DISTRIBUTED FOR BEAM BOX GIRDERS.

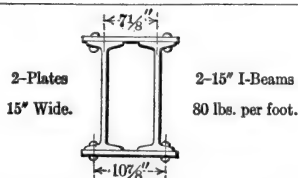
Safe loads below are figured for fibre stress of 15 000 pounds per square inch, with $\frac{11}{16}$ " rivet holes in both flanges deducted, and include weight of girder.



| Distance Center to Center of Bearings in Feet. | Thickness of Plates in Inches. For Thicknesses Greater than $\frac{3}{4}$ " Use Two Plates. | | | | | | | | | | | |
|--|--|-----------------|---------------|-----------------|---------------|-----------------|-------------|-----------------|----------------|-----------------|----------------|--|
| | $\frac{5}{8}$ | $\frac{11}{16}$ | $\frac{3}{4}$ | $\frac{13}{16}$ | $\frac{7}{8}$ | $\frac{15}{16}$ | 1 | $1\frac{1}{16}$ | $1\frac{1}{8}$ | $1\frac{3}{16}$ | $1\frac{1}{2}$ | |
| 10 | 259 | 271 | 282 | 294 | 306 | 318 | 329 | 341 | 353 | 365 | 377 | |
| 11 | 236 | 246 | 257 | 267 | 278 | 289 | 299 | 310 | 321 | 332 | 342 | |
| 12 | 216 | 226 | 235 | 245 | 255 | 265 | 274 | 284 | 294 | 304 | 314 | |
| 13 | 199 | 208 | 217 | 226 | 235 | 244 | 253 | 262 | 272 | 281 | 290 | |
| 14 | 185 | 193 | 202 | 210 | 218 | 227 | 235 | 244 | 252 | 261 | 269 | |
| 15 | 173 | 181 | 188 | 196 | 204 | 212 | 220 | 227 | 235 | 243 | 251 | |
| 16 | 162 | 169 | 177 | 184 | 191 | 198 | 206 | 213 | 221 | 228 | 235 | |
| 17 | 152 | 159 | 166 | 173 | 180 | 187 | 194 | 201 | 208 | 215 | 222 | |
| 18 | 144 | 150 | 157 | 163 | 170 | 176 | 183 | 190 | 196 | 203 | 209 | |
| 19 | 136 | 143 | 149 | 155 | 161 | 167 | 173 | 180 | 186 | 192 | 198 | |
| 20 | 130 | 135 | 141 | 147 | 153 | 159 | 165 | 171 | 176 | 182 | 188 | |
| 21 | 123 | 129 | 134 | 140 | 146 | 151 | 157 | 162 | 168 | 174 | 179 | |
| 22 | 118 | 123 | 128 | 134 | 139 | 144 | 150 | 155 | 160 | 166 | 171 | |
| 23 | 113 | 118 | 123 | 128 | 133 | 138 | 143 | 148 | 153 | 159 | 164 | |
| 24 | 108 | 113 | 118 | 123 | 127 | 132 | 137 | 142 | 147 | 152 | 157 | |
| 25 | 104 | 108 | 113 | 118 | 122 | 127 | 132 | 136 | 141 | 146 | 151 | |
| 26 | 100 | 104 | 109 | 113 | 118 | 122 | 127 | 131 | 136 | 140 | 145 | |
| 27 | 96 | 100 | 105 | 109 | 113 | 118 | 122 | 126 | 131 | 135 | 140 | |
| 28 | 93 | 97 | 101 | 105 | 109 | 113 | 118 | 122 | 126 | 130 | 135 | |
| 29 | 89 | 93 | 97 | 101 | 105 | 109 | 114 | 118 | 122 | 126 | 130 | |
| 30 | 86 | 90 | 94 | 98 | 102 | 106 | 110 | 114 | 118 | 122 | 126 | |
| 31 | 84 | 87 | 91 | 95 | 99 | 102 | 106 | 110 | 114 | 118 | 122 | |
| 32 | 81 | 85 | 88 | 92 | 96 | 99 | 103 | 107 | 110 | 114 | 118 | |
| 33 | 79 | 82 | 86 | 89 | 93 | 96 | 100 | 103 | 107 | 111 | 114 | |
| 34 | 76 | 80 | 83 | 87 | 90 | 93 | 97 | 100 | 104 | 107 | 111 | |
| Weight per Foot in Pounds. | 187.6 | 194.0 | 200.4 | 206.7 | 213.1 | 219.5 | 225.8 | 232.2 | 238.6 | 245.0 | 251.4 | |
| Section Modulus | 259.2 | 270.8 | 282.4 | 294.1 | 305.8 | 317.5 | 329.3 | 341.1 | 353.0 | 364.9 | 376.8 | |
| Coefficient of Deflection. | 0.000000350 | | | 0.000000303 | | | 0.000000266 | | | 0.000000240 | | |

SAFE LOADS IN THOUSANDS OF POUNDS UNIFORMLY DISTRIBUTED FOR BEAM BOX GIRDERS.

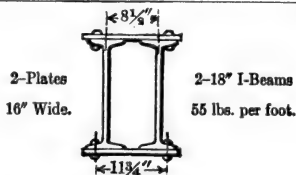
Safe loads below are figured for fibre stress of 15 000 pounds per square inch; with $\frac{11}{16}$ " rivet holes in both flanges deducted, and include weight of girder.



| Distance Center to Center of Bearings in Feet. | Thickness of Plates in Inches. For Thicknesses Greater than $\frac{3}{4}$ " Use Two Plates. | | | | | | | | | | |
|---|--|-----------------|---------------|-----------------|---------------|-----------------|-------------|-----------------|----------------|-----------------|----------------|
| | $\frac{5}{8}$ | $\frac{11}{16}$ | $\frac{3}{4}$ | $\frac{13}{16}$ | $\frac{7}{8}$ | $\frac{15}{16}$ | 1 | $1\frac{1}{16}$ | $1\frac{1}{8}$ | $1\frac{3}{16}$ | $1\frac{1}{2}$ |
| 10 | 300 | 311 | 322 | 334 | 345 | 357 | 368 | 380 | 391 | 403 | 414 |
| 11 | 272 | 283 | 293 | 303 | 314 | 324 | 335 | 345 | 356 | 366 | 377 |
| 12 | 250 | 259 | 269 | 278 | 288 | 297 | 307 | 316 | 326 | 336 | 345 |
| 13 | 231 | 239 | 248 | 257 | 265 | 274 | 283 | 292 | 301 | 310 | 319 |
| 14 | 214 | 222 | 230 | 238 | 247 | 255 | 263 | 271 | 279 | 288 | 296 |
| 15 | 200 | 207 | 215 | 222 | 230 | 238 | 245 | 253 | 261 | 269 | 276 |
| 16 | 187 | 194 | 201 | 209 | 216 | 223 | 230 | 237 | 244 | 252 | 259 |
| 17 | 176 | 183 | 190 | 196 | 203 | 210 | 217 | 223 | 230 | 237 | 244 |
| 18 | 167 | 173 | 179 | 185 | 192 | 198 | 204 | 211 | 217 | 224 | 230 |
| 19 | 158 | 164 | 170 | 176 | 182 | 188 | 194 | 200 | 206 | 212 | 218 |
| 20 | 150 | 156 | 161 | 167 | 173 | 178 | 184 | 190 | 196 | 201 | 207 |
| 21 | 143 | 148 | 154 | 159 | 164 | 170 | 175 | 181 | 186 | 192 | 197 |
| 22 | 136 | 141 | 147 | 152 | 157 | 162 | 167 | 173 | 178 | 183 | 188 |
| 23 | 130 | 135 | 140 | 145 | 150 | 155 | 160 | 165 | 170 | 173 | 180 |
| 24 | 125 | 130 | 134 | 139 | 144 | 149 | 153 | 158 | 163 | 168 | 173 |
| 25 | 120 | 124 | 129 | 133 | 138 | 143 | 147 | 152 | 156 | 161 | 166 |
| 26 | 115 | 120 | 124 | 128 | 133 | 137 | 142 | 146 | 150 | 155 | 159 |
| 27 | 111 | 115 | 119 | 124 | 128 | 132 | 136 | 141 | 145 | 149 | 153 |
| 28 | 107 | 111 | 115 | 119 | 123 | 127 | 131 | 136 | 140 | 144 | 148 |
| 29 | 103 | 107 | 111 | 115 | 119 | 123 | 127 | 131 | 135 | 139 | 143 |
| 30 | 100 | 104 | 107 | 111 | 115 | 119 | 123 | 127 | 130 | 134 | 138 |
| 31 | 97 | 100 | 104 | 108 | 111 | 115 | 119 | 122 | 126 | 130 | 134 |
| 32 | 94 | 97 | 101 | 104 | 108 | 111 | 115 | 119 | 122 | 126 | 130 |
| 33 | 91 | 94 | 98 | 101 | 105 | 108 | 112 | 115 | 119 | 122 | 126 |
| 34 | 88 | 91 | 95 | 98 | 102 | 105 | 108 | 112 | 115 | 118 | 122 |
| Weight per Foot in Pounds. | 227.6 | 234.0 | 240.4 | 246.7 | 253.1 | 259.5 | 265.8 | 272.2 | 278.6 | 285.0 | 291.4 |
| Section Modulus. | 299.7 | 311.0 | 322.4 | 333.7 | 345.1 | 356.6 | 368.1 | 379.6 | 391.2 | 402.8 | 414.4 |
| Coefficient of Deflection. | 0.000000305 | | | 0.000000269 | | | 0.000000239 | | | 0.000000218 | |

SAFE LOADS IN THOUSANDS OF POUNDS UNIFORMLY DISTRIBUTED FOR BEAM BOX GIRDERS.

Safe loads below are figured for fibre stress of 15 000 pounds per square inch, with $\frac{1}{8}$ " rivet holes in both flanges deducted, and include weight of girder.



| Distance Center to Center of Bearings in Feet. | Thickness of Plates in Inches. | | | | | | | | | | |
|---|--|---------------|---------------|---------------|-------|-----------------|----------------|-----------------|----------------|-----------------|----------------|
| | For Thicknesses Greater than $\frac{3}{4}$ " Use Two Plates. | | | | | | | | | | |
| | $\frac{3}{4}$ | $\frac{1}{2}$ | $\frac{7}{8}$ | $\frac{1}{2}$ | 1 | $1\frac{1}{16}$ | $1\frac{1}{8}$ | $1\frac{3}{16}$ | $1\frac{1}{4}$ | $1\frac{5}{16}$ | $1\frac{3}{8}$ |
| 15 | 227 | 237 | 247 | 258 | 268 | 278 | 289 | 299 | 309 | 320 | 330 |
| 16 | 213 | 222 | 232 | 242 | 251 | 261 | 271 | 280 | 290 | 300 | 310 |
| 17 | 200 | 209 | 218 | 227 | 237 | 246 | 255 | 264 | 273 | 282 | 291 |
| 18 | 189 | 198 | 206 | 215 | 223 | 232 | 241 | 249 | 258 | 267 | 275 |
| 19 | 179 | 187 | 195 | 203 | 212 | 220 | 228 | 236 | 244 | 253 | 261 |
| 20 | 170 | 178 | 186 | 193 | 201 | 209 | 217 | 224 | 232 | 240 | 248 |
| 21 | 162 | 169 | 177 | 184 | 191 | 199 | 206 | 214 | 221 | 228 | 236 |
| 22 | 155 | 162 | 169 | 176 | 183 | 190 | 197 | 204 | 211 | 218 | 225 |
| 23 | 148 | 155 | 161 | 168 | 175 | 182 | 188 | 195 | 202 | 209 | 215 |
| 24 | 142 | 148 | 155 | 161 | 168 | 174 | 180 | 187 | 193 | 200 | 206 |
| 25 | 136 | 142 | 148 | 155 | 161 | 167 | 173 | 179 | 186 | 192 | 198 |
| 26 | 131 | 137 | 143 | 149 | 155 | 161 | 167 | 173 | 179 | 185 | 191 |
| 27 | 126 | 132 | 137 | 143 | 149 | 155 | 160 | 166 | 172 | 178 | 183 |
| 28 | 122 | 127 | 133 | 138 | 144 | 149 | 155 | 160 | 166 | 171 | 177 |
| 29 | 117 | 123 | 128 | 133 | 139 | 144 | 149 | 155 | 160 | 165 | 171 |
| 30 | 113 | 119 | 124 | 129 | 134 | 139 | 144 | 150 | 155 | 160 | 165 |
| 31 | 110 | 115 | 120 | 125 | 130 | 135 | 140 | 145 | 150 | 155 | 160 |
| 32 | 106 | 111 | 116 | 121 | 126 | 130 | 135 | 140 | 145 | 150 | 155 |
| 33 | 103 | 108 | 112 | 117 | 122 | 127 | 131 | 136 | 141 | 145 | 150 |
| 34 | 100 | 105 | 109 | 114 | 118 | 123 | 127 | 132 | 137 | 141 | 146 |
| 35 | 97 | 102 | 106 | 110 | 115 | 119 | 124 | 128 | 133 | 137 | 142 |
| 36 | 95 | 99 | 103 | 107 | 112 | 116 | 120 | 125 | 129 | 133 | 138 |
| 37 | 92 | 96 | 100 | 104 | 109 | 113 | 117 | 121 | 125 | 130 | 134 |
| 38 | 90 | 94 | 98 | 102 | 106 | 110 | 114 | 118 | 122 | 126 | 130 |
| 39 | 87 | 91 | 95 | 99 | 103 | 107 | 111 | 115 | 119 | 123 | 127 |
| Weight per Foot in Pounds. | 195.5 | 202.2 | 209.0 | 215.8 | 222.6 | 229.4 | 236.2 | 243.1 | 249.8 | 256.7 | 263.4 |
| Section Modulus. | 340.5 | 355.8 | 371.2 | 386.6 | 402.1 | 417.5 | 433.0 | 448.6 | 464.2 | 479.8 | 495.4 |
| Coefficient of Deflection. | 0.000000223 | | | 0.000000193 | | | 0.000000170 | | | 0.000000154 | |

SAFE LOADS IN THOUSANDS OF POUNDS UNIFORMLY DISTRIBUTED FOR BEAM BOX GIRDERS.

Safe loads below are figured for fibre stress of 15 000 pounds per square inch, with $\frac{11}{16}$ " rivet holes in both flanges deducted, and include weight of girder.

2-Plates
16" Wide.

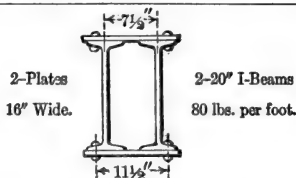


2-20" I-Beams
65 lbs. per foot.

| Distance Center to Center of Bearings in Feet. | Thickness of Plates in Inches. For Thicknesses Greater than $\frac{3}{4}$ " Use Two Plates. | | | | | | | | | | |
|--|--|-----------------|---------------|-----------------|-------|-----------------|----------------|-----------------|----------------|-----------------|----------------|
| | $\frac{3}{4}$ | $\frac{13}{16}$ | $\frac{7}{8}$ | $\frac{15}{16}$ | 1 | $1\frac{1}{16}$ | $1\frac{1}{8}$ | $1\frac{3}{16}$ | $1\frac{1}{4}$ | $1\frac{5}{16}$ | $1\frac{3}{8}$ |
| 15 | 275 | 286 | 297 | 308 | 320 | 331 | 343 | 354 | 365 | 377 | 388 |
| 16 | 257 | 268 | 279 | 289 | 300 | 310 | 321 | 332 | 343 | 350 | 364 |
| 17 | 242 | 252 | 262 | 272 | 282 | 292 | 302 | 312 | 322 | 333 | 343 |
| 18 | 229 | 238 | 248 | 257 | 266 | 276 | 285 | 295 | 305 | 314 | 324 |
| 19 | 217 | 226 | 235 | 244 | 252 | 261 | 270 | 280 | 288 | 298 | 307 |
| 20 | 206 | 214 | 223 | 231 | 240 | 248 | 257 | 266 | 274 | 283 | 291 |
| 21 | 196 | 204 | 212 | 220 | 228 | 237 | 245 | 253 | 261 | 269 | 277 |
| 22 | 187 | 195 | 203 | 210 | 218 | 226 | 234 | 241 | 249 | 257 | 265 |
| 23 | 179 | 186 | 194 | 201 | 209 | 216 | 223 | 231 | 238 | 246 | 253 |
| 24 | 172 | 179 | 186 | 193 | 200 | 207 | 214 | 221 | 228 | 236 | 243 |
| 25 | 165 | 171 | 178 | 185 | 192 | 199 | 206 | 212 | 219 | 226 | 233 |
| 26 | 158 | 165 | 171 | 178 | 184 | 191 | 198 | 204 | 211 | 217 | 224 |
| 27 | 153 | 159 | 165 | 171 | 178 | 184 | 190 | 197 | 203 | 209 | 216 |
| 28 | 147 | 153 | 159 | 165 | 171 | 177 | 184 | 190 | 196 | 202 | 208 |
| 29 | 142 | 148 | 154 | 160 | 165 | 171 | 177 | 183 | 189 | 195 | 201 |
| 30 | 137 | 143 | 149 | 154 | 160 | 166 | 171 | 177 | 183 | 188 | 194 |
| 31 | 133 | 138 | 144 | 149 | 155 | 160 | 166 | 171 | 177 | 182 | 188 |
| 32 | 129 | 134 | 139 | 145 | 150 | 155 | 161 | 166 | 171 | 177 | 182 |
| 33 | 125 | 130 | 135 | 140 | 145 | 151 | 156 | 161 | 166 | 171 | 177 |
| 34 | 121 | 126 | 131 | 136 | 141 | 146 | 151 | 156 | 161 | 166 | 171 |
| 35 | 118 | 122 | 127 | 132 | 137 | 142 | 147 | 152 | 157 | 162 | 166 |
| 36 | 114 | 119 | 124 | 129 | 133 | 138 | 143 | 148 | 152 | 157 | 162 |
| 37 | 111 | 116 | 120 | 125 | 130 | 134 | 139 | 144 | 148 | 153 | 157 |
| 38 | 108 | 113 | 117 | 122 | 126 | 131 | 135 | 140 | 144 | 149 | 153 |
| 39 | 106 | 110 | 114 | 119 | 123 | 127 | 132 | 136 | 141 | 145 | 149 |
| Weight per Foot in Pounds. | 215.5 | 222.2 | 229.0 | 235.8 | 242.6 | 249.4 | 256.2 | 263.1 | 269.8 | 276.7 | 283.4 |
| Section Modulus. | 411.8 | 428.7 | 445.7 | 462.7 | 479.7 | 496.7 | 513.8 | 531.2 | 548.1 | 565.3 | 582.5 |
| Coefficient of Deflection. | 0.000000168 | | | 0.000000147 | | | 0.000000131 | | | 0.000000119 | |

SAFE LOADS IN THOUSANDS OF POUNDS UNIFORMLY DISTRIBUTED FOR BEAM BOX GIRDERS.

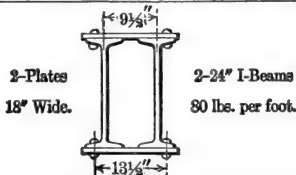
Safe loads below are figured for fibre stress of 15 000 pounds per square inch, with $\frac{11}{16}$ " rivet holes in both flanges deducted, and include weight of girder.



| Distance Center to Center of Bearings in Feet. | Thickness of Plates in Inches. For Thicknesses Greater than $\frac{3}{4}$ " Use Two Plates. | | | | | | | | | | |
|---|--|-----------------|---------------|-----------------|-------|-----------------|----------------|-----------------|----------------|-----------------|----------------|
| | $\frac{3}{4}$ | $\frac{13}{16}$ | $\frac{7}{8}$ | $\frac{15}{16}$ | 1 | $1\frac{1}{16}$ | $1\frac{1}{8}$ | $1\frac{3}{16}$ | $1\frac{1}{4}$ | $1\frac{5}{16}$ | $1\frac{3}{8}$ |
| 15 | 309 | 320 | 331 | 343 | 354 | 365 | 376 | 387 | 399 | 410 | 421 |
| 16 | 290 | 300 | 311 | 321 | 332 | 342 | 353 | 363 | 374 | 384 | 395 |
| 17 | 273 | 283 | 292 | 302 | 312 | 322 | 332 | 342 | 352 | 362 | 372 |
| 18 | 258 | 267 | 276 | 285 | 295 | 304 | 313 | 323 | 332 | 342 | 351 |
| 19 | 244 | 253 | 262 | 270 | 279 | 288 | 297 | 306 | 315 | 324 | 332 |
| 20 | 232 | 240 | 249 | 257 | 265 | 274 | 282 | 291 | 299 | 307 | 316 |
| 21 | 221 | 229 | 237 | 245 | 253 | 261 | 269 | 277 | 285 | 293 | 301 |
| 22 | 211 | 218 | 226 | 234 | 241 | 249 | 256 | 264 | 272 | 279 | 287 |
| 23 | 202 | 209 | 216 | 223 | 231 | 238 | 245 | 253 | 260 | 267 | 275 |
| 24 | 193 | 200 | 207 | 214 | 221 | 228 | 235 | 243 | 249 | 256 | 263 |
| 25 | 186 | 192 | 199 | 206 | 212 | 219 | 226 | 232 | 239 | 246 | 253 |
| 26 | 178 | 185 | 191 | 198 | 204 | 211 | 217 | 224 | 230 | 236 | 243 |
| 27 | 172 | 178 | 184 | 190 | 196 | 203 | 209 | 215 | 221 | 228 | 234 |
| 28 | 166 | 172 | 178 | 184 | 189 | 195 | 201 | 208 | 214 | 220 | 226 |
| 29 | 160 | 166 | 171 | 177 | 183 | 189 | 195 | 200 | 206 | 212 | 218 |
| 30 | 155 | 160 | 166 | 171 | 177 | 182 | 188 | 194 | 199 | 205 | 211 |
| 31 | 150 | 155 | 160 | 166 | 171 | 177 | 182 | 187 | 193 | 198 | 204 |
| 32 | 145 | 150 | 155 | 161 | 166 | 171 | 176 | 182 | 187 | 192 | 197 |
| 33 | 141 | 146 | 151 | 156 | 161 | 166 | 171 | 176 | 181 | 186 | 191 |
| 34 | 136 | 141 | 146 | 151 | 156 | 161 | 166 | 171 | 176 | 181 | 186 |
| 35 | 133 | 137 | 142 | 147 | 152 | 156 | 161 | 166 | 171 | 176 | 180 |
| 36 | 129 | 133 | 138 | 143 | 147 | 152 | 157 | 161 | 166 | 171 | 175 |
| 37 | 125 | 130 | 134 | 139 | 143 | 148 | 152 | 157 | 162 | 166 | 171 |
| 38 | 122 | 126 | 131 | 135 | 140 | 144 | 148 | 153 | 157 | 162 | 166 |
| 39 | 119 | 123 | 127 | 132 | 136 | 140 | 145 | 149 | 153 | 158 | 162 |
| Weight per Foot in Pounds. | 245.5 | 252.2 | 259.0 | 265.8 | 272.6 | 279.4 | 286.2 | 293.1 | 299.8 | 306.7 | 313.4 |
| Section Modulus. | 463.8 | 480.4 | 497.1 | 513.8 | 530.6 | 547.3 | 564.1 | 581.2 | 597.8 | 614.7 | 631.7 |
| Coefficient of Deflection. | 0.000000149 | | | 0.000000133 | | | 0.000000119 | | | 0.000000110 | |

SAFE LOADS IN THOUSANDS OF POUNDS UNIFORMLY DISTRIBUTED FOR BEAM BOX GIRDERS.

Safe loads below are figured for fibre stress of 15 000 pounds per square inch, with $\frac{11}{16}$ " rivet holes in both flanges deducted, and include weight of girder.



| Distance Center to Center of Bearings in Feet. | Thickness of Plates in Inches. For Thicknesses Greater than $\frac{3}{4}$ " Use Two Plates. | | | | | | | | | | |
|---|--|-----------------|---------------|-----------------|-------|-----------------|----------------|-----------------|----------------|-----------------|----------------|
| | $\frac{3}{4}$ | $\frac{13}{16}$ | $\frac{7}{8}$ | $\frac{15}{16}$ | 1 | $1\frac{1}{16}$ | $1\frac{1}{8}$ | $1\frac{3}{16}$ | $1\frac{1}{4}$ | $1\frac{5}{16}$ | $1\frac{3}{8}$ |
| 15 | 396 | 411 | 427 | 442 | 458 | 473 | 489 | 505 | 520 | 536 | 551 |
| 16 | 371 | 386 | 400 | 415 | 429 | 444 | 458 | 473 | 488 | 502 | 517 |
| 17 | 349 | 363 | 377 | 390 | 404 | 418 | 431 | 445 | 459 | 473 | 487 |
| 18 | 330 | 343 | 356 | 369 | 381 | 394 | 407 | 421 | 433 | 446 | 460 |
| 19 | 312 | 325 | 337 | 349 | 361 | 374 | 386 | 398 | 411 | 423 | 435 |
| 20 | 297 | 308 | 320 | 332 | 343 | 355 | 367 | 379 | 390 | 402 | 414 |
| 21 | 283 | 294 | 305 | 316 | 327 | 338 | 349 | 361 | 372 | 383 | 394 |
| 22 | 270 | 280 | 291 | 302 | 312 | 323 | 333 | 344 | 355 | 365 | 376 |
| 23 | 258 | 268 | 278 | 288 | 299 | 309 | 319 | 329 | 339 | 349 | 360 |
| 24 | 247 | 257 | 267 | 276 | 286 | 296 | 306 | 315 | 325 | 335 | 345 |
| 25 | 237 | 247 | 256 | 265 | 275 | 284 | 293 | 303 | 312 | 321 | 331 |
| 26 | 228 | 237 | 246 | 255 | 264 | 273 | 282 | 291 | 300 | 309 | 318 |
| 27 | 220 | 228 | 237 | 246 | 254 | 263 | 272 | 280 | 289 | 298 | 306 |
| 28 | 212 | 220 | 229 | 237 | 245 | 254 | 262 | 270 | 279 | 287 | 295 |
| 29 | 205 | 213 | 221 | 229 | 237 | 245 | 253 | 261 | 269 | 277 | 285 |
| 30 | 198 | 206 | 213 | 221 | 229 | 237 | 244 | 252 | 260 | 268 | 276 |
| 31 | 192 | 199 | 206 | 214 | 222 | 229 | 237 | 244 | 252 | 259 | 267 |
| 32 | 186 | 193 | 200 | 207 | 215 | 222 | 229 | 237 | 244 | 251 | 258 |
| 33 | 180 | 187 | 194 | 201 | 208 | 215 | 222 | 229 | 236 | 244 | 251 |
| 34 | 175 | 181 | 188 | 195 | 202 | 209 | 216 | 223 | 229 | 236 | 243 |
| 35 | 170 | 176 | 183 | 190 | 196 | 203 | 210 | 216 | 223 | 230 | 236 |
| 36 | 165 | 171 | 178 | 184 | 191 | 197 | 204 | 210 | 217 | 223 | 230 |
| 37 | 160 | 167 | 173 | 179 | 186 | 192 | 198 | 205 | 211 | 217 | 224 |
| 38 | 156 | 162 | 168 | 175 | 181 | 187 | 193 | 199 | 205 | 211 | 218 |
| 39 | 152 | 158 | 164 | 170 | 176 | 182 | 188 | 194 | 200 | 206 | 212 |
| Weight per Foot in Pounds. | 255.7 | 263.3 | 271.0 | 278.6 | 286.2 | 293.9 | 301.5 | 309.2 | 316.8 | 324.5 | 332.1 |
| Section Modulus. | 593.7 | 616.9 | 640.1 | 663.4 | 686.7 | 710.0 | 733.3 | 757.1 | 780.2 | 803.6 | 827.1 |
| Coefficient of Deflection. | 0.0000000983 | | | 0.0000000870 | | | 0.0000000778 | | | 0.0000000713 | |

SAFE LOADS IN THOUSANDS OF POUNDS UNIFORMLY DISTRIBUTED FOR BEAM BOX GIRDERS.

Safe loads below are figured for fibre stress of 15 000 pounds per square inch, with $\frac{11}{16}$ " rivet holes in both flanges deducted, and include weight of girder.

2 Plates

18" Wide.



2-24" I-Beams

105 lbs. per foot.



Distance Center
to Center of
Bearings in
Feet.

Thickness of Plates in Inches.
For Thicknesses Greater than $\frac{3}{4}$ ", Use Two Plates.

| | $\frac{3}{8}$ | $\frac{13}{16}$ | $\frac{7}{8}$ | $\frac{15}{16}$ | 1 | $1\frac{1}{16}$ | $1\frac{1}{8}$ | $1\frac{3}{16}$ | $1\frac{1}{4}$ | $1\frac{5}{16}$ | $1\frac{3}{4}$ |
|--|---------------|-----------------|---------------|-----------------|-------|-----------------|----------------|-----------------|----------------|-----------------|----------------|
| 15 | 466 | 481 | 496 | 511 | 526 | 541 | 557 | 572 | 587 | 602 | 618 |
| 16 | 437 | 451 | 465 | 479 | 493 | 507 | 522 | 536 | 550 | 565 | 579 |
| 17 | 411 | 424 | 437 | 451 | 464 | 478 | 491 | 505 | 518 | 532 | 545 |
| 18 | 388 | 401 | 413 | 426 | 438 | 451 | 464 | 477 | 489 | 502 | 515 |
| 19 | 368 | 379 | 391 | 403 | 415 | 427 | 439 | 451 | 463 | 476 | 488 |
| 20 | 349 | 361 | 372 | 383 | 395 | 406 | 417 | 429 | 440 | 452 | 463 |
| 21 | 333 | 343 | 354 | 365 | 376 | 387 | 398 | 408 | 419 | 430 | 441 |
| 22 | 317 | 328 | 338 | 348 | 359 | 369 | 379 | 390 | 400 | 411 | 421 |
| 23 | 304 | 314 | 323 | 333 | 352 | 353 | 363 | 373 | 383 | 393 | 403 |
| 24 | 291 | 300 | 310 | 319 | 329 | 338 | 348 | 357 | 367 | 376 | 386 |
| 25 | 279 | 288 | 297 | 307 | 316 | 325 | 334 | 343 | 352 | 361 | 371 |
| 26 | 269 | 277 | 286 | 295 | 303 | 312 | 321 | 330 | 339 | 347 | 356 |
| 27 | 259 | 267 | 275 | 284 | 292 | 301 | 309 | 318 | 326 | 335 | 343 |
| 28 | 249 | 258 | 265 | 274 | 282 | 290 | 298 | 306 | 314 | 323 | 331 |
| 29 | 241 | 249 | 256 | 264 | 272 | 280 | 288 | 296 | 304 | 312 | 319 |
| 30 | 233 | 240 | 248 | 255 | 263 | 271 | 278 | 286 | 293 | 301 | 309 |
| 31 | 225 | 232 | 240 | 247 | 254 | 262 | 269 | 277 | 284 | 291 | 299 |
| 32 | 218 | 225 | 232 | 239 | 246 | 254 | 261 | 268 | 275 | 282 | 289 |
| 33 | 211 | 218 | 225 | 232 | 239 | 246 | 253 | 260 | 267 | 274 | 281 |
| 34 | 205 | 212 | 219 | 225 | 232 | 239 | 245 | 252 | 259 | 266 | 272 |
| 35 | 199 | 206 | 212 | 219 | 225 | 232 | 238 | 245 | 251 | 258 | 265 |
| 36 | 194 | 200 | 206 | 213 | 219 | 225 | 232 | 238 | 245 | 251 | 257 |
| 37 | 189 | 195 | 201 | 207 | 213 | 219 | 226 | 232 | 238 | 244 | 250 |
| 38 | 184 | 190 | 196 | 202 | 208 | 214 | 220 | 226 | 237 | 238 | 244 |
| 39 | 179 | 185 | 191 | 196 | 202 | 208 | 214 | 220 | 226 | 232 | 237 |
| Weight per Foot in Pounds | 305.6 | 313.3 | 320.9 | 328.6 | 336.2 | 343.9 | 351.5 | 359.2 | 366.8 | 374.5 | 382.1 |
| Section Modulus. | 698.6 | 721.3 | 744.0 | 766.8 | 789.6 | 812.4 | 835.3 | 858.2 | 881.1 | 904.1 | 927.1 |
| Coefficient of Deflection = $0.000000001 \times$ | 87 | 84 | 81 | 78 | 76 | 73 | 71 | 69 | 66 | 64 | 63 |



SAFE UNIFORMLY DISTRIBUTED LOADS FOR PLATE GIRDERS IN THOUSANDS OF POUNDS.

The safe loads below include the weight of the girder and are calculated for a fibre stress of 15 000 pounds per square inch on the net section. The net section is obtained by deducting holes figured at $\frac{1}{8}$ of an inch in diameter (for $\frac{3}{4}$ " rivets) from both flanges.

| <div>Web Plate<div></div></div> | | | | | <div>Flange Angles<div></div></div> | | | | |
|--|--|------|------|-------|--|------|-------|-------|--|
| 24" × 3⁄8" | | | | | 5" × 3½" | | | | |
| Distance Center to Center of Bearings in Feet. | Thickness of Flange Angles in Inches. | | | | Thickness of Flange Angles in Inches. | | | | |
| | 3⁄8 | 1⁄2 | 5⁄8 | 3⁄4 | 3⁄8 | 1⁄2 | 5⁄8 | 3⁄4 | |
| 25 | 59 | 74 | 87 | | 69 | 85 | 101 | | |
| 26 | 57 | 71 | 84 | | 67 | 82 | 97 | | |
| 27 | 55 | 68 | 81 | 92 | 64 | 79 | 93 | | |
| 28 | 53 | 66 | 78 | 89 | 62 | 76 | 90 | 103 | |
| 29 | 51 | 63 | 75 | 86 | 60 | 74 | 87 | 99 | |
| 30 | 50 | 61 | 73 | 83 | 58 | 71 | 84 | 96 | |
| 31 | 48 | 59 | 70 | 80 | 56 | 69 | 81 | 93 | |
| 32 | 46 | 57 | 68 | 78 | 54 | 67 | 79 | 90 | |
| 33 | 45 | 56 | 66 | 75 | 53 | 65 | 76 | 87 | |
| 34 | 44 | 54 | 64 | 73 | 51 | 63 | 74 | 85 | |
| 35 | 42 | 53 | 62 | 71 | 50 | 61 | 72 | 82 | |
| 36 | 41 | 51 | 60 | 69 | 48 | 59 | 70 | 80 | |
| 37 | 40 | 50 | 59 | 67 | 47 | 58 | 68 | 78 | |
| 38 | 39 | 48 | 57 | 66 | 46 | 56 | 66 | 76 | |
| 39 | 38 | 47 | 56 | 64 | 44 | 55 | 65 | 74 | |
| 40 | 37 | 46 | 54 | 62 | 43 | 53 | 63 | 72 | |
| 41 | 36 | 45 | 53 | 61 | 42 | 52 | 61 | 70 | |
| 42 | 35 | 44 | 52 | 59 | 41 | 51 | 60 | 69 | |
| 43 | 35 | 43 | 51 | 58 | 40 | 50 | 59 | 67 | |
| 44 | 34 | 42 | 49 | 57 | 39 | 49 | 57 | 65 | |
| 45 | 33 | 41 | 48 | 55 | 39 | 47 | 56 | 64 | |
| 46 | 32 | 40 | 47 | 54 | 38 | 46 | 55 | 63 | |
| 47 | 32 | 39 | 46 | 53 | 37 | 45 | 54 | 61 | |
| 48 | 31 | 38 | 45 | 52 | 36 | 44 | 53 | 60 | |
| 49 | 30 | 38 | 44 | 51 | 35 | 44 | 51 | 59 | |
| 50 | 30 | 37 | 44 | 50 | 35 | 43 | 50 | 58 | |
| 51 | 29 | 36 | 43 | 49 | 34 | 42 | 49 | 57 | |
| 52 | 29 | 35 | 42 | 48 | 33 | 41 | 48 | 55 | |
| 53 | 28 | 35 | 41 | 47 | 33 | 40 | 48 | 54 | |
| 54 | 28 | 34 | 40 | 46 | 32 | 40 | 47 | 53 | |
| Weight per Foot in Pounds. | 74.1 | 86.9 | 99.7 | 111.7 | 78 | 90.8 | 103.6 | 115.6 | |

SAFE UNIFORMLY DISTRIBUTED LOADS FOR PLATE GIRDERS IN THOUSANDS OF POUNDS.

The safe loads below include the weight of the girder and are calculated for a fibre stress of 15 000 pounds per square inch on the net section. The net section is obtained by deducting holes figured at $\frac{1}{8}$ of an inch in diameter (for $\frac{3}{4}$ " rivets) from both flanges.

| <div>Web Plate</div> <div></div> <div>Flange Angles</div> <div>$30'' \times \frac{3}{8}''$</div> <div>$6'' \times 3\frac{1}{2}''$</div> | | | | | <div>Web Plate</div> <div></div> <div>Flange Angles</div> <div>$33'' \times \frac{3}{8}''$</div> <div>$6'' \times 3\frac{1}{2}''$</div> | | | | |
|--|--|---------------|---------------|---------------|--|---------------|---------------|---------------|--|
| Distance Center to Center of Bearings in Feet. | Thickness of Flange Angles in Inches. | | | | Thickness of Flange Angles in Inches. | | | | |
| | $\frac{3}{8}$ | $\frac{1}{2}$ | $\frac{5}{8}$ | $\frac{3}{4}$ | $\frac{3}{8}$ | $\frac{1}{2}$ | $\frac{5}{8}$ | $\frac{3}{4}$ | |
| 30 | 74 | 91 | 108 | | 83 | 103 | 122 | | |
| 31 | 71 | 88 | 105 | | 81 | 100 | 118 | | |
| 32 | 69 | 86 | 101 | 116 | 78 | 97 | 114 | 131 | |
| 33 | 67 | 83 | 98 | 113 | 76 | 94 | 111 | 127 | |
| 34 | 65 | 81 | 95 | 109 | 74 | 91 | 107 | 123 | |
| 35 | 63 | 78 | 93 | 106 | 72 | 88 | 104 | 119 | |
| 36 | 61 | 76 | 90 | 103 | 70 | 86 | 101 | 116 | |
| 37 | 60 | 74 | 88 | 101 | 68 | 84 | 99 | 113 | |
| 38 | 58 | 72 | 85 | 98 | 66 | 81 | 96 | 110 | |
| 39 | 57 | 70 | 83 | 95 | 64 | 79 | 94 | 107 | |
| 40 | 55 | 69 | 81 | 93 | 63 | 77 | 91 | 104 | |
| 41 | 54 | 67 | 79 | 91 | 61 | 75 | 89 | 102 | |
| 42 | 53 | 65 | 77 | 89 | 60 | 74 | 87 | 99 | |
| 43 | 51 | 64 | 75 | 86 | 58 | 72 | 85 | 97 | |
| 44 | 50 | 62 | 74 | 85 | 57 | 70 | 83 | 95 | |
| 45 | 49 | 61 | 72 | 83 | 56 | 69 | 81 | 93 | |
| 46 | 48 | 60 | 71 | 81 | 54 | 67 | 79 | 91 | |
| 47 | 47 | 58 | 69 | 79 | 53 | 66 | 78 | 89 | |
| 48 | 46 | 57 | 68 | 77 | 52 | 64 | 76 | 87 | |
| 49 | 45 | 56 | 66 | 76 | 51 | 63 | 75 | 85 | |
| 50 | 44 | 55 | 65 | 74 | 50 | 62 | 73 | 84 | |
| 51 | 43 | 54 | 64 | 73 | 49 | 61 | 72 | 82 | |
| 52 | 43 | 53 | 62 | 72 | 48 | 59 | 70 | 80 | |
| 53 | 42 | 52 | 61 | 70 | 47 | 58 | 69 | 79 | |
| 54 | 41 | 51 | 60 | 69 | 46 | 57 | 68 | 77 | |
| 55 | 40 | 50 | 59 | 68 | 46 | 56 | 66 | 76 | |
| 56 | 39 | 49 | 58 | 66 | 45 | 55 | 65 | 75 | |
| 57 | 39 | 48 | 57 | 65 | 44 | 54 | 64 | 73 | |
| 58 | 38 | 47 | 56 | 64 | 43 | 53 | 63 | 72 | |
| 59 | 37 | 46 | 55 | 63 | 42 | 52 | 62 | 71 | |
| Weight per Foot in Pounds. | 87.0 | 101.4 | 115.8 | 129.8 | 90.8 | 105.2 | 119.6 | 133.5 | |

SAFE UNIFORMLY DISTRIBUTED LOADS FOR PLATE GIRDERS IN THOUSANDS OF POUNDS.

The safe loads below include the weight of the girder and are calculated for a fibre stress of 15 000 pounds per square inch on the net section. The net section is obtained by deducting holes figured at one inch in diameter (for $\frac{3}{8}$ " rivets) from both flanges.

Web Plate $36" \times \frac{3}{8}"$

Flange Angles $6" \times 4"$



Web Plate $36" \times \frac{3}{8}"$

Flange Angles $6" \times 4" \times \frac{3}{4}"$

Flange Plate $14"$

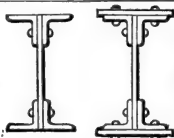
| Distance Center to Center of Bearings in Feet. | Thickness of Flange Angles in Inches. | | | | | Thickness of Flange Plate in Inches. | | | | | |
|---|--|---------------|---------------|---------------|---------------|---|---------------|---------------|---------------|---------------|-------|
| | $\frac{3}{8}$ | $\frac{1}{2}$ | $\frac{5}{8}$ | $\frac{3}{4}$ | $\frac{7}{8}$ | $\frac{3}{8}$ | $\frac{1}{2}$ | $\frac{5}{8}$ | $\frac{3}{4}$ | $\frac{7}{8}$ | 1 |
| 30 | 95 | 117 | 138 | 158 | 177 | 191 | 209 | 226 | 243 | 260 | 277 |
| 31 | 92 | 113 | 133 | 152 | 171 | 185 | 202 | 218 | 235 | 252 | 268 |
| 32 | 89 | 109 | 129 | 148 | 166 | 179 | 196 | 212 | 227 | 244 | 260 |
| 33 | 86 | 106 | 125 | 143 | 161 | 174 | 190 | 205 | 221 | 236 | 252 |
| 34 | 84 | 103 | 121 | 139 | 156 | 169 | 184 | 199 | 214 | 229 | 244 |
| 35 | 81 | 100 | 118 | 135 | 151 | 164 | 179 | 193 | 208 | 223 | 237 |
| 36 | 79 | 97 | 115 | 131 | 147 | 159 | 174 | 188 | 202 | 217 | 231 |
| 37 | 77 | 94 | 112 | 128 | 143 | 155 | 169 | 183 | 197 | 211 | 225 |
| 38 | 75 | 92 | 109 | 124 | 140 | 151 | 165 | 178 | 192 | 205 | 219 |
| 39 | 73 | 90 | 106 | 121 | 136 | 147 | 160 | 174 | 187 | 200 | 213 |
| 40 | 71 | 87 | 103 | 118 | 132 | 143 | 156 | 169 | 182 | 195 | 208 |
| 41 | 69 | 85 | 101 | 115 | 129 | 140 | 153 | 165 | 178 | 190 | 203 |
| 42 | 68 | 83 | 98 | 113 | 126 | 137 | 149 | 161 | 173 | 186 | 198 |
| 43 | 66 | 81 | 96 | 110 | 123 | 133 | 146 | 157 | 169 | 181 | 193 |
| 44 | 65 | 79 | 94 | 107 | 120 | 130 | 142 | 154 | 165 | 177 | 189 |
| 45 | 63 | 78 | 92 | 105 | 118 | 127 | 139 | 150 | 162 | 173 | 185 |
| 46 | 62 | 76 | 90 | 103 | 115 | 125 | 136 | 147 | 158 | 169 | 181 |
| 47 | 61 | 74 | 88 | 101 | 113 | 122 | 133 | 144 | 155 | 166 | 177 |
| 48 | 59 | 73 | 86 | 98 | 110 | 120 | 130 | 141 | 152 | 162 | 173 |
| 49 | 58 | 71 | 84 | 96 | 108 | 117 | 128 | 138 | 149 | 158 | 170 |
| 50 | 57 | 70 | 83 | 95 | 106 | 115 | 125 | 135 | 146 | 156 | 166 |
| 51 | 56 | 69 | 81 | 93 | 104 | 112 | 123 | 133 | 143 | 153 | 163 |
| 52 | 55 | 67 | 79 | 91 | 102 | 110 | 120 | 130 | 140 | 150 | 160 |
| 53 | 54 | 66 | 78 | 89 | 100 | 108 | 118 | 128 | 137 | 147 | 157 |
| 54 | 53 | 65 | 76 | 88 | 98 | 106 | 116 | 125 | 135 | 144 | 154 |
| 55 | 52 | 64 | 75 | 86 | 96 | 104 | 114 | 123 | 132 | 142 | 151 |
| 56 | 51 | 62 | 74 | 84 | 95 | 102 | 112 | 121 | 130 | 139 | 148 |
| 57 | 50 | 61 | 72 | 83 | 93 | 101 | 110 | 119 | 128 | 137 | 146 |
| 58 | 49 | 60 | 71 | 82 | 91 | 99 | 108 | 117 | 125 | 134 | 143 |
| 59 | 48 | 59 | 70 | 80 | 90 | 97 | 106 | 115 | 123 | 132 | 141 |
| Weight per Foot in Pounds. | 98.0 | 113.6 | 128.8 | 143.2 | 157.6 | 184.8 | 196.7 | 208.6 | 220.5 | 232.4 | 244.3 |

SAFE UNIFORMLY DISTRIBUTED LOADS FOR PLATE GIRDERS IN THOUSANDS OF POUNDS.

The safe loads below include the weight of the girder and are calculated for a fibre stress of 15,000 pounds per square inch on the net section. The net section is obtained by deducting holes figured at $\frac{7}{8}$ of an inch in diameter (for $\frac{3}{4}$ " rivets) from both flanges.

Web Plate $36" \times \frac{3}{8}"$

Flange Angles $6" \times 6"$



Web Plate $36" \times \frac{3}{8}"$

Flange Angles $6" \times 6" \times \frac{3}{4}"$

Flange Plates $14"$

| Distance Center to Center of Bearings in Feet. | Thickness of Flange Angles in Inches. | | | | Thickness of Flange Plate in Inches. | | | | |
|---|--|---------------|---------------|---------------|---|---------------|---------------|---------------|-------|
| | $\frac{3}{8}$ | $\frac{1}{2}$ | $\frac{5}{8}$ | $\frac{3}{4}$ | $\frac{1}{2}$ | $\frac{5}{8}$ | $\frac{3}{4}$ | $\frac{7}{8}$ | 1 |
| 30 | 108 | 134 | 159 | 183 | 238 | 255 | | | |
| 31 | 104 | 130 | 154 | 177 | 230 | 247 | 264 | | |
| 32 | 101 | 125 | 149 | 171 | 223 | 239 | 256 | | |
| 33 | 98 | 122 | 144 | 166 | 216 | 232 | 248 | 264 | |
| 34 | 95 | 118 | 140 | 161 | 210 | 225 | 241 | 256 | |
| 35 | 92 | 115 | 136 | 157 | 204 | 219 | 234 | 249 | 264 |
| 36 | 90 | 112 | 132 | 152 | 198 | 213 | 227 | 242 | 257 |
| 37 | 87 | 109 | 129 | 148 | 193 | 207 | 221 | 235 | 250 |
| 38 | 85 | 106 | 125 | 144 | 188 | 201 | 215 | 229 | 243 |
| 39 | 83 | 103 | 122 | 141 | 183 | 196 | 210 | 223 | 237 |
| 40 | 81 | 100 | 119 | 137 | 178 | 191 | 205 | 218 | 231 |
| 41 | 79 | 98 | 116 | 134 | 174 | 187 | 200 | 213 | 225 |
| 42 | 77 | 96 | 113 | 131 | 170 | 182 | 195 | 207 | 220 |
| 43 | 75 | 93 | 111 | 128 | 166 | 178 | 190 | 203 | 215 |
| 44 | 74 | 91 | 108 | 125 | 162 | 174 | 186 | 198 | 210 |
| 45 | 72 | 89 | 106 | 122 | 158 | 170 | 182 | 194 | 205 |
| 46 | 70 | 87 | 104 | 119 | 155 | 166 | 178 | 189 | 201 |
| 47 | 69 | 85 | 101 | 117 | 152 | 163 | 174 | 185 | 197 |
| 48 | 67 | 84 | 99 | 114 | 149 | 160 | 171 | 182 | 193 |
| 49 | 66 | 82 | 97 | 112 | 146 | 156 | 167 | 178 | 189 |
| 50 | 65 | 80 | 95 | 110 | 143 | 153 | 164 | 174 | 185 |
| 51 | 63 | 79 | 93 | 108 | 140 | 150 | 160 | 171 | 181 |
| 52 | 62 | 77 | 92 | 106 | 137 | 147 | 157 | 168 | 178 |
| 53 | 61 | 76 | 90 | 104 | 135 | 144 | 154 | 164 | 174 |
| 54 | 60 | 74 | 88 | 102 | 132 | 142 | 152 | 161 | 171 |
| 55 | 59 | 73 | 87 | 100 | 130 | 139 | 149 | 158 | 168 |
| 56 | 58 | 72 | 85 | 98 | 127 | 137 | 146 | 156 | 165 |
| 57 | 57 | 70 | 84 | 96 | 125 | 134 | 144 | 153 | 162 |
| 58 | 56 | 69 | 82 | 95 | 123 | 132 | 141 | 150 | 159 |
| 59 | 55 | 68 | 81 | 93 | 121 | 130 | 139 | 148 | 157 |
| Weight per Foot in Pounds. | 107.5 | 126.3 | 144.7 | 162.7 | 214.1 | 226 | 237.9 | 249.8 | 261.7 |

NOTE.—When Flange plates are thicker than $\frac{3}{4}"$, use two plates.

SAFE UNIFORMLY DISTRIBUTED LOADS FOR PLATE GIRDERS IN THOUSANDS OF POUNDS.

The safe loads below include the weight of the girder and are calculated for a fibre stress of 15 000 pounds per square inch on the net section. The net section is obtained by deducting holes figured at one inch in diameter (for $\frac{1}{8}$ " rivets) from both flanges.

Web Plate $42" \times \frac{3}{8}"$

Flange Angles $6" \times 4"$



Web Plate $42" \times \frac{3}{8}"$

Flange Angles $6" \times 4" \times \frac{3}{4}"$

Flange Plates $14"$

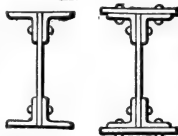
| Distance Center to Center of Bearings in Feet. | Thickness of Flange Angles in Inches. | | | | | Thickness of Flange Plate in Inches. | | | | | |
|---|--|---------------|---------------|---------------|---------------|---|---------------|---------------|---------------|---------------|-------|
| | $\frac{3}{8}$ | $\frac{1}{2}$ | $\frac{5}{8}$ | $\frac{3}{4}$ | $\frac{7}{8}$ | $\frac{3}{8}$ | $\frac{1}{2}$ | $\frac{5}{8}$ | $\frac{3}{4}$ | $\frac{7}{8}$ | 1 |
| 35 | 100 | 122 | 143 | 164 | 183 | 198 | 215 | 232 | 249 | 267 | 284 |
| 36 | 97 | 119 | 139 | 159 | 178 | 192 | 209 | 226 | 242 | 259 | 276 |
| 37 | 95 | 116 | 136 | 155 | 173 | 187 | 203 | 220 | 236 | 252 | 269 |
| 38 | 92 | 113 | 132 | 151 | 169 | 182 | 198 | 214 | 230 | 246 | 261 |
| 39 | 90 | 110 | 129 | 147 | 165 | 178 | 193 | 208 | 224 | 239 | 255 |
| 40 | 87 | 107 | 125 | 143 | 160 | 173 | 188 | 203 | 218 | 233 | 248 |
| 41 | 86 | 104 | 122 | 140 | 157 | 169 | 184 | 198 | 213 | 228 | 242 |
| 42 | 83 | 102 | 119 | 137 | 153 | 165 | 179 | 193 | 208 | 222 | 237 |
| 43 | 81 | 99 | 117 | 133 | 149 | 161 | 175 | 189 | 203 | 217 | 231 |
| 44 | 79 | 97 | 114 | 130 | 146 | 157 | 171 | 185 | 198 | 212 | 226 |
| 45 | 78 | 95 | 111 | 127 | 143 | 154 | 167 | 181 | 194 | 207 | 221 |
| 46 | 76 | 93 | 109 | 125 | 140 | 151 | 164 | 177 | 190 | 203 | 216 |
| 47 | 74 | 91 | 107 | 122 | 137 | 147 | 160 | 173 | 186 | 199 | 211 |
| 48 | 73 | 89 | 105 | 120 | 134 | 144 | 157 | 169 | 182 | 194 | 207 |
| 49 | 71 | 87 | 102 | 117 | 131 | 141 | 154 | 166 | 178 | 191 | 203 |
| 50 | 70 | 86 | 100 | 115 | 128 | 139 | 151 | 163 | 175 | 187 | 199 |
| 51 | 69 | 84 | 98 | 112 | 126 | 136 | 148 | 159 | 171 | 183 | 195 |
| 52 | 67 | 82 | 96 | 110 | 123 | 133 | 145 | 156 | 168 | 180 | 191 |
| 53 | 66 | 81 | 95 | 108 | 121 | 131 | 142 | 153 | 165 | 176 | 187 |
| 54 | 65 | 79 | 93 | 106 | 119 | 128 | 139 | 150 | 162 | 173 | 184 |
| 55 | 64 | 78 | 91 | 104 | 117 | 126 | 137 | 148 | 159 | 170 | 181 |
| 56 | 62 | 76 | 90 | 102 | 115 | 124 | 134 | 145 | 156 | 167 | 177 |
| 57 | 61 | 75 | 88 | 101 | 113 | 121 | 132 | 143 | 153 | 164 | 174 |
| 58 | 60 | 74 | 86 | 99 | 111 | 119 | 130 | 140 | 150 | 161 | 171 |
| 59 | 59 | 73 | 85 | 97 | 109 | 117 | 128 | 138 | 148 | 158 | 168 |
| 60 | 58 | 71 | 84 | 96 | 107 | 115 | 125 | 135 | 145 | 156 | 166 |
| 61 | 57 | 70 | 82 | 94 | 105 | 114 | 123 | 133 | 143 | 153 | 163 |
| 62 | 56 | 69 | 81 | 92 | 103 | 112 | 121 | 131 | 141 | 151 | 160 |
| 63 | 55 | 68 | 80 | 91 | 102 | 110 | 119 | 129 | 138 | 148 | 158 |
| 64 | 55 | 67 | 78 | 90 | 100 | 108 | 118 | 127 | 136 | 146 | 155 |
| Weight per Foot in Pounds. | 105.7 | 121.3 | 136.5 | 150.9 | 165.3 | 192.5 | 204.4 | 216.3 | 228.2 | 240.1 | 252.0 |

SAFE UNIFORMLY DISTRIBUTED LOADS FOR PLATE GIRDERS IN THOUSANDS OF POUNDS.

The safe loads below include the weight of the girder and are calculated for a fibre stress of 15 000 pounds per square inch on the net section. The net section is obtained by deducting holes figured at one inch in diameter (for $\frac{3}{8}$ " rivets) from both flanges.

Web Plate $42" \times \frac{3}{8}"$

Flange Angles $6" \times 6"$



Web Plate $42" \times \frac{3}{8}"$

Flange Angles $6" \times 6" \times \frac{3}{4}"$

Flange Plates $14"$

| Distance Center to Center of Bearings in Feet. | Thickness of Flange Angles in Inches. | | | Thickness of Flange Plate in Inches. | | | | | |
|---|---|---------------|---------------|---|---------------|---------------|---------------|-------|----------------|
| | $\frac{1}{2}$ | $\frac{5}{8}$ | $\frac{3}{4}$ | $\frac{1}{2}$ | $\frac{5}{8}$ | $\frac{3}{4}$ | $\frac{7}{8}$ | 1 | $1\frac{1}{4}$ |
| 35 | 139 | 164 | 189 | 240 | 257 | 275 | 292 | 309 | |
| 36 | 135 | 160 | 184 | 234 | 250 | 267 | 284 | 301 | |
| 37 | 131 | 155 | 179 | 227 | 244 | 260 | 276 | 293 | |
| 38 | 128 | 151 | 174 | 221 | 237 | 253 | 269 | 285 | |
| 39 | 125 | 148 | 169 | 216 | 231 | 247 | 260 | 278 | 309 |
| 40 | 122 | 144 | 165 | 210 | 225 | 240 | 256 | 271 | 301 |
| 41 | 119 | 140 | 161 | 205 | 220 | 235 | 249 | 264 | 294 |
| 42 | 116 | 137 | 157 | 200 | 215 | 229 | 243 | 258 | 287 |
| 43 | 113 | 134 | 154 | 195 | 210 | 224 | 238 | 252 | 280 |
| 44 | 111 | 131 | 150 | 191 | 205 | 219 | 232 | 246 | 274 |
| 45 | 108 | 128 | 147 | 187 | 200 | 214 | 227 | 241 | 268 |
| 46 | 106 | 125 | 144 | 183 | 196 | 209 | 222 | 235 | 262 |
| 47 | 103 | 122 | 141 | 179 | 192 | 205 | 217 | 230 | 256 |
| 48 | 101 | 120 | 138 | 175 | 188 | 200 | 213 | 226 | 251 |
| 49 | 99 | 117 | 135 | 172 | 184 | 196 | 209 | 221 | 246 |
| 50 | 97 | 115 | 132 | 168 | 180 | 192 | 204 | 217 | 241 |
| 51 | 95 | 113 | 130 | 165 | 177 | 189 | 200 | 212 | 236 |
| 52 | 94 | 111 | 127 | 162 | 173 | 185 | 197 | 208 | 232 |
| 53 | 92 | 109 | 125 | 159 | 170 | 181 | 193 | 204 | 227 |
| 54 | 90 | 107 | 122 | 156 | 167 | 178 | 189 | 201 | 223 |
| 55 | 88 | 105 | 120 | 153 | 164 | 175 | 186 | 197 | 219 |
| 56 | 87 | 103 | 118 | 150 | 161 | 172 | 183 | 193 | 215 |
| 57 | 85 | 101 | 116 | 147 | 158 | 169 | 179 | 190 | 211 |
| 58 | 84 | 99 | 114 | 145 | 155 | 166 | 176 | 187 | 208 |
| 59 | 82 | 98 | 112 | 142 | 153 | 163 | 173 | 184 | 204 |
| 60 | 81 | 96 | 110 | 140 | 150 | 160 | 170 | 180 | 201 |
| 61 | 80 | 94 | 108 | 138 | 148 | 158 | 168 | 178 | 197 |
| 62 | 78 | 93 | 107 | 136 | 145 | 155 | 165 | 175 | 194 |
| 63 | 77 | 91 | 105 | 133 | 143 | 153 | 162 | 172 | 191 |
| 64 | 76 | 90 | 103 | 131 | 141 | 150 | 160 | 169 | 188 |
| Weight per Foot in Pounds. | 134.9 | 153.3 | 171.3 | 224.7 | 236.6 | 248.5 | 260.4 | 272.3 | 296.1 |

NOTE.—When Flange plates are thicker than $\frac{3}{4}"$, use two plates.

SAFE UNIFORMLY DISTRIBUTED LOADS FOR PLATE GIRDERS IN THOUSANDS OF POUNDS.

The safe loads below include the weight of the girder and are calculated for a fibre stress of 15 000 pounds per square inch on the net section. The net section is obtained by deducting holes figured at one inch in diameter (for $\frac{3}{8}$ " rivets) from both flanges.

Web Plate $48" \times \frac{3}{8}"$

Flange Angles $6" \times 4"$



Web Plate $48" \times \frac{3}{8}"$

Flange Angles $6" \times 4" \times \frac{3}{4}"$

Flange Plates $14"$

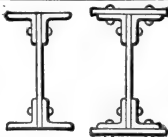
| Distance Center to Center of Bearings in Feet. | Thickness of Flange Angles in Inches. | | | | | Thickness of Flange Plate in Inches. | | | | | | |
|---|--|---------------|---------------|---------------|---------------|---|---------------|---------------|---------------|---------------|-------|--|
| | $\frac{3}{8}$ | $\frac{1}{2}$ | $\frac{5}{8}$ | $\frac{3}{4}$ | $\frac{7}{8}$ | $\frac{3}{8}$ | $\frac{1}{2}$ | $\frac{5}{8}$ | $\frac{3}{4}$ | $\frac{7}{8}$ | 1 | |
| 35 | 120 | 146 | 170 | 194 | 217 | 233 | 253 | 273 | 293 | 312 | 332 | |
| 36 | 117 | 142 | 165 | 189 | 211 | 227 | 246 | 265 | 284 | 303 | 322 | |
| 37 | 113 | 138 | 161 | 183 | 205 | 220 | 239 | 258 | 276 | 295 | 314 | |
| 38 | 110 | 134 | 157 | 179 | 199 | 215 | 233 | 251 | 269 | 287 | 305 | |
| 39 | 108 | 131 | 153 | 174 | 194 | 209 | 227 | 245 | 262 | 280 | 298 | |
| 40 | 105 | 127 | 149 | 170 | 189 | 204 | 221 | 238 | 256 | 273 | 290 | |
| 41 | 102 | 124 | 145 | 166 | 185 | 199 | 216 | 233 | 249 | 266 | 283 | |
| 42 | 100 | 121 | 142 | 162 | 180 | 194 | 211 | 227 | 243 | 260 | 276 | |
| 43 | 98 | 119 | 139 | 158 | 176 | 190 | 206 | 222 | 238 | 254 | 270 | |
| 44 | 95 | 116 | 135 | 154 | 172 | 185 | 201 | 217 | 232 | 248 | 264 | |
| 45 | 93 | 113 | 132 | 151 | 168 | 181 | 197 | 212 | 227 | 243 | 258 | |
| 46 | 91 | 111 | 130 | 148 | 165 | 177 | 192 | 207 | 222 | 237 | 252 | |
| 47 | 89 | 108 | 127 | 144 | 161 | 174 | 188 | 203 | 218 | 232 | 247 | |
| 48 | 87 | 106 | 124 | 141 | 158 | 170 | 184 | 199 | 213 | 227 | 242 | |
| 49 | 86 | 104 | 122 | 138 | 156 | 166 | 181 | 195 | 209 | 223 | 237 | |
| 50 | 84 | 102 | 119 | 136 | 152 | 163 | 177 | 191 | 205 | 218 | 232 | |
| 51 | 82 | 100 | 117 | 133 | 149 | 160 | 174 | 187 | 201 | 214 | 228 | |
| 52 | 81 | 98 | 115 | 131 | 146 | 157 | 170 | 183 | 197 | 210 | 223 | |
| 53 | 79 | 96 | 112 | 128 | 143 | 154 | 167 | 180 | 193 | 206 | 219 | |
| 54 | 78 | 94 | 110 | 126 | 140 | 151 | 164 | 177 | 189 | 202 | 215 | |
| 55 | 76 | 93 | 108 | 123 | 138 | 148 | 161 | 173 | 186 | 198 | 211 | |
| 56 | 75 | 91 | 106 | 121 | 135 | 146 | 158 | 170 | 182 | 195 | 207 | |
| 57 | 74 | 89 | 104 | 119 | 133 | 143 | 155 | 167 | 179 | 192 | 204 | |
| 58 | 72 | 88 | 103 | 117 | 131 | 141 | 153 | 164 | 176 | 188 | 200 | |
| 59 | 71 | 86 | 101 | 115 | 128 | 138 | 150 | 162 | 173 | 185 | 197 | |
| 60 | 70 | 85 | 99 | 113 | 126 | 136 | 147 | 159 | 170 | 182 | 193 | |
| 61 | 69 | 84 | 98 | 111 | 124 | 134 | 145 | 156 | 168 | 179 | 190 | |
| 62 | 68 | 82 | 96 | 109 | 122 | 132 | 143 | 154 | 165 | 176 | 187 | |
| 63 | 67 | 81 | 95 | 108 | 120 | 129 | 140 | 151 | 162 | 173 | 184 | |
| 64 | 66 | 80 | 93 | 106 | 118 | 127 | 138 | 149 | 160 | 171 | 181 | |
| Weight per Foot in Pounds. | 113.3 | 128.9 | 144.1 | 158.5 | 172.9 | 200.1 | 212.0 | 223.9 | 235.8 | 247.7 | 259.6 | |

SAFE UNIFORMLY DISTRIBUTED LOADS FOR PLATE GIRDERS IN THOUSANDS OF POUNDS.

The safe loads below include the weight of the girder and are calculated for a fibre stress of 15 000 pounds per square inch on the net section. The net section is obtained by deducting holes figured at one inch in diameter (for $\frac{1}{8}$ " rivets) from both flanges.

Web Plate 48" $\times \frac{3}{8}$ "

Flange Angles 6" $\times 6$ " $\times \frac{3}{4}$ "



Web Plate 48" $\times \frac{3}{8}$ "

Flange Angles 6" $\times 6$ " $\times \frac{3}{4}$ "

Flange Plates 14"

| Distance Center to Center of Bearings in Feet. | Thickness of Flange Angles in Inches. | | | Thickness of Flange Plate in Inches. | | | | | |
|---|---|---------------|---------------|---|---------------|---------------|---------------|-------|-----------------|
| | $\frac{1}{2}$ | $\frac{5}{8}$ | $\frac{3}{4}$ | $\frac{1}{2}$ | $\frac{5}{8}$ | $\frac{3}{4}$ | $\frac{7}{8}$ | 1 | 1 $\frac{1}{4}$ |
| 35 | 166 | 195 | 224 | 283 | 303 | 322 | 342 | 362 | |
| 36 | 161 | 190 | 218 | 275 | 294 | 313 | 333 | 352 | |
| 37 | 157 | 185 | 212 | 267 | 286 | 305 | 324 | 342 | |
| 38 | 153 | 180 | 206 | 260 | 279 | 297 | 315 | 333 | |
| 39 | 149 | 175 | 201 | 254 | 272 | 289 | 307 | 325 | 361 |
| 40 | 145 | 171 | 196 | 247 | 265 | 282 | 299 | 317 | 352 |
| 41 | 141 | 167 | 191 | 241 | 258 | 275 | 292 | 309 | 343 |
| 42 | 138 | 163 | 187 | 236 | 252 | 269 | 285 | 302 | 335 |
| 43 | 135 | 159 | 182 | 230 | 246 | 263 | 279 | 295 | 327 |
| 44 | 132 | 155 | 178 | 225 | 241 | 256 | 272 | 288 | 320 |
| 45 | 129 | 152 | 174 | 220 | 235 | 251 | 266 | 282 | 312 |
| 46 | 126 | 149 | 170 | 215 | 230 | 245 | 260 | 275 | 306 |
| 47 | 123 | 145 | 167 | 211 | 225 | 240 | 255 | 270 | 299 |
| 48 | 121 | 142 | 163 | 206 | 221 | 235 | 249 | 264 | 293 |
| 49 | 118 | 140 | 160 | 202 | 216 | 230 | 244 | 259 | 287 |
| 50 | 116 | 137 | 157 | 198 | 212 | 226 | 240 | 253 | 281 |
| 51 | 114 | 134 | 154 | 194 | 208 | 221 | 235 | 248 | 276 |
| 52 | 112 | 131 | 151 | 190 | 204 | 217 | 230 | 244 | 270 |
| 53 | 109 | 129 | 148 | 187 | 200 | 213 | 226 | 239 | 265 |
| 54 | 107 | 127 | 145 | 183 | 196 | 209 | 222 | 235 | 260 |
| 55 | 105 | 124 | 142 | 180 | 193 | 205 | 218 | 230 | 256 |
| 56 | 104 | 122 | 140 | 177 | 189 | 201 | 214 | 226 | 251 |
| 57 | 102 | 120 | 137 | 174 | 186 | 198 | 210 | 222 | 247 |
| 58 | 100 | 118 | 135 | 171 | 183 | 195 | 206 | 218 | 242 |
| 59 | 98 | 116 | 133 | 168 | 179 | 191 | 203 | 215 | 238 |
| 60 | 97 | 114 | 131 | 165 | 176 | 188 | 200 | 211 | 234 |
| 61 | 95 | 112 | 128 | 162 | 174 | 185 | 196 | 208 | 231 |
| 62 | 94 | 110 | 126 | 160 | 171 | 182 | 193 | 204 | 227 |
| 63 | 92 | 109 | 124 | 157 | 168 | 179 | 190 | 201 | 223 |
| 64 | 91 | 107 | 122 | 155 | 165 | 176 | 187 | 198 | 220 |
| Weight per Foot in Pounds. | 142.5 | 160.9 | 173.9 | 232.3 | 244.2 | 256.2 | 268 | 279.9 | 303.7 |

SAFE UNIFORMLY DISTRIBUTED LOADS FOR PLATE GIRDERS IN THOUSANDS OF POUNDS.

The safe loads below include the weight of the girder and are calculated for a fibre stress of 15000 pounds per square inch on the net section. The net section is obtained by deducting holes figured at one inch in diameter (for $\frac{1}{8}$ " rivets) from both flanges.

Web Plate $60" \times \frac{3}{8}"$

Flange Angles $6" \times 4"$



Web Plate $60" \times \frac{3}{8}"$

Flange Angles $6" \times 4" \times \frac{3}{4}"$

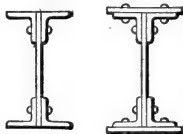
Flange Plates $14"$

| Distance Center to Center of Bearings in Feet. | Thickness of Flange Angles in Inches. | | | | | Thickness of Flange Plate in Inches. | | | | | |
|---|--|---------------|---------------|---------------|---------------|---|---------------|---------------|---------------|---------------|-------|
| | $\frac{3}{8}$ | $\frac{1}{2}$ | $\frac{5}{8}$ | $\frac{3}{4}$ | $\frac{7}{8}$ | $\frac{3}{8}$ | $\frac{1}{2}$ | $\frac{5}{8}$ | $\frac{3}{4}$ | $\frac{7}{8}$ | 1 |
| 40 | 143 | 172 | 199 | 226 | 251 | 269 | 291 | 312 | 334 | 356 | 377 |
| 41 | 140 | 168 | 195 | 220 | 245 | 262 | 284 | 305 | 326 | 347 | 368 |
| 42 | 137 | 164 | 190 | 215 | 239 | 256 | 277 | 297 | 318 | 339 | 359 |
| 43 | 133 | 161 | 186 | 210 | 234 | 250 | 270 | 290 | 311 | 331 | 351 |
| 44 | 130 | 156 | 181 | 205 | 228 | 244 | 264 | 284 | 304 | 323 | 343 |
| 45 | 127 | 153 | 177 | 201 | 223 | 239 | 258 | 277 | 297 | 316 | 335 |
| 46 | 125 | 149 | 173 | 196 | 218 | 234 | 253 | 271 | 290 | 309 | 328 |
| 47 | 122 | 146 | 170 | 192 | 214 | 229 | 247 | 266 | 284 | 303 | 321 |
| 48 | 120 | 143 | 166 | 188 | 209 | 224 | 242 | 260 | 278 | 296 | 314 |
| 49 | 117 | 140 | 163 | 184 | 205 | 220 | 237 | 255 | 273 | 290 | 308 |
| 50 | 115 | 138 | 160 | 181 | 201 | 215 | 233 | 250 | 267 | 285 | 302 |
| 51 | 112 | 135 | 156 | 177 | 197 | 211 | 228 | 245 | 262 | 279 | 296 |
| 52 | 110 | 132 | 153 | 174 | 193 | 207 | 224 | 240 | 257 | 274 | 290 |
| 53 | 108 | 130 | 150 | 171 | 190 | 203 | 219 | 236 | 252 | 268 | 285 |
| 54 | 106 | 127 | 148 | 167 | 186 | 200 | 215 | 231 | 247 | 263 | 280 |
| 55 | 104 | 125 | 145 | 164 | 183 | 196 | 211 | 227 | 243 | 259 | 274 |
| 56 | 102 | 123 | 142 | 161 | 179 | 192 | 208 | 223 | 238 | 254 | 270 |
| 57 | 101 | 121 | 140 | 159 | 176 | 189 | 204 | 219 | 234 | 250 | 265 |
| 58 | 99 | 119 | 138 | 156 | 173 | 185 | 200 | 215 | 230 | 245 | 260 |
| 59 | 97 | 117 | 135 | 153 | 170 | 182 | 197 | 212 | 226 | 241 | 256 |
| 60 | 96 | 115 | 133 | 151 | 167 | 179 | 194 | 208 | 223 | 237 | 252 |
| 61 | 94 | 113 | 131 | 148 | 165 | 176 | 191 | 205 | 219 | 233 | 247 |
| 62 | 92 | 111 | 129 | 146 | 162 | 173 | 187 | 201 | 215 | 229 | 243 |
| 63 | 91 | 109 | 127 | 143 | 159 | 171 | 185 | 198 | 212 | 226 | 240 |
| 64 | 90 | 107 | 125 | 141 | 157 | 168 | 182 | 195 | 209 | 222 | 236 |
| 65 | 88 | 106 | 123 | 139 | 155 | 165 | 179 | 191 | 205 | 220 | 232 |
| 66 | 87 | 104 | 121 | 137 | 152 | 163 | 176 | 189 | 202 | 216 | 229 |
| 67 | 86 | 103 | 119 | 135 | 150 | 160 | 173 | 186 | 199 | 213 | 225 |
| 68 | 84 | 101 | 117 | 133 | 148 | 158 | 171 | 184 | 196 | 210 | 222 |
| 69 | 83 | 100 | 116 | 131 | 146 | 156 | 168 | 181 | 194 | 207 | 219 |
| 70 | 82 | 98 | 114 | 129 | 143 | 154 | 166 | 178 | 191 | 204 | 216 |
| Weight per Foot in Pounds. | 128.6 | 144.2 | 159.4 | 173.8 | 188.2 | 215.4 | 227.3 | 239.2 | 251.1 | 263.0 | 274.9 |

SAFE UNIFORMLY DISTRIBUTED LOADS FOR PLATE GIRDERS IN THOUSANDS OF POUNDS.

The safe loads below include the weight of the girder and are calculated for a fibre stress of 15 000 pounds per square inch on the net section. The net section is obtained by deducting holes figured at one inch in diameter (for $\frac{7}{8}$ " rivets) from both flanges.

Web Plate 60" $\times \frac{3}{8}$ "
Flange Angles 6" $\times 6$ "



Web Plate 60" $\times \frac{3}{8}$ "
Flange Angles 6" $\times 6$ " $\times \frac{3}{4}$ "
Flange Plates 14"

| Distance Center to Center of Bearings in Feet. | Thickness of Flange Angles in Inches. | | | | | Thickness of Flange Plate in Inches. | | | | | |
|---|--|---------------|---------------|---------------|---------------|---|---------------|---------------|---------------|-------|-----------------|
| | $\frac{3}{8}$ | $\frac{1}{2}$ | $\frac{5}{8}$ | $\frac{3}{4}$ | $\frac{7}{8}$ | $\frac{1}{2}$ | $\frac{5}{8}$ | $\frac{3}{4}$ | $\frac{7}{8}$ | 1 | 1 $\frac{1}{4}$ |
| 40 | 160 | 194 | 227 | 259 | 290 | 323 | 345 | 366 | 388 | 410 | 453 |
| 41 | 157 | 190 | 222 | 253 | 283 | 316 | 336 | 357 | 379 | 400 | 442 |
| 42 | 153 | 185 | 217 | 247 | 276 | 308 | 328 | 349 | 370 | 390 | 431 |
| 43 | 149 | 181 | 212 | 241 | 270 | 301 | 321 | 341 | 361 | 381 | 421 |
| 44 | 146 | 177 | 207 | 236 | 264 | 294 | 314 | 333 | 353 | 372 | 412 |
| 45 | 143 | 173 | 202 | 230 | 258 | 287 | 307 | 326 | 345 | 364 | 403 |
| 46 | 140 | 169 | 198 | 225 | 252 | 281 | 300 | 319 | 338 | 356 | 394 |
| 47 | 137 | 165 | 194 | 221 | 247 | 275 | 294 | 312 | 330 | 349 | 385 |
| 48 | 134 | 162 | 190 | 216 | 242 | 269 | 287 | 305 | 323 | 341 | 377 |
| 49 | 131 | 159 | 186 | 212 | 237 | 264 | 282 | 299 | 317 | 334 | 370 |
| 50 | 128 | 156 | 182 | 207 | 232 | 259 | 276 | 293 | 311 | 328 | 362 |
| 51 | 126 | 152 | 178 | 203 | 227 | 254 | 270 | 287 | 304 | 321 | 355 |
| 52 | 123 | 150 | 175 | 199 | 223 | 249 | 265 | 282 | 298 | 315 | 348 |
| 53 | 121 | 147 | 172 | 196 | 219 | 244 | 260 | 277 | 293 | 309 | 342 |
| 54 | 119 | 144 | 168 | 192 | 215 | 240 | 255 | 271 | 287 | 303 | 335 |
| 55 | 117 | 141 | 165 | 188 | 211 | 235 | 251 | 266 | 282 | 298 | 329 |
| 56 | 115 | 139 | 162 | 185 | 207 | 231 | 246 | 262 | 277 | 293 | 323 |
| 57 | 113 | 136 | 160 | 182 | 203 | 227 | 242 | 257 | 272 | 287 | 318 |
| 58 | 111 | 134 | 157 | 179 | 200 | 223 | 238 | 253 | 268 | 282 | 312 |
| 59 | 109 | 132 | 154 | 176 | 197 | 219 | 234 | 248 | 263 | 278 | 307 |
| 60 | 107 | 130 | 152 | 173 | 193 | 216 | 230 | 244 | 259 | 273 | 302 |
| 61 | 105 | 127 | 149 | 170 | 190 | 212 | 226 | 240 | 254 | 269 | 297 |
| 62 | 103 | 125 | 147 | 167 | 187 | 209 | 222 | 236 | 250 | 264 | 292 |
| 63 | 102 | 123 | 144 | 165 | 184 | 205 | 219 | 232 | 246 | 260 | 288 |
| 64 | 100 | 121 | 142 | 162 | 181 | 202 | 216 | 229 | 243 | 256 | 283 |
| 65 | 99 | 120 | 140 | 159 | 178 | 199 | 212 | 225 | 239 | 252 | 279 |
| 66 | 97 | 118 | 138 | 157 | 176 | 196 | 209 | 222 | 235 | 248 | 274 |
| 67 | 96 | 116 | 136 | 155 | 173 | 193 | 206 | 219 | 232 | 245 | 270 |
| 68 | 94 | 114 | 134 | 152 | 171 | 190 | 203 | 215 | 228 | 241 | 267 |
| 69 | 93 | 113 | 132 | 150 | 168 | 187 | 200 | 212 | 225 | 237 | 263 |
| 70 | 92 | 111 | 130 | 148 | 166 | 185 | 197 | 209 | 222 | 234 | 259 |
| Weight per Foot in Pounds. | 139.0 | 157.8 | 176.2 | 194.2 | 211.8 | 247.7 | 259.6 | 271.5 | 283.4 | 295.3 | 319.1 |

GRILLAGE BEAMS FOR FOUNDATIONS.

In designing foundations for walls or columns carrying heavy loads resting upon the soil, it is necessary to distribute the weight over a suitable area, and this is readily accomplished, in a small depth, by using a grillage composed of steel beams imbedded in concrete, thus obviating the necessity of large masses of masonry and deep excavations. For heavy loads on soil of small bearing power three tiers of beams may be necessary, while for lighter loads and soil of greater bearing power two tiers of beams will ordinarily suffice.

The grillage beams which are to be surrounded by concrete should be spaced not less than 3" apart in the clear between the flanges, so that the concrete may be thoroughly rammed between them, and gas-pipe, or standard cast-iron separators should be used to maintain the beams in proper position.

Knowing the total weight to be carried and the allowable intensity of loading per square foot of the supporting soil, the area of the footing required can be readily found, which, taken into consideration with any other conditions limiting the form or proportions of the footing, will determine the external dimensions of the foundation. The beams may be considered as subjected to a uniform load extending over a portion of their upper surfaces, the center of which is at the center of length of the beams, and as being uniformly supported from below throughout their length.

Under these circumstances, the maximum bending moment will occur at the center of the beam and, using the notation given for the upper tier in the sketch below, this bending moment for one beam will be as follows:

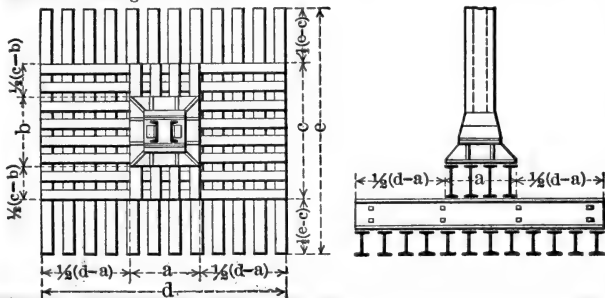
$$\text{Bending moment in inch pounds} = \frac{W}{8} (c - b)$$

in which c and b are expressed in inches and W is the total weight in pounds on one beam, obtained by dividing the total load by the number of beams composing the tier in question.

This formula for the bending moment is the same as that for a beam of the length $(c - b)$ supported at the ends and uniformly loaded with the total weight W , so that the proper sizes of beams, bending considered, may be obtained directly from the tables of safe loads uniformly distributed for Cambria I-Beams, on pages 106 to 117 inclusive, or for cases in which the lengths are shorter than those given in these tables, the sizes may be calculated from the coefficients of strength or the section moduli given in the tables of properties of I-Beams, pages 182 to 185 inclusive, taking care, however, to use as the length, the distance $(c - b)$, for the upper tier, and the corresponding figures for the other tiers.

After determining the size of beam required based upon bending, as stated above, an examination should also be made of the capacity of the beam web to resist buckling. This may be done by considering the web as a column of height equal to the clear distance between the fillets and calculating the safe load therefor by the use of the tables of strength for steel columns or struts, on pages 218 to 221, using the proper safety factor.

If the beam web is found insufficient as a column when calculated in this manner, a beam with a web of greater thickness should be tried until one is found that will meet this requirement and the conditions for bending; or it might be more economical, in some cases, to use the beam with the thinner web and provide it with sufficient separators, fitting between the beam flanges, or stiffeners secured to the web to assist it in resisting as a column.



EXTRACTS FROM THE BUILDING LAWS OF VARIOUS CITIES.

Live Loads for Floors in Different Classes of Buildings, Exclusive of the Weight of the Materials of Construction.

(Revised to 1917.)

Pounds per Square Foot.

| No. | City. | Dwell's, Apartments, Hotels, Tenements or Lodgings. | Office Buildings. | | Schools or Places of Instruction. | Buildings for Public Assembly. |
|-----|-------------------|---|-------------------|---------------|-----------------------------------|--------------------------------|
| | | | First Floor. | Upper Floors. | | |
| 1 | Atlanta..... | 60 | 150 | 75 | 75 | 90 |
| 2 | Baltimore..... | 60 | 150 | 75 | 75 | 75(a), 125 |
| 3 | Boston..... | 100(b) 50 | 100 | 100 | 125(c) 60 | 125 |
| 4 | Buffalo..... | 40(d) 70 | 70 | 70 | 100 | 100 |
| 5 | Chicago..... | 50(e) 40 | 50 | 50 | 75 | 100 |
| 6 | Cincinnati..... | 40 | 100 | 50 | 60 | 100 |
| 7 | Cleveland..... | 60(u) 80 | 125 | 80 | 80(a) 125 | 125(c) 100 |
| 8 | Denver..... | 40 50(h) | 70 | 70 | 50(a) | 80(a) 120(f) |
| 9 | Detroit..... | 80(f) 50 | 125 | 75 | 100(c) 75 | 80(a) 100 |
| 10 | Hartford..... | 50 | 100 | 100 | | 120 |
| 11 | Jersey City..... | 60 | 150 | 75 | 75 | 90 |
| 12 | Los Angeles..... | 125(t) 60 | 75 | 75 | | 125 |
| 13 | Louisville..... | 60 | 150 | 75 | 75 | 100 |
| 14 | Milwaukee..... | 30 | 80 | 40 | 40 60 | 80 50(a) |
| 15 | Minneapolis..... | 50 | 100 | 75 | 100 | 125 |
| 16 | Newark, N. J..... | 60 | 150 | 75 | 75 | 90 |
| 17 | New Haven..... | 100(g) 60 | | | 75 | 110 |
| 18 | New Orleans..... | 70(b) 40 | 70 | 70 | 125(c) 60 | 125 |
| 19 | New York..... | 40 | 60 | 60 | 75 | 100 |
| 20 | Philadelphia..... | 70 | 100 | 100 | | 120 |
| 21 | Pittsburgh..... | 50 70(h) | 70 | 70 | 70 | 125 |
| 22 | Portland, Ore.... | 80(f) 50 | 100 | 60 | 80(c) 60 | 80(a) 100 |
| 23 | Providence..... | 100(b) 50 | 150 | 75 | 125(c) 60 | 25 |
| 24 | Rochester..... | 60(h) 50 | 70 | 70 | 70 | 70 |
| 25 | St. Louis..... | 60 | 150 | 70 | 100 | 100 |
| 26 | St. Paul..... | 50 | 125 | 60 | 125(c) 60 | 125 |
| 27 | San Francisco.... | 60 | 60 | 60 | 125(c) 75(a) | 75(a) 125(c) |
| 28 | Seattle..... | 75(b) 40 | 125 | 50 | 100(c) 75 | 75(a) 100 |
| 29 | Syracuse..... | 60 | 100(g) 75 | 100(g) 75 | 90(c) 75 | 80(a) 100 |
| 30 | Washington..... | 75(g) 50 | 110(g) 75 | 110(g) 75 | 75 | 110 |
| 31 | Worcester, Mass.. | 60 | 125 | 75 | 75 | 125 |

(a) Where seats are fixed; (b) Public rooms exceeding 500 sq. ft. area; (c) Assembly rooms; (d) Occupied by less than 25 persons; (e) Sleeping accommodations for 20 or more persons; (f) First floor—Hotels, Tenements and Lodging Houses; (g) Rooms and spaces for public use or common use of tenants; (h) Tenement Houses and Hotels.

EXTRACTS FROM THE BUILDING LAWS OF VARIOUS CITIES.**Live Loads for Floors in Different Classes of Buildings, Exclusive of the Weight of the Materials of Construction.****(Revised to 1917.)****Pounds per Square Foot.**

| Stables or Carriage Houses. | Garages. | Ord. Stores, Light Manufacturing, Light Storage. | Stores (Heavy Materials,) Warehouses, Factories. | Roofs. | | Side-walks. | No. |
|-----------------------------|-----------------|--|--|------------------|------------------|-------------|-------|
| | | | | Slope <20°. | Slope >20°. | | |
| 75 | | 120 | 150 | 40(i) | 30(j) | 200 | 1 |
| 100 | | 125 | 250(k), 175 | 40(i) | 20(j)(l) | 200 | 2 |
| | | 125 | 250 | 40(m) | | | 3 |
| 40 (n) | | 120 | 150 | 40(j) | 40(j) | | 4 |
| { 40 (o) | { 40(o) | 100 | 100 | 25(j) | 25(j) | | 5 |
| { 100 | { 100 | 100 | 150 | 25(j) | 25(j) | 300 | 6 |
| 75 | | 100 | 200 | 35(m) | 30(i) | 200 | 7 |
| 80 | { 100 150(q) | { 125(q) 100 | | | | | |
| | | 150 | 150 | 40 | 20 | | 8 |
| { 60(p) | { 60(p) | { 125(q) 130(r), 100 | { 200(s) 175 | 40 | 40 | 250 | 9 |
| { 80 | { 80 | 125 | 125 | 50(i) | 50(i) | | 10 |
| 75 | | 120 | 150 | 50(i) | 30(j) | 300 | 11 |
| | | 150 | 150 | { 20(v)(u) 30 | { 20(v)(u) 30 | | 12 |
| 100 | 100 | | 150 | 40 | 30(j) | 300 | 13 |
| 80 | 80 | 100 | | 30 | 30 | 150 | 14 |
| 85 | 100 | 100 | | 30(i) | 30(i) | 300(j) | 15 |
| 75 | | 120 | 150 | 50(i) | 30(j) | 300 | 16 |
| | | 120 | 150 | 40(i) | 40(i) | | 17 |
| | | 125 | 200 | 30(m) | | 300 | 18 |
| 120 | 120 | 120 | 120 | 40 | 30(j) | 300 | 19 |
| | | 120 | 150 | 30 | 30 | | 20 |
| | | 125 | 200 | { 50(j) 40(m) | 50(j) | | 21 |
| 80 | | { 125(q) 100 | 200 | 40 | 40 | 300 | 22 |
| | | 125 | 250 | 40(m) | | | 23 |
| { 50(n) | { 50'(n) | 100 | 200 | 40(j) | 40(j) | | 24 |
| { 100 | { 100 | 150 | 150 | 40(m) | | | 25 |
| 85 | | 100 | 200 | 30(j) | 30(j) | 300 | 26 |
| 75 | | 125 | 250 | 30(i) | 20(j) | 150 | 27 |
| 75 | 125 | 125 | | 40(j) | 40(j) | | 28 |
| 80 | 125 | 125 | 200 | 40 | 40 | 250 | 29 |
| | | 110 | 150 | 25(i) | 25(i) | | 30 |
| 125 | 125-175 | 125 | 200 | 50(i) | 30(j) | 300 | 31 |

(i) Per square foot of surface; (j) Per square foot, measured horizontally; (k) Heavy storage; (l) Where used for public assembly or special purpose use same load as floors; (m) Flat; (n) Private; (o) Ground area less than 500 sq. ft.; (p) Small; (q) 1st floor; (r) Light storage and manufacturing; (s) Heavy Merchandise storage; (t) Hotel corridors; (u) Dwellings; (v) Sheds and outbuildings.

EXTRACTS FROM THE BUILDING LAWS OF VARIOUS CITIES.

ALLOWABLE UNIT STRESSES FOR STEEL AND IRON.

(Revised to 1917.)

Pounds per Square Inch.

| No. | City. | Tension. | | | |
|-----|----------------------|--------------------------|--------------------------|---------------|------------|
| | | Rolled Steel. | Cast Steel. | Wrought Iron. | Cast Iron. |
| 1 | Atlanta..... | 16 000 | 16 000 | 12 000 | 3 000 |
| 2 | Baltimore..... | 16 000 | 16 000 | 12 000 | 5 000 |
| 3 | Boston..... | 16 000 | 16 000 | 12 000 | |
| 4 | Buffalo..... | 16 000 | 16 000 | 12 000 | 3 000 |
| 5 | Chicago..... | 16 000 | 16 000 | 12 000 | |
| 6 | Cincinnati..... | 16 000 | 16 000 | 12 000 | 3 000 |
| 7 | Cleveland..... | 16 000 | | 12 000 | |
| 8 | Denver..... | 16 000 | 16 000 | 12 000 | 3 000 |
| 9 | Detroit..... | 16 000(d) | 16 000(d) | 12 000 | 3 000 |
| 10 | Hartford(f)..... | | | | |
| 11 | Jersey City..... | 16 000 | 16 000 | 12 000 | 3 000 |
| 12 | Los Angeles(e)..... | | | | |
| 13 | Louisville..... | 16 000 | 16 000 | 12 000 | |
| 14 | Milwaukee..... | 16 000 | 16 000 | 12 000 | |
| 15 | Minneapolis..... | 16 000 | 16 000 | 12 000 | 3 000 |
| 16 | Newark, N. J..... | 16 000 | 16 000 | 12 000 | 3 000 |
| 17 | New Haven..... | 16 000 | | 12 000 | |
| 18 | New Orleans..... | 16 000 | 16 000 | 12 000 | 3 000 |
| 19 | New York..... | 16 000 | 16 000 | | 3 000 |
| 20 | Philadelphia..... | { 14 500(c) 16 250(d) | | 12 500 | |
| 21 | Pittsburgh..... | 16 000 | | 12 000 | |
| 22 | Portland, Ore..... | 16 000 | 16 000 | 12 000 | 3 000 |
| 23 | Providence(e)..... | | | | |
| 24 | Rochester..... | 16 000 | 16 000 | 12 000 | 3 000 |
| 25 | St. Louis(f)..... | | | | |
| 26 | St. Paul..... | 16 000 | 16 000 | 12 000 | 3 000 |
| 27 | San Francisco..... | 16 000 | 16 000 | 12 000 | |
| 28 | Seattle..... | 16 000 | 16 000 | 12 000 | |
| 29 | Syracuse..... | 16 000 | { 10 000(b) 16 000(a) | | 3 000 |
| 30 | Washington..... | 16 000 | 16 000 | 12 000 | 3 000 |
| 31 | Worcester, Mass..... | 16 000 | 16 000 | 12 000 | 3 000 |

(a) Annealed; (b) Not annealed; (c) Mild Steel; (d) Medium Steel; (e)

EXTRACTS FROM THE BUILDING LAWS OF VARIOUS CITIES.

ALLOWABLE UNIT STRESSES FOR STEEL AND IRON.

(Revised to 1917.)

Pounds per Square Inch.

| Extreme Fibre Stress (Bending). | | | | | | | | No. |
|---------------------------------|--------------------------------|-----------------------------------|---------------|--------------------------------|-----------------------------------|-------------------|---------------|-----|
| Steel. | | | Wrought Iron. | | | Cast Iron. | | |
| Rolled Beams. | Rolled Pins, Rivets and Bolts. | Riveted Beams Net Flange Section. | Rolled Beams. | Rolled Pins, Rivets and Bolts. | Riveted Beams Net Flange Section. | Compression Side. | Tension Side. | |
| 16 000 | 20 000 | 14 000 | 12 000 | 15 000 | 12 000 | 16 000 | 3 000 | 1 |
| 16 000 | 20 000 | 15 000 | | 15 000 | | 16 000 | 5 000 | 2 |
| 16 000 | 22 500 | | 12 000 | 18 000 | | 16 000 | 3 00 | 3 |
| 16 000 | | 16 000 | 12 000 | | 12 000 | 13 000 | 3 000 | 4 |
| 16 000 | 25 000 | | 12 000 | | | 10 000 | 3 000 | 5 |
| 16 000 | 24 000 | 16 000 | 12 000 | | 12 000 | 16 000 | 3 000 | 6 |
| 16 000 | 24 000 | 16 000 | | | | | | 7 |
| 16 000 | | 16 000 | 12 000 | | 12 000 | | | 8 |
| 16 000 | | 16 000 | 12 000 | | 12 000 | | | 9 |
| 16 000 | 20 000 | 14 000 | 12 000 | 15 000 | 12 000 | 16 000 | 3 000 | 10 |
| | | | | | | | | 11 |
| 16 000 | 20 000 | 15 000 | | 15 000 | | 16 000 | 3 000 | 12 |
| 16 000 | 25 000 | | 12 000 | | | 10 000 | 3 000 | 13 |
| 16 000 | | 16 000 | 12 000 | | 12 000 | | | 14 |
| 16 000 | 20 000 | 14 000 | 12 000 | 15 000 | 12 000 | 16 000 | 3 000 | 15 |
| 16 000 | 20 000 | 16 000 | 12 000 | 15 000 | 12 000 | | | 16 |
| 16 000 | 22 000 | | 12 000 | 18 000 | | 16 000 | 3 000 | 17 |
| 16 000 | 20 000 | 16 000 | | | | 16 000 | 3 000 | 18 |
| | | | | | | | 3 750 | 19 |
| 16 000 | 24 000 | 16 000 | | | | | | 20 |
| 16 000 | 20 000 | 15 000 | 12 000 | 15 000 | 12 000 | 16 000 | 3 000 | 21 |
| | | 15 000 | | | | | 3 000 | 22 |
| 16 000 | 24 000 | 16 000 | 12 000 | | 12 000 | 10 000 | 3 000 | 23 |
| 16 000 | 20 000 | 14 000 | 12 000 | 15 000 | 12 000 | 16 000 | 3 000 | 24 |
| | | | | | | | | 25 |
| 16 000 | 20 000 | 14 000 | 12 000 | 15 000 | 12 000 | 16 000 | 3 000 | 26 |
| 16 000 | | 15 000 | | | | | 3 000 | 27 |
| 16 000 | 24 000 | 16 000 | 12 000 | | 12 000 | 10 000 | 3 000 | 28 |
| 16 000 | 20 000 | 16 000 | | | | 16 000 | 2 500 | 29 |
| 16 000 | 20 000 | 14 000 | 12 000 | 15 000 | 12 000 | 16 000 | 3 000 | 30 |
| 16 000 | 20 000 | 16 000 | 12 000 | 15 000 | 12 000 | 16 000 | 3 000 | 31 |

Determined by the best modern practice; (f) Building Laws being revised, 1917.

EXTRACTS FROM THE BUILDING LAWS OF VARIOUS CITIES.

ALLOWABLE UNIT STRESSES FOR STEEL AND IRON.

(Revised to 1917.)

Pounds per Square Inch.

| No. | City. | Compression. | | | | | |
|-----|-------------------|--------------------------|--------------------------|---------------|------------------------------|--|---------------------------------------|
| | | Rolled Steel. | Cast Steel. | Wrought Iron. | Cast Iron (in short blocks). | Steel Pins and Rivets Bearing. | Wrought Iron Pins and Rivets Bearing. |
| 1 | Atlanta..... | 16 000 | 16 000 | 12 000 | 16 000 | 20 000 | 15 000 |
| 2 | Baltimore..... | 16 000 | 16 000 | 12 000 | 16 000 | 20 000 | 15 000 |
| 3 | Boston..... | 16 000 | 16 000 | 12 000 | 16 000 | 18 000 | 15 000 |
| 4 | Buffalo..... | | | | 15 000 | 15 000 | 15 000 |
| 5 | Chicago..... | 14 000(a) | 14 000(a) | 10 000(a) | 10 000(a) | {20 000(f) 25 000(s)} | |
| 6 | Cincinnati..... | 16 000 | 16 000 | 12 000 | 16 000 | 20 000 | |
| 7 | Cleveland..... | | 16 000 | 12 000 | | 20 000 | 12 000(t) |
| 8 | Denver..... | | | | 15 000 | 18 000 | 15 000 |
| 9 | Detroit..... | (b) | (b) | 75% Steel | (b) | {15 000(f) 20 000(s)} | 12 000(t) |
| 10 | Hartford(l).... | | | | | | |
| 11 | Jersey City.... | 16 000 | 16 000 | 12 000 | 16 000 | 20 000 | 15 000 |
| 12 | Los Angeles(j) .. | | | | | | |
| 13 | Louisville.... | 16 000 | 16 000 | 12 000 | 16 000 | 20 000 | 15 000 |
| 14 | Milwaukee.... | 12 000(a) | 12 000(a) | 10 000(a) | 8 000(a) | 20 000(k) | |
| 15 | Minneapolis.... | 16 000 | 16 000 | 12 000 | 16 000 | 18 000 | 15 000 |
| 16 | Newark, N. J.... | 16 000 | 16 000 | 12 000 | 16 000 | 20 000 | 15 000 |
| 17 | New Haven.... | 16 000 | | 12 000 | | 20 000 | 15 000 |
| 18 | New Orleans.... | 16 000 | | 12 000 | | 18 000 | 15 000 |
| 19 | New York.... | 16 000 | 16 000 | | 16 000 | 24 000 | 15 000 |
| 20 | Philadelphia.. | {14 500(c) 16 250(d)} | | 12 500 | 11 670 | {17 600(f) 22 000(s) 20 000(f) 24 000(s)} | {14 400(f) 18 000(s) 20 000(t)} |
| 21 | Pittsburgh.... | 16 000 | 16 000 | 12 000 | 12 000 | 20 000 | 15 000 |
| 22 | Portland, Ore.. | 16 000 | 16 000 | 12 000 | 16 000 | 20 000 | 15 000 |
| 23 | Providence(j) .. | | | | | | |
| 24 | Rochester.... | 16 000 | 16 000 | 12 000 | 16 000 | 20 000 | 15 000 |
| 25 | St. Louis(l).... | | | | | | |
| 26 | St. Paul..... | 16 000 | 16 000 | 12 000 | 16 000 | 20 000 | 15 000 |
| 27 | San Francisco.. | 16 000 | 16 000 | 12 000 | 16 000 | 20 000 | |
| 28 | Seattle..... | 16 000 | 16 000 | 12 000 | 10 000(a) | {20 000(f) 24 000(s)} | |
| 29 | Syracuse..... | 16 000 | {10 000(g) 16 000(e)} | | {10 000(g) 16 000} | {16 000(h) 20 000} | |
| 30 | Washington.... | 16 000 | 16 000 | 12 000 | 16 000 | 20 000 | 15 000 |
| 31 | Worcester.... | 16 000 | 16 000 | 12 000 | 16 000 | 20 000 | 15 000 |

(a) Based on gross section; (b) Based on values given by standard steel manufacturer's handbook; (c) Mild steel; (d) Medium steel; (e) Annealed; (f) Field rivets; (g) Not annealed; (h) Field rivets driven by hand;

EXTRACTS FROM THE BUILDING LAWS OF VARIOUS CITIES.

ALLOWABLE UNIT STRESSES FOR STEEL AND IRON.

(Revised to 1917.)

Pounds per Square Inch.

| Shear. | | | | | | | | | No. |
|-------------|-----------------------|-------------------------|--------------|---------------|-----------------------|---------------|--------------|------------|-----|
| Steel. | | | | Wrought Iron. | | | | Cast Iron. | |
| Web Plates. | Shop Rivets and Pins. | Field Rivets. | Field Bolts. | Web Plates. | Shop Rivets and Pins. | Field Rivets. | Field Bolts. | | |
| 9 000 | 10 000 | 8 000 | 7 000 | 6 000 | 7 500 | 6 000 | 5 500 | 3 000 | 1 |
| 9 000 | 10 000 | 8 000 | 7 000 | 6 000 | 7 500 | 6 000 | 5 500 | 3 000 | 2 |
| 10 000 | 10 000 | 10 000 | 8 000 | 9 000 | 9 000 | 9 000 | 7 200 | | 3 |
| 7 000 | 9 000 | 8 000 | | 6 000 | 7 500 | 6 000 | | | 4 |
| 10 000(a) | 12 000 | 10 000 | | | | | | 2 000(i) | 5 |
| 10 000 | 10 000 | 9 000 | 7 500 | 6 000 | 6 000 | 6 000 | 6 000 | 3 000 | 6 |
| 10 000 | 10 000 | | 6 000 | | | | | | 7 |
| 9 000 | 10 000 | 7 000 | | 6 000 | 7 500 | 5 000 | | | 8 |
| 10 000 | 10 000 | 7 500 | 6 000 | | | | | 3 000 | 9 |
| 9 000 | 10 000 | 10 000 | 7 000 | 6 000 | 7 500 | 6 000 | 5 500 | 3 000 | 10 |
| | | | | | | | | | 11 |
| 9 000 | 10 000 | 8 000 | 8 000 | | 7 500 | 6 000 | 5 000 | 2 500 | 12 |
| 10 000 | 10 000 | 8 000 | 7 000 | | 7 500 | | | 2 000(i) | 13 |
| 10 000 | 9 000 | 6 750 | | 6 000 | 7 500 | 6 000 | | | 14 |
| 9 000 | 10 000 | 8 000 | 7 000 | 6 000 | 7 500 | 6 000 | 5 500 | 3 000 | 15 |
| 10 000 | 10 000 | 8 000 | | 6 000 | 7 500 | 6 000 | | | 16 |
| 10 000 | 10 000 | 10 000 | 8 000 | 9 000 | 9 000 | 9 000 | 7 200 | | 17 |
| 10 000 | 12 000 | 8 000 | 7 000 | | | | | 3 000 | 18 |
| { 8 750(c) | 11 000 | 8 800 | | 7 500 | 9 000 | 7 200 | | | 19 |
| { 10 000(d) | | | | | | | | | 20 |
| 10 000 | 12 000 | 10 000 | 10 000 | | | | | | 21 |
| 9 000 | 10 000 | 8 000 | 7 000 | 6 000 | 7 500 | 6 000 | 5 500 | 3 000 | 22 |
| 9 000 | 10 000 | 8 000 | 7 000 | 6 000 | 7 500 | 6 000 | 5 500 | 3 000 | 23 |
| 9 000 | 10 000 | 8 000 | 7 000 | 6 000 | 7 500 | 6 000 | 5 500 | 3 000 | 24 |
| 9 000 | 10 000 | 8 000 | 7 000 | 6 000 | 7 500 | 6 000 | 5 500 | 3 000 | 25 |
| 9 000 | 10 000 | 8 000 | 7 000 | 6 000 | 7 500 | 6 000 | 5 500 | 3 000 | 26 |
| 9 000 | 10 000 | 8 000 | 7 000 | 6 000 | 7 500 | 6 000 | 5 500 | 3 000 | 27 |
| 10 000(a) | 12 000 | 10 000 | | | | | | 2 000(i) | 28 |
| 10 000 | 10 000 | { 8 000(h) 10 000(k) | 7 000 | | | | | 2 000 | 29 |
| 9 000 | 10 000 | 8 000 | 7 000 | 6 000 | 7 500 | 6 000 | 5 500 | 3 000 | 30 |
| 10 000 | 10 000 | 8 000 | 7 000 | 6 000 | 7 500 | 6 000 | 5 500 | 3 000 | 31 |

(i) Brackets; (j) Based on best modern practice; (k) Power driven; (l) Building Laws being revised, 1917; (s) Shop rivets; (t) Bearing on steel bolts.

EXTRACTS FROM THE BUILDING LAWS OF VARIOUS CITIES.

ALLOWABLE UNIT STRESSES FOR STEEL AND IRON.

(Revised to 1917.)

Pounds per Square Inch.

| No. | City. | Columns. | | | | | |
|-----|----------------|---------------------------------|-------------------|---|-------------------|-------------------------|-------------------|
| | | Steel. | | Cast Iron. | | Wrought Iron. | |
| | | Formula. | Max. Length L= | Formula. | Max. Length L= | Formula. | Max. Length L= |
| 1 | Atlanta..... | (A) | 120 R | (B) | 70 R | (C) | 120 R |
| 2 | Baltimore... | {Soft Steel (E) Medium " (F) | 120 R | {<50 R—10 000 > " (G) | 60 R | | |
| 3 | Boston..... | (H) | 120 R | (B) | 70 R | (I) | |
| 4 | Buffalo..... | {<90 R—12 000 > " (J) | 40 D | {Round (M) Rectangular (N) | 30 D | {<90 R—8 000 > " (K) | 40 D |
| 5 | Chicago..... | {(O) 14 000 max. | 120 R | (Q) | 70 R | {(P) 10 000 max. | |
| 6 | Cincinnati... | {<70 R—13 000 > " (J) | 180 R | {Round (T) Rectangular (S) Others (U) | 180 R | | |
| 7 | Cleveland(f). | (f) | 120 R | (f) | 30 D | (f) | |
| 8 | Denver..... | (J) | | (EE) | 30 D | (K) | |
| 9 | Detroit..... | {<60 R—12 000 > " (O)(b) | 44 D | Round (T) | 30 D | 75% Steel | |
| 10 | Hartford(e)... | | | | | | |
| 11 | Jersey City... | (A) | 120 R | (B) | 70 R | (C) | 120 R |
| 12 | Los Angeles(d) | | | | | | |
| 13 | Louisville.... | {<70 R—13 000 > " (CC) | 120 R | {Round (T) Rectangular(S) Others (U) | 120 R | | |
| 14 | Milwaukee... | (J) | 120 R | (Q) | 25 D | (P) | 120 R |
| 15 | Minneapolis.. | (J) | 40 D | {Round (V) Rectangular(W) | 30 D | (K) | 40 D |
| 16 | Newark, N.J. | (A) | 120 R | (B) | 70 R | (C) | 120 R |

L = Length in inches; R = Radius of Gyration in inches; D = Diameter or Least Dimension in inches.

FORMULÆ:—

| | | |
|---|---|---|
| (A) $15\,200 - 58 \frac{L}{R}$ | (G) $\frac{11\,000}{1 + \frac{L^2}{1\,000 R^2}}$ | (M) $\frac{14\,000}{1 + \frac{L^2}{600 D^2}}$ |
| (B) $11\,300 - 30 \frac{L}{R}$ | (H) $\frac{16\,000}{1 + \frac{L^2}{20\,000 R^2}}$ | (N) $\frac{14\,000}{1 + \frac{L^2}{850 D^2}}$ |
| (C) $14\,000 - 80 \frac{L}{R}$ | (I) $\frac{12\,000}{1 + \frac{L^2}{20\,000 R^2}}$ | (O) $16\,000 - 70 \frac{L}{R}$ |
| (E) $\frac{14\,000}{1 + \frac{L^2}{13\,500 R^2}}$ | (J) $17\,100 - 57 \frac{L}{R}$ | (P) $12\,000 - 60 \frac{L}{R}$ |
| (F) $\frac{15\,000}{1 + \frac{L^2}{13\,500 R^2}}$ | (K) $10\,600 - 30 \frac{L}{R}$ | (Q) $10\,000 - 60 \frac{L}{R}$ |

(b) 85% for soft steel.

EXTRACTS FROM THE BUILDING LAWS OF VARIOUS CITIES.

ALLOWABLE UNIT STRESSES FOR STEEL AND IRON.

(Revised to 1917.)

Pounds per Square Inch.

| No. | City | Columns | | | | | |
|-----|-----------------|---------------------------------|-------------------|----------------------------------|-------------------|--------------|-------------------|
| | | Steel | | Cast Iron | | Wrought Iron | |
| | | Formula | Max. Length L= | Formula | Max. Length L= | Formula | Max. Length L= |
| 17 | New Haven... | 12 500(c) | { 40 D 120 R | 13 330(c) | 20 D | 10 000(c) | { 40 D 120 R |
| 18 | New Orleans.. | (H) | 120 R | (B) | 70 R | (I) | 120 R |
| 19 | New York.... | (O) | 120 R | (BB) | 70 R | | |
| 20 | Philadelphia.. | { Mild Steel (X) Med'm " (Y) | 140 R | (Z) | 20 D | (AA) | 140 R |
| 21 | Pittsburgh.... | (GG) Max. 13000 | 120 R | (HH) Max. 9000 | 70 R | | 120 R |
| 22 | Portland, Ore. | (A) | 120 R | (B) | 70 R | (C) | 120 R |
| 23 | Providence.... | | | | | | |
| 24 | Rochester.... | (A) | 120 R | (B) | 70 R | (C) | 120 R |
| 25 | St. Louis | (f)..... | | (II) | 25 D | | |
| 26 | St. Paul..... | (T) | | (T) | | | |
| 27 | San Francisco. | { <30 R-12 000 > " (DD) | 120 R | { Round (EE) Rectangular (FF) | 20 D | | |
| 28 | Seattle | (O) 14 000 max. | 120 R | (Q) | 70 R | (P) | |
| 29 | Syracuse..... | (A) | 120 R | (BB) | 70 R | | |
| 30 | Washington.... | (A) | 120 R | (B) | 70 R | (C) | 120 R |
| 31 | Worcester.... | (A) | | (BB) | | | |

L = Length in inches; R = Least Radius of Gyration in inches; D = Diameter or Least Dimension in inches.

FORMULÆ (continued):—

$$(S) \frac{10\,000}{1 + \frac{L^2}{1\,067\,D^2}}$$

$$(X) \frac{14\,500}{1 + \frac{L^2}{13\,500\,R^2}}$$

$$(CC) 17\,000 - 57 \frac{L}{R}$$

$$(DD) 15\,000 - 50 \frac{L}{R}$$

$$(T) \frac{10\,000}{1 + \frac{L^2}{800\,D^2}}$$

$$(Y) \frac{16\,250}{1 + \frac{L^2}{11\,000\,R^2}}$$

$$(EE) \frac{8\,000}{1 + \frac{L^2}{800\,D^2}}$$

$$(U) \frac{10\,000}{1 + \frac{L^2}{6\,400\,R^2}}$$

$$(Z) \frac{11\,670}{1 + \frac{L^2}{400\,D^2}}$$

$$(FF) \frac{8\,000}{1 + \frac{L^2}{1\,067\,D^2}}$$

$$(V) \frac{13\,330}{1 + \frac{L^2}{400\,D^2}}$$

$$(AA) \frac{12\,500}{1 + \frac{L^2}{15\,000\,R^2}}$$

$$(GG) 19\,000 - 100 \frac{L}{R}$$

$$(HH) 10\,500 - 50 \frac{L}{R}$$

$$(W) \frac{13\,330}{1 + \frac{L^2}{500\,D^2}}$$

$$(BB) 9\,000 - 40 \frac{L}{R}$$

$$(II) 11\,100 - 220 \frac{L}{R}$$

(c) Coefficients for use with Gordon's Formula. (d) Based on best modern practice. (e) Building Laws being revised, 1917. (f) See Building Laws.

EXTRACTS FROM THE BUILDING LAWS OF VARIOUS CITIES.

Allowable Unit Stresses for Masonry and Building Materials.
(Revised to 1917.) Pounds per Square Inch.

| No. | City. | Compression. | | | | | | | |
|-----|----------------|-----------------------------|-----------------------------|------------------------------|------------------------------|--|--------------------------------|--|---|
| | | Concrete. | | | | Rubble Stonework. | | | |
| | | Portland Cement 1:2:4 | Portland Cement 1:2:5 | Rosendale Cement 1:2:4 | Rosendale Cement 1:2:5 | Portland Cement Mortar | Rosendale Cement Mortar. | Lime and Cement Mortar. | Lime Mortar. |
| 1 | Atlanta..... | 230 | 208 | 125 | 111 | 140 | 111 | 97 | 70 |
| 2 | Baltimore... | 400 | 350 | 125 | 111 | 125 | 100 | 70 | 50 |
| 3 | Boston..... | 417 | | | | | | | |
| 4 | Buffalo..... | 56 (a) | 56 (a) | | | 70 | | | |
| 5 | Chicago..... | { 400 (d) 350 (e) | { 350 (d,f) 300 (e,f) | | 150 | { 200 (b) 100 (c) | | | { 120 (b) 60 (c) |
| 6 | Cincinnati... | 208 | 208 | | | 167 | 125 | | 83 |
| 7 | Cleveland.... | 400 | 350 (h) | | | | | | |
| 8 | Denver..... | 56 | 139 | | | | 167 | | 56-111 |
| 9 | Detroit..... | 417 | 417 | 111 | 111 | 139 | 111 | { 83 97 (g) | 70 |
| 10 | Hartford.... | 153 | 153 | | | | | | |
| 11 | Jersey City.. | 230 | 208 | 125 | 111 | 140 | 111 | 97 | 70 |
| 12 | Los Angeles.. | 278 (a) | 278 (a) | | | | | | |
| 13 | Louisville.... | | | | | | 167 | | |
| 14 | Milwaukee... | 400 | { 250 (k) 300 (f) | 111 | 83 | 175 | 125 | 97 | 90 |
| 15 | Minneapolis.. | { 500 (i) 300 | 208 (h) | | | 167 | 125 | 111 | 83 |
| 16 | Newark, N. J. | 230 | 208 | 125 | 111 | 140 | 111 | 97 | 70 |
| 17 | New Haven.. | 208 (a) | 208 (a) | | | | | | |
| 18 | New Orleans.. | | | | | | | | |
| 19 | New York.... | 500 | 400 (f) | 210 | 150 (f) | 140 | 110 | 100 | |
| 20 | Philadelphia. | 208 | 208 | | | 139 | | 111 | 70 |
| 21 | Pittsburgh(j). | | | | | | | | |
| 22 | Portland, Ore. | 347 | 278 (k) | | | { 208 (b) 167 (c) 139 (c) 153 (b) | { 125 (b) 97 (c) | { 167 (b) 139 (c) 97 (b) 70 (c) | { 139 (b) 83 (c) 83 (b) 56 (c) |
| 23 | Providence... | 222 | 195 | 111 | 83 | | | | |
| 24 | Rochester... | 230 | 208 | 125 | 111 | 140 | 111 | 97 | 70 |
| 25 | St. Louis.... | 250 (h) | | | | | | | |
| 26 | St. Paul..... | 500 | 400 | 125 | 111 | 200 | 100 | 125 (g) | 80 |
| 27 | San Francisco | 277 | 277 | | | | | | |
| 28 | Seattle..... | 400 | 350 (f) | | | { 200 (b) 100 (c) | | | { 120 (b) 60 (c) |
| 29 | Syracuse.... | 400 | 300 | 100 | 80 | 110 | | | |
| 30 | Washington.. | 400 | 320 | 125 | 111 | 140 | 111 | 97 | 70 |
| 31 | Worcester.... | 278 | 208 (k) | 111 | 111 | 139 | 111 | 97 | 70 |

(a) Foundations; (b) Coursed; (c) Ordinary; (d) Machine-mixed; (e) Hand-mixed; (f) 1:2½:5; (g) Portland Cement Mortar; (h) 1:3:5; (i) 300 where height is 12 diameters; 500 for 5 diameters or under; intermediate heights, intermediate values; (j) Based on best modern practice; (k) 1:3:6.

EXTRACTS FROM THE BUILDING LAWS OF VARIOUS CITIES.

Allowable Unit Stresses on Masonry and Building Materials.

(Revised to 1917.)

Pounds per Square Inch.

| Compression | | | | | | | | | | | | | | No. |
|-----------------------------------|------------------------------------|------------------------------------|----------------------------------|------------------------|--------------------|--------|-------------------------|----------------------|-------------------------|-----------|--------------------------------|-------|----|-----|
| Brickwork | | | | Granites (per Test) | Greenwich Stone | Gneiss | Limestone (per Test) | Marble (per Test) | Sandstone (per Test) | Bluestone | Hard-burned Brick, flatwise | Slate | | |
| Portland Cem. Mor- tar 1:3 | Roseendale Cem. Mor- tar 1:3 | Lime and Cem. Mor- tar 1:1:6 | Lime Mortar 1:4 | | | | | | | | | | | |
| 250 | 208 | 160 | 111 | {1000- 2400 | | 1200 | {700- 2300 | {600- 1200 | {400- 1600 | 2000 | 300 | 1000 | 1 | |
| 250 | 208 | 160 | 111 (l) | {1000- 2400 | | | 1000 | {1000- 2000 | 400 n | 1500 m | | | 2 | |
| {278 q 250 r 167 q | {250 q 208 r 125 t 70 u | {167 q 139 r | {111 q p 97 r p 42 u | 833 | | | 556 | 556 | 417 | | | | 3 | |
| {350 v 175 u | 150 | 125 | 100 | 600 | | | | | 400 | | | | 4 | |
| 250 | 167 | | 111 | {1000- 2400 | | | | | {400- 1600 | | | | 5 | |
| 200 | 175 | 150 | 100 | 1000 | | | 600 | | 400 | | | | 6 | |
| 125 | 125 | | 40 | 560 | | | | | 167 | | | | 7 | |
| 208 | | {153 g 125 | 97 | | | | | | | | | | 8 | |
| 208 t | 208 t | 160 | 111 t | | | | | | | | | | 9 | |
| 250 | 208 | 160 | 111 | {1000- 2400 | | 1200 | {700- 2300 | {600- 1200 | {400- 1600 | 2000 | 300 | 1000 | 10 | |
| 208 | 208 | | 111 | | | | | | | | | | 11 | |
| 250 | 167 | | 111 | | | | | | | | | | 12 | |
| {180 250 t | {139 160 t | 111 | {83 120 t | | | | | | | | | | 13 | |
| 208 | | 160 | 111 | | | | | | | | | | 14 | |
| 250 | 208 | 160 | 111 | {1000- 2400 | | 1200 | {700- 2300 | {600- 1200 | {400- 1600 | 2000 | 300 | 1000 | 15 | |
| 208 | | 160 | 111 | | | | | | | | | | 16 | |
| {250 q 167 u | | | {125 q 83 u | 830 | | | 550 | 550 | 415 | | | | 17 | |
| 250 | 210 | 160 | 110 | 1000 | 1200 | 1000 | 700 | 600 | 400 | 2000 | | 1000 | 18 | |
| 208 | | 167 | 111 | | | | | | | | | | 19 | |
| {167 u 222 v 181 u 222 v | | {139 u 167 v 139 v | {111 u 139 v 83 u 111 v | | | | | | | | | | 20 | |
| 250 | 208 | 160 | 111 | {1000- 2400 | 1200 | | {1300 w, x | {600- 1200 | {400- 1600 | | 300 | 1000 | 21 | |
| 300 | 210 | | 120 | | | | | | | | | | 22 | |
| 250 | 208 | 225 g | 111 | {1000- 2000 | | | {700- 2300 | {600- 1200 | {400- 1600 | | {150- 300 | | 23 | |
| 208 | 208 | 139 | 97 | 389 y | | | | | | | | | 24 | |
| 175 v | | 125 v | 100 | 800 y | | | 400 | | {235- 350 | | | | 25 | |
| 250 | 175 | 160 g | 110 | {1000- 2400 | 1200 | 1300 | {700- 2300 | {600- 1200 | {400- 1600 | 2000 | 300 | 1000 | 26 | |
| 250 | | 160 | 111 | " | 1200 | 1300 | " | " | " | 2000 | | 1000 | 27 | |
| 208 | 167 | 139 | 111 | " | | 1200 | " | " | " | 2000 | 300 | 1000 | 28 | |

(l) Mortar 1:3; (m) Falls Road Stone; (n) Cement Stone; (o) Mortar 1:2; (p) Mortar 1:6; (q) Hard-burned Brick—first-class work; (r) Same—Ordinary work; (t) Hard-burned Brick; (u) Common Brick; (v) Higher values for special Brick; (w) Local; (x) Medina—2000; (y) Granite Masonry.

EXTRACTS FROM THE BUILDING LAWS OF VARIOUS CITIES.

Allowable Unit Stresses for Masonry, Etc.

(Revised to 1917.)

Pounds per Square Inch

| No. | City. | Extreme Fibre Stress (Bending). | | | | | |
|-------|------------------|---------------------------------|------------------|---------|------------|--------|---------|
| | | Granite. | Greenwich Stone. | Gneiss. | Limestone. | Slate. | Marble. |
| 1, 16 | Atlanta, Newark | 180 | | 150 | 150 | 400 | 120 |
| 11 | Jersey City..... | | | | | | |
| 31 | Worcester..... | | | | | | |
| 2 | Baltimore..... | 180 | 150 | | 150 | 400 | 120 |
| 6 | Cincinnati..... | 50 | | | | | |
| 14 | Milwaukee..... | | | | | | |
| 24 | Rochester..... | 180 | | | 150(b) | 400 | 120 |
| 26 | St. Paul..... | 180 | | | 150 | 400 | 120 |
| 29 | Syracuse..... | 180 | 150 | 150 | 150 | 400 | 120 |

**Safe Bearing Capacity of Soils, Etc.
Tons per Square Foot.**

| No. | City. | Soft Clay. | Ordinary Clay and Sand, in Layers, Wet and Springy. | Loam, Clay or Fine Sand, Firm and Dry. | Very Firm Coarse Sand, Stiff Gravel or Hard Clay | Piers of Stone, Brick and Concrete in Caissons. | | |
|-----|-------------------|----------------------|---|--|--|---|---|--|
| | | | | | | Carried down to Rock. | Carried down to Firm Gravel or Hard Clay. | Open Caissons or Sheet Pile Trenches, to Rock. |
| 1 | Atlanta..... | 1 | 2 | 2-3 | 3-4 | 15 | 8-10 | 8 |
| 2 | Baltimore..... | 1 | 2 | 3 | 6(a), 4 | 20-24 | 12-18(d) | |
| 3 | Boston..... | | | | | | | |
| 4 | Buffalo..... | | | | 3½ | | | |
| 5 | Chicago..... | | 1½ | 1¾-2½ | 1¾-2½ | | | |
| 6 | Cincinnati..... | 1 | 1-2 | 4 | 8(c), 5 | | | |
| 7 | Cleveland..... | 1 | 1½ | 2-4 | 3-8 | 10(h) | | |
| 8 | Denver..... | ½(g), 1 | 1-2 | 3 | 4, 8(d) | | | |
| 9 | Detroit..... | | 2 | 3 | 4 | | | |
| 11 | Jersey City..... | 1 | 2 | 3 | 4 | 15 | 10 | 8 |
| 12 | Los Angeles..... | 1-3 | 1 e | 2-4 | 4 | | | |
| 13 | Louisville..... | | | 2½ | 4 | | | |
| 14 | Milwaukee..... | { ½(g) 1 | 2 | 3 | { 4-5(c) 6(d) 20(h) | | | |
| 15 | Minneapolis..... | 1 | 2 | 3 | 4 | | | |
| 16 | Newark, N. J.... | 1 | 2 | 3 | 4 | 15 | 10 | 8 |
| 17 | New Haven..... | | | | 4(f) | | | |
| 18 | New Orleans..... | 0.7 | | | | | | |
| 19 | New York..... | 1 | 2 | 3-4 | 4-6 | 8-40 | | |
| 20 | Philadelphia..... | | | | 6(c), 3½ | | | |
| 21 | Pittsburgh..... | | | | | | | |
| 22 | Portland, Ore... | { ½(g) 1½ ½(g) | 3 | 4 | 8(c) | | | |
| 23 | Providence..... | 1 | 2-3 | 2-5 | 4-10(c) | 25-50(h) | | 10-15(d) |
| 24 | Rochester..... | 1 | 2 | 3 | 10(c), 6 | 15 | 10 | 8 |
| 26 | St. Paul..... | 1 | 2 | 3 | 6(a), 4 | | | |
| 27 | San Francisco... | 1 | 2 | 3 | 6(a), 4 | 20(h) | | 10(d) |
| 28 | Seattle..... | 1 | 2 | 2½ | { 8(c) 3½-5 | | | |
| 29 | Syracuse..... | 1 | 2 | 3 | 4 | | | |
| 30 | Washington..... | 1 | 2 | 3 | 4 | | | |

(a) Coarse Gravel; (b) Local; (c) Well cemented; (d) Bearing—Hardpan or Hard Shale rock unexposed to air, frost and water; (e) Sandy loam; (f) Good, solid, natural earth; (g) Quicksand or alluvial soil; (h) Bearing—Very hard, native bed rock.

EXTRACTS FROM THE BUILDING LAWS OF VARIOUS CITIES.

Allowable Unit Stresses for Masonry, Etc.

(Revised to 1917.)

Pounds per Square Inch.

Extreme Fibre Stress (Bending).

| Sand-stone. | Blue-stone. | Portland Concrete. | | Rosendale Concrete. | | Brick— Hardburned | Brickwork in Cement. | No. |
|-------------|-------------|--------------------|------------|---------------------|------------|----------------------|-------------------------|------|
| | | 1 : 2 : 4. | 1 : 2 : 5. | 1 : 2 : 4. | 1 : 2 : 5. | | | |
| 100 | 300 | 30 | 20 | 16 | 10 | 50 | 30 | 1,16 |
| 100 | 300 | 30 | 20 | 16 | 10 | 50 | 30 | 11 |
| 50 | 300 | 30 | 20 | 16 | 10 | 50 | 30 | 31 |
| 100(j) | 300 | 35 | 25(k)30(l) | 16 | 10 | 50(i) | 30 | 2 |
| 100 | 300 | 30 | 20 | 16 | 10 | 50(i) | 30 | 6 |
| 100 | 300 | 30 | 20 | 16 | 10 | 50(i) | 30 | 14 |
| 100 | 300 | 30 | 20 | 16 | 10 | 50(i) | 30 | 24 |
| 100 | 300 | 30 | 20 | 16 | 10 | 50(i) | 30 | 26 |
| 100 | 300 | 30 | 20 | 16 | 10 | 50(i) | 30 | 29 |

Allowable Safe Loads and Sizes for Wooden Piles.

| Spacing | | Minimum Diameter. | | | Safe Load—Tons. | | Concrete Capping. | | No. |
|---|---|--------------------------------|---|---|-----------------------------------|------------------------------|---|--|-----|
| Maxi- mum C. to C. in inches. | Mini- mum C. to C. in inches. | Of Small End. Inches. | Of Butt. Lengths =<20ft. Inches. | Of Butt. Lengths >20 ft. Inches. | Formula for Single Pile. | Not to exceed per Pile | Thickness Rammed Between Heads. Inches. | Width Outside of Piles. Inches. | |
| 36 | 20 | 5 | 10 | 12 | (D) | 20 | 12 | 12 | 1 |
| 36 | 24 | 8(m), 6 | 10 | 10 | | | 12(n), 6 | | 2 |
| 36 | 24 | 6 | 12 | 12 | | 25 | 16(n) | 12 | 3 |
| 36 | 24 | 6 | 12 | 12 | (D)&(S) | 25 | 12 | 12 | 4 |
| 36 | 24 | 6 | 12 | 12 | | | 12 | 12 | 5 |
| 36 | 24 | 6 | 12 | 12 | (D) | 25 | 12 | 12 | 6 |
| 36 | 24 | 5 | 10 | 12 | (D) | 7-20 | 10 | 12 | 7 |
| 36 | 24 | 5 | 10 | 12 | (D) | 7-20 | 12 | 12 | 8 |
| 36 | 20 | 5 | 10 | 12 | (D) | 20 | | | 9 |
| 36 | 20 | 6 | 12 | 12 | (D)&(S) | 500(p) | | | 11 |
| 36 | 20 | 5 | 10 | 12 | (D) | 20 | 12 | 12 | 12 |
| 36 | 20 | 5 | 10 | 12 | (D) | 7-20 | 12 | 12 | 13 |
| 36 | 20 | 6 | 12 | 12 | | 20 | 12 | 12 | 14 |
| 36 | 20 | 5 | 10 | 12 | (D)&(S) | 20 | 6(n), 12 | 6 | 15 |
| 36 | 20 | 5 | 10 | 12 | (D)&(S) | 20 | 12 | 12 | 16 |
| 36 | 20 | 6 | 12 | 12 | (D)&(S) | 20 | 12 | 12 | 17 |
| 36 | 20 | 6 | 12 | 12 | (D)&(S) | 20 | 12 | 12 | 18 |
| 36 | 20 | 6 | 12 | 12 | (D)&(S) | 20 | 12 | 12 | 19 |
| 36 | 20 | 6 | 12 | 12 | (D) | 25 | 6 | 12 | 20 |
| 36 | 24 | 5 | 10 | 12 | (D) | 20 | 12 | 12 | 21 |
| 36 | 24 | 5 | 10 | 12 | (D) | 25 | 12 | 12 | 22 |
| 36 | 24 | 5 | 10 | 12 | (D) | 25 | 12 | 12 | 23 |
| 36 | 24 | 5 | 10 | 12 | (D) | 25 | 12 | 12 | 24 |
| 36 | 24 | 5 | 10 | 12 | (D) | 25 | 12 | 12 | 25 |
| 36 | 24 | 5 | 10 | 12 | (D) | 25 | 12 | 12 | 26 |
| 36 | 24 | 5 | 10 | 12 | (D) | 25 | 12 | 12 | 27 |
| 36 | 24 | 5 | 10 | 12 | (D) | 25 | 12 | 12 | 28 |
| 36 | 24 | 5 | 10 | 12 | (D) | 25 | 12 | 12 | 29 |
| 36 | 24 | 5 | 10 | 12 | (D) | 25 | 12 | 12 | 30 |

(i) Common; (j) Medina; (k) 1:3:6 mixture; (l) 1:2½:5 mixture; (m) Length =>20 ft.; (n) Capping, on top of heads; (o) In clear between piles; (D) For Drop Hammer, $\frac{2WH}{P+1}$; (S) For Steam Hammer, $\frac{2WH}{P+1\frac{1}{10}}$ where W=Weight of hammer in Tons; H=Height of drop in Feet; P=Penetration of last blow (or average of last several blows) in Ins.; (p) Pounds per sq. in.; (q) Lengths <or>25 ft.

EXTRACTS FROM THE BUILDING LAWS OF VARIOUS CITIES.

ALLOWABLE UNIT STRESSES FOR TIMBER.

(Revised to 1917.)

Pounds per Square Inch.

| No. | City. | Compression. | | | | | |
|-----|---------------------|--------------|---------------|-----------------------|----------------------|-------------|---------------|
| | | Oak. | | Yellow Pine. | | White Pine. | |
| | | With Grain. | Across Grain. | With Grain. | Across Grain. | With Grain. | Across Grain. |
| 1 | Atlanta..... | 900 | 800 | 1000 | 600 | 800 | 400 |
| 2 | Baltimore..... | 1000 | 600 | 1000 | 600 | 800 | 400 |
| 3 | Boston..... | 810(e) | 600(e) | 900 | 500 | 630 | 250 |
| 4 | Buffalo..... | 800(c) | | 1000(g) | | 700 | |
| 5 | Chicago..... | 900 | 500 | { 1100(g,d) 800(f) | 250(d) | 700(c) | 200(c) |
| 6 | Cincinnati..... | 900 | 800 | 1000 | 600 | 800 | 400 |
| 7 | Cleveland..... | | 300 | | 350 | | 300 |
| 8 | Denver..... | 800(c) | | 1000 | | 700 | |
| 9 | Detroit..... | 1000 | | 1250 | | 875 | |
| 10 | Hartford(q)..... | | | | | | |
| 11 | Jersey City..... | 900 | 800 | 1000 | 600 | 800 | 400 |
| 12 | Los Angeles(a)..... | | | | | | |
| 13 | Louisville..... | 1000 | 600 | 1000 | 600 | 800 | 400 |
| 14 | Milwaukee..... | 1500(e) | 500(e) | { 1500(g) 1200(f) | { 350(g) 300(f) | 1100(d) | 200(d) |
| 15 | Minneapolis..... | 800(e) | | 1000(h) | | 700 | |
| 16 | Newark, N. J..... | 1100 | 800 | 1500 | 600 | 800 | 400 |
| 17 | New Haven(a)..... | | | | | | |
| 18 | New Orleans..... | | | | { 400(f) 500(g) | | |
| 19 | New York..... | 1400 | 1000 | 1600(g) | 1000(g) | 1000(b,f) | 800(b,f) |
| 20 | Philadelphia..... | | | 750 | 550 | | |
| 21 | Pittsburgh(a)..... | | | | | | |
| 22 | Portland, Ore..... | | | | | 900(l) | 200(l) |
| 23 | Providence(a)..... | | | | | | |
| 24 | Rochester..... | 900 | 800 | 1000 | 600 | 800 | 400 |
| 25 | St. Louis(q)..... | | | | | | |
| 26 | St. Paul..... | 1000 | 700 | 1100(h) | 600(h) | 900 | 400 |
| 27 | San Francisco..... | | | | | 800(l) | 200(l) |
| 28 | Seattle..... | | | | | | |
| 29 | Syracuse..... | 900 | 800 | { 800(f,b) 1000(g) | { 400(f,b) 600(g) | 800 | 400 |
| 30 | Washington..... | 900 | 800 | 1000 | 600 | 800 | 400 |
| 31 | Worcester(a)..... | | | | | | |

(a) Based on best modern practice; (b) Applies also to North Carolina Pine; (c) Also for Norway Pine; (d) Also for Douglas Fir; (e) White Oak; (f) Shortleaf; (g) Longleaf; (h) Also for Washington or Oregon Fir; (i) Douglas or Yellow Fir only.

EXTRACTS FROM THE BUILDING LAWS OF VARIOUS CITIES.

ALLOWABLE UNIT STRESSES FOR TIMBER.

(Revised to 1917.)

Pounds per Square Inch.

| Compression. | | | | | | | | No. |
|--------------|--------------|-------------|---------------|-------------|---------------|-------------|---------------|-----|
| Spruce | | Locust. | | Hemlock. | | Chestnut. | | |
| With Grain | Across Grain | With Grain. | Across Grain. | With Grain. | Across Grain. | With Grain. | Across Grain. | |
| 800 | 400 | 1200 | 1000 | 500 | 500 | | | 1 |
| 800(b,k) | 400(b,k) | 1200 | 1000 | 600 | 500 | | | 2 |
| 630 | 250 | | | | | | | 3 |
| | | | | 700 | | | | 4 |
| | | | | 500 | 150 | | | 5 |
| 800 | 400 | 1200 | 1000 | 500 | 500 | 500 | 1000 | 6 |
| 700 | | | | 700 | 200 | | | 7 |
| 950(n) | | 850(m) | | 750 | | 600(r) | | 8 |
| | | | | | | | | 9 |
| | | | | | | | | 10 |
| 800 | 400 | 1800 | 1000 | 500 | 500 | 500 | 1000 | 11 |
| | | | | 600 | 500 | 600 | 1000 | 12 |
| | | | | | | | | 13 |
| 1100(o) | 300(o) | 1000(n) | 250(n) | 900 | 200 | 1100(m) | 240(m) | 14 |
| 1000 | 200 | | | 800 | | | | 15 |
| 800 | | 760(n) | | | | | | 16 |
| 800 | 400 | 1200 | 1000 | 600 | 500 | 500 | 1000 | 17 |
| | | | | | | | | 18 |
| | 200(m) | | | | | | | 19 |
| 1200(d) | 800(d) | 1200 | 1000 | 800 | 800 | | | 20 |
| 500 | 300 | | | 350 | 250 | | | 21 |
| | | | | | | | | 22 |
| | | | | | | | | 23 |
| 1500(i) | 400(i) | 1200(j) | 250(j) | | | | | 24 |
| | | | | | | | | 25 |
| 800 | 400 | 1200 | 1000 | 500 | 500 | 500 | 1000 | 26 |
| | | | | | | | | 27 |
| 800 | 400 | 1200 | 1000 | 500 | 300 | 800 | 400 | 28 |
| 800 | 200 | 1600(i) | 300(i) | 900(j) | 250(j) | | | 29 |
| 800 | 300 | 1600(i) | 400(i) | 1400(p) | 350(p) | | | 30 |
| 800 | 400 | | | 800 | 300 | | | 31 |
| 800(k) | 400(k) | 1200 | 1000 | | | 500 | 1000 | 32 |
| | | | | | | | | 33 |

(j) Red Fir only; (k) Also for Virginia Pine; (l) Also for Redwood; (m) Cypress only; (n) Norway Pine only; (o) Cedar; (p) Western Hemlock; (q) Building Laws being revised, 1917; (r) Colorado, Texas or Mexican Hemlock.

EXTRACTS FROM THE BUILDING LAWS OF VARIOUS CITIES.

ALLOWABLE UNIT STRESSES FOR TIMBER.

(Revised to 1917.)

Pounds per Square Inch.

| No. | City. | Extreme Fibre Stress (Bending). | | | | | | |
|-----|------------------|---------------------------------|-------------------|---------|---------|---------|----------|-----------|
| | | Yellow Pine. | White Pine. | Spruce. | Oak. | Locust. | Hemlock. | Chestnut. |
| 1 | Atlanta..... | 1200 | 800 | 800 | 1000 | 1200 | 600 | 800 |
| 2 | Baltimore..... | 1800(l) | 1000 | 1350(f) | 1500 | | 1000 | |
| 3 | Boston..... | 1500(l) | 1000 | 1000 | 1000(d) | | | |
| 4 | Buffalo..... | 1800(l) | 1080(b) | | 1350 | | 1080 | |
| 5 | Chicago..... | { 1000(s) 1300(l,m) | 800(b) | | 1200 | | 600 | |
| 6 | Cincinnati..... | 1200 | 800 | 800 | 1000 | 1200 | 600 | 800 |
| 7 | Cleveland..... | 1600 | 1250 | | 1250 | | 1000 | |
| 8 | Denver..... | 1260(a) | | | 1170(w) | | 720(v) | |
| 9 | Detroit..... | 1250 | 750 | 750 | 1000(d) | 950(e) | | |
| 10 | Hartford(u)..... | | | | | | | |
| 11 | Jersey City.... | 1200 | 800 | 800 | 1000 | 1200 | 600 | 800 |
| 12 | Los Angeles.... | 1620(c) | 1260 | 1260 | 2160 | | | |
| 13 | Louisville..... | 1200 | | | 1000 | | 800 | |
| 14 | Milwaukee..... | { 1500(s) 1800(l) | { 1200(e) 1000 | 1000 | 1500(d) | 1300(h) | 700 | 1100(p) |
| 15 | Minneapolis.... | 1620(a) | 1080(b) | | 1350 | | 1080 | |
| 16 | Newark, N. J.. | 1500 | 800 | 800 | 1100 | 1200 | 600 | 800 |
| 17 | New Haven..... | 1800 | 1080 | 1260 | 1350 | | 954 | |
| 18 | New Orleans.... | { 1200(s) 1500(l) | | | | 900(o) | | |
| 19 | New York..... | 1600(l) | 1200 | 1200(m) | 1200 | | 800 | 1000(s,g) |
| 20 | Philadelphia... | 1600(l) | | 1100 | | | 900 | |
| 21 | Pittsburgh(k)... | | | | | | | |
| 22 | Portland,Ore... | 1600(h) | 900 | 1000(i) | 800(j) | | | |
| 23 | Providence(k)... | | | | | | | |
| 24 | Rochester..... | 1200 | 800 | 800 | 1000 | 1200 | 600 | 800 |
| 25 | St. Louis(u).... | | | | | | | |
| 26 | St. Paul..... | 1200(a) | 800 | 800 | 1000 | 1200 | 600 | 800 |
| 27 | San Francisco.. | 1200(h) | 700 | 700 | 800(i) | 750(j) | | |
| 28 | Seattle..... | 1600(h) | | 1000 | | | 1400(t) | |
| 29 | Syracuse..... | { 800(s)(g) 1200(l) | 700 | 800 | 1200 | | 600 | |
| 30 | Washington.... | 1200 | 800(f) | 800 | 1000 | 1200 | | 800 |
| 31 | Worcester(k)... | | | | | | | |

(a) Also for Washington and Oregon Fir; (b) Also for Norway Pine; (c) Oregon Pine only; (d) White Oak; (e) Norway Pine only; (f) Also for Virginia Pine; (g) Also for North Carolina Pine; (h) Douglas Oregon Yellow Fir only; (i) Washington or Red Fir only; (j) Redwood only; (k) Based on best modern practice;

EXTRACTS FROM THE BUILDING LAWS OF VARIOUS CITIES.

ALLOWABLE UNIT STRESSES FOR TIMBER.

(Revised to 1917.)

Pounds per Square Inch.

| Tension. | | | | | No. |
|-------------------------|-------------|-----------|---------|----------|-----|
| Yellow Pine. | White Pine. | Spruce. | Oak. | Hemlock. | |
| 1200 | 800 | 800 | 1000 | 600 | 1 |
| 1800(l) | 1000 | 1200(f) | 1500 | 800 | 2 |
| | | | | | 3 |
| | | | | | 4 |
| { 1000(s) 1300(l)(m) | 800(b) | | 1200 | 600 | 5 |
| 1200 | 800 | 800 | 1000 | 600 (n) | 6 |
| | | | | | 7 |
| | | | | | 8 |
| | | | | | 9 |
| | | | | | 10 |
| 1200 | 800 | 800 | 1000 | 600 | 11 |
| | | | | | 12 |
| 1200 | | | 1000 | | 13 |
| { 1000(s) 1200(l) | 700(q) | 800(m)(b) | 1200(d) | 600(r) | 14 |
| 1200(a) | 800 | 800 | 1000 | | 15 |
| 1200 | 800 | 800 | 1000 | 600 | 16 |
| | | | | | 17 |
| | | | | | 18 |
| { 900(s) 1200(l) | 700 | 800(m) | 1200 | 600 | 19 |
| 1800(l) | | 1250 | | 1000 | 20 |
| | | | | | 21 |
| 1300(h) | 800 | 1000(i) | | 700(j) | 22 |
| | | | | | 23 |
| 1200 | 800 | 800 | 1000 | 600 | 24 |
| | | | | | 25 |
| 1200(a) | 800 | 800 | 1000 | 600 | 26 |
| 1200(h) | 700 | 700 | 1000(i) | 700(j) | 27 |
| 1600(h) | | 1000 | | 1400(t) | 28 |
| { 800(s) 1200(l) | 800 | 800 | 1000 | 600 | 29 |
| 1200 | 800 | 800(f) | 1000 | | 30 |
| | | | | | 31 |

(l) Longleaf; (m) Also for Douglas Fir; (n) Also for Chestnut; (o) Cypress only; (p) Cypress and Cedar only; (q) Also for Cedar; (r) Also Cypress; (s) Shortleaf; (t) Western Hemlock; (u) Building Laws being revised, 1917; (v) Colorado or Mexican; (w) Also for Texas Pine, Spruce or Hemlock.

EXTRACTS FROM THE BUILDING LAWS OF VARIOUS CITIES.

ALLOWABLE UNIT STRESSES FOR TIMBER.

(Revised to 1917.)

Pounds per Square Inch.

| No. | City. | Shear. | | | | | |
|-----|---------------------|-----------------------|----------------------|-----------------|---------------|-------------|---------------|
| | | Yellow Pine. | | White Pine. | | Spruce. | |
| | | With Fibre. | Across Fibre. | With Fibre. | Across Fibre. | With Fibre. | Across Fibre. |
| 1 | Atlanta..... | 70 | 500 | 40 | 250 | 50 | 320 |
| 2 | Baltimore..... | 100(l) | 500(l) | 85 | 350 | 90 | 350 |
| 3 | Boston..... | 100(l) | | 80 | | 80 | |
| 4 | Buffalo(r)..... | | | | | | |
| 5 | Chicago..... | { 120(s) 130(l)(c) | | 80(d) | | | |
| 6 | Cincinnati..... | 70 | 500 | 40 | 250 | 40 | 250 |
| 7 | Cleveland..... | 150 | 500 | 100 | 400 | | |
| 8 | Denver(q)..... | | | | | | |
| 9 | Detroit..... | 100(l) | | 80 | | 80 | |
| 10 | Hartford(q)..... | | | | | | |
| 11 | Jersey City..... | 70 | 500 | 40 | 250 | 50 | 320 |
| 12 | Los Angeles(e)..... | | | | | | |
| 13 | Louisville..... | 80 | 400 | | | | |
| 14 | Milwaukee..... | { 150(s)(c) 175(l) | { 1000(s) 1250(l) | { 120(n) 100 | 500 | 125 | 750 |
| 15 | Minneapolis(r)..... | | | | | | |
| 16 | Newark, N. J..... | 70 | 500 | 40 | 250 | 50 | 320 |
| 17 | New Haven(e)..... | | | | | | |
| 18 | New Orleans..... | { 65(s) 70(l) | | 50(f) | | | |
| 19 | New York..... | 150(l) | 1000(l) | 100 | 500 | 100 | 500 |
| 20 | Philadelphia..... | 100(l) | 1125 | | | 75 | 750 |
| 21 | Pittsburgh(e)..... | | | | | | |
| 22 | Portland, Ore..... | 150(g) | 500(g) | 100 | 500 | 100(h) | 600(h) |
| 23 | Providence(e)..... | | | | | | |
| 24 | Rochester..... | 70 | 500 | 40 | 250 | 50 | 320 |
| 25 | St. Louis(q)..... | | | | | | |
| 26 | St. Paul..... | 70(j) | 500(j) | 50 | 250 | 50 | 320 |
| 27 | San Francisco..... | 150(g) | 750(g) | 100 | 500 | 100 | 500 |
| 28 | Seattle..... | 200(g) | | | | 130 | |
| 29 | Syracuse..... | { 50(s) 70(l) | { 300(s) 500(l) | 50 | 300 | 50 | 300 |
| 30 | Washington..... | 70 | 500 | 40 | 250 | 50(k) | 320(k) |
| 31 | Worcester(e)..... | | | | | | |

(a) Virginia Pine only; (b) White Oak; (c) Also for Douglas Fir; (d) Also for Norway Pine; (e) Based upon best modern practice; (f) Cypress only; (g) Douglas or Yellow Fir only; (h) Red Fir only;

EXTRACTS FROM THE BUILDING LAWS OF VARIOUS CITIES.

ALLOWABLE UNIT STRESSES FOR TIMBER.

(Revised to 1917.)

Pounds per Square Inch.

| Shear. | | | | | | | No. |
|-------------|---------------|-------------|---------------|-------------|---------------|---------------|-----|
| Oak. | | Locust | | Hemlock. | | Chestnut. | |
| With Fibre. | Across Fibre. | With Fibre. | Across Fibre. | With Fibre. | Across Fibre. | Across Fibre. | |
| 100 | 600 | 100 | 720 | 40 | 275 | 150 | 1 |
| 100 | 720 | 90(a) | 400(a) | 75 | 350 | 150 | 2 |
| 150(b) | | | | | | | 3 |
| | | | | | | | 4 |
| 200 | | | | 60 | | | 5 |
| | | | | | | | |
| 100 | 600 | 100 | 720 | 40 | 270 | 150 | 6 |
| 100 | 400 | | | 80 | 300 | | 7 |
| | | | | | | | 8 |
| 150(b) | | 90(n) | | | | | 9 |
| | | | | | | | 10 |
| 100 | 600 | 100 | 720 | 40 | 275 | 150 | 11 |
| | | | | | | | 12 |
| 80 | 400 | | | | | | 13 |
| 240(b) | 1000(b) | 100(m) | 400(m) | 100(o) | 600 | | 14 |
| | | | | | | | 15 |
| 100 | 600 | 100 | 720 | 40 | 275 | 150 | 16 |
| | | | | | | | 17 |
| | | | | | | | 18 |
| 200 | 1000(c) (s) | | | 100 | 600 | | 19 |
| | | | | 63 | 625 | | 20 |
| | | | | | | | 21 |
| 80(i) | 400(i) | | | | | | 22 |
| | | | | | | | 23 |
| 100 | 600 | 100 | 720 | 40 | 275 | 150 | 24 |
| | | | | | | | 25 |
| 100 | 600 | 100 | 720 | 40 | 275 | 150 | 26 |
| 125(h) | 600(h) | 100(i) | 400(i) | | | | 27 |
| | | | | 180(p) | | | 28 |
| 100 | 600 | | | 35 | 250 | | 29 |
| 100 | 600 | 100 | 720 | | | | 30 |
| | | | | | | | 31 |

(i) Redwood only; (j) Also for Washington Fir; (k) Also for Virginia Pine; (l) Longleaf; (s) Shortleaf; (m) Cedar only; (n) Norway Pine only; (o) Also for Cypress; (p) Western Hemlock; (q) Building Laws being revised, 1917. (r) Do not specify.

EXTRACTS FROM THE BUILDING LAWS OF VARIOUS CITIES.

ALLOWABLE UNIT STRESSES FOR TIMBER.

(Revised to 1917.)

Pounds per Square Inch.

| No. | City. | Columns. | | | | | |
|-----|-----------------|--|---|--|--|--|-------------------------------|
| | | Longleaf Yellow Pine. | White Pine, Norway Pine and Spruce. | Oak. | Chestnut and Hemlock. | Locust. | Maxi- mum Length L = |
| 1 | Atlanta..... | (A) | (B) | (I) | $\frac{5}{8}$ (B) | $1\frac{1}{2}$ (B) | 30 D |
| 2 | Baltimore.... | $\left\{ \begin{array}{l} <12D \text{ (C)} \\ > \text{ " (E)} \end{array} \right.$ | $\left\{ \begin{array}{l} <12D \text{ (C)} \\ > \text{ " (E)} \end{array} \right.$ | $\left\{ \begin{array}{l} <12D \text{ (C)} \\ > \text{ " (E)} \end{array} \right.$ | $\left\{ \begin{array}{l} <12D \text{ (C)} \\ > \text{ " (E)} \end{array} \right.$ | $\left\{ \begin{array}{l} <12D \text{ (C)} \\ > \text{ " (E)} \end{array} \right.$ | |
| 3 | Boston..... | (F) | (G) | (H) | | | 30 D |
| 4 | Buffalo..... | $\left\{ \begin{array}{l} <12D-1000 \\ > \text{ " (F)} \end{array} \right.$ | $\left\{ \begin{array}{l} <12D-700 \\ > \text{ " (J)(b)} \end{array} \right.$ | $\left\{ \begin{array}{l} <12D-800 \\ > \text{ " (K)(a)} \end{array} \right.$ | $\left\{ \begin{array}{l} <12D-700 \\ > \text{ " (J)(c)} \end{array} \right.$ | | |
| 5 | Chicago..... | (M) | (M) | (M) | (M) (c) | | 30 D |
| 6 | Cincinnati.... | $\left\{ \begin{array}{l} <12D-1000 \\ > \text{ " (F)} \end{array} \right.$ | $\left\{ \begin{array}{l} <12D-700 \\ > \text{ " (J)} \end{array} \right.$ | $\left\{ \begin{array}{l} <12D-800 \\ > \text{ " (K)} \end{array} \right.$ | | | 180 R |
| 7 | Cleveland(m) | (u) | (u) | (u) | (u) | | 150 R |
| 8 | Denver.... | $\left\{ \begin{array}{l} <12D-1000 \\ \text{ (O)} \end{array} \right.$ | $\left\{ \begin{array}{l} <12D-700 \\ \text{ (O)} \end{array} \right.$ | $\left\{ \begin{array}{l} <12D-800 \\ \text{ (O)} \end{array} \right.$ | $\left\{ \begin{array}{l} <12D-700 \text{ (e)} \\ \text{ (O)} \end{array} \right.$ | $\left\{ \begin{array}{l} <12D-600 \text{ (v)} \\ \text{ (O)} \end{array} \right.$ | |
| 9 | Detroit..... | $\left\{ \begin{array}{l} <12D-1250 \\ > \text{ " (F)} \end{array} \right.$ | $\left\{ \begin{array}{l} <10D-875 \\ > \text{ " (J)(d)} \end{array} \right.$ | $\left\{ \begin{array}{l} <10D-1000 \\ > \text{ " (K)(a)} \end{array} \right.$ | | | 24 D |
| 10 | Hartford(m)... | | | | | | |
| 11 | Jersey City... | (A) | (B) | (I) | $\frac{5}{8}$ (B) | $1\frac{1}{2}$ (B) | 30 D |
| 12 | Los Angeles (l) | | | | | | |
| 13 | Louisville.... | $\left\{ \begin{array}{l} <12D-1000 \\ > \text{ " (F)} \end{array} \right.$ | | $\left\{ \begin{array}{l} <12D-1000 \\ > \text{ " (F)} \end{array} \right.$ | | | 120 R |
| 14 | Milwaukee... | $\left\{ \begin{array}{l} <15D-1125 \\ > \text{ " (T)(k)} \end{array} \right.$ | $\left\{ \begin{array}{l} <15D-825 \text{ i} \\ > \text{ " (T)(b)} \end{array} \right.$ | $\left\{ \begin{array}{l} <15D-1125 \\ > \text{ " (T)} \end{array} \right.$ | $\left\{ \begin{array}{l} <15D-675 \\ > \text{ " (T)(c)} \end{array} \right.$ | $\left\{ \begin{array}{l} <15D-750 \text{ j} \\ > \text{ " (T)} \end{array} \right.$ | 30 D |
| 15 | Minneapolis.. | $\left\{ \begin{array}{l} <12D-1000 \\ > \text{ " (F)(e)} \end{array} \right.$ | $\left\{ \begin{array}{l} <12D-700 \\ > \text{ " (J)(b)} \end{array} \right.$ | $\left\{ \begin{array}{l} <12D-800 \\ > \text{ " (K)(a)} \end{array} \right.$ | $\left\{ \begin{array}{l} <12D-600 \\ > \text{ " (J)(c)} \end{array} \right.$ | | |
| 16 | Newark, N. J. | (A) | (B) | (I) | $\frac{5}{8}$ (B) | $1\frac{1}{2}$ (B) | 30 D |

L = Length of column in inches; D = Diameter or least dimension of column in inches; R = Least radius of gyration in inches; C = Allowable compressive unit stress (with grain) for that wood.

(a) Also for Norway Pine; (b) White Pine only; (c) Hemlock only; (d) White Pine and Spruce only; (e) Also for Washington and Oregon Fir; (f) Spruce only; (g) Oregon Pine only; (h) White Pine and Virginia Pine only; (i) Also Douglas

FORMULÆ:—

$$(E) \ C - 125 \frac{L}{12D}$$

$$(H) \ 900 - 9 \frac{L}{D}$$

$$(A) \ 1\ 000 - 18 \frac{L}{D}$$

$$(F) \ 1\ 000 - 10 \frac{L}{D}$$

$$(I) \ 900 - 17 \frac{L}{D}$$

$$(B) \ 800 - 15 \frac{L}{D}$$

$$(G) \ 700 - 7 \frac{L}{D}$$

$$(J) \ 625 - 6 \frac{L}{D}$$

EXTRACTS FROM THE BUILDING LAWS OF VARIOUS CITIES.

ALLOWABLE UNIT STRESSES FOR TIMBER.

(Revised to 1917.)

Pounds per Square Inch.

| No. | City. | Columns. | | | | | Maximum Length L = |
|-----|-------------------|-----------------------------|---|--------|-----------------------------|-----------|--------------------------|
| | | Longleaf Yellow Pine. | White Pine, Norway Pine and Spruce. | Oak. | Chestnut and Hemlock. | Locust. | |
| 17 | New Haven..... | 1000 (N) | { 700(b) 800(f) (N) | 900(N) | | | |
| 18 | New Orleans..... | (F) | | | (V) (k) | (U) (t) | 30 D |
| 19 | New York..... | (W) | (I) | (W) | | | 30 D |
| 20 | Philadelphia.... | (O) | (O) | (O) | (O) | (O) | |
| 21 | Pittsburgh(l).... | | | | | | |
| 22 | Portland, Ore.... | (P) | (P) | (P) | (P) | (P) | 20 D |
| 23 | Providence(l).... | | | | | | 20 D |
| 24 | Rochester..... | (A) | (B) | (I) | 5/8 (B) | 1 1/2 (B) | 30 D |
| 25 | St. Louis..... | | | | | | |
| 26 | St. Paul..... | (M) | (M) | (M) | (M) | (M) | |
| 27 | San Francisco... | > 15D(Q) (g) | | | | | |
| 28 | Seattle..... | (P) | (P) | (P) | (P) | (P) | 24 D |
| 29 | Syracuse..... | { 3/4 (A) (s) (A) | (B) | (I) | (S) (c) | | 30 D |
| 30 | Washington..... | (A) | (B) (h) | (I) | | (A) | 30 D |
| 31 | Worcester(l).... | | | | | | |

L = Length of column in inches; D = Diameter or least dimension of column in inches; R = Least radius of gyration in inches; C = Allowable compressive unit stress (with grain) for that wood.

Fir, Cypress and Cedar; (j) For Norway Pine, Spruce and Eastern Fir only; (k) Shortleaf; (< 15D = 900); (l) Based on best modern practice; (s) Shortleaf; (t) Cypress only; (u) See Building Laws; (v) Colorado, Texas or Mexican Hemlock.

$$(K) 750 - 7.5 \frac{L}{D}$$

$$(P) C \left(1 - \frac{L}{70D}\right)$$

$$(U) 450 - 5 \frac{L}{D}$$

$$(M) C \left(1 - \frac{L}{80D}\right)$$

$$(Q) 1300 - 20 \frac{L}{D}$$

$$(V) 815 - 8 \frac{L}{D}$$

(N) Coefficients to apply
to Gordon's Formula.

$$(S) 500 - 9 \frac{L}{D}$$

$$(W) 1200 - 20 \frac{L}{D}$$

$$(O) C \left(1 - \frac{L}{100D}\right)$$

$$(T) C \left(1 - \frac{L}{60D}\right)$$

EXTRACTS FROM THE BUILDING LAWS OF VARIOUS CITIES.

Allowable Unit Stresses for Reinforced Concrete.

(Revised to 1917.)

Pounds per Square Inch.

| No. | City. | Concrete Mixture. | Ratio Moduli or Elasticity Steel to Concrete. | Concrete—Allowable Unit Stresses. | | | | | |
|-----|-----------------|---------------------------|---|-----------------------------------|-----------------------|---------------------------|---------------------------|----------|------------------|
| | | | | Compression. | | | Shear. | Tension. | Bond. |
| | | | | Direct. | Extreme Fibre Bending | In Hooped Columns | | | |
| 2 | Baltimore..... | 1 : 2 : 4 | 15 | {500(b) 500 | 500 | 1200(ff) | 50 | | 60 |
| 3 | Boston..... | 1 : 5 (h) | 15 | | 500 | | 60 | | 60 |
| 4 | Buffalo..... | 1 : 2 : 5 | 12 | 350 | 500 | | 50 | | 50 |
| 5 | Chicago..... | 1 : 2 : 4 | 15 | 400 | 700 | {500 (l) 500(d) | 40 | 40(w) | {50(x) 70(y) |
| 6 | Cincinnati..... | 1 : 2 : 4 | 15 | 600 | 700 | (z) | 65 | | |
| 7 | Cleveland..... | 1 : 2 : 4 | 15 | 500 | 700 | 650 (j) | 40 | 40(w) | {70 50 m |
| 8 | Denver..... | 1 : 2 : 3 | 15 | 450 | 500 | | 50 | | 75 |
| 9 | Detroit..... | {1 : 1½ : 3t 1 : 2 : 4 | {12 15 | 450 | 650 | {(z) 800 (l) | 40 | | {80 100(q) |
| 11 | Jersey City... | 1 : 2 : 4 | 18 | 350 | 500 | (z) | 50 | | 50 |
| 12 | Los Angeles... | 1:2½:3½ | 15 | | 650 | 800 | {40 120(n) | | {80(y) 120(q) |
| 13 | Louisville..... | 1 : 2 : 4 | 15 | {450(b) 650 | 650 | {650 d,l 540 | 50 | | |
| 14 | Milwaukee..... | 1 : 2 : 4 | 15 | 500(b) | 700 | {800(d) 600 600 (l) | {120(n) 60 cc 40 bb | | {40aa 80 |
| 15 | Minneapolis.... | 1 : 2 : 4 | {10 15 | 600 dd | 650 | {800ee 1830 ff | 50 | | {100(q) 75(u) |
| 16 | Newark, N. J.. | 1 : 2 : 4 | 15 | 450(b) | 650 | {650(d) 540 | 40 | | 40 |
| 18 | New Orleans... | | 15 | 500 (r) | 650 (r) | | 50 (r) | | 50 |
| 19 | New York..... | 1 : 6 (h) | 15 | 500 | 650 | 725 | {40 150(n) | | {100(q) 80 |
| 20 | Philadelphia... | 1 : 2 : 4 | 15 | 500 | 650 | 750 | {120(n) 40 | | {100(q) 80 |
| 21 | Pittsburgh..... | 1 : 6 (h) | {8gg 15 | 500 | 650 | {540(ff) 450 | 120 | 90(w) | 80 |
| 24 | Rochester..... | 1 : 6 (h) | 15 | {450(b) 650 | 650 | {540 (l) 650 | 60 | | {150(p) 80 |
| 25 | St. Louis..... | 1 : 6 (h) | {20(ii) 15 | {300(ii) 500 | {400(ii) 800 | 500 | {100(ii) 175 | | 65 |
| 26 | St. Paul..... | 1 : 2 : 4 | 15 | 500(b) | 650 | 750(d) | 50 | | {80(q) 50 |
| 27 | San Francisco.. | 1 : 6 (h) | 15 | 500 | 500 | 700 | 75 | | 60 |
| 28 | Seattle..... | 1 : 2 : 4 | 15 | 450 | 667 | 500 (j) | {120(n) 60cc | | {50(x) 70(y) |
| 30 | Washington.... | 1 : 2 : 4 | 15 | {120(c) 450 | {150(c) 650 | | 60 | 50 | |

(b) Columns not hooped; (c) Cinder-Concrete; (d) Vertical bars with hoops; (e) Actual compression in concrete surrounding steel; (f) Floor slabs; (g) Girders and beams; (h) Cement; aggregate; (i) Pure shear; (j) Spiral reinforcement; (k) Minimum area, gross section; (l) Structural steel units encasing concrete; (m) High carbon steel; (n) Where thoroughly reinforced for shear; (o) Without sign or crack; (p) Where adequate mechanical bond is provided; (q) Deformed bars; (r) Rock or gravel concrete; (s) Slag concrete;

EXTRACTS FROM THE BUILDING LAWS OF VARIOUS CITIES.**Allowable Unit Stresses for Reinforced Concrete.**

(Revised to 1917.)

Pounds per Square Inch.

| Steel—Allowable Unit Stresses. | | | | Columns. | | | Tests. | | No. |
|--------------------------------|--------------|---|---------|---|---|--|---|---|-----|
| Tension. | Compression. | Compression Vertical Reinforce- ment in Columns | Shear. | Maxi- mum Length $\frac{L}{D}$ | Mini- mum Allow- able Dimen- sion Inches. | Actual less Effective Diam. — Inches. | Ratio Test to Calcu- lated Load. | Ratio Span to Maximum Deflection. | |
| { 12000 (v) | { 8000v | | { 8000v | 16 | | 3 | | | 2 |
| { 15000 | { 7500 | | { 10000 | | | 3 | | | 3 |
| 16000 | | | 10000 | 16 | | | 3 | | 4 |
| 18000 | 10500 | 7500 | 12000 | 12 | 64(k) | 3 | 2 | 800 | 5 |
| 16000 | 16000 | | 10000 | 32(z) | | 2 | 4 | | 6 |
| { 18000(m) | { 16000(l) | { 9750(j) | 10000w | 15 | | 4 | | | 7 |
| { 16000 | | { 7500 | | 15 | | 2 | 2 | 700 | 8 |
| $\frac{1}{2}$ (hh) | | (z) | 10000 | 15 | 10 | 4 | 2 | 400 | 9 |
| { 18000m,q | 15 × (e) | { 12000 (l) | | 12 | | 2 | | | 11 |
| { 16000 | 16000 | 6000 | | 30 | 7 | 3 | 2 | | 12 |
| 16000 | 15 × (e) | (ff) | | 15 | | 3 | 4 | | 13 |
| 16000 | 16000 | | | 15 | | 3 | 2(o) | | 14 |
| 16000 | 10500 | { 12000(d) | | 15 | 64(k) | 3 | | | 15 |
| { 20000(m) | { 8000- | { 8000 dd | 10000 | 15 | 12 | 3 | 2 | { 1000 g | 16 |
| { 16000 | { 12000 | { 10000 ee | | 15 | | 4 | | { 300(f) | 17 |
| { 20000(m) | | { 8100(d) | | | | 4 | | | 18 |
| { 16000 | | { 6750(b) | 10000 | | | 4 | | | 19 |
| { 20000(aa) | 16000 | 7500 | | 15 | 12 | 4 | 1 $\frac{3}{4}$ | | 20 |
| { 16000 | | | | 15 | 12 | 4 | 2(o) | | 21 |
| 16000 | 16000 | { 6000 | | 15 | 12 | 4 | | | 22 |
| 16000 | 7500 | { 9000(d) | | 15 | 9 | 3 | 2 | | 23 |
| { 20000(m) | 9750 | { 16000 (l) | 4500 | 15 | | 3 | | | 24 |
| { 16000 | | { 6750 | | 15 | | 3 | | | 25 |
| { 20000(m) | 20000m | { 8100(ff) | | 15 | | 3 | | | 26 |
| { 14000 | { 14000 | { 9750(d) | | 15 | | 3 | | | 27 |
| { 20000(m) | { 8000- | { 6750(b) | 10000 | 15 | 12 | 4 | 2 | | 28 |
| { 16000 | { 12000 | { 7500(b) | | 15 | 12 | 4 | 2 | { 100 gg | 29 |
| 20000 | 7500 | { 10000(d) | 10000 | 15 | 10 | 4 | 2 | { 300(f) | 30 |
| 18000 | | (ff) | 10000 | 15 | 8 | 3 | 2 | 700 | 31 |
| 16000 | 14000 | { 7500 (j) | 12000 | 15 | 50(k) | 4 | | | 32 |
| | | { 6750 | | | | | | | 33 |

(t) For columns; (u) Bars $\frac{3}{4}$ inch or less; larger bars, proportionately less; (v) Soft steel; (w) Diagonal tension; (x) Flat bars with size ratio less than 2, and high carbon rounds and squares; (y) Structural steel rounds and squares; (z) For hooped columns, see Building Laws; (aa) Cold drawn material as wire; (bb) Horizontal bars; (cc) Bent up bars; (dd) Square columns; (ee) Round core columns; (ff) Special cases, see Building Laws; (gg) For calculating deflections; (hh) Elastic limit; (ii) Burnt clay concrete.

EXPLANATION OF TABLES OF RIVETS AND PINS.

RIVETS.

In the design of riveted joints the total stress transmitted is assumed to be taken up by the rivets, no allowance being made for the friction between the plates riveted together, and the manner of failure of the joint will be by shearing of the rivet or crushing of the plate. This assumes that the rules given on page 358 are followed and failure by tearing off the plate caused by the rivets being too near the edge is thus prevented.

In the table of "Shearing Value of Rivets and Bearing Value of Riveted Plates," pages 352 and 353, these values are given for all customary sizes and thicknesses corresponding to various usual allowable unit stresses.

For any given size of rivet or thickness of plate to be used, an inspection of the table will show at once if the bearing value of the plate or the shearing value of the rivet is to govern the design and the amount of stress that can be transmitted by each rivet.

PINS.















In designing pin-connected joints the points which govern the design are the bending moments produced in the pin by the bars or plates connected, and the bearing value of the plates themselves. The bearing value in the case of eye-bars of proper proportions is sufficiently ample and need not be computed. Shear in pins need not ordinarily be considered, as the bending and bearing stresses usually determine the size.

In the table of "Maximum Bending Moments on Pins," pages 360 and 361, is given the allowable bending moments on pins of various diameters for the usual allowable fibre stresses.

In the table of "Bearing Values of Pin Plates for One-Inch Thickness of Plate," on page 359, is given the allowable bearing values of plates against pins of various usual diameters, corresponding to the customary unit stresses of this character.

If the bearing value exceeds the allowable limit in any given case pin-plates must be added, thus increasing the bearing value until it is reduced to a safe limit as shown by the tables.

CONVENTIONAL SIGNS FOR RIVETING.

| | SHOP | FIELD |
|--|---|---|
| Two Full Heads. |  |  |
| Countersunk Inside (Farside) and Chipped. |  |  |
| Countersunk Outside (Nearside) and Chipped. |  |  |
| Countersunk both Sides and Chipped. |  |  |
| | INSIDE. (FARSIDE.) | OUTSIDE. (NEARSIDE.) BOTH SIDES. |
| Flattened to $\frac{1}{8}$" high or Countersunk and not Chipped. |  |  |
| Flattened to $\frac{1}{4}$" high. |  |  |
| Flattened to $\frac{3}{8}$" high. |  |  |

This system, designed by F. C. Osborn, C. E., has for foundation the diagonal cross to represent a countersink, the blackened circle for a field rivet and the diagonal stroke to indicate a flattened head. The position of the cross, with respect to the circle (inside, outside or both sides), indicates the location of the countersink and, similarly, the number and position of the diagonal strokes indicate the height and position of the flattened heads.

Any combination of field, countersunk and flattened head rivets liable to occur may be readily indicated by the proper combination of above signs.

SHEARING VALUE OF RIVETS AND BEARING VALUE OF RIVETED PLATES.

All Dimensions in Inches.

Shearing Value = Area of Rivet × Allowable Shearing Stress per Square Inch.

| Diameter of Rivet. | Area in Square Inches. | Unit Stress = 6 000 lbs. | | Bearing Value for Different | | | |
|--------------------------|------------------------------|--------------------------|------------------|-----------------------------|----------------|---------------|----------------|
| | | Single Shear. | Double Shear. | $\frac{1}{4}$ | $\frac{5}{16}$ | $\frac{3}{8}$ | $\frac{7}{16}$ |
| $\frac{3}{8}$ | .1105 | 663 | 1325 | 1125 | 1406 | 1688 | |
| $\frac{1}{2}$ | .1964 | 1178 | 2356 | 1500 | 1875 | 2250 | 2625 |
| $\frac{5}{8}$ | .3068 | 1841 | 3682 | 1875 | 2344 | 2813 | 3281 |
| $\frac{3}{4}$ | .4418 | 2651 | 5301 | 2250 | 2813 | 3375 | 3938 |
| $\frac{7}{8}$ | .6013 | 3608 | 7216 | 2625 | 3281 | 3938 | 4594 |
| 1 | .7854 | 4712 | 9425 | 3000 | 3750 | 4500 | 5250 |

| Diameter of Rivet. | Area in Square Inches. | Unit Stress = 8 000 lbs. | | Bearing Value for Different | | | |
|--------------------------|------------------------------|--------------------------|------------------|-----------------------------|----------------|---------------|----------------|
| | | Single Shear. | Double Shear. | $\frac{1}{4}$ | $\frac{5}{16}$ | $\frac{3}{8}$ | $\frac{7}{16}$ |
| $\frac{3}{8}$ | .1105 | 884 | 1767 | 1500 | 1875 | 2250 | |
| $\frac{1}{2}$ | .1964 | 1571 | 3142 | 2000 | 2500 | 3000 | 3500 |
| $\frac{5}{8}$ | .3068 | 2454 | 4909 | 2500 | 3125 | 3750 | 4375 |
| $\frac{3}{4}$ | .4418 | 3534 | 7069 | 3000 | 3750 | 4500 | 5250 |
| $\frac{7}{8}$ | .6013 | 4811 | 9621 | 3500 | 4375 | 5250 | 6125 |
| 1 | .7854 | 6283 | 12566 | 4000 | 5000 | 6000 | 7000 |

| Diameter of Rivet. | Area in Square Inches. | Unit Stress = 10 000 lbs. | | Bearing Value for Different | | | |
|--------------------------|------------------------------|---------------------------|------------------|-----------------------------|----------------|---------------|----------------|
| | | Single Shear. | Double Shear. | $\frac{1}{4}$ | $\frac{5}{16}$ | $\frac{3}{8}$ | $\frac{7}{16}$ |
| $\frac{3}{8}$ | .1105 | 1105 | 2209 | 1875 | 2344 | 2813 | |
| $\frac{1}{2}$ | .1964 | 1964 | 3927 | 2500 | 3125 | 3750 | 4375 |
| $\frac{5}{8}$ | .3068 | 3068 | 6136 | 3125 | 3906 | 4688 | 5469 |
| $\frac{3}{4}$ | .4418 | 4418 | 8836 | 3750 | 4688 | 5625 | 6563 |
| $\frac{7}{8}$ | .6013 | 6013 | 12026 | 4375 | 5469 | 6563 | 7656 |
| 1 | .7854 | 7854 | 15708 | 5000 | 6250 | 7500 | 8750 |

| Diameter of Rivet. | Area in Square Inches. | Unit Stress = 12 000 lbs. | | Bearing Value for Different | | | |
|--------------------------|------------------------------|---------------------------|------------------|-----------------------------|----------------|---------------|----------------|
| | | Single Shear. | Double Shear. | $\frac{1}{4}$ | $\frac{5}{16}$ | $\frac{3}{8}$ | $\frac{7}{16}$ |
| $\frac{3}{8}$ | .1105 | 1325 | 2651 | 2250 | 2813 | 3375 | |
| $\frac{1}{2}$ | .1964 | 2356 | 4712 | 3000 | 3750 | 4500 | 5220 |
| $\frac{5}{8}$ | .3068 | 3682 | 7363 | 3750 | 4688 | 5625 | 6562 |
| $\frac{3}{4}$ | .4418 | 5301 | 10603 | 4500 | 5625 | 6750 | 7875 |
| $\frac{7}{8}$ | .6013 | 7216 | 14432 | 5250 | 6563 | 7875 | 9187 |
| 1 | .7854 | 9425 | 18850 | 6000 | 7500 | 9000 | 10500 |

In the above tables the bearing values between the lower and upper zigzag black lines are greater than single and less than double shear for the corresponding dimensions, so that in case of single shear, the single shearing value governs, and in case of double shear, the bearing value governs the design.

SHEARING VALUE OF RIVETS AND BEARING VALUE OF RIVETED PLATES.

All Dimensions in Inches.

Bearing Value = Diameter of Rivet \times Thickness of Plate \times Allowable Bearing Stress per Square Inch.

Thicknesses of Plate in Inches at 12 000 Pounds per Square Inch.

| $\frac{1}{2}$ | $\frac{9}{16}$ | $\frac{5}{8}$ | $\frac{11}{16}$ | $\frac{3}{4}$ | $\frac{13}{16}$ | $\frac{7}{8}$ | $\frac{15}{16}$ | 1 |
|---------------|----------------|---------------|-----------------|---------------|-----------------|---------------|-----------------|-------|
| 3000 | | | | | | | | |
| 3750 | 4219 | 4688 | | | | | | |
| 4500 | 5083 | 5625 | 6188 | 6750 | | | | |
| 5250 | 5906 | 6563 | 7219 | 7875 | 8531 | 9188 | 9844 | |
| 6000 | 6750 | 7500 | 8250 | 9000 | 9750 | 10500 | 11250 | 12000 |

Thicknesses of Plate in Inches at 16 000 Pounds per Square Inch.

| $\frac{1}{2}$ | $\frac{9}{16}$ | $\frac{5}{8}$ | $\frac{11}{16}$ | $\frac{3}{4}$ | $\frac{13}{16}$ | $\frac{7}{8}$ | $\frac{15}{16}$ | 1 |
|---------------|----------------|---------------|-----------------|---------------|-----------------|---------------|-----------------|-------|
| 4000 | | | | | | | | |
| 5000 | 5625 | 6250 | | | | | | |
| 6000 | 6750 | 7500 | 8250 | 9000 | | | | |
| 7000 | 7875 | 8750 | 9625 | 10500 | 11375 | 12250 | 13125 | |
| 8000 | 9000 | 10000 | 11000 | 12000 | 13000 | 14000 | 15000 | 16000 |

Thicknesses of Plate in Inches at 20 000 Pounds per Square Inch.

| $\frac{1}{2}$ | $\frac{9}{16}$ | $\frac{5}{8}$ | $\frac{11}{16}$ | $\frac{3}{4}$ | $\frac{13}{16}$ | $\frac{7}{8}$ | $\frac{15}{16}$ | 1 |
|---------------|----------------|---------------|-----------------|---------------|-----------------|---------------|-----------------|-------|
| 5000 | | | | | | | | |
| 6250 | 7031 | 7813 | | | | | | |
| 7500 | 8438 | 9375 | 10313 | 11250 | | | | |
| 8750 | 9844 | 10938 | 12031 | 13125 | 14219 | 15313 | 16406 | |
| 10000 | 11250 | 12500 | 13750 | 15000 | 16250 | 17500 | 18750 | 20000 |

Thicknesses of Plate in Inches at 24 000 Pounds per Square Inch.

| $\frac{1}{2}$ | $\frac{9}{16}$ | $\frac{5}{8}$ | $\frac{11}{16}$ | $\frac{3}{4}$ | $\frac{13}{16}$ | $\frac{7}{8}$ | $\frac{15}{16}$ | 1 |
|---------------|----------------|---------------|-----------------|---------------|-----------------|---------------|-----------------|-------|
| 6000 | | | | | | | | |
| 7500 | 8437 | 9375 | | | | | | |
| 9000 | 10125 | 11250 | 12375 | 13500 | | | | |
| 10500 | 11812 | 13125 | 14437 | 15750 | 17062 | 18375 | 19687 | |
| 12000 | 13500 | 15000 | 16500 | 18000 | 19500 | 21000 | 22500 | 24000 |

The bearing values above and to the right of the upper zigzag black lines are greater than double shear for the corresponding dimensions, so that in these cases the shearing values govern the design.

The bearing values below and to the left of the lower zigzag black lines are less than single shear, so that in these cases the bearing values govern the design.

LENGTH OF RIVETS REQUIRED FOR VARIOUS GRIPS INCLUDING AMOUNT NECESSARY TO FORM ONE HEAD.



| Grip of Rivet in Inches. | Diameter of Rivet in Inches. | | | | | | | |
|--------------------------|------------------------------|-----------------|-----------------|-----------------|-----------------|-----------------|----------------|------------------|
| | $\frac{1}{4}$ " | $\frac{3}{8}$ " | $\frac{1}{2}$ " | $\frac{5}{8}$ " | $\frac{3}{4}$ " | $\frac{7}{8}$ " | 1" | $1\frac{1}{8}$ " |
| $\frac{1}{8}$ | 1 | $1\frac{1}{4}$ | $1\frac{1}{2}$ | $1\frac{3}{4}$ | $1\frac{7}{8}$ | 2 | $2\frac{1}{8}$ | $2\frac{1}{4}$ |
| $\frac{5}{16}$ | $1\frac{1}{8}$ | $1\frac{3}{8}$ | $1\frac{5}{8}$ | $1\frac{7}{8}$ | 2 | $2\frac{1}{8}$ | $2\frac{1}{4}$ | $2\frac{3}{8}$ |
| $\frac{3}{4}$ | $1\frac{1}{4}$ | $1\frac{1}{2}$ | $1\frac{3}{4}$ | 2 | $2\frac{1}{8}$ | $2\frac{1}{4}$ | $2\frac{3}{8}$ | $2\frac{5}{8}$ |
| $\frac{7}{8}$ | $1\frac{3}{8}$ | $1\frac{5}{8}$ | $1\frac{7}{8}$ | $2\frac{1}{8}$ | $2\frac{1}{4}$ | $2\frac{3}{8}$ | $2\frac{5}{8}$ | $2\frac{7}{8}$ |
| 1 | $1\frac{1}{2}$ | $1\frac{3}{4}$ | 2 | $2\frac{1}{4}$ | $2\frac{3}{8}$ | $2\frac{1}{2}$ | $2\frac{5}{8}$ | $2\frac{3}{4}$ |
| $1\frac{1}{8}$ | $1\frac{5}{8}$ | $1\frac{7}{8}$ | $2\frac{1}{8}$ | $2\frac{3}{8}$ | $2\frac{1}{2}$ | $2\frac{5}{8}$ | $2\frac{3}{4}$ | $2\frac{7}{8}$ |
| $1\frac{1}{4}$ | $1\frac{3}{4}$ | 2 | $2\frac{1}{4}$ | $2\frac{1}{2}$ | $2\frac{3}{8}$ | $2\frac{1}{2}$ | $2\frac{5}{8}$ | 3 |
| $1\frac{3}{8}$ | $1\frac{7}{8}$ | $2\frac{1}{8}$ | $2\frac{3}{8}$ | $2\frac{5}{8}$ | $2\frac{7}{8}$ | 3 | 3 | $3\frac{1}{8}$ |
| $1\frac{1}{2}$ | 2 | $2\frac{1}{4}$ | $2\frac{1}{2}$ | $2\frac{3}{4}$ | 3 | $3\frac{1}{8}$ | $3\frac{1}{4}$ | $3\frac{1}{2}$ |
| $1\frac{5}{8}$ | $2\frac{1}{8}$ | $2\frac{3}{8}$ | $2\frac{5}{8}$ | $2\frac{7}{8}$ | $3\frac{1}{8}$ | $3\frac{1}{4}$ | $3\frac{1}{2}$ | $3\frac{3}{8}$ |
| $1\frac{3}{4}$ | $2\frac{3}{4}$ | $2\frac{1}{2}$ | $2\frac{3}{4}$ | 3 | $3\frac{3}{4}$ | $3\frac{3}{8}$ | $3\frac{3}{2}$ | $3\frac{3}{4}$ |
| $1\frac{7}{8}$ | $2\frac{5}{8}$ | $2\frac{5}{8}$ | $2\frac{7}{8}$ | $3\frac{1}{4}$ | $3\frac{3}{8}$ | $3\frac{1}{2}$ | $3\frac{3}{8}$ | $3\frac{3}{4}$ |
| 2 | $2\frac{1}{2}$ | $2\frac{3}{4}$ | $3\frac{1}{8}$ | $3\frac{3}{8}$ | $3\frac{1}{2}$ | $3\frac{5}{8}$ | $3\frac{3}{4}$ | $3\frac{3}{8}$ |
| $2\frac{1}{8}$ | $2\frac{5}{8}$ | $2\frac{7}{8}$ | $3\frac{1}{4}$ | $3\frac{1}{2}$ | $3\frac{5}{8}$ | $3\frac{3}{4}$ | $3\frac{7}{8}$ | 4 |
| $2\frac{1}{4}$ | $2\frac{3}{4}$ | 3 | $3\frac{3}{8}$ | $3\frac{3}{8}$ | $3\frac{3}{4}$ | $3\frac{7}{8}$ | 4 | $4\frac{1}{8}$ |
| $2\frac{3}{8}$ | $2\frac{7}{8}$ | $3\frac{1}{8}$ | $3\frac{1}{2}$ | $3\frac{3}{4}$ | $3\frac{7}{8}$ | 4 | $4\frac{1}{8}$ | $4\frac{1}{4}$ |
| $2\frac{1}{2}$ | 3 | $3\frac{1}{4}$ | $3\frac{5}{8}$ | $3\frac{3}{4}$ | 4 | $4\frac{1}{8}$ | $4\frac{1}{4}$ | $4\frac{3}{8}$ |
| $2\frac{5}{8}$ | $3\frac{1}{8}$ | $3\frac{1}{2}$ | $3\frac{3}{4}$ | 4 | $4\frac{1}{8}$ | $4\frac{1}{4}$ | $4\frac{3}{8}$ | $4\frac{1}{2}$ |
| $2\frac{3}{4}$ | $3\frac{3}{4}$ | $3\frac{5}{8}$ | $3\frac{3}{8}$ | $4\frac{1}{8}$ | $4\frac{1}{4}$ | $4\frac{3}{8}$ | $4\frac{1}{2}$ | $4\frac{3}{4}$ |
| $2\frac{7}{8}$ | $3\frac{5}{8}$ | $3\frac{3}{4}$ | 4 | $4\frac{1}{4}$ | $4\frac{3}{8}$ | $4\frac{1}{2}$ | $4\frac{3}{8}$ | $4\frac{3}{4}$ |
| 3 | $3\frac{1}{2}$ | $3\frac{7}{8}$ | $4\frac{1}{8}$ | $4\frac{3}{8}$ | $4\frac{1}{2}$ | $4\frac{5}{8}$ | $4\frac{3}{4}$ | $4\frac{7}{8}$ |
| $3\frac{1}{8}$ | $3\frac{5}{8}$ | 4 | $4\frac{1}{4}$ | $4\frac{1}{2}$ | $4\frac{3}{4}$ | $4\frac{5}{8}$ | 5 | 5 |
| $3\frac{1}{4}$ | $3\frac{3}{4}$ | $4\frac{1}{8}$ | $4\frac{3}{8}$ | $4\frac{1}{2}$ | $4\frac{7}{8}$ | 5 | $5\frac{1}{8}$ | $5\frac{1}{4}$ |
| $3\frac{3}{8}$ | $3\frac{7}{8}$ | $4\frac{1}{4}$ | $4\frac{1}{2}$ | $4\frac{3}{4}$ | 5 | $5\frac{1}{8}$ | $5\frac{1}{4}$ | $5\frac{3}{8}$ |
| $3\frac{1}{2}$ | 4 | $4\frac{3}{8}$ | $4\frac{5}{8}$ | 5 | $5\frac{1}{8}$ | $5\frac{1}{4}$ | $5\frac{3}{8}$ | $5\frac{1}{2}$ |
| $3\frac{5}{8}$ | $4\frac{1}{8}$ | $4\frac{1}{2}$ | $4\frac{3}{4}$ | $5\frac{1}{8}$ | $5\frac{1}{4}$ | $5\frac{3}{8}$ | $5\frac{1}{2}$ | $5\frac{5}{8}$ |
| $3\frac{3}{4}$ | $4\frac{3}{4}$ | $4\frac{5}{8}$ | $4\frac{7}{8}$ | $5\frac{1}{4}$ | $5\frac{3}{8}$ | $5\frac{1}{2}$ | $5\frac{5}{8}$ | $5\frac{3}{4}$ |
| $3\frac{7}{8}$ | $4\frac{5}{8}$ | $4\frac{3}{4}$ | 5 | $5\frac{3}{8}$ | $5\frac{1}{2}$ | $5\frac{5}{8}$ | $5\frac{3}{4}$ | $5\frac{7}{8}$ |
| 4 | $4\frac{1}{2}$ | $4\frac{7}{8}$ | $5\frac{1}{8}$ | $5\frac{1}{2}$ | $5\frac{5}{8}$ | $5\frac{3}{4}$ | $5\frac{7}{8}$ | 6 |
| $4\frac{1}{8}$ | $4\frac{5}{8}$ | 5 | $5\frac{1}{4}$ | $5\frac{3}{8}$ | $5\frac{3}{4}$ | $5\frac{7}{8}$ | 6 | $6\frac{1}{8}$ |
| $4\frac{1}{4}$ | $4\frac{3}{4}$ | $5\frac{1}{8}$ | $5\frac{1}{2}$ | $5\frac{3}{4}$ | $5\frac{7}{8}$ | 6 | $6\frac{1}{8}$ | $6\frac{1}{4}$ |
| $4\frac{3}{8}$ | $4\frac{7}{8}$ | $5\frac{1}{4}$ | $5\frac{5}{8}$ | $5\frac{7}{8}$ | 6 | $6\frac{1}{8}$ | $6\frac{1}{4}$ | $6\frac{3}{8}$ |
| $4\frac{1}{2}$ | 5 | $5\frac{3}{8}$ | $5\frac{3}{4}$ | 6 | $6\frac{1}{8}$ | $6\frac{1}{4}$ | $6\frac{3}{8}$ | $6\frac{1}{2}$ |
| $4\frac{5}{8}$ | $5\frac{1}{8}$ | $5\frac{1}{2}$ | $5\frac{7}{8}$ | $6\frac{1}{8}$ | $6\frac{1}{4}$ | $6\frac{3}{8}$ | $6\frac{1}{2}$ | $6\frac{5}{8}$ |
| $4\frac{3}{4}$ | $5\frac{3}{4}$ | $5\frac{5}{8}$ | 6 | $6\frac{3}{4}$ | $6\frac{1}{2}$ | $6\frac{5}{8}$ | $6\frac{3}{4}$ | $6\frac{3}{4}$ |
| $4\frac{7}{8}$ | $5\frac{5}{8}$ | $5\frac{3}{4}$ | $6\frac{1}{8}$ | $6\frac{1}{2}$ | $6\frac{5}{8}$ | $6\frac{3}{4}$ | $6\frac{3}{8}$ | $6\frac{7}{8}$ |
| 5 | $5\frac{1}{2}$ | $5\frac{7}{8}$ | $6\frac{1}{4}$ | $6\frac{5}{8}$ | $6\frac{3}{4}$ | $6\frac{7}{8}$ | 7 | 7 |
| $5\frac{1}{8}$ | $5\frac{5}{8}$ | 6 | $6\frac{3}{8}$ | $6\frac{3}{4}$ | $6\frac{7}{8}$ | 7 | $7\frac{1}{8}$ | $7\frac{1}{8}$ |
| $5\frac{1}{4}$ | $5\frac{3}{4}$ | $6\frac{1}{8}$ | $6\frac{1}{2}$ | $6\frac{7}{8}$ | 7 | $7\frac{1}{8}$ | $7\frac{1}{4}$ | $7\frac{1}{4}$ |
| $5\frac{3}{8}$ | $5\frac{7}{8}$ | $6\frac{1}{4}$ | $6\frac{5}{8}$ | 7 | $7\frac{1}{8}$ | $7\frac{1}{4}$ | $7\frac{3}{8}$ | $7\frac{3}{8}$ |
| $5\frac{1}{2}$ | 6 | $6\frac{3}{8}$ | $6\frac{3}{4}$ | $7\frac{1}{8}$ | $7\frac{1}{4}$ | $7\frac{3}{8}$ | $7\frac{1}{2}$ | $7\frac{1}{2}$ |
| $5\frac{5}{8}$ | $6\frac{1}{8}$ | $6\frac{1}{2}$ | $6\frac{7}{8}$ | $7\frac{1}{4}$ | $7\frac{3}{8}$ | $7\frac{1}{2}$ | $7\frac{5}{8}$ | $7\frac{5}{8}$ |
| $5\frac{3}{4}$ | $6\frac{3}{4}$ | $6\frac{3}{4}$ | 7 | $7\frac{3}{8}$ | $7\frac{3}{4}$ | $7\frac{5}{8}$ | $7\frac{3}{4}$ | $7\frac{3}{4}$ |
| $5\frac{7}{8}$ | $6\frac{5}{8}$ | $6\frac{7}{8}$ | $7\frac{1}{8}$ | $7\frac{1}{2}$ | $7\frac{3}{4}$ | $7\frac{3}{4}$ | $7\frac{7}{8}$ | $7\frac{7}{8}$ |
| 6 | $6\frac{1}{2}$ | 7 | $7\frac{1}{4}$ | $7\frac{5}{8}$ | $7\frac{7}{8}$ | $7\frac{7}{8}$ | 8 | $8\frac{1}{8}$ |

Amount in Inches to be subtracted from above lengths for
Countersunk Heads.

| | | | | | | | |
|---------------|---------------|---------------|---------------|---------------|---------------|---------------|---------------|
| $\frac{1}{8}$ | $\frac{1}{4}$ | $\frac{1}{2}$ | $\frac{1}{2}$ | $\frac{5}{8}$ | $\frac{3}{4}$ | $\frac{7}{8}$ | $\frac{7}{8}$ |
|---------------|---------------|---------------|---------------|---------------|---------------|---------------|---------------|

WEIGHT OF 100 STEEL RIVETS.
INCLUDING 100 HEADS.

| Length Under Head. | Diameter of Rivet in Inches. | | | | |
|--------------------------|------------------------------|---------------|---------------|---------------|-------|
| | $\frac{1}{2}$ | $\frac{5}{8}$ | $\frac{3}{4}$ | $\frac{7}{8}$ | 1 |
| Inches. | Average Weight in Pounds. | | | | |
| $1\frac{1}{4}$ | 9.2 | | | | |
| 1 | 10.5 | 17.0 | | | |
| $1\frac{1}{2}$ | 11.15 | 18.0 | | | |
| $1\frac{3}{4}$ | 11.80 | 19.0 | 28.0 | 41.3 | |
| $1\frac{7}{8}$ | 12.45 | 20.0 | 29.5 | 43.4 | |
| $1\frac{1}{2}$ | 13.10 | 21.0 | 31.0 | 45.5 | 63.5 |
| $1\frac{3}{4}$ | 13.75 | 22.0 | 32.5 | 47.6 | 66.2 |
| $1\frac{7}{8}$ | 14.40 | 23.0 | 34.0 | 49.7 | 68.9 |
| $1\frac{1}{2}$ | 15.00 | 24.0 | 35.5 | 51.8 | 71.7 |
| 2 | 15.70 | 25.0 | 37.0 | 53.9 | 74.4 |
| $2\frac{1}{4}$ | 16.35 | 26.0 | 38.5 | 56.0 | 77.1 |
| $2\frac{1}{2}$ | 17.00 | 27.0 | 40.0 | 58.0 | 79.8 |
| $2\frac{3}{4}$ | 17.65 | 28.0 | 41.5 | 60.1 | 82.6 |
| $2\frac{1}{2}$ | 18.30 | 29.0 | 43.0 | 62.2 | 85.3 |
| $2\frac{3}{4}$ | 18.95 | 30.0 | 44.5 | 64.3 | 88.0 |
| $2\frac{7}{8}$ | 19.60 | 31.0 | 46.0 | 66.4 | 90.7 |
| $2\frac{1}{2}$ | 20.25 | 32.0 | 47.5 | 68.5 | 93.5 |
| 3 | 20.90 | 33.0 | 49.0 | 70.6 | 96.2 |
| $3\frac{1}{4}$ | | 34.0 | 50.5 | 72.7 | 99.0 |
| $3\frac{1}{2}$ | | 35.0 | 52.0 | 74.7 | 101.6 |
| $3\frac{3}{4}$ | | 36.0 | 53.5 | 76.8 | 103.8 |
| $3\frac{1}{2}$ | | 37.0 | 55.0 | 78.9 | 107.1 |
| $3\frac{3}{4}$ | | 38.0 | 56.5 | 81.0 | 109.8 |
| $3\frac{7}{8}$ | | 39.0 | 58.0 | 83.1 | 112.6 |
| $3\frac{1}{2}$ | | 40.0 | 59.5 | 85.2 | 115.2 |
| 4 | | 41.0 | 61.0 | 87.3 | 118.0 |
| $4\frac{1}{4}$ | | | 64.0 | 91.4 | 123.5 |
| $4\frac{1}{2}$ | | | 67.0 | 95.6 | 128.9 |
| $4\frac{3}{4}$ | | | 70.0 | 99.8 | 134.4 |
| 5 | | | 73.0 | 104.0 | 139.8 |
| $5\frac{1}{4}$ | | | 76.0 | 108.2 | 145.3 |
| $5\frac{1}{2}$ | | | 79.0 | 112.3 | 150.7 |
| $5\frac{3}{4}$ | | | 82.0 | 116.5 | 156.2 |
| 6 | | | 85.0 | 120.7 | 161.6 |
| Weight of 100 Heads. | 5.3 | 9.0 | 13.0 | 20.5 | 30.8 |

AREAS TO BE DEDUCTED TO OBTAIN NET AREA OF RIVETED PLATE.

Square Inches.

| Thick- ness Plates in Inches. | SIZE OF HOLE. Inches. | | | | | | | | | | | | | | | |
|---|--------------------------|------|-----|------|------|------|------|------|------|-------|-------|-------|-------|------|-------|-------|
| | 1/4 | 5/16 | 3/8 | 7/16 | 1/2 | 5/8 | 3/4 | 7/8 | 1 | 1 1/8 | 1 1/4 | 1 1/2 | 1 3/4 | 2 | 2 1/4 | 2 1/2 |
| 1/4 | .06 | .08 | .09 | .11 | .13 | .14 | .16 | .17 | .19 | .20 | .22 | .23 | .25 | .27 | .29 | .31 |
| 5/16 | .08 | .10 | .12 | .14 | .16 | .18 | .20 | .21 | .23 | .25 | .27 | .29 | .31 | .33 | .35 | .38 |
| 3/8 | .09 | .12 | .14 | .16 | .19 | .21 | .23 | .26 | .28 | .30 | .33 | .35 | .38 | .40 | .44 | .46 |
| 7/16 | .11 | .14 | .16 | .19 | .22 | .25 | .27 | .30 | .33 | .36 | .38 | .41 | .44 | .46 | .50 | .53 |
| 1/2 | .13 | .16 | .19 | .22 | .25 | .28 | .31 | .34 | .38 | .41 | .44 | .47 | .50 | .53 | .56 | .60 |
| 5/8 | .14 | .18 | .21 | .25 | .28 | .32 | .35 | .39 | .42 | .46 | .49 | .53 | .56 | .60 | .63 | .66 |
| 3/4 | .16 | .20 | .23 | .27 | .31 | .35 | .39 | .43 | .47 | .51 | .55 | .59 | .63 | .66 | .70 | .73 |
| 7/8 | .17 | .21 | .26 | .30 | .34 | .39 | .43 | .47 | .52 | .56 | .60 | .64 | .69 | .73 | .77 | .80 |
| 1 | .19 | .23 | .28 | .33 | .38 | .42 | .47 | .52 | .56 | .61 | .66 | .70 | .75 | .80 | .84 | .88 |
| 1 1/8 | .20 | .25 | .30 | .36 | .41 | .46 | .51 | .56 | .61 | .66 | .71 | .76 | .81 | .86 | .91 | .96 |
| 1 1/4 | .22 | .27 | .33 | .38 | .44 | .49 | .55 | .60 | .66 | .71 | .77 | .82 | .88 | .93 | .99 | 1.04 |
| 1 1/2 | .23 | .29 | .35 | .41 | .47 | .53 | .59 | .64 | .70 | .76 | .82 | .88 | .94 | 1.00 | 1.06 | 1.12 |
| 1 3/4 | .25 | .31 | .38 | .44 | .50 | .56 | .63 | .69 | .75 | .81 | .88 | .94 | 1.00 | 1.06 | 1.13 | 1.20 |
| 2 | .27 | .33 | .40 | .46 | .53 | .60 | .66 | .73 | .80 | .86 | .93 | 1.00 | 1.06 | 1.13 | 1.20 | 1.26 |
| 2 1/4 | .28 | .35 | .42 | .49 | .56 | .63 | .70 | .77 | .84 | .91 | .98 | 1.05 | 1.13 | 1.20 | 1.26 | 1.33 |
| 2 1/2 | .30 | .37 | .45 | .52 | .59 | .67 | .74 | .82 | .89 | .96 | 1.04 | 1.11 | 1.19 | 1.26 | 1.33 | 1.40 |
| 2 3/4 | .31 | .39 | .47 | .55 | .63 | .70 | .78 | .86 | .94 | 1.02 | 1.09 | 1.17 | 1.25 | 1.33 | 1.40 | 1.48 |
| 3 | .33 | .41 | .49 | .57 | .66 | .74 | .82 | .90 | .98 | 1.07 | 1.15 | 1.23 | 1.31 | 1.39 | 1.46 | 1.53 |
| 3 1/4 | .34 | .43 | .52 | .60 | .69 | .77 | .86 | .95 | 1.03 | 1.12 | 1.20 | 1.29 | 1.38 | 1.46 | 1.53 | 1.60 |
| 3 1/2 | .36 | .45 | .54 | .63 | .72 | .81 | .90 | .99 | 1.08 | 1.17 | 1.26 | 1.35 | 1.44 | 1.53 | 1.60 | 1.68 |
| 3 3/4 | .38 | .47 | .56 | .66 | .75 | .84 | .94 | 1.03 | 1.13 | 1.22 | 1.31 | 1.41 | 1.50 | 1.59 | 1.68 | 1.77 |
| 4 | .39 | .49 | .59 | .68 | .78 | .88 | .98 | 1.07 | 1.17 | 1.27 | 1.37 | 1.46 | 1.56 | 1.66 | 1.75 | 1.85 |
| 4 1/4 | .41 | .51 | .61 | .71 | .81 | .91 | 1.02 | 1.12 | 1.22 | 1.32 | 1.42 | 1.52 | 1.63 | 1.73 | 1.83 | 1.93 |
| 4 1/2 | .42 | .53 | .63 | .74 | .84 | .95 | 1.05 | 1.16 | 1.27 | 1.37 | 1.47 | 1.58 | 1.69 | 1.79 | 1.89 | 1.99 |
| 4 3/4 | .44 | .55 | .66 | .77 | .88 | .98 | 1.09 | 1.20 | 1.31 | 1.42 | 1.53 | 1.64 | 1.75 | 1.86 | 1.97 | 2.08 |
| 5 | .45 | .57 | .68 | .79 | .91 | 1.02 | 1.13 | 1.25 | 1.36 | 1.47 | 1.59 | 1.70 | 1.81 | 1.93 | 2.04 | 2.15 |
| 5 1/4 | .47 | .59 | .70 | .82 | .94 | 1.05 | 1.17 | 1.29 | 1.41 | 1.52 | 1.64 | 1.76 | 1.88 | 1.99 | 2.10 | 2.21 |
| 5 1/2 | .48 | .61 | .73 | .85 | .97 | 1.09 | 1.21 | 1.33 | 1.45 | 1.57 | 1.70 | 1.82 | 1.94 | 2.06 | 2.18 | 2.30 |
| 5 3/4 | .50 | .63 | .75 | .88 | 1.00 | 1.13 | 1.25 | 1.38 | 1.50 | 1.63 | 1.75 | 1.88 | 2.00 | 2.13 | 2.25 | 2.38 |

MAXIMUM SIZE OF RIVETS IN ANGLES AND IN FLANGES OF BEAMS AND CHANNELS.

| I-BEAMS. | | | | | | CHANNELS. | | | ANGLES. | | | |
|---------------------|--------------------------|----------------------|---------------------|--------------------------|----------------------|---------------------------|--------------------------|----------------------|------------------------|----------------------|------------------------|----------------------|
| Depth of Beam. Ins. | Weight per Foot. Pounds. | Size of Rivet. Inch. | Depth of Beam. Ins. | Weight per Foot. Pounds. | Size of Rivet. Inch. | Depth of Channel. Inches. | Weight per Foot. Pounds. | Size of Rivet. Inch. | Length of Leg. Inches. | Size of Rivet. Inch. | Length of Leg. Inches. | Size of Rivet. Inch. |
| 3 | 5.5 | 3/8 | 15 | 42.0 | 3/4 | 3 | 4.0 | 3/8 | 3/4 | 1/4 | 3 | 7/8 |
| 4 | 7.5 | 1/2 | 15 | 60.0 | 3/4 | 4 | 5.25 | 1/2 | 1 1/4 | 3/8 | 3 1/2 | 7/8 |
| 5 | 9.75 | 1/2 | 15 | 80.0 | 1/2 | 5 | 6.50 | 1/2 | 1 3/8 | 3/8 | 4 | 7/8 |
| 6 | 12.25 | 5/8 | 18 | 55.0 | 7/8 | 6 | 8.0 | 5/8 | 1 3/8 | 3/8 | 4 1/2 | 7/8 |
| 7 | 15.0 | 5/8 | 20 | 65.0 | 1 | 7 | 9.75 | 5/8 | 1 1/2 | 3/8 | 5 | 7/8 |
| 8 | 18.00 | 3/4 | 20 | 80.0 | 1 | 8 | 11.25 | 3/4 | 1 3/4 | 1/2 | 6 | 7/8 |
| 9 | 21.0 | 3/4 | 24 | 80.0 | 1 | 9 | 13.25 | 3/4 | 2 | 5/8 | 7 | 1 1/8 |
| 10 | 25.0 | 3/4 | 24 | 105.0 | 1 | 10 | 15.0 | 3/4 | 2 1/4 | 3/4 | 8 | 1 1/8 |
| 12 | 31.5 | 3/4 | | | | 12 | 20.50 | 3/4 | 2 1/2 | 3/4 | | |
| 12 | 40.0 | 3/4 | | | | 15 | 33.0 | 3/4 | 2 3/4 | 3/4 | | |

AREAS TO BE DEDUCTED TO OBTAIN NET AREA OF RIVETED PLATE.

Square Inches.

| SIZE OF HOLE. Inches. | | | | | | | | | | | | | | | | | | Thick- ness Plates in Inches. |
|--------------------------|-----------------|----------------|-----------------|----------------|-----------------|----------------|-----------------|----------------|------------------|----------------|------------------|----------------|------------------|------|--|--|----------------|---|
| $1\frac{1}{8}$ | $1\frac{1}{16}$ | $1\frac{1}{4}$ | $1\frac{5}{16}$ | $1\frac{3}{8}$ | $1\frac{7}{16}$ | $1\frac{1}{2}$ | $1\frac{9}{16}$ | $1\frac{5}{8}$ | $1\frac{11}{16}$ | $1\frac{3}{4}$ | $1\frac{13}{16}$ | $1\frac{7}{8}$ | $1\frac{15}{16}$ | 2 | | | | |
| .28 | .30 | .31 | .33 | .34 | .36 | .38 | .39 | .41 | .42 | .44 | .45 | .47 | .48 | .50 | | | $\frac{1}{4}$ | |
| .35 | .37 | .39 | .41 | .43 | .45 | .47 | .49 | .51 | .53 | .55 | .57 | .59 | .61 | .63 | | | $\frac{1}{8}$ | |
| .42 | .45 | .47 | .49 | .52 | .54 | .56 | .59 | .61 | .63 | .66 | .68 | .70 | .73 | .75 | | | $\frac{3}{8}$ | |
| .49 | .52 | .55 | .57 | .60 | .63 | .66 | .68 | .71 | .74 | .77 | .79 | .82 | .85 | .88 | | | $\frac{1}{2}$ | |
| .56 | .59 | .63 | .66 | .69 | .72 | .75 | .78 | .81 | .84 | .88 | .91 | .94 | .97 | 1.00 | | | $\frac{3}{4}$ | |
| .63 | .67 | .70 | .74 | .77 | .81 | .84 | .88 | .91 | .95 | .98 | 1.02 | 1.05 | 1.09 | 1.13 | | | $1\frac{1}{8}$ | |
| .70 | .74 | .78 | .82 | .86 | .90 | .94 | .98 | 1.02 | 1.05 | 1.09 | 1.13 | 1.17 | 1.21 | 1.25 | | | $1\frac{1}{4}$ | |
| .77 | .82 | .86 | .90 | .95 | .99 | 1.03 | 1.07 | 1.12 | 1.16 | 1.20 | 1.25 | 1.29 | 1.33 | 1.38 | | | $1\frac{3}{4}$ | |
| .84 | .89 | .94 | .98 | 1.03 | 1.08 | 1.13 | 1.17 | 1.22 | 1.27 | 1.31 | 1.36 | 1.41 | 1.45 | 1.50 | | | $1\frac{7}{8}$ | |
| .91 | .96 | 1.02 | 1.07 | 1.12 | 1.17 | 1.22 | 1.27 | 1.32 | 1.37 | 1.42 | 1.47 | 1.52 | 1.57 | 1.63 | | | $1\frac{1}{2}$ | |
| .98 | 1.04 | 1.09 | 1.15 | 1.20 | 1.26 | 1.31 | 1.37 | 1.42 | 1.48 | 1.53 | 1.59 | 1.64 | 1.70 | 1.75 | | | $1\frac{5}{8}$ | |
| 1.05 | 1.11 | 1.17 | 1.23 | 1.29 | 1.35 | 1.41 | 1.46 | 1.52 | 1.58 | 1.64 | 1.70 | 1.76 | 1.82 | 1.88 | | | $1\frac{3}{8}$ | |
| 1.13 | 1.19 | 1.25 | 1.31 | 1.38 | 1.44 | 1.50 | 1.56 | 1.63 | 1.69 | 1.75 | 1.81 | 1.88 | 1.94 | 2.00 | | | 1 | |
| 1.20 | 1.26 | 1.33 | 1.39 | 1.46 | 1.53 | 1.59 | 1.66 | 1.73 | 1.79 | 1.86 | 1.93 | 1.99 | 2.06 | 2.13 | | | $1\frac{1}{4}$ | |
| 1.27 | 1.34 | 1.41 | 1.48 | 1.55 | 1.62 | 1.69 | 1.76 | 1.83 | 1.90 | 1.97 | 2.04 | 2.11 | 2.18 | 2.25 | | | $1\frac{1}{8}$ | |
| 1.34 | 1.41 | 1.48 | 1.56 | 1.63 | 1.71 | 1.78 | 1.86 | 1.93 | 2.00 | 2.08 | 2.15 | 2.23 | 2.30 | 2.38 | | | $1\frac{3}{4}$ | |
| 1.41 | 1.48 | 1.56 | 1.64 | 1.72 | 1.80 | 1.88 | 1.95 | 2.03 | 2.11 | 2.19 | 2.27 | 2.34 | 2.42 | 2.50 | | | $1\frac{1}{2}$ | |
| 1.48 | 1.56 | 1.64 | 1.72 | 1.80 | 1.89 | 1.97 | 2.05 | 2.13 | 2.21 | 2.30 | 2.38 | 2.46 | 2.54 | 2.63 | | | $1\frac{5}{8}$ | |
| 1.55 | 1.63 | 1.72 | 1.80 | 1.89 | 1.98 | 2.06 | 2.15 | 2.23 | 2.32 | 2.41 | 2.49 | 2.58 | 2.66 | 2.75 | | | $1\frac{3}{8}$ | |
| 1.62 | 1.71 | 1.80 | 1.89 | 1.98 | 2.07 | 2.16 | 2.25 | 2.34 | 2.43 | 2.52 | 2.61 | 2.70 | 2.79 | 2.88 | | | $1\frac{1}{4}$ | |
| 1.69 | 1.78 | 1.88 | 1.97 | 2.06 | 2.16 | 2.25 | 2.34 | 2.44 | 2.53 | 2.63 | 2.72 | 2.81 | 2.91 | 3.00 | | | $1\frac{1}{2}$ | |
| 1.76 | 1.86 | 1.95 | 2.05 | 2.15 | 2.25 | 2.34 | 2.44 | 2.54 | 2.64 | 2.73 | 2.83 | 2.93 | 3.03 | 3.13 | | | $1\frac{5}{8}$ | |
| 1.83 | 1.93 | 2.03 | 2.13 | 2.23 | 2.34 | 2.44 | 2.54 | 2.64 | 2.74 | 2.84 | 2.95 | 3.05 | 3.15 | 3.25 | | | $1\frac{3}{4}$ | |
| 1.90 | 2.00 | 2.11 | 2.21 | 2.32 | 2.43 | 2.53 | 2.64 | 2.74 | 2.85 | 2.95 | 3.06 | 3.16 | 3.27 | 3.38 | | | $1\frac{1}{8}$ | |
| 1.97 | 2.08 | 2.19 | 2.30 | 2.41 | 2.52 | 2.63 | 2.73 | 2.84 | 2.95 | 3.06 | 3.17 | 3.28 | 3.39 | 3.50 | | | $1\frac{3}{8}$ | |
| 2.04 | 2.15 | 2.27 | 2.38 | 2.49 | 2.61 | 2.72 | 2.83 | 2.95 | 3.06 | 3.17 | 3.29 | 3.40 | 3.51 | 3.63 | | | $1\frac{1}{2}$ | |
| 2.11 | 2.23 | 2.34 | 2.46 | 2.58 | 2.70 | 2.81 | 2.93 | 3.05 | 3.16 | 3.28 | 3.40 | 3.52 | 3.63 | 3.75 | | | $1\frac{5}{8}$ | |
| 2.18 | 2.30 | 2.42 | 2.54 | 2.66 | 2.79 | 2.91 | 3.03 | 3.15 | 3.27 | 3.39 | 3.51 | 3.63 | 3.75 | 3.88 | | | $1\frac{3}{4}$ | |
| 2.25 | 2.38 | 2.50 | 2.63 | 2.75 | 2.88 | 3.00 | 3.13 | 3.25 | 3.38 | 3.50 | 3.63 | 3.75 | 3.88 | 4.00 | | | 2 | |

RIVET SPACING.

All Dimensions in Inches.

| Size of Rivet. | Minimum Pitch. | | Maximum Pitch at Ends of Compression Members. | Minimum Distance from Edge of Piece to Center of Rivet Hole. | | Maximum Pitch in Line of Stress for Plate and Shape Members. |
|----------------|----------------|----------------|---|--|----------------|--|
| | Allowable. | Preferable. | | Sheared Edge. | Rolled Edge. | |
| $\frac{1}{4}$ | $\frac{3}{4}$ | | | | | |
| $\frac{3}{8}$ | $1\frac{1}{8}$ | | | | | |
| $\frac{1}{2}$ | $1\frac{1}{2}$ | | | | | |
| $\frac{5}{8}$ | $1\frac{7}{8}$ | $1\frac{3}{4}$ | | 1 | $\frac{7}{8}$ | 4 |
| $\frac{3}{4}$ | $2\frac{1}{4}$ | $2\frac{1}{2}$ | $2\frac{1}{2}$ | $1\frac{1}{8}$ | 1 | $4\frac{1}{2}$ |
| $\frac{7}{8}$ | $2\frac{3}{8}$ | 3 | 3 | $1\frac{1}{4}$ | $1\frac{1}{8}$ | 6 |
| 1 | 3 | | $3\frac{1}{2}$ | $1\frac{1}{2}$ | $1\frac{1}{4}$ | 8 |
| $1\frac{1}{8}$ | $3\frac{3}{8}$ | | 4 | | | |
| | | | $4\frac{1}{2}$ | | | |

For General Rules for Rivet Spacing see next page.

GENERAL RULES FOR RIVET SPACING FOR BRIDGE AND STRUCTURAL WORK.

The pitch or distance from center to center of rivets should not be less than 3 diameters of the rivet, preferably not less than 3 inches for $\frac{7}{8}$ inch rivets, $2\frac{1}{2}$ inches for $\frac{3}{4}$ inch rivets, 2 inches for $\frac{5}{8}$ inch rivets and $1\frac{3}{4}$ inches for $\frac{1}{2}$ inch rivets.

At the ends of compression members the pitch should not exceed 4 diameters of the rivet for a length equal to $1\frac{1}{2}$ times the maximum width of the member.

Where two or more plates are in contact, rivets spaced not more than 12 inches in either direction shall be used to hold them together.

For members composed of plates and shapes the pitch in the direction of the line of stress should not exceed 6 inches for $\frac{7}{8}$ and $\frac{3}{4}$ inch rivets, $4\frac{1}{2}$ inches for $\frac{5}{8}$ inch rivets and 4 inches for $\frac{1}{2}$ inch rivets. For angles with two gauge lines in built-up members, rivets staggered, the maximum pitch in each line may be twice these distances.

The distance between the sheared edge of any piece and the center of the rivet hole should not be less than $1\frac{1}{2}$ inches for $\frac{7}{8}$ inch rivets, $1\frac{1}{4}$ inches for $\frac{3}{4}$ inch rivets, $1\frac{1}{8}$ inches for $\frac{5}{8}$ inch rivets and 1 inch for $\frac{1}{2}$ inch rivets; for a rolled edge, these distances may be $1\frac{1}{4}$, $1\frac{1}{8}$, 1 and $\frac{7}{8}$ inches, respectively; when practicable it should, for all sizes, be at least 2 diameters of the rivet and should not exceed 8 times the thickness of the plate.

Minimum spacing is generally used in pin plates, at ends of columns, girders, etc., etc.

In figuring clearance of rivets for special cases, allow $\frac{5}{8}$ inch in addition to diameter of head.

BEARING VALUES OF PIN PLATES.

For One Inch Thickness of Plate.

Bearing value = Diameter of Pin \times 1" \times Stress per Square Inch.

| Diam- eter of Pin. | Area of Pin. | Bearing Value at 12 000 Pounds per Square Inch. | Bearing Value at 13 500 Pounds per Square Inch. | Bearing Value at 15 000 Pounds per Square Inch. | Diam- eter of Pin. | Area of Pin. | Bearing Value at 12 000 Pounds per Square Inch. | Bearing Value at 13 500 Pounds per Square Inch. | Bearing Value at 15 000 Pounds per Square Inch. |
|--------------------------|--------------------|---|---|---|--------------------------|--------------------|---|---|---|
| Inches. | Sq. Ins. | Pounds. | Pounds. | Pounds. | Inches. | Sq. Ins. | Pounds. | Pounds. | Pounds. |
| 1 | .785 | 12000 | 13500 | 15000 | 4 $\frac{1}{2}$ | 15.90 | 54000 | 60750 | 67500 |
| 1 $\frac{1}{8}$ | .994 | 13500 | 15190 | 16880 | 4 $\frac{3}{8}$ | 16.80 | 55500 | 62440 | 69380 |
| 1 $\frac{1}{4}$ | 1.227 | 15000 | 16880 | 18750 | 4 $\frac{1}{4}$ | 17.72 | 57000 | 64130 | 71250 |
| 1 $\frac{3}{8}$ | 1.485 | 16500 | 18560 | 20630 | 4 $\frac{1}{8}$ | 18.67 | 58500 | 65810 | 73130 |
| 1 $\frac{1}{2}$ | 1.767 | 18000 | 20250 | 22500 | 5 | 19.64 | 60000 | 67500 | 75000 |
| 1 $\frac{5}{8}$ | 2.074 | 19500 | 21940 | 24380 | 5 $\frac{1}{8}$ | 20.63 | 61500 | 69190 | 76880 |
| 1 $\frac{3}{4}$ | 2.405 | 21000 | 23630 | 26250 | 5 $\frac{1}{4}$ | 21.65 | 63000 | 70880 | 78750 |
| 1 $\frac{7}{8}$ | 2.761 | 22500 | 25310 | 28130 | 5 $\frac{3}{8}$ | 22.69 | 64500 | 72560 | 80630 |
| 2 | 3.142 | 24000 | 27000 | 30000 | 5 $\frac{1}{2}$ | 23.76 | 66000 | 74250 | 82500 |
| 2 $\frac{1}{8}$ | 3.547 | 25500 | 28690 | 31880 | 5 $\frac{5}{8}$ | 24.85 | 67500 | 75940 | 84380 |
| 2 $\frac{1}{4}$ | 3.976 | 27000 | 30380 | 33750 | 5 $\frac{3}{4}$ | 25.97 | 69000 | 77630 | 86250 |
| 2 $\frac{3}{8}$ | 4.430 | 28500 | 32060 | 35630 | 5 $\frac{7}{8}$ | 27.11 | 70500 | 79310 | 88130 |
| 2 $\frac{1}{2}$ | 4.909 | 30000 | 33750 | 37500 | 6 | 28.27 | 72000 | 81000 | 90000 |
| 2 $\frac{5}{8}$ | 5.412 | 31500 | 35440 | 39380 | 6 $\frac{1}{8}$ | 29.46 | 73500 | 82690 | 91880 |
| 2 $\frac{3}{4}$ | 5.940 | 33000 | 37130 | 41250 | 6 $\frac{1}{4}$ | 30.68 | 75000 | 84380 | 93750 |
| 2 $\frac{7}{8}$ | 6.492 | 34500 | 38810 | 43130 | 6 $\frac{3}{8}$ | 31.92 | 76500 | 86060 | 95630 |
| 3 | 7.069 | 36000 | 40500 | 45000 | 6 $\frac{1}{2}$ | 33.18 | 78000 | 87750 | 97500 |
| 3 $\frac{1}{8}$ | 7.670 | 37500 | 42190 | 46880 | 6 $\frac{5}{8}$ | 34.47 | 79500 | 89440 | 99380 |
| 3 $\frac{1}{4}$ | 8.296 | 39000 | 43880 | 48750 | 6 $\frac{3}{4}$ | 35.79 | 81000 | 91130 | 101250 |
| 3 $\frac{3}{8}$ | 8.946 | 40500 | 45560 | 50630 | 6 $\frac{7}{8}$ | 37.12 | 82500 | 92810 | 103130 |
| 3 $\frac{1}{2}$ | 9.621 | 42000 | 47250 | 52500 | 7 | 38.48 | 84000 | 94500 | 105000 |
| 3 $\frac{5}{8}$ | 10.32 | 43500 | 48940 | 54380 | 7 $\frac{1}{2}$ | 44.18 | 90000 | 101250 | 112500 |
| 3 $\frac{3}{4}$ | 11.05 | 45000 | 50630 | 56250 | 8 | 50.27 | 96000 | 108000 | 120000 |
| 3 $\frac{7}{8}$ | 11.79 | 46500 | 52310 | 58130 | 8 $\frac{1}{2}$ | 56.75 | 102000 | 114750 | 127500 |
| 4 | 12.57 | 48000 | 54000 | 60000 | 9 | 63.62 | 108000 | 121500 | 135000 |
| 4 $\frac{1}{8}$ | 13.36 | 49500 | 55690 | 61880 | 10 | 78.54 | 120000 | 135000 | 150000 |
| 4 $\frac{1}{4}$ | 14.19 | 51000 | 57380 | 63750 | 11 | 95.03 | 132000 | 148600 | 165000 |
| 4 $\frac{3}{8}$ | 15.03 | 52500 | 59060 | 65630 | 12 | 113.10 | 144000 | 162000 | 180000 |

EXAMPLE.—The stress in the end post of a bridge is 250 000 pounds and the diameter of the pin is 5 $\frac{5}{8}$ ". Required the total thickness of steel pin plates for a bearing value of 15 000 pounds per square inch.

From the table the bearing value of a 5 $\frac{5}{8}$ " pin in a 1" plate for 15 000 pounds unit stress is 84 380 pounds. Therefore the total thickness of metal required is 250 000

$$84\,380 = 2.96".$$

The nearest commercial size would therefore be 1 $\frac{1}{2}$ " on each side, including web and necessary reinforcing plates.

MAXIMUM BENDING MOMENTS ON PINS.

With Extreme Fibre Stresses Varying from 15 000 to 25 000
Pounds per Square Inch.

| Diameter of Pin in Inches. | Area of Pin in Square Inches. | Moments in Inch-Pounds for Fibre Stresses of | | | | |
|-------------------------------------|--|--|-----------------------------------|------------------------------------|------------------------------------|------------------------------------|
| | | 15 000 Lbs. per Square Inch. | 18 000 Lbs. per Square Inch | 20 000 Lbs. per Square Inch. | 22 500 Lbs. per Square Inch. | 25 000 Lbs. per Square Inch. |
| 1 | .785 | 1470 | 1770 | 1960 | 2210 | 2450 |
| 1 $\frac{1}{8}$ | .994 | 2100 | 2520 | 2800 | 3150 | 3490 |
| 1 $\frac{1}{4}$ | 1.227 | 2900 | 3450 | 3830 | 4310 | 4790 |
| 1 $\frac{3}{8}$ | 1.485 | 3830 | 4590 | 5100 | 5740 | 6380 |
| 1 $\frac{1}{2}$ | 1.767 | 4970 | 5960 | 6630 | 7460 | 8280 |
| 1 $\frac{5}{8}$ | 2.074 | 6320 | 7580 | 8430 | 9480 | 10530 |
| 1 $\frac{3}{4}$ | 2.405 | 7890 | 9470 | 10520 | 11840 | 13150 |
| 1 $\frac{7}{8}$ | 2.761 | 9710 | 11650 | 12940 | 14560 | 16180 |
| 2 | 3.142 | 11780 | 14140 | 15710 | 17670 | 19630 |
| 2 $\frac{1}{8}$ | 3.547 | 14130 | 16960 | 18840 | 21200 | 23550 |
| 2 $\frac{1}{4}$ | 3.976 | 16770 | 20130 | 22370 | 25160 | 27960 |
| 2 $\frac{3}{8}$ | 4.430 | 19730 | 23670 | 26300 | 29590 | 32880 |
| 2 $\frac{1}{2}$ | 4.909 | 23010 | 27610 | 30680 | 34510 | 38350 |
| 2 $\frac{5}{8}$ | 5.412 | 26640 | 31960 | 35520 | 39960 | 44400 |
| 2 $\frac{3}{4}$ | 5.940 | 30630 | 36750 | 40830 | 45940 | 51040 |
| 2 $\frac{7}{8}$ | 6.492 | 34990 | 41990 | 46660 | 52490 | 58320 |
| 3 | 7.069 | 39730 | 47680 | 52970 | 59600 | 66220 |
| 3 $\frac{1}{8}$ | 7.670 | 44940 | 53930 | 59920 | 67410 | 74900 |
| 3 $\frac{1}{4}$ | 8.296 | 50550 | 60660 | 67400 | 75830 | 84250 |
| 3 $\frac{3}{8}$ | 8.946 | 56610 | 67940 | 75480 | 84920 | 94350 |
| 3 $\frac{1}{2}$ | 9.621 | 63140 | 75770 | 84180 | 94710 | 105230 |
| 3 $\frac{5}{8}$ | 10.321 | 70150 | 84180 | 93530 | 105220 | 116910 |
| 3 $\frac{3}{4}$ | 11.045 | 77660 | 93190 | 103540 | 116490 | 129430 |
| 3 $\frac{7}{8}$ | 11.793 | 85690 | 102820 | 114250 | 128530 | 142810 |
| 4 | 12.566 | 94250 | 113100 | 125660 | 141370 | 157080 |
| 4 $\frac{1}{8}$ | 13.364 | 103360 | 124040 | 137820 | 155040 | 172270 |
| 4 $\frac{1}{4}$ | 14.186 | 113050 | 135660 | 150730 | 169570 | 188410 |
| 4 $\frac{3}{8}$ | 15.033 | 123320 | 147980 | 164420 | 184980 | 205530 |
| 4 $\frac{1}{2}$ | 15.904 | 134190 | 161030 | 178920 | 201290 | 223650 |
| 4 $\frac{5}{8}$ | 16.800 | 145690 | 174830 | 194250 | 218510 | 242810 |
| 4 $\frac{3}{4}$ | 17.721 | 157820 | 189390 | 210430 | 236740 | 263040 |
| 4 $\frac{7}{8}$ | 18.665 | 170580 | 204740 | 227490 | 255920 | 284360 |
| 5 | 19.635 | 184080 | 220890 | 245440 | 276120 | 306800 |
| 5 $\frac{1}{8}$ | 20.629 | 198230 | 237880 | 264310 | 297350 | 330390 |
| 5 $\frac{1}{4}$ | 21.648 | 213090 | 255710 | 284120 | 319640 | 355160 |
| 5 $\frac{3}{8}$ | 22.691 | 228680 | 274420 | 304910 | 343020 | 381130 |
| 5 $\frac{1}{2}$ | 23.758 | 245010 | 294010 | 326680 | 367510 | 408350 |
| 5 $\frac{5}{8}$ | 24.850 | 262100 | 314510 | 349460 | 393140 | 436830 |
| 5 $\frac{3}{4}$ | 25.967 | 279960 | 335950 | 373280 | 419940 | 466600 |
| 5 $\frac{7}{8}$ | 27.109 | 298620 | 358340 | 398160 | 447930 | 497700 |

MAXIMUM BENDING MOMENTS ON PINS.

With Extreme Fibre Stresses Varying from 15 000 to 25 000
Pounds per Square Inch.

| Diameter of Pin in Inches. | Area of Pin in Square Inches. | Moments in Inch-Pounds for Fibre Stresses of. | | | | |
|-------------------------------------|--|---|------------------------------------|------------------------------------|------------------------------------|------------------------------------|
| | | 15 000 Lbs. per Square Inch. | 18 000 Lbs. per Square Inch. | 20 000 Lbs. per Square Inch. | 22 500 Lbs. per Square Inch. | 25 000 Lbs. per Square Inch. |
| 6 | 28.274 | 318090 | 381700 | 424120 | 477130 | 530140 |
| 6 $\frac{1}{8}$ | 29.465 | 338380 | 406060 | 451180 | 507580 | 563970 |
| 6 $\frac{1}{4}$ | 30.680 | 359530 | 431430 | 479370 | 539290 | 599210 |
| 6 $\frac{3}{8}$ | 31.919 | 381530 | 457840 | 508710 | 572300 | 635890 |
| 6 $\frac{1}{2}$ | 33.183 | 404420 | 485400 | 539230 | 606530 | 674030 |
| 6 $\frac{5}{8}$ | 34.472 | 428200 | 513840 | 570940 | 642300 | 713670 |
| 6 $\frac{3}{4}$ | 35.785 | 452900 | 543480 | 603870 | 679350 | 754830 |
| 6 $\frac{7}{8}$ | 37.122 | 478530 | 574240 | 638040 | 717800 | 797550 |
| 7 | 38.485 | 505110 | 606130 | 673480 | 757660 | 841850 |
| 7 $\frac{1}{8}$ | 39.871 | 532650 | 639190 | 710210 | 798980 | 887760 |
| 7 $\frac{1}{4}$ | 41.282 | 561180 | 673420 | 748250 | 841780 | 935310 |
| 7 $\frac{3}{8}$ | 42.718 | 590710 | 708860 | 787620 | 886070 | 984520 |
| 7 $\frac{1}{2}$ | 44.179 | 621260 | 745510 | 828350 | 931890 | 1035440 |
| 7 $\frac{5}{8}$ | 45.664 | 652850 | 783410 | 870460 | 979270 | 1088080 |
| 7 $\frac{3}{4}$ | 47.173 | 685480 | 822580 | 913980 | 1028220 | 1142470 |
| 7 $\frac{7}{8}$ | 48.707 | 719190 | 863030 | 958920 | 1078780 | 1198650 |
| 8 | 50.265 | 753980 | 904780 | 1005310 | 1130970 | 1256640 |
| 8 $\frac{1}{8}$ | 51.849 | 789880 | 947860 | 1053170 | 1184820 | 1316470 |
| 8 $\frac{1}{4}$ | 53.456 | 826900 | 992280 | 1102530 | 1240350 | 1378170 |
| 8 $\frac{3}{8}$ | 55.088 | 865060 | 1038070 | 1153410 | 1297590 | 1441760 |
| 8 $\frac{1}{2}$ | 56.745 | 904370 | 1085250 | 1205830 | 1356560 | 1507290 |
| 8 $\frac{5}{8}$ | 58.426 | 944860 | 1133830 | 1259820 | 1417290 | 1574770 |
| 8 $\frac{3}{4}$ | 60.132 | 986540 | 1183850 | 1315390 | 1479810 | 1644240 |
| 8 $\frac{7}{8}$ | 61.862 | 1029430 | 1235310 | 1372570 | 1544140 | 1715710 |
| 9 | 63.617 | 1073540 | 1288250 | 1431390 | 1610310 | 1789240 |
| 9 $\frac{1}{8}$ | 65.397 | 1118900 | 1342680 | 1491860 | 1678340 | 1864830 |
| 9 $\frac{1}{4}$ | 67.201 | 1165510 | 1398610 | 1554010 | 1748270 | 1942520 |
| 9 $\frac{3}{8}$ | 69.029 | 1213400 | 1456080 | 1617870 | 1820100 | 2022340 |
| 9 $\frac{1}{2}$ | 70.882 | 1262590 | 1515110 | 1683450 | 1893880 | 2104310 |
| 9 $\frac{5}{8}$ | 72.760 | 1313090 | 1575700 | 1750780 | 1969630 | 2188480 |
| 9 $\frac{3}{4}$ | 74.662 | 1364910 | 1637900 | 1819880 | 2047370 | 2274850 |
| 9 $\frac{7}{8}$ | 76.590 | 1418090 | 1701700 | 1890780 | 2127130 | 2363480 |
| 10 | 78.540 | 1472620 | 1767150 | 1963500 | 2208930 | 2454370 |
| 10 $\frac{1}{4}$ | 82.516 | 1585850 | 1903020 | 2114470 | 2378780 | 2643090 |
| 10 $\frac{1}{2}$ | 86.590 | 1704740 | 2045690 | 2272990 | 2557120 | 2841240 |
| 10 $\frac{3}{4}$ | 90.763 | 1829430 | 2195320 | 2439250 | 2744150 | 3049060 |
| 11 | 95.033 | 1960060 | 2352070 | 2613410 | 2940090 | 3266770 |
| 11 $\frac{1}{4}$ | 99.402 | 2096760 | 2516110 | 2795680 | 3145140 | 3494600 |
| 11 $\frac{1}{2}$ | 103.869 | 2239670 | 2687610 | 2986230 | 3359510 | 3732790 |
| 12 | 113.098 | 2544690 | 3053630 | 3392920 | 3817040 | 4241150 |

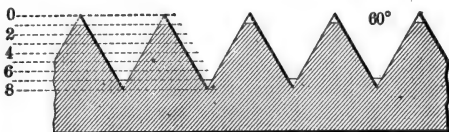
DIMENSIONS OF BOLTS AND NUTS.

Franklin Institute Standard.

| Bolts and Threads. | | | | | | Rough Nuts and Heads. | | | | |
|--------------------|-------------------|-----------------------------|----------------|--------------------|---------------------------------|---------------------------------------|--------------------------|---------------------------|--------------------|---------------------|
| Diameter of Bolt. | Threads per Inch. | Diameter at Root of Thread. | Width of Flat. | Area of Bolt Body. | Area of Bolt at Root of Thread. | Short Diameter of Square and Hexagon. | Long Diameter of Square. | Long Diameter of Hexagon. | Thickness of Nuts. | Thickness of Heads. |
| Inch. | No. | Inch. | Inch. | Sq. Inch. | Sq. Inch. | Inch. | Inch. | Inch. | Inch. | Inch. |
| $\frac{1}{4}$ | 20 | .185 | .0062 | .049 | .027 | $\frac{1}{2}$ | .707 | .577 | $\frac{1}{4}$ | $\frac{1}{4}$ |
| $\frac{5}{16}$ | 18 | .240 | .0070 | .077 | .045 | $\frac{3}{8}$ | .840 | .686 | $\frac{5}{16}$ | $\frac{5}{16}$ |
| $\frac{3}{8}$ | 16 | .294 | .0078 | .110 | .068 | $\frac{1}{2}$ | .972 | .794 | $\frac{3}{8}$ | $\frac{3}{8}$ |
| $\frac{7}{16}$ | 14 | .344 | .0089 | .150 | .093 | $\frac{5}{8}$ | 1.105 | .902 | $\frac{7}{16}$ | $\frac{7}{16}$ |
| $\frac{1}{2}$ | 13 | .400 | .0096 | .196 | .126 | $\frac{3}{4}$ | 1.238 | 1.010 | $\frac{1}{2}$ | $\frac{1}{2}$ |
| $\frac{9}{16}$ | 12 | .454 | .0104 | .249 | .162 | $\frac{7}{8}$ | 1.370 | 1.119 | $\frac{9}{16}$ | $\frac{9}{16}$ |
| $\frac{5}{8}$ | 11 | .507 | .0113 | .307 | .202 | 1 | 1.503 | 1.227 | 1 | 1 |
| $\frac{3}{4}$ | 10 | .620 | .0125 | .442 | .302 | 1 $\frac{1}{8}$ | 1.768 | 1.443 | 1 $\frac{1}{8}$ | 1 $\frac{1}{8}$ |
| $\frac{7}{8}$ | 9 | .731 | .0140 | .601 | .420 | 1 $\frac{1}{4}$ | 2.033 | 1.660 | 1 $\frac{1}{4}$ | 1 $\frac{1}{4}$ |
| 1 | 8 | .837 | .0156 | .785 | .550 | 1 $\frac{3}{8}$ | 2.298 | 1.876 | 1 $\frac{3}{8}$ | 1 $\frac{3}{8}$ |
| 1 $\frac{1}{8}$ | 7 | .940 | .0180 | .994 | .694 | 1 $\frac{1}{2}$ | 2.563 | 2.093 | 1 $\frac{1}{2}$ | 1 $\frac{1}{2}$ |
| 1 $\frac{1}{4}$ | 7 | 1.065 | .0180 | 1.227 | .893 | 2 | 2.829 | 2.309 | 1 $\frac{3}{4}$ | 1 |
| 1 $\frac{3}{8}$ | 6 | 1.160 | .0210 | 1.485 | 1.057 | 2 $\frac{1}{8}$ | 3.094 | 2.526 | 1 $\frac{7}{8}$ | 1 $\frac{3}{4}$ |
| 1 $\frac{1}{2}$ | 6 | 1.284 | .0210 | 1.767 | 1.295 | 2 $\frac{1}{2}$ | 3.359 | 2.742 | 1 $\frac{1}{2}$ | 1 $\frac{1}{2}$ |
| 1 $\frac{3}{4}$ | 5 $\frac{1}{2}$ | 1.389 | .0227 | 2.074 | 1.515 | 2 $\frac{3}{8}$ | 3.624 | 2.959 | 1 $\frac{5}{8}$ | 1 $\frac{3}{4}$ |
| 1 $\frac{7}{8}$ | 5 | 1.490 | .0250 | 2.405 | 1.744 | 2 $\frac{1}{2}$ | 3.889 | 3.175 | 1 $\frac{3}{4}$ | 1 $\frac{7}{8}$ |
| 2 | 5 | 1.615 | .0250 | 2.761 | 2.048 | 2 $\frac{5}{8}$ | 4.154 | 3.392 | 1 $\frac{7}{8}$ | 1 $\frac{7}{8}$ |
| 2 $\frac{1}{8}$ | 4 $\frac{1}{2}$ | 1.712 | .0280 | 3.142 | 2.302 | 3 | 4.420 | 3.608 | 2 | 1 $\frac{9}{16}$ |
| 2 $\frac{1}{4}$ | 4 $\frac{1}{2}$ | 1.962 | .0280 | 3.976 | 3.023 | 3 $\frac{1}{2}$ | 4.950 | 4.042 | 2 $\frac{1}{4}$ | 1 $\frac{1}{2}$ |
| 2 $\frac{3}{8}$ | 4 | 2.175 | .0310 | 4.909 | 3.715 | 3 $\frac{3}{8}$ | 5.480 | 4.475 | 2 $\frac{1}{2}$ | 1 $\frac{1}{2}$ |
| 2 $\frac{1}{2}$ | 4 | 2.425 | .0310 | 5.940 | 4.619 | 4 $\frac{1}{4}$ | 6.011 | 4.908 | 2 $\frac{3}{4}$ | 1 $\frac{1}{2}$ |
| 3 | 3 $\frac{1}{2}$ | 2.629 | .0357 | 7.069 | 5.428 | 4 $\frac{3}{8}$ | 6.541 | 5.341 | 3 | 2 $\frac{1}{8}$ |
| 3 $\frac{1}{4}$ | 3 $\frac{1}{2}$ | 2.879 | .0357 | 8.296 | 6.510 | 5 | 7.071 | 5.774 | 3 $\frac{1}{4}$ | 2 $\frac{1}{4}$ |
| 3 $\frac{1}{2}$ | 3 $\frac{1}{4}$ | 3.100 | .0384 | 9.621 | 7.548 | 5 $\frac{3}{8}$ | 7.602 | 6.207 | 3 $\frac{1}{2}$ | 2 $\frac{1}{2}$ |
| 3 $\frac{3}{4}$ | 3 | 3.317 | .0410 | 11.045 | 8.641 | 5 $\frac{1}{2}$ | 8.132 | 6.640 | 3 $\frac{3}{4}$ | 2 $\frac{3}{4}$ |
| 4 | 3 | 3.567 | .0410 | 12.566 | 9.993 | 6 $\frac{1}{2}$ | 8.662 | 7.073 | 4 | 3 $\frac{1}{8}$ |
| 4 $\frac{1}{4}$ | 2 $\frac{7}{8}$ | 3.798 | .0435 | 14.186 | 11.329 | 6 $\frac{3}{8}$ | 9.193 | 7.506 | 4 $\frac{1}{4}$ | 3 $\frac{1}{4}$ |
| 4 $\frac{1}{2}$ | 2 $\frac{3}{4}$ | 4.028 | .0460 | 15.904 | 12.743 | 6 $\frac{1}{2}$ | 9.723 | 7.939 | 4 $\frac{1}{2}$ | 3 $\frac{1}{2}$ |
| 4 $\frac{3}{4}$ | 2 $\frac{5}{8}$ | 4.255 | .0480 | 17.721 | 14.220 | 7 $\frac{1}{4}$ | 10.253 | 8.372 | 4 $\frac{3}{4}$ | 3 $\frac{3}{8}$ |
| 5 | 2 $\frac{1}{2}$ | 4.480 | .0500 | 19.635 | 15.763 | 7 $\frac{1}{2}$ | 10.784 | 8.805 | 5 | 3 $\frac{1}{2}$ |
| 5 $\frac{1}{4}$ | 2 $\frac{1}{2}$ | 4.730 | .0500 | 21.648 | 17.572 | 8 | 11.314 | 9.238 | 5 $\frac{1}{4}$ | 4 |
| 5 $\frac{1}{2}$ | 2 | 4.953 | .0526 | 23.758 | 19.267 | 8 $\frac{3}{8}$ | 11.844 | 9.671 | 5 $\frac{1}{2}$ | 4 $\frac{1}{2}$ |
| 5 $\frac{3}{4}$ | 2 | 5.203 | .0526 | 25.967 | 21.262 | 8 $\frac{1}{2}$ | 12.375 | 10.104 | 5 $\frac{3}{4}$ | 4 $\frac{3}{4}$ |
| 6 | 2 $\frac{1}{4}$ | 5.423 | .0555 | 28.274 | 23.098 | 9 $\frac{1}{8}$ | 12.905 | 10.537 | 6 | 4 $\frac{9}{16}$ |

RULES FOR PROPORTIONS OF BOLTS AND NUTS.

Franklin Institute Standard.



The dimensions of nuts and bolts are determined by the following rules, which apply to both square and hexagon.

Short diameter of rough nut = $1\frac{1}{2} \times$ diameter of bolt + $\frac{1}{8}$ in.

Short diameter of finished nut = $1\frac{1}{2} \times$ diameter of bolt + $\frac{1}{16}$ in.

Thickness of rough nut = diameter of bolt.

Thickness of finished nut = diameter of bolt - $\frac{1}{16}$ in.

Short diameter of rough head = $1\frac{1}{2} \times$ diameter of bolt + $\frac{1}{8}$ in.

Short diameter of finished head = $1\frac{1}{2} \times$ diameter of bolt + $\frac{1}{16}$ in.

Thickness of rough head = $\frac{1}{2}$ of short diameter of head.

Thickness of finished head = diameter of bolt - $\frac{1}{16}$ in.

In 1864, a committee of the Franklin Institute recommended the above system of screw threads and bolts which was devised by Mr. William Sellers, of Philadelphia. This system as far as it relates to screw threads is generally used in the United States, but the proportions of bolt heads and nuts are not adhered to because the sizes of bar required to make the nuts are special and extra work is necessary to make the bolt heads. Sizes of nuts and bolt heads in accordance with the *Manufacturers' Standard* are given on pages 369, 370 and 371.

WEIGHTS OF 100 MACHINE BOLTS WITH SQUARE HEADS AND HEXAGON NUTS.

Franklin Institute Standard Sizes.

Basis—1 cubic foot Iron = 480 pounds.

| Length under Head to Point. Inches. | Diameter of Bolts in Inches. | | | | | | |
|---|------------------------------|----------------|---------------|----------------|---------------|----------------|---------------|
| | $\frac{1}{4}$ | $\frac{5}{16}$ | $\frac{3}{8}$ | $\frac{7}{16}$ | $\frac{1}{2}$ | $\frac{9}{16}$ | $\frac{5}{8}$ |
| $1\frac{1}{2}$ | 4.9 | 8.2 | 12.2 | 17.5 | 24.0 | 31.8 | 41.1 |
| $1\frac{3}{4}$ | 5.3 | 8.7 | 13.0 | 18.5 | 25.3 | 33.5 | 43.2 |
| 2 | 5.6 | 9.2 | 13.8 | 19.6 | 26.7 | 35.2 | 45.3 |
| $2\frac{1}{4}$ | 6.0 | 9.8 | 14.5 | 20.6 | 28.1 | 37.0 | 47.5 |
| $2\frac{1}{2}$ | 6.3 | 10.3 | 15.3 | 21.6 | 29.4 | 38.7 | 49.6 |
| $2\frac{3}{4}$ | 6.6 | 10.8 | 16.1 | 22.7 | 30.8 | 40.4 | 51.7 |
| 3 | 7.0 | 11.4 | 16.8 | 23.7 | 32.1 | 42.1 | 53.9 |
| $3\frac{1}{4}$ | 7.3 | 11.9 | 17.6 | 24.8 | 33.5 | 43.9 | 56.0 |
| $3\frac{1}{2}$ | 7.7 | 12.4 | 18.4 | 25.8 | 34.9 | 45.6 | 58.1 |
| $3\frac{3}{4}$ | 8.0 | 13.0 | 19.1 | 26.9 | 36.2 | 47.3 | 60.3 |
| 4 | 8.3 | 13.5 | 19.9 | 27.9 | 37.6 | 49.0 | 62.4 |
| $4\frac{1}{2}$ | 9.0 | 14.6 | 21.4 | 30.0 | 40.3 | 52.5 | 66.6 |
| 5 | 9.7 | 15.6 | 23.0 | 32.1 | 43.0 | 55.9 | 70.9 |
| $5\frac{1}{2}$ | 10.4 | 16.7 | 24.5 | 34.2 | 45.8 | 59.4 | 75.2 |
| 6 | 11.1 | 17.8 | 26.0 | 36.2 | 48.5 | 62.8 | 79.4 |
| $6\frac{1}{2}$ | 11.7 | 18.8 | 27.6 | 38.3 | 51.2 | 66.3 | 83.7 |
| 7 | 12.4 | 19.9 | 29.1 | 40.4 | 53.9 | 69.7 | 87.9 |
| $7\frac{1}{2}$ | 13.1 | 21.0 | 30.6 | 42.5 | 56.7 | 73.2 | 92.2 |
| 8 | 13.8 | 22.0 | 32.2 | 44.6 | 59.4 | 76.6 | 96.5 |
| $8\frac{1}{2}$ | 14.5 | 23.1 | 33.7 | 46.7 | 62.1 | 80.1 | 100.7 |
| 9 | 15.1 | 24.2 | 35.3 | 48.8 | 64.8 | 83.5 | 105.0 |
| $9\frac{1}{2}$ | 15.8 | 25.2 | 36.8 | 50.8 | 67.6 | 87.0 | 109.2 |
| 10 | 16.5 | 26.3 | 38.3 | 52.9 | 70.3 | 90.4 | 113.5 |
| $10\frac{1}{2}$ | 17.2 | 27.4 | 39.9 | 55.0 | 73.0 | 93.9 | 117.8 |
| 11 | 17.9 | 28.4 | 41.4 | 57.1 | 75.7 | 97.3 | 122.0 |
| $11\frac{1}{2}$ | 18.5 | 29.5 | 42.9 | 59.2 | 78.5 | 100.8 | 126.3 |
| 12 | | 30.5 | 44.5 | 61.3 | 81.2 | 104.2 | 130.5 |
| $12\frac{1}{2}$ | | 31.6 | 46.0 | 63.3 | 83.9 | 107.7 | 134.8 |
| 13 | | 32.7 | 47.5 | 65.4 | 86.6 | 111.1 | 139.1 |
| $13\frac{1}{2}$ | | 33.7 | 49.1 | 67.5 | 89.4 | 114.6 | 143.3 |
| 14 | | | 50.6 | 69.6 | 92.1 | 118.0 | 147.6 |
| $14\frac{1}{2}$ | | | 52.1 | 71.7 | 94.8 | 121.5 | 151.8 |
| 15 | | | 53.7 | 73.8 | 97.5 | 124.9 | 156.1 |
| $15\frac{1}{2}$ | | | 55.2 | 75.9 | 100.3 | 128.4 | 160.4 |
| 16 | | | | 77.9 | 103.0 | 131.8 | 164.6 |
| $16\frac{1}{2}$ | | | | 80.0 | 105.7 | 135.3 | 168.9 |
| 17 | | | | 82.1 | 108.4 | 138.7 | 173.1 |
| $17\frac{1}{2}$ | | | | 84.2 | 111.2 | 142.2 | 177.4 |
| 18 | | | | | 113.9 | 145.6 | 181.7 |
| $18\frac{1}{2}$ | | | | | 116.6 | 149.1 | 185.9 |
| 19 | | | | | 119.3 | 152.5 | 190.2 |
| $19\frac{1}{2}$ | | | | | 122.1 | 156.0 | 194.4 |
| 20 | | | | | 124.8 | 159.4 | 198.7 |
| One inch in length of 100 Bolts. | 1.36 | 2.13 | 3.07 | 4.18 | 5.45 | 6.90 | 8.52 |
| To obtain Weights with Square Nuts per 100: Add | .23 | .41 | .66 | .99 | 1.42 | 1.96 | 2.62 |
| Weight of one Hexagon Nut..... | .0116 | .020 | .031 | .046 | .065 | .088 | .117 |
| Weight of one Hexagon Head..... | .0150 | .025 | .039 | .057 | .081 | .109 | .144 |
| Weight of one Square Nut..... | .0139 | .024 | .038 | .056 | .079 | .108 | .143 |
| Weight of one Square Head..... | .0173 | .029 | .045 | .066 | .093 | .126 | .167 |

All weights are approximate.

WEIGHTS OF 100 MACHINE BOLTS WITH SQUARE HEADS AND HEXAGON NUTS.

Franklin Institute Standard Sizes.

Basis—1 cubic foot Iron = 480 pounds.

| Length under Head to Point. Inches. | Diameter of Bolt in Inches. | | | | | | |
|--|-----------------------------|---------------|-------|----------------|----------------|----------------|----------------|
| | $\frac{3}{4}$ | $\frac{7}{8}$ | 1 | $1\frac{1}{8}$ | $1\frac{1}{2}$ | $1\frac{3}{4}$ | $1\frac{7}{8}$ |
| $1\frac{1}{2}$ | 64.5 | 95.2 | 134 | 182 | 240 | 309 | 390 |
| $1\frac{3}{4}$ | 67.6 | 99.4 | 140 | 189 | 248 | 319 | 402 |
| 2 | 70.6 | 103.5 | 145 | 196 | 257 | 329 | 414 |
| $2\frac{1}{4}$ | 73.7 | 107.7 | 150 | 203 | 265 | 340 | 426 |
| $2\frac{1}{2}$ | 76.8 | 111.9 | 156 | 210 | 274 | 350 | 439 |
| $2\frac{3}{4}$ | 79.8 | 116.1 | 161 | 216 | 282 | 360 | 451 |
| 3 | 82.9 | 120.2 | 167 | 223 | 291 | 371 | 463 |
| $3\frac{1}{4}$ | 86.0 | 124.4 | 172 | 230 | 300 | 381 | 475 |
| $3\frac{1}{2}$ | 89.1 | 128.6 | 178 | 237 | 308 | 391 | 488 |
| $3\frac{3}{4}$ | 92.1 | 132.8 | 183 | 244 | 317 | 402 | 500 |
| 4 | 95.2 | 136.9 | 189 | 251 | 325 | 412 | 512 |
| $4\frac{1}{4}$ | 101.3 | 145.3 | 199 | 265 | 342 | 432 | 537 |
| 5 | 107.4 | 153.6 | 210 | 279 | 359 | 453 | 561 |
| $5\frac{1}{2}$ | 113.6 | 162.0 | 221 | 292 | 376 | 474 | 586 |
| 6 | 119.7 | 170.3 | 232 | 306 | 393 | 494 | 610 |
| $6\frac{1}{4}$ | 125.9 | 178.7 | 243 | 320 | 410 | 515 | 635 |
| 7 | 132.0 | 187.0 | 254 | 334 | 427 | 536 | 659 |
| $7\frac{1}{2}$ | 138.1 | 195.4 | 265 | 348 | 444 | 556 | 684 |
| 8 | 144.3 | 203.7 | 276 | 361 | 461 | 577 | 709 |
| $8\frac{1}{4}$ | 150.4 | 212.1 | 287 | 375 | 478 | 597 | 733 |
| 9 | 156.5 | 220.4 | 298 | 389 | 495 | 618 | 758 |
| $9\frac{1}{2}$ | 162.7 | 228.8 | 308 | 402 | 513 | 639 | 782 |
| 10 | 168.8 | 237.1 | 319 | 417 | 530 | 659 | 807 |
| $10\frac{1}{4}$ | 174.9 | 245.5 | 330 | 430 | 547 | 680 | 831 |
| 11 | 181.1 | 253.8 | 341 | 444 | 564 | 701 | 856 |
| $11\frac{1}{4}$ | 187.2 | 262.2 | 352 | 458 | 581 | 721 | 880 |
| 12 | 193.3 | 270.5 | 363 | 472 | 598 | 742 | 905 |
| $12\frac{1}{4}$ | 199.5 | 278.9 | 374 | 486 | 615 | 762 | 929 |
| 13 | 205.6 | 287.2 | 385 | 499 | 632 | 783 | 954 |
| $13\frac{1}{4}$ | 211.7 | 295.6 | 396 | 513 | 649 | 804 | 978 |
| 14 | 217.9 | 303.9 | 407 | 527 | 666 | 824 | 1003 |
| $14\frac{1}{4}$ | 224.0 | 312.3 | 417 | 541 | 683 | 845 | 1027 |
| 15 | 230.1 | 320.6 | 428 | 555 | 700 | 866 | 1052 |
| $15\frac{1}{4}$ | 236.3 | 329.0 | 439 | 568 | 717 | 886 | 1077 |
| 16 | 242.4 | 337.3 | 450 | 582 | 734 | 907 | 1101 |
| $16\frac{1}{4}$ | 248.5 | 345.7 | 461 | 596 | 751 | 927 | 1126 |
| 17 | 254.7 | 354.0 | 472 | 610 | 768 | 948 | 1150 |
| $17\frac{1}{4}$ | 260.8 | 362.4 | 483 | 624 | 785 | 969 | 1175 |
| 18 | 266.9 | 370.7 | 494 | 637 | 802 | 989 | 1199 |
| $18\frac{1}{4}$ | 273.1 | 379.1 | 505 | 651 | 819 | 1010 | 1224 |
| 19 | 279.2 | 387.4 | 516 | 665 | 836 | 1031 | 1248 |
| $19\frac{1}{4}$ | 285.3 | 395.8 | 526 | 679 | 853 | 1051 | 1273 |
| 20 | 291.5 | 404.1 | 537 | 693 | 870 | 1072 | 1297 |
| One inch in length of 100 Bolts... | 12.27 | 16.70 | 21.82 | 27.61 | 34.09 | 41.25 | 49.09 |
| To obtain Weights with Square Nuts per 100: Add | 4.35 | 6.72 | 9.81 | 13.73 | 18.57 | 24.42 | 31.42 |
| Weight of one Hexagon Nut..... | .190 | .289 | .417 | .579 | .777 | 1.016 | 1.299 |
| Weight of one Hexagon Head..... | .235 | .357 | .516 | .616 | .962 | 1.259 | 1.611 |
| Weight of one Square Nut..... | .234 | .356 | .515 | .716 | .963 | 1.260 | 1.614 |
| Weight of one Square Head..... | .271 | .412 | .596 | .827 | 1.111 | 1.453 | 1.860 |

All weights are approximate.

WEIGHTS OF 100 MACHINE BOLTS WITH SQUARE HEADS AND NUTS.

WROUGHT IRON.

Manufacturers' Standard Sizes.

Basis—Hoopes & Townsend's List.

| Length under Head to Point. Inches. | Diameter of Bolt in Inches. | | | | | | | |
|---|-----------------------------|----------------|---------------|----------------|---------------|----------------|---------------|---------------|
| | $\frac{1}{4}$ | $\frac{5}{16}$ | $\frac{3}{8}$ | $\frac{7}{16}$ | $\frac{1}{2}$ | $\frac{9}{16}$ | $\frac{5}{8}$ | $\frac{3}{4}$ |
| $1\frac{1}{2}$ | 3.4 | 6.0 | 9.2 | 13.6 | 19.1 | 26.0 | 33.8 | 55.3 |
| 2 | 4.1 | 7.1 | 10.8 | 15.7 | 21.8 | 29.5 | 38.1 | 61.5 |
| $2\frac{1}{2}$ | 4.8 | 8.2 | 12.3 | 17.8 | 24.6 | 33.0 | 42.4 | 67.7 |
| 3 | 5.5 | 9.2 | 13.8 | 19.9 | 27.4 | 36.5 | 46.7 | 73.9 |
| $3\frac{1}{2}$ | 6.2 | 10.3 | 15.3 | 21.8 | 29.8 | 40.0 | 51.0 | 80.1 |
| 4 | 6.9 | 11.4 | 16.9 | 24.0 | 32.6 | 43.5 | 55.4 | 86.3 |
| $4\frac{1}{2}$ | 7.5 | 12.4 | 18.4 | 26.1 | 35.4 | 46.7 | 59.3 | 92.1 |
| 5 | 8.2 | 13.5 | 19.9 | 28.2 | 38.1 | 50.2 | 63.6 | 98.3 |
| $5\frac{1}{2}$ | 8.9 | 14.6 | 21.5 | 30.3 | 40.9 | 53.7 | 67.9 | 104.5 |
| 6 | 9.6 | 15.6 | 23.0 | 32.4 | 43.7 | 57.2 | 72.3 | 110.7 |
| $6\frac{1}{2}$ | 10.3 | 16.7 | 24.6 | 34.5 | 46.4 | 60.7 | 76.6 | 116.9 |
| 7 | 11.0 | 17.8 | 26.1 | 36.6 | 49.2 | 64.2 | 80.9 | 123.1 |
| $7\frac{1}{2}$ | 11.7 | 18.9 | 27.7 | 38.8 | 51.9 | 67.6 | 85.2 | 129.4 |
| 8 | 12.4 | 20.0 | 29.2 | 40.9 | 54.7 | 71.1 | 89.5 | 135.6 |
| 9 | 13.7 | 22.1 | 32.4 | 44.9 | 60.0 | 77.8 | 97.9 | 147.5 |
| 10 | 15.1 | 24.3 | 35.5 | 49.1 | 65.5 | 84.8 | 106.4 | 160.0 |
| 11 | 16.5 | 26.4 | 38.6 | 53.4 | 71.0 | 91.8 | 115.1 | 172.4 |
| 12 | 17.9 | 28.6 | 41.7 | 57.6 | 76.5 | 98.8 | 123.7 | 184.8 |
| 13 | 19.3 | 30.7 | 44.8 | 61.8 | 82.0 | 105.5 | 132.0 | 197.2 |
| 14 | 20.6 | 32.9 | 47.9 | 66.0 | 87.6 | 112.5 | 140.6 | 209.7 |
| 15 | 22.0 | 35.1 | 51.0 | 70.3 | 93.1 | 119.5 | 149.2 | 222.1 |
| 16 | 23.4 | 37.2 | 54.1 | 74.5 | 98.6 | 126.4 | 157.9 | 234.5 |
| 17 | 24.8 | 39.4 | 57.2 | 78.7 | 104.1 | 133.4 | 166.5 | 246.9 |
| 18 | 26.2 | 41.5 | 60.3 | 82.9 | 109.7 | 140.4 | 175.1 | 259.4 |
| 19 | 27.5 | 43.7 | 63.4 | 87.2 | 115.2 | 147.4 | 183.7 | 271.8 |
| 20 | 28.9 | 45.8 | 66.5 | 91.4 | 120.7 | 154.4 | 192.4 | 284.2 |
| 21 | 30.3 | 48.0 | 69.6 | 95.6 | 126.2 | 161.4 | 201.0 | 296.6 |
| 22 | 31.7 | 50.2 | 72.7 | 99.9 | 131.7 | 168.4 | 209.6 | 309.1 |
| 23 | 33.1 | 52.3 | 75.8 | 104.1 | 137.3 | 175.4 | 218.3 | 321.5 |
| 24 | 34.4 | 54.5 | 78.9 | 108.3 | 142.8 | 182.4 | 226.9 | 333.9 |
| 25 | 35.8 | 56.6 | 82.1 | 112.5 | 148.3 | 189.3 | 235.5 | 346.3 |

WEIGHTS OF 100 MACHINE BOLTS WITH SQUARE HEADS AND NUTS.

WROUGHT IRON.

Manufacturers' Standard Sizes.

Basis—Hoopes & Townsend's List.

| Length under Head to Point. Inches. | Diameter of Bolt in Inches. | | | | | | | |
|---|-----------------------------|-------|----------------|----------------|----------------|----------------|----------------|-------|
| | $\frac{7}{8}$ | 1 | $1\frac{1}{8}$ | $1\frac{1}{4}$ | $1\frac{3}{8}$ | $1\frac{1}{2}$ | $1\frac{3}{4}$ | 2 |
| $1\frac{1}{2}$ | 83.4 | | | | | | | |
| 2 | 91.8 | 129.0 | 184.5 | | | | | |
| $2\frac{1}{2}$ | 99.7 | 140.1 | 198.4 | 264.8 | | | | |
| 3 | 108.1 | 151.1 | 212.4 | 282.0 | 350 | 470 | | |
| $3\frac{1}{2}$ | 116.6 | 162.2 | 226.4 | 299.3 | 370 | 495 | | |
| 4 | 125.0 | 173.2 | 240.4 | 316.6 | 390 | 520 | 720 | |
| $4\frac{1}{2}$ | 132.9 | 182.7 | 253.3 | 332.6 | 410 | 525 | 753 | |
| 5 | 141.3 | 193.7 | 267.3 | 349.9 | 430 | 570 | 786 | 1180 |
| $5\frac{1}{2}$ | 149.8 | 204.8 | 281.2 | 367.1 | 450 | 595 | 820 | 1225 |
| 6 | 158.2 | 215.8 | 295.2 | 384.4 | 470 | 620 | 854 | 1270 |
| $6\frac{1}{2}$ | 166.7 | 226.9 | 309.2 | 401.6 | 490 | 645 | 888 | 1315 |
| 7 | 175.1 | 237.9 | 323.2 | 418.9 | 510 | 670 | 922 | 1316 |
| $7\frac{1}{2}$ | 183.6 | 248.9 | 337.2 | 436.2 | 530 | 695 | 956 | 1405 |
| 8 | 192.0 | 260.0 | 351.1 | 453.4 | 550 | 725 | 990 | 1450 |
| 9 | 208.3 | 281.3 | 377.0 | 486.7 | 590 | 775 | 1058 | 1540 |
| 10 | 225.2 | 303.3 | 404.9 | 521.2 | 630 | 825 | 1126 | 1630 |
| 11 | 242.2 | 325.5 | 432.9 | 555.8 | 670 | 875 | 1194 | 1720 |
| 12 | 259.1 | 347.6 | 460.8 | 590.3 | 710 | 925 | 1262 | 1810 |
| 13 | 276.0 | 369.6 | 488.8 | 624.8 | 751 | 975 | 1330 | 1900 |
| 14 | 292.9 | 391.7 | 516.7 | 659.3 | 793 | 1025 | 1398 | 1990 |
| 15 | 309.8 | 413.8 | 544.7 | 693.8 | 835 | 1075 | 1468 | 2080 |
| 16 | 326.7 | 435.9 | 572.7 | 728.3 | 877 | 1125 | 1536 | 2170 |
| 17 | 343.6 | 458.0 | 600.6 | 762.8 | 919 | 1175 | 1604 | 2260 |
| 18 | 360.5 | 480.1 | 628.6 | 797.4 | 961 | 1225 | 1672 | 2350 |
| 19 | 377.5 | 502.2 | 656.5 | 831.9 | 1003 | 1275 | 1740 | 2440 |
| 20 | 394.4 | 524.3 | 684.5 | 866.4 | 1045 | 1325 | 1808 | 2530 |
| 21 | 411.3 | 546.4 | 712.4 | 900.9 | 1087 | 1375 | 1876 | 2620 |
| 22 | 428.2 | 568.4 | 740.4 | 935.4 | 1129 | 1425 | 1944 | 2710 |
| 23 | 445.1 | 590.5 | 768.3 | 969.9 | 1171 | 1475 | 2012 | 2800 |
| 24 | 462.0 | 612.6 | 796.3 | 1004.5 | 1213 | 1525 | 2080 | 2890 |
| 25 | 478.9 | 634.7 | 824.3 | 1039.0 | 1255 | 1575 | 2148 | 2980 |

Bolts from $1\frac{1}{8}$ Inch to 2 Inches, inclusive, are fitted with nuts made to U. S. Standard.

WEIGHTS OF 100 ROUND-HEADED RIVETS OR ROUND-HEADED BOLTS WITHOUT NUTS.

WROUGHT IRON.

Basis—1 cubic foot Iron = 480 pounds.

| Length under Head to Point. | Diameter of Rivet in Inches. | | | | | | |
|----------------------------------|------------------------------|---------------|---------------|---------------|---------------|-------|----------------|
| | $\frac{3}{8}$ | $\frac{1}{2}$ | $\frac{5}{8}$ | $\frac{3}{4}$ | $\frac{7}{8}$ | 1 | $1\frac{1}{8}$ |
| Inches. | | | | | | | |
| 1 | 4.7 | 9.3 | 16.0 | 25.2 | 37.2 | 52.6 | 71.3 |
| $1\frac{1}{4}$ | 5.5 | 10.7 | 18.1 | 28.3 | 41.3 | 58.0 | 78.2 |
| $1\frac{1}{2}$ | 6.2 | 12.1 | 20.2 | 31.3 | 45.5 | 63.5 | 85.1 |
| $1\frac{3}{4}$ | 7.0 | 13.4 | 22.4 | 34.4 | 49.7 | 68.9 | 92.0 |
| 2 | 7.8 | 14.8 | 24.5 | 37.5 | 53.9 | 74.4 | 98.9 |
| $2\frac{1}{4}$ | 8.5 | 16.2 | 26.6 | 40.5 | 58.0 | 79.8 | 105.8 |
| $2\frac{1}{2}$ | 9.3 | 17.5 | 28.8 | 43.6 | 62.2 | 85.3 | 112.7 |
| $2\frac{3}{4}$ | 10.1 | 18.9 | 30.9 | 46.7 | 66.4 | 90.7 | 119.6 |
| 3 | 10.8 | 20.3 | 33.0 | 49.8 | 70.6 | 96.2 | 126.5 |
| $3\frac{1}{4}$ | 11.6 | 21.6 | 35.1 | 52.8 | 74.7 | 101.6 | 133.4 |
| $3\frac{1}{2}$ | 12.4 | 23.0 | 37.3 | 55.9 | 78.9 | 107.1 | 140.3 |
| $3\frac{3}{4}$ | 13.1 | 24.3 | 39.4 | 59.0 | 83.1 | 112.6 | 147.2 |
| 4 | 13.9 | 25.7 | 41.5 | 62.0 | 87.3 | 118.0 | 154.1 |
| $4\frac{1}{4}$ | 14.7 | 27.1 | 43.7 | 65.1 | 91.4 | 123.5 | 161.0 |
| $4\frac{1}{2}$ | 15.4 | 28.4 | 45.8 | 68.2 | 95.6 | 128.9 | 167.9 |
| $4\frac{3}{4}$ | 16.2 | 29.8 | 47.9 | 71.2 | 99.8 | 134.4 | 174.8 |
| 5 | 17.0 | 31.2 | 50.1 | 74.3 | 104.0 | 139.8 | 181.7 |
| $5\frac{1}{4}$ | 17.7 | 32.5 | 52.2 | 77.4 | 108.2 | 145.3 | 188.6 |
| $5\frac{1}{2}$ | 18.5 | 33.9 | 54.3 | 80.4 | 112.3 | 150.7 | 195.6 |
| $5\frac{3}{4}$ | 19.3 | 35.3 | 56.4 | 83.5 | 116.5 | 156.2 | 202.5 |
| 6 | 20.0 | 36.6 | 58.6 | 86.6 | 120.7 | 161.6 | 209.4 |
| $6\frac{1}{4}$ | 20.8 | 38.0 | 60.7 | 89.6 | 124.8 | 167.1 | 216.3 |
| $6\frac{1}{2}$ | 21.6 | 39.3 | 62.8 | 92.7 | 129.0 | 172.5 | 223.2 |
| $6\frac{3}{4}$ | 22.3 | 40.7 | 65.0 | 95.8 | 133.2 | 178.0 | 230.1 |
| 7 | 23.1 | 42.1 | 67.1 | 98.8 | 137.4 | 183.5 | 237.0 |
| $7\frac{1}{4}$ | 23.9 | 43.4 | 69.2 | 101.9 | 141.6 | 188.9 | 243.9 |
| $7\frac{1}{2}$ | 24.6 | 44.8 | 71.4 | 105.0 | 145.7 | 194.4 | 250.8 |
| $7\frac{3}{4}$ | 25.4 | 46.2 | 73.5 | 108.0 | 149.9 | 199.8 | 257.7 |
| 8 | 26.2 | 47.5 | 75.6 | 111.1 | 154.1 | 205.3 | 264.6 |
| $8\frac{1}{2}$ | 27.7 | 50.2 | 79.9 | 117.2 | 162.4 | 216.2 | 278.4 |
| 9 | 29.2 | 53.0 | 84.1 | 123.4 | 170.8 | 227.1 | 292.2 |
| $9\frac{1}{2}$ | 30.8 | 55.7 | 88.4 | 129.5 | 179.1 | 238.0 | 306.0 |
| 10 | 32.3 | 58.4 | 92.7 | 135.6 | 187.5 | 248.8 | 319.8 |
| $10\frac{1}{2}$ | 33.8 | 61.2 | 96.9 | 141.8 | 195.8 | 259.8 | 333.6 |
| 11 | 35.4 | 63.9 | 101.2 | 147.9 | 204.2 | 270.7 | 347.4 |
| $11\frac{1}{2}$ | 36.9 | 66.6 | 105.4 | 154.1 | 212.5 | 281.6 | 361.2 |
| 12 | 38.4 | 69.3 | 109.7 | 160.2 | 220.9 | 292.5 | 375.0 |
| One inch in length of 100 Rivets | 3.07 | 5.45 | 8.52 | 12.27 | 16.70 | 21.82 | 27.61 |
| Weight of 100 Rivet Heads..... | 1.78 | 4.82 | 9.95 | 16.12 | 24.29 | 34.77 | 47.67 |

WEIGHTS AND DIMENSIONS OF BOLT HEADS.

MANUFACTURERS' STANDARD SIZES.

Basis—Hoopes & Townsend's List.

| Diameter of Bolt. | Square. | | | | Hexagon. | | | |
|-------------------------|--------------------|-------------------|------------------|--------------------|--------------------|-------------------|------------------|--------------------|
| | Short Diameter. | Long Diameter. | Thickness. | Weight per 100. | Short Diameter. | Long Diameter. | Thickness. | Weight per 100. |
| Inches. | Inches. | Inches. | Inch. | Pounds. | Inches. | Inches. | Inches. | Pounds. |
| $\frac{1}{4}$ | $\frac{3}{8}$ | .530 | $\frac{3}{16}$ | .7 | $\frac{3}{8}$ | .433 | $\frac{3}{16}$ | .6 |
| $\frac{5}{16}$ | $\frac{11}{32}$ | .664 | $\frac{1}{8}$ | 1.4 | $\frac{11}{32}$ | .541 | $\frac{1}{8}$ | 1.2 |
| $\frac{3}{8}$ | $\frac{9}{16}$ | .795 | $\frac{9}{32}$ | 2.5 | $\frac{9}{16}$ | .670 | $\frac{9}{32}$ | 2.2 |
| $\frac{7}{16}$ | $\frac{21}{32}$ | .928 | $\frac{21}{64}$ | 4.0 | $\frac{21}{32}$ | .758 | $\frac{21}{64}$ | 3.4 |
| $\frac{1}{2}$ | $\frac{3}{4}$ | 1.061 | $\frac{3}{8}$ | 5.9 | $\frac{3}{4}$ | .866 | $\frac{3}{8}$ | 5.1 |
| $\frac{9}{16}$ | $\frac{27}{32}$ | 1.193 | $\frac{27}{64}$ | 8.4 | $\frac{27}{32}$ | .974 | $\frac{27}{64}$ | 7.3 |
| $\frac{5}{8}$ | $1\frac{1}{8}$ | 1.326 | $\frac{1}{2}$ | 11.5 | $1\frac{1}{8}$ | 1.083 | $\frac{1}{2}$ | 10.0 |
| $\frac{3}{4}$ | $1\frac{1}{2}$ | 1.591 | $\frac{9}{16}$ | 19.9 | $1\frac{1}{2}$ | 1.299 | $\frac{9}{16}$ | 17.3 |
| $\frac{7}{8}$ | $1\frac{5}{8}$ | 1.856 | $\frac{23}{32}$ | 31.1 | $1\frac{5}{8}$ | 1.516 | $\frac{23}{32}$ | 27.4 |
| 1 | $1\frac{1}{2}$ | 2.122 | $\frac{3}{4}$ | 47.3 | $1\frac{1}{2}$ | 1.733 | $\frac{3}{4}$ | 42.0 |
| $1\frac{1}{8}$ | $1\frac{11}{16}$ | 2.386 | $\frac{27}{32}$ | 67.3 | $1\frac{11}{16}$ | 1.944 | $\frac{27}{32}$ | 58.3 |
| $1\frac{1}{4}$ | $1\frac{7}{8}$ | 2.652 | $1\frac{1}{8}$ | 92.3 | $1\frac{7}{8}$ | 2.166 | $1\frac{1}{8}$ | 80.0 |
| $1\frac{3}{8}$ | $2\frac{1}{16}$ | 2.917 | $1\frac{1}{32}$ | 122.8 | $2\frac{1}{16}$ | 2.383 | $1\frac{1}{32}$ | 106.5 |
| $1\frac{1}{2}$ | $2\frac{1}{4}$ | 3.182 | $1\frac{1}{8}$ | 159.5 | $2\frac{1}{4}$ | 2.599 | $1\frac{1}{8}$ | 138.2 |
| $1\frac{5}{8}$ | $2\frac{7}{16}$ | 3.447 | $1\frac{7}{32}$ | 202.7 | $2\frac{7}{16}$ | 2.818 | $1\frac{7}{32}$ | 175.7 |
| $1\frac{3}{4}$ | $2\frac{5}{8}$ | 3.712 | $1\frac{5}{16}$ | 253.2 | $2\frac{5}{8}$ | 3.032 | $1\frac{5}{16}$ | 219.5 |
| $1\frac{7}{8}$ | $2\frac{11}{16}$ | 3.977 | $1\frac{11}{32}$ | 311.5 | $2\frac{11}{16}$ | 3.349 | $1\frac{11}{32}$ | 269.8 |
| 2 | 3 | 4.243 | $1\frac{1}{2}$ | 378.0 | 3 | 3.464 | $1\frac{1}{2}$ | 327.6 |

WEIGHTS AND DIMENSIONS OF HEXAGON NUTS.

MANUFACTURERS' STANDARD SIZES.

Basis—Hoopes & Townsend's List.

| Diameter of Bolt. | Short Diameter. | Long Diameter. | Thickness. | Diameter of Rough Hole. | Plain. | | Cupped. | |
|-------------------------|--------------------|-------------------|----------------|----------------------------------|--------------------|------------------|--------------------|------------------|
| | | | | | Weight per 100. | Number in 100 | Weight per 100. | Number in 100 |
| Inches. | Inches. | Inches. | Inches. | Inch. | Pounds. | Pounds. | Pounds. | Pounds. |
| $\frac{1}{4}$ | $\frac{1}{2}$ | .578 | $\frac{3}{4}$ | $\frac{7}{32}$ | 1.3 | 7800 | 1.2 | 8500 |
| $\frac{5}{16}$ | $\frac{2}{8}$ | .722 | $\frac{5}{16}$ | $\frac{9}{32}$ | 2.3 | 4440 | 2.1 | 4790 |
| $\frac{3}{8}$ | $\frac{3}{4}$ | .866 | $\frac{3}{8}$ | $\frac{11}{32}$ | 4.3 | 2330 | 4.0 | 2510 |
| $\frac{7}{16}$ | $\frac{7}{8}$ | 1.011 | $\frac{7}{16}$ | $\frac{13}{32}$ | 7.0 | 1430 | 6.3 | 1580 |
| $\frac{1}{2}$ | | 1.011 | $\frac{1}{2}$ | $\frac{7}{16}$ | 7.5 | 1330 | 6.9 | 1440 |
| $\frac{1}{2}$ | 1 | 1.155 | $\frac{1}{2}$ | $\frac{1}{2}$ | 9.9 | 1010 | 9.2 | 1090 |
| $\frac{1}{2}$ | 1 | 1.155 | $\frac{9}{16}$ | $\frac{1}{2}$ | 10.8 | 930 | 10.2 | 980 |
| $\frac{1}{2}$ | $1\frac{1}{8}$ | 1.299 | $\frac{9}{16}$ | $\frac{1}{2}$ | 13.7 | 730 | 12.5 | 800 |
| $\frac{1}{2}$ | $1\frac{1}{8}$ | 1.299 | $\frac{5}{8}$ | $\frac{9}{16}$ | 15.9 | 630 | 15.2 | 660 |
| $\frac{1}{2}$ | $1\frac{1}{8}$ | 1.299 | $\frac{3}{4}$ | $\frac{9}{16}$ | 17.9 | 560 | 17.0 | 588 |
| $\frac{1}{2}$ | $1\frac{1}{4}$ | 1.444 | $\frac{3}{4}$ | $\frac{9}{16}$ | 19.5 | 514 | 18.5 | 541 |
| $\frac{1}{2}$ | $1\frac{1}{4}$ | 1.444 | $\frac{3}{4}$ | $\frac{9}{16}$ | 23.0 | 435 | 21.7 | 460 |
| $\frac{1}{2}$ | $1\frac{1}{4}$ | 1.444 | $\frac{3}{4}$ | $\frac{21}{32}$ | 22.2 | 450 | 20.6 | 485 |
| $\frac{1}{2}$ | $1\frac{3}{8}$ | 1.588 | $\frac{3}{4}$ | $\frac{21}{32}$ | 26.6 | 376 | 25.4 | 394 |
| $\frac{1}{2}$ | $1\frac{3}{8}$ | 1.588 | $\frac{7}{8}$ | $\frac{21}{32}$ | 30.3 | 330 | 28.8 | 347 |
| $\frac{1}{2}$ | $1\frac{3}{8}$ | 1.733 | $\frac{3}{4}$ | $\frac{21}{32}$ | 34.5 | 290 | 32.3 | 310 |
| $\frac{1}{2}$ | $1\frac{1}{2}$ | 1.733 | $\frac{7}{8}$ | $\frac{21}{32}$ | 40.0 | 250 | 37.6 | 266 |
| $\frac{1}{2}$ | $1\frac{1}{2}$ | 1.733 | $\frac{7}{8}$ | $\frac{21}{32}$ | 37.7 | 265 | 35.3 | 283 |
| $\frac{1}{2}$ | $1\frac{1}{2}$ | 1.733 | 1 | $\frac{21}{32}$ | 45.9 | 218 | 43.5 | 230 |
| $\frac{1}{2}$ | $1\frac{5}{8}$ | 1.877 | $\frac{7}{8}$ | $\frac{21}{32}$ | 45.3 | 221 | 42.6 | 235 |
| $\frac{1}{2}$ | $1\frac{5}{8}$ | 1.877 | 1 | $\frac{21}{32}$ | 50.8 | 197 | 47.6 | 210 |
| $\frac{1}{2}$ | $1\frac{5}{8}$ | 2.021 | 1 | $\frac{21}{32}$ | 57.5 | 174 | 53.8 | 186 |
| 1 | $1\frac{3}{4}$ | 2.021 | $1\frac{1}{8}$ | $\frac{1}{2}$ | 63.7 | 157 | 59.5 | 168 |
| 1 | 2 | 2.309 | $1\frac{1}{4}$ | $\frac{1}{2}$ | 100.0 | 100 | 90.9 | 110 |
| $1\frac{1}{8}$ | $2\frac{1}{4}$ | 2.599 | $1\frac{3}{8}$ | $1\frac{1}{16}$ | 138.9 | 72 | 126.6 | 79 |
| $1\frac{1}{4}$ | $2\frac{1}{2}$ | 2.888 | $1\frac{1}{2}$ | $1\frac{1}{8}$ | 185.2 | 54 | 169.5 | 59 |
| $1\frac{3}{8}$ | $2\frac{3}{4}$ | 3.176 | $1\frac{5}{8}$ | $1\frac{1}{4}$ | 243.9 | 41 | 222.2 | 45 |
| $1\frac{1}{2}$ | 3 | 3.464 | $1\frac{3}{4}$ | $1\frac{1}{2}$ | 333.3 | 30 | 303.0 | 33 |
| $1\frac{3}{4}$ | $3\frac{1}{4}$ | 3.754 | $1\frac{7}{8}$ | $1\frac{1}{2}$ | 408.2 | $24\frac{1}{2}$ | 370.4 | 27 |
| $1\frac{1}{2}$ | $3\frac{1}{2}$ | 4.043 | 2 | $1\frac{1}{2}$ | 493.8 | $20\frac{1}{2}$ | 459.8 | $21\frac{1}{2}$ |
| 2 | $3\frac{3}{4}$ | 4.043 | 2 | $1\frac{3}{4}$ | 487.8 | $20\frac{1}{2}$ | 454.5 | 22 |
| 2 | $3\frac{1}{2}$ | 4.043 | $2\frac{1}{4}$ | $1\frac{3}{4}$ | 512.8 | 19 $\frac{1}{2}$ | 487.8 | $20\frac{1}{2}$ |

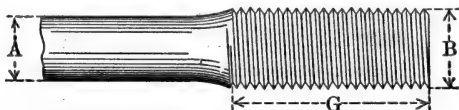
WEIGHTS AND DIMENSIONS OF SQUARE NUTS.

MANUFACTURERS' STANDARD SIZES.

Basis—Hoopes & Townsend's List.

| Diameter of Bolt. | Short Diameter. | Long Diameter. | Thickness. | Diameter of Rough Hole. | Plain. | | Cupped. | |
|-------------------------|--------------------|-------------------|----------------|----------------------------------|--------------------|------------------|--------------------|------------------|
| | | | | | Weight per 100. | Number in 100 | Weight per 100. | Number in 100 |
| Inches. | Inches. | Inches. | Inches. | Inch. | Pounds. | Pounds. | Pounds. | Pounds. |
| $\frac{1}{4}$ | $\frac{1}{2}$ | .707 | $\frac{1}{4}$ | $\frac{7}{32}$ | 1.5 | 6750 | 1.4 | 7200 |
| $\frac{5}{16}$ | $\frac{5}{8}$ | .884 | $\frac{5}{16}$ | $\frac{9}{32}$ | 2.8 | 3540 | 2.5 | 4000 |
| $\frac{3}{8}$ | $\frac{3}{4}$ | 1.061 | $\frac{3}{8}$ | $\frac{11}{32}$ | 4.8 | 2100 | 4.2 | 2380 |
| $\frac{7}{16}$ | $\frac{7}{8}$ | 1.237 | $\frac{7}{16}$ | $\frac{13}{32}$ | 7.5 | 1330 | 6.8 | 1460 |
| $\frac{1}{2}$ | $\frac{7}{8}$ | 1.237 | $\frac{1}{2}$ | $\frac{7}{16}$ | 8.9 | 1120 | 8.1 | 1230 |
| $\frac{1}{2}$ | 1 | 1.414 | $\frac{1}{2}$ | $\frac{7}{16}$ | 11.9 | 840 | 10.8 | 930 |
| $\frac{9}{16}$ | $1\frac{1}{8}$ | 1.591 | $\frac{9}{16}$ | $\frac{1}{2}$ | 15.4 | 650 | 14.3 | 700 |
| $\frac{5}{8}$ | $1\frac{1}{8}$ | 1.591 | $\frac{5}{8}$ | $\frac{9}{16}$ | 17.3 | 575 | 16.1 | 620 |
| $\frac{5}{8}$ | $1\frac{1}{4}$ | 1.768 | $\frac{5}{8}$ | $\frac{9}{16}$ | 23.0 | 435 | 21.1 | 475 |
| $\frac{3}{4}$ | $1\frac{1}{4}$ | 1.768 | $\frac{3}{4}$ | $\frac{21}{32}$ | 27.8 | 360 | 25.0 | 400 |
| $\frac{3}{4}$ | $1\frac{3}{8}$ | 1.945 | $\frac{3}{4}$ | $\frac{21}{32}$ | 31.7 | 315 | 29.0 | 345 |
| $\frac{3}{4}$ | $1\frac{1}{2}$ | 2.122 | $\frac{3}{4}$ | $\frac{21}{32}$ | 41.0 | 244 | 37.0 | 270 |
| $\frac{7}{8}$ | $1\frac{1}{2}$ | 2.122 | $\frac{7}{8}$ | $\frac{23}{32}$ | 46.5 | 215 | 41.7 | 240 |
| $\frac{7}{8}$ | $1\frac{5}{8}$ | 2.298 | $\frac{7}{8}$ | $\frac{23}{32}$ | 55.6 | 180 | 48.8 | 205 |
| $\frac{7}{8}$ | $1\frac{3}{4}$ | 2.475 | $\frac{7}{8}$ | $\frac{23}{32}$ | 61.3 | 163 | 54.6 | 183 |
| 1 | $1\frac{3}{4}$ | 2.475 | 1 | $\frac{7}{8}$ | 70.9 | 141 | 64.1 | 156 |
| 1 | 2 | 2.828 | 1 | $\frac{7}{8}$ | 95.2 | 105 | 87.0 | 115 |
| $1\frac{1}{8}$ | 2 | 2.828 | $1\frac{1}{8}$ | $\frac{15}{16}$ | 102.0 | 98 | 94.3 | 106 |
| $1\frac{1}{8}$ | $2\frac{1}{4}$ | 3.182 | $1\frac{1}{8}$ | $\frac{15}{16}$ | 135.1 | 74 | 123.5 | 81 |
| $1\frac{1}{2}$ | $2\frac{1}{4}$ | 3.182 | $1\frac{1}{2}$ | $1\frac{1}{16}$ | 156.3 | 64 | 142.9 | 70 |
| $1\frac{1}{2}$ | $2\frac{1}{2}$ | 3.536 | $1\frac{1}{2}$ | $1\frac{1}{16}$ | 192.3 | 52 | 175.4 | 57 |
| $1\frac{3}{8}$ | $2\frac{3}{4}$ | 3.889 | $1\frac{3}{8}$ | $1\frac{3}{16}$ | 250.0 | 40 | 227.3 | 44 |
| $1\frac{1}{2}$ | 3 | 4.243 | $1\frac{1}{2}$ | $1\frac{5}{16}$ | 307.7 | 32 $\frac{1}{2}$ | 285.7 | 35 |
| $1\frac{5}{8}$ | $3\frac{1}{4}$ | 4.597 | $1\frac{5}{8}$ | $1\frac{7}{16}$ | 454.5 | 22 | 400.0 | 25 |
| $1\frac{3}{4}$ | $3\frac{1}{2}$ | 4.950 | $1\frac{3}{4}$ | $1\frac{9}{16}$ | 555.6 | 18 | 500.0 | 20 |
| $1\frac{7}{8}$ | $3\frac{3}{4}$ | 5.303 | $1\frac{7}{8}$ | $1\frac{11}{16}$ | 666.7 | 15 | 625.0 | 16 |
| 2 | 4 | 5.657 | 2 | $1\frac{13}{16}$ | 816.3 | 12 $\frac{1}{4}$ | 784.3 | 12 $\frac{1}{2}$ |

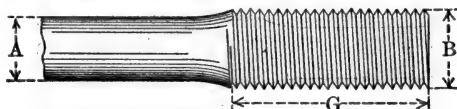
UPSET SCREW ENDS FOR ROUND BARS.



| Diameter of Bar. | Area of Body of Bar. | Diameter of Screw. | Length of Upset. | Area at Root of Thread. | Number of Threads per Inch. | Weight per Foot of Bar. | Add for Upset. | Excess of Area at Root of Thread Over that of Body of Bar. |
|------------------|----------------------|--------------------|------------------|-------------------------|-----------------------------|-------------------------|----------------|--|
| A | | B | G | | | | | |
| Inch. | Sq. Ins. | Inches. | Inches. | Sq. Ins. | | Pounds. | Inches. | Per Cent. |
| $\frac{1}{2}$ | .196 | $\frac{3}{4}$ | $4\frac{1}{2}$ | .302 | 10 | .668 | $6\frac{1}{2}$ | 54 |
| $\frac{5}{16}$ | .249 | $\frac{3}{4}$ | $4\frac{1}{2}$ | .302 | 10 | .845 | $4\frac{1}{2}$ | 21 |
| $\frac{3}{8}$ | .307 | $\frac{3}{4}$ | $4\frac{1}{2}$ | .420 | 9 | 1.043 | $5\frac{1}{2}$ | 37 |
| $\frac{1}{2}$ | .371 | 1 | $4\frac{1}{2}$ | .550 | 8 | 1.262 | $6\frac{1}{2}$ | 48 |
| $\frac{3}{4}$ | .442 | 1 | $4\frac{1}{2}$ | .550 | 8 | 1.502 | $4\frac{1}{2}$ | 25 |
| $\frac{7}{8}$ | .519 | $1\frac{1}{8}$ | $4\frac{1}{2}$ | .694 | 7 | 1.763 | $5\frac{1}{2}$ | 34 |
| $\frac{1}{2}$ | .601 | $1\frac{1}{8}$ | $4\frac{1}{2}$ | .893 | 7 | 2.044 | $6\frac{1}{2}$ | 49 |
| $\frac{3}{4}$ | .690 | $1\frac{1}{8}$ | $4\frac{1}{2}$ | .893 | 7 | 2.347 | $4\frac{1}{2}$ | 29 |
| 1 | .785 | $1\frac{3}{8}$ | 5 | 1.057 | 6 | 2.670 | $5\frac{1}{2}$ | 35 |
| $1\frac{1}{8}$ | .887 | $1\frac{3}{8}$ | 5 | 1.057 | 6 | 3.014 | $4\frac{1}{2}$ | 19 |
| $1\frac{1}{4}$ | .994 | $1\frac{3}{8}$ | 5 | 1.295 | 6 | 3.379 | $4\frac{1}{2}$ | 30 |
| $1\frac{3}{8}$ | 1.108 | $1\frac{3}{8}$ | 5 | 1.295 | 6 | 3.766 | $3\frac{1}{2}$ | 17 |
| $1\frac{1}{2}$ | 1.227 | $1\frac{3}{4}$ | $5\frac{1}{2}$ | 1.515 | $5\frac{1}{2}$ | 4.173 | $4\frac{1}{2}$ | 23 |
| $1\frac{5}{8}$ | 1.353 | $1\frac{3}{4}$ | $5\frac{1}{2}$ | 1.744 | 5 | 4.600 | 5 | 29 |
| $1\frac{3}{4}$ | 1.485 | $1\frac{3}{4}$ | $5\frac{1}{2}$ | 1.744 | 5 | 5.049 | 4 | 18 |
| $1\frac{7}{8}$ | 1.623 | $1\frac{3}{4}$ | $5\frac{1}{2}$ | 2.048 | 5 | 5.518 | $4\frac{1}{2}$ | 26 |
| $1\frac{1}{2}$ | 1.767 | 2 | $5\frac{1}{2}$ | 2.302 | $4\frac{1}{2}$ | 6.008 | $5\frac{1}{2}$ | 30 |
| $1\frac{9}{16}$ | 1.918 | 2 | $5\frac{1}{2}$ | 2.302 | $4\frac{1}{2}$ | 6.520 | $4\frac{1}{2}$ | 20 |
| $1\frac{5}{8}$ | 2.074 | $2\frac{1}{8}$ | $5\frac{1}{2}$ | 2.650 | $4\frac{1}{2}$ | 7.051 | 5 | 28 |
| $1\frac{11}{16}$ | 2.237 | $2\frac{1}{8}$ | $5\frac{1}{2}$ | 2.650 | $4\frac{1}{2}$ | 7.604 | $4\frac{1}{2}$ | 18 |
| $1\frac{3}{4}$ | 2.405 | $2\frac{1}{4}$ | $5\frac{1}{2}$ | 3.023 | $4\frac{1}{2}$ | 8.178 | $4\frac{1}{2}$ | 26 |
| $1\frac{7}{8}$ | 2.580 | $2\frac{1}{4}$ | $5\frac{1}{2}$ | 3.023 | $4\frac{1}{2}$ | 8.773 | 4 | 17 |
| $1\frac{15}{16}$ | 2.761 | $2\frac{3}{8}$ | 6 | 3.419 | $4\frac{1}{2}$ | 9.388 | $4\frac{1}{2}$ | 24 |
| $1\frac{1}{2}$ | 2.948 | $2\frac{3}{8}$ | 6 | 3.715 | 4 | 10.020 | 5 | 26 |

Lengths of Upset Ends above are best adapted for use with Turnbuckles of standard length, six inches between heads, as shown on page 378, and with Clevises shown on page 380. Lengths of Upset Ends for use with ordinary Right and Left Nuts, shown on page 379 may be one inch shorter than above.

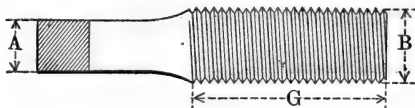
UPSET SCREW ENDS FOR ROUND BARS.



| Diameter of Bar. | Area of Body of Bar. | Diameter of Screw. | Length of Upset. | Area at Root of Thread. | Number of Threads per Inch. | Weight per Foot of Bar. | Add for Upset. | Excess of Area at Root of Thread Over that of Body of Bar. |
|------------------|----------------------|--------------------|------------------|-------------------------|-----------------------------|-------------------------|----------------|--|
| A | B | G | | | | | | |
| Inches. | Sq. Ins. | Inches. | Inches. | Sq. Ins. | | Pounds. | Inches. | Per Cent. |
| 2 | 3.142 | 2½ | 6 | 3.715 | 4 | 10.68 | 4¼ | 18 |
| 2⅛ | 3.341 | 2⅝ | 6½ | 4.155 | 4 | 11.36 | 4¾ | 24 |
| 2¼ | 3.547 | 2⅞ | 6½ | 4.155 | 4 | 12.06 | 4 | 17 |
| 2½ | 3.758 | 2¾ | 6½ | 4.619 | 4 | 12.78 | 4½ | 23 |
| 2¾ | 3.976 | 2⅞ | 6½ | 5.108 | 4 | 13.52 | 5¼ | 28 |
| 2⅞ | 4.200 | 2⅞ | 6½ | 5.108 | 4 | 14.28 | 4½ | 22 |
| 3 | 4.430 | 3 | 6½ | 5.428 | 3½ | 15.07 | 4¾ | 23 |
| 3⅛ | 4.666 | 3½ | 6½ | 5.957 | 3½ | 15.86 | 5½ | 28 |
| 3¼ | 4.909 | 3½ | 6¾ | 5.957 | 3½ | 16.69 | 4¾ | 21 |
| 3½ | 5.157 | 3½ | 6¾ | 6.510 | 3½ | 17.53 | 5¼ | 26 |
| 3¾ | 5.412 | 3½ | 6¾ | 6.510 | 3½ | 18.40 | 4½ | 20 |
| 4 | 5.673 | 3¾ | 7 | 7.087 | 3½ | 19.29 | 5 | 25 |
| 4¼ | 5.940 | 3¾ | 7 | 7.087 | 3½ | 20.20 | 4½ | 19 |
| 4½ | 6.213 | 3¾ | 7 | 7.548 | 3½ | 21.12 | 4¾ | 22 |
| 4¾ | 6.492 | 3¾ | 7½ | 8.171 | 3½ | 22.07 | 5¼ | 26 |
| 5 | 6.777 | 3¾ | 7½ | 8.171 | 3½ | 23.04 | 4¾ | 21 |
| 5¼ | 7.069 | 3¾ | 7½ | 8.641 | 3 | 24.03 | 5 | 22 |
| 5½ | 7.670 | 3¾ | 7½ | 9.305 | 3 | 26.08 | 5¼ | 21 |
| 5¾ | 8.296 | 4 | 7½ | 9.993 | 3 | 28.20 | 4¾ | 20 |
| 6 | 8.946 | 4½ | 7½ | 10.706 | 3 | 30.42 | 4¾ | 20 |
| 6¼ | 9.621 | 4½ | 8 | 11.329 | 2⅞ | 32.71 | 4½ | 18 |
| 6½ | 10.321 | 4½ | 8 | 12.743 | 2¾ | 35.09 | 5¼ | 23 |
| 6¾ | 11.045 | 4½ | 8½ | 13.544 | 2¾ | 37.56 | 5¼ | 23 |
| 7 | 11.793 | 4½ | 8½ | 14.220 | 2⅝ | 40.10 | 5 | 21 |
| 4 | 12.566 | 5 | 8½ | 15.763 | 2½ | 42.73 | 5¼ | 25 |

Lengths of Upset Ends above are best adapted for use with Turnbuckles of standard length, six inches between heads, as shown on page 378, and with Clevises shown on page 380. Lengths of Upset Ends for use with ordinary Right and Left Nuts, shown on page 379, may be one inch shorter than above.

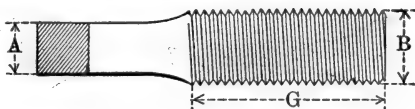
UPSET SCREW ENDS FOR SQUARE BARS.



| Side of Square Bar. | Area of Body of Bar. | Diameter of Screw. | Length of Upset. | Area at Root of Thread. | Number of Threads per Inch. | Weight per Foot of Bar. | Add for Upset. | Excess of Area at Root of Thread Over that of Body of Bar. |
|---------------------|----------------------|--------------------|------------------|-------------------------|-----------------------------|-------------------------|----------------|--|
| A | B | G | | | | | | |
| Inch. | Sq. Ins. | Inches. | Inches. | Sq. Ins. | | Pounds. | Inches. | Per Cent. |
| $\frac{1}{2}$ | .250 | $\frac{3}{4}$ | $4\frac{1}{4}$ | .302 | 10 | .850 | 4 | 21 |
| $\frac{9}{16}$ | .316 | $\frac{7}{8}$ | $4\frac{1}{2}$ | .420 | 9 | 1.076 | 5 | 33 |
| $\frac{5}{8}$ | .391 | 1 | $4\frac{1}{2}$ | .550 | 8 | 1.328 | $5\frac{3}{4}$ | 41 |
| $\frac{11}{16}$ | .473 | 1 | $4\frac{1}{2}$ | .550 | 8 | 1.607 | $3\frac{3}{4}$ | 17 |
| $\frac{3}{4}$ | .563 | $1\frac{1}{8}$ | $4\frac{3}{4}$ | .694 | 7 | 1.913 | $4\frac{1}{2}$ | 23 |
| $\frac{13}{16}$ | .660 | $1\frac{1}{4}$ | $4\frac{3}{4}$ | .893 | 7 | 2.245 | 5 | 35 |
| $\frac{7}{8}$ | .766 | $1\frac{3}{8}$ | 5 | 1.057 | 6 | 2.603 | $5\frac{3}{4}$ | 38 |
| $\frac{15}{16}$ | .879 | $1\frac{3}{8}$ | 5 | 1.057 | 6 | 2.989 | $4\frac{1}{4}$ | 20 |
| 1 | 1.000 | $1\frac{1}{2}$ | 5 | 1.295 | 6 | 3.400 | $4\frac{3}{4}$ | 29 |
| $1\frac{1}{16}$ | 1.129 | $1\frac{5}{8}$ | $5\frac{1}{4}$ | 1.515 | $5\frac{1}{2}$ | 3.838 | $5\frac{1}{4}$ | 34 |
| $1\frac{1}{8}$ | 1.266 | $1\frac{5}{8}$ | $5\frac{1}{4}$ | 1.515 | $5\frac{1}{2}$ | 4.303 | $4\frac{1}{4}$ | 20 |
| $1\frac{3}{16}$ | 1.410 | $1\frac{3}{4}$ | $5\frac{1}{4}$ | 1.744 | 5 | 4.795 | $4\frac{3}{4}$ | 24 |
| $1\frac{1}{4}$ | 1.563 | $1\frac{7}{8}$ | $5\frac{1}{2}$ | 2.048 | 5 | 5.312 | $5\frac{1}{4}$ | 31 |
| $1\frac{5}{16}$ | 1.723 | $1\frac{7}{8}$ | $5\frac{1}{2}$ | 2.048 | 5 | 5.851 | $4\frac{1}{4}$ | 19 |
| $1\frac{3}{8}$ | 1.891 | 2 | $5\frac{1}{2}$ | 2.302 | $4\frac{1}{2}$ | 6.428 | $4\frac{1}{4}$ | 22 |
| $1\frac{7}{16}$ | 2.066 | $2\frac{1}{8}$ | $5\frac{3}{4}$ | 2.650 | $4\frac{1}{2}$ | 7.026 | $5\frac{1}{4}$ | 28 |
| $1\frac{1}{2}$ | 2.250 | $2\frac{1}{8}$ | $5\frac{3}{4}$ | 2.650 | $4\frac{1}{2}$ | 7.650 | $4\frac{1}{4}$ | 18 |
| $1\frac{9}{16}$ | 2.441 | $2\frac{1}{4}$ | $5\frac{3}{4}$ | 3.023 | $4\frac{1}{2}$ | 8.300 | $4\frac{1}{2}$ | 24 |
| $1\frac{5}{8}$ | 2.641 | $2\frac{3}{8}$ | 6 | 3.419 | $4\frac{1}{2}$ | 8.978 | 5 | 30 |
| $1\frac{11}{16}$ | 2.848 | $2\frac{3}{8}$ | 6 | 3.419 | $4\frac{1}{2}$ | 9.682 | $4\frac{1}{4}$ | 20 |
| $1\frac{3}{4}$ | 3.063 | $2\frac{1}{2}$ | 6 | 3.715 | 4 | 10.410 | $4\frac{1}{2}$ | 21 |
| $1\frac{13}{16}$ | 3.285 | $2\frac{5}{8}$ | $6\frac{1}{4}$ | 4.155 | 4 | 11.170 | 5 | 26 |
| $1\frac{7}{8}$ | 3.516 | $2\frac{5}{8}$ | $6\frac{1}{4}$ | 4.155 | 4 | 11.950 | $4\frac{1}{4}$ | 18 |
| $1\frac{15}{16}$ | 3.754 | $2\frac{3}{4}$ | $6\frac{1}{4}$ | 4.619 | 4 | 12.760 | $4\frac{1}{2}$ | 23 |

Lengths of Upset Ends above are best adapted for use with Turnbuckles of standard length, six inches between heads, as shown on page 378, and with Clevises shown on page 380. Lengths of Upset Ends for use with ordinary Right and Left Nuts, shown on page 379, may be one inch shorter than above.

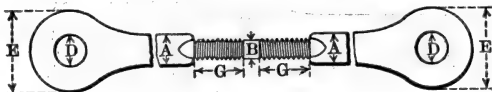
UPSET SCREW ENDS FOR SQUARE BARS.



| Side of Square Bar. | Area of Body of Bar. | Diameter of Screw. | Length of Upset. | Area at Root of Thread. | Number of Threads per Inch. | Weight per Foot of Bar. | Add for Upset. | Excess of Area at Root of Thread Over that of Body of Bar. |
|---------------------|----------------------|--------------------|------------------|-------------------------|-----------------------------|-------------------------|----------------|--|
| A | B | G | | | | | | |
| Inches. | Sq. Ins. | Inches. | Inches. | Sq. Ins. | | Pounds. | Inches. | Per Cent. |
| 2 | 4.000 | $2\frac{7}{8}$ | $6\frac{1}{2}$ | 5.108 | 4 | 13.60 | 5 | 28 |
| $2\frac{1}{16}$ | 4.254 | $2\frac{7}{8}$ | $6\frac{1}{2}$ | 5.108 | 4 | 14.46 | $4\frac{1}{4}$ | 20 |
| $2\frac{1}{8}$ | 4.516 | 3 | $6\frac{1}{2}$ | 5.428 | $3\frac{1}{2}$ | 15.35 | $4\frac{1}{2}$ | 20 |
| $2\frac{3}{16}$ | 4.785 | $3\frac{1}{8}$ | $6\frac{3}{4}$ | 5.957 | $3\frac{1}{2}$ | 16.27 | 5 | 24 |
| $2\frac{1}{4}$ | 5.063 | $3\frac{1}{8}$ | $6\frac{3}{4}$ | 5.957 | $3\frac{1}{2}$ | 17.22 | $4\frac{1}{4}$ | 18 |
| $2\frac{5}{16}$ | 5.348 | $3\frac{1}{4}$ | $6\frac{3}{4}$ | 6.510 | $3\frac{1}{2}$ | 18.19 | $4\frac{3}{4}$ | 22 |
| $2\frac{3}{8}$ | 5.641 | $3\frac{3}{8}$ | 7 | 7.087 | $3\frac{1}{2}$ | 19.18 | $5\frac{1}{4}$ | 26 |
| $2\frac{7}{16}$ | 5.941 | $3\frac{3}{8}$ | 7 | 7.087 | $3\frac{1}{2}$ | 20.20 | $4\frac{1}{2}$ | 19 |
| $2\frac{1}{2}$ | 6.250 | $3\frac{1}{2}$ | 7 | 7.548 | $3\frac{1}{4}$ | 21.25 | $4\frac{3}{4}$ | 21 |
| $2\frac{9}{16}$ | 6.566 | $3\frac{5}{8}$ | $7\frac{1}{4}$ | 8.171 | $3\frac{1}{4}$ | 22.33 | $5\frac{1}{4}$ | 24 |
| $2\frac{5}{8}$ | 6.891 | $3\frac{5}{8}$ | $7\frac{1}{4}$ | 8.171 | $3\frac{1}{4}$ | 23.43 | $4\frac{1}{2}$ | 19 |
| $2\frac{11}{16}$ | 7.223 | $3\frac{3}{4}$ | $7\frac{1}{4}$ | 8.641 | 3 | 24.56 | $4\frac{3}{4}$ | 20 |
| $2\frac{3}{4}$ | 7.563 | $3\frac{7}{8}$ | $7\frac{1}{2}$ | 9.305 | 3 | 25.71 | $5\frac{1}{4}$ | 23 |
| $2\frac{7}{8}$ | 7.910 | $3\frac{7}{8}$ | $7\frac{1}{2}$ | 9.305 | 3 | 26.90 | $4\frac{3}{4}$ | 18 |
| $2\frac{15}{16}$ | 8.266 | 4 | $7\frac{1}{2}$ | 9.993 | 3 | 28.10 | $4\frac{3}{4}$ | 21 |
| $2\frac{1}{2}$ | 8.629 | $4\frac{1}{8}$ | $7\frac{1}{2}$ | 10.706 | 3 | 29.34 | 5 | 24 |
| 3 | 9.000 | $4\frac{1}{8}$ | $7\frac{3}{4}$ | 10.706 | 3 | 30.60 | $4\frac{1}{2}$ | 19 |
| $3\frac{1}{8}$ | 9.766 | $4\frac{3}{8}$ | 8 | 12.087 | $2\frac{7}{8}$ | 33.20 | $5\frac{1}{4}$ | 24 |
| $3\frac{1}{4}$ | 10.563 | $4\frac{1}{2}$ | 8 | 12.743 | $2\frac{1}{2}$ | 35.92 | 5 | 21 |
| $3\frac{3}{8}$ | 11.391 | $4\frac{5}{8}$ | $8\frac{1}{4}$ | 13.544 | $2\frac{1}{4}$ | 38.73 | 5 | 19 |
| $3\frac{1}{2}$ | 12.250 | $4\frac{7}{8}$ | $8\frac{1}{2}$ | 15.068 | $2\frac{5}{8}$ | 41.65 | $5\frac{1}{2}$ | 23 |
| $3\frac{3}{4}$ | 13.141 | 5 | $8\frac{1}{2}$ | 15.763 | $2\frac{1}{2}$ | 44.68 | $5\frac{1}{4}$ | 20 |
| $3\frac{7}{8}$ | 14.063 | $5\frac{1}{8}$ | $8\frac{3}{4}$ | 16.658 | $2\frac{1}{2}$ | 47.82 | 5 | 18 |
| $3\frac{15}{16}$ | 15.016 | $5\frac{1}{4}$ | $8\frac{3}{4}$ | 17.572 | $2\frac{1}{2}$ | 51.05 | $4\frac{3}{4}$ | 17 |
| 4 | 16.000 | $5\frac{1}{2}$ | 9 | 19.267 | $2\frac{3}{8}$ | 54.40 | $5\frac{1}{4}$ | 20 |

Lengths of Upset Ends above are best adapted for use with Turnbuckles of standard length, six inches between heads, as shown on page 378, and with Clevises shown on page 380. Lengths of Upset Ends for use with ordinary Right and Left Nuts, shown on page 379, may be one inch shorter than above.

UPSET SCREW ENDS FOR FLAT BARS.



| Width of Bar. | Thickness of Bar. | Diameter of Upset. | Area of Bar. | Area at Root of Thread. | Length of Upset. | Add for Upset. |
|---------------|-------------------|--------------------|--------------|-------------------------|------------------|----------------|
| A | T | B | | | G | |
| Inches. | Inch. | Inches. | Sq. Inches. | Sq. Inches. | Inches. | Inches. |
| 2 | 1 | 2 | 2.00 | 2.30 | 5½ | 6 |
| 3 | ¾ | 2½ | 2.63 | 3.023 | 6½ | 11½ |
| 3 | 1 | 2½ | 3.00 | 3.719 | 6½ | 11½ |
| 3 | 1½ | 2½ | 3.38 | 4.159 | 7 | 11½ |
| 3 | 1½ | 2½ | 3.75 | 4.62 | 7 | 11 |
| 3 | 1½ | 2½ | 4.13 | 4.92 | 7 | 10 |
| 3 | 1½ | 3 | 4.50 | 5.43 | 7 | 10 |
| 4 | ¾ | 2½ | 3.00 | 3.719 | 6½ | 12½ |
| 4 | ¾ | 2½ | 3.50 | 4.159 | 7 | 12 |
| 4 | 1 | 2½ | 4.00 | 4.62 | 7 | 11 |
| 4 | 1½ | 3 | 4.50 | 5.43 | 7 | 11 |
| 4 | 1½ | 3½ | 5.00 | 6.51 | 7½ | 11 |
| 4 | 1½ | 3½ | 5.50 | 6.51 | 7½ | 11 |
| 4 | 1½ | 3½ | 6.00 | 7.54 | 7½ | 10 |
| 4 | 1½ | 3½ | 6.50 | 7.54 | 7½ | 10 |
| 4 | 1½ | 3½ | 7.00 | 8.64 | 7½ | 9½ |
| 5 | ¾ | 2½ | 3.75 | 4.62 | 7 | 11 |
| 5 | ¾ | 3 | 4.38 | 5.43 | 7 | 11 |
| 5 | 1 | 3½ | 5.00 | 6.51 | 7½ | 10½ |
| 5 | 1½ | 3½ | 5.63 | 6.51 | 7½ | 10½ |
| 5 | 1½ | 3½ | 6.25 | 7.55 | 7½ | 9½ |
| 5 | 1½ | 3½ | 6.88 | 8.64 | 7½ | 9½ |
| 5 | 1½ | 3½ | 7.50 | 8.64 | 7½ | 9½ |
| 5 | 1½ | .. | 8.13 | 9.99 | .. | .. |
| 5 | 1½ | .. | 8.75 | 9.99 | .. | .. |
| 6 | 1½ | 3½ | 6.75 | 8.64 | 7½ | 10 |
| 6 | 1½ | 3½ | 7.50 | 8.64 | 7½ | 9 |
| 6 | 1½ | .. | 8.25 | 9.99 | .. | .. |
| 6 | 1½ | .. | 9.00 | 9.99 | .. | .. |

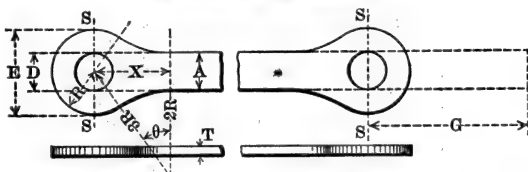
For dimensions of heads corresponding to different-sized pins, see table of Eye Bars on page 377.

Shortest length of bar permissible on account of method of manufacture is 6' 0" center to end.

The above length is used only for bars having heads 12½" diameter or less.

When possible lengths of 7' 0" are preferred.

STEEL EYE BARS.



A_s = Area of Excess to form one Head = Plane Area of Head - AX .

$$A_s = \frac{(180 + 2\theta)}{360} \pi R^2 + \left(4R^2 - \frac{A^2}{4}\right) \tan \theta - .0698 R^2 \theta.$$

$$\cos \theta = \frac{2R + \frac{A}{2}}{3R}.$$

$$G = \frac{5A_s}{4A}.$$

$$\text{Log. } \frac{\pi}{360} = 7.940848 - 10.$$

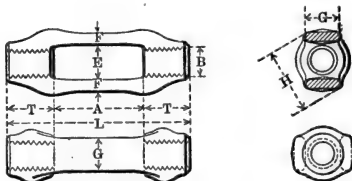
$$.0698 = 8.843855 - 10.$$

| Width of Body of Bar. | Minimum Thickness. | Diameter of Head. | Diameter of Largest Pin Hole. | Sectional Area of the Head on Line S-S in Excess of that in Body of Bar. | Additional Length of Bar Beyond Center of Eye Required to Form One Head. |
|-----------------------|--------------------|-------------------|-------------------------------|--|--|
| A | T | E | D | | G |
| Inches. | Inch. | Inches. | Inches. | | Inches. |
| 2 | .. | 4½ | 1½ | 33% | 7½ |
| 2 | .. | 5½ | 2½ | " | 12½ |
| 2½ | .. | 5½ | 2½ | " | 9½ |
| 2½ | .. | 6½ | 3½ | " | 13½ |
| 3 | .. | 6½ | 2½ | " | 10½ |
| 3 | .. | 8 | 4 | " | 17½ |
| 3 | .. | 9 | 5 | " | 22½ |
| 4 | .. | 9½ | 4½ | " | 17½ |
| 4 | .. | 10½ | 5½ | " | 21 |
| 4 | .. | 11½ | 6½ | " | 27½ |
| 5 | .. | 11½ | 4½ | 37% | 20 |
| 5 | .. | 12½ | 5½ | " | 24 |
| 5 | 1 | 13 | 6½ | " | 27½ |
| 5 | 1 | 14 | 7½ | " | 32 |
| 6 | 1 | 13½ | 5½ | " | 21½ |
| 6 | 1 | 14½ | 6½ | " | 27 |
| 6 | 1 | 15½ | 7½ | " | 31½ |
| 7 | 1½ | 15½ | 5½ | 40% | 26 |
| 7 | 1½ | 17 | 7½ | " | 32 |
| 8 | 1 | 17 | 5½ | " | 25½ |
| 8 | 1 | 18 | 6½ | " | 30½ |
| 8 | 1 | 19 | 8 | " | 35 |
| 9 | 1½ | 19½ | 7 | " | 32½ |
| 9 | 1½ | 21½ | 9 | " | 36½ |
| 9 | 1½ | 22½ | 10 | .. | .. |
| 10 | 1½ | 24½ | 10½ | .. | .. |

The size of head given is the size of die. The size of finished head will overrun this about ¼". Eye Bars are Hydraulic Forged without the addition of extraneous metal and without buckles or welds. The heads on Eye Bars are finished of the same thickness "T" as body of bar.

TURNBUCKLES.

PRESSED WROUGHT IRON.



The Cleveland City Forge and Iron Co.

Dimensions of Bar.

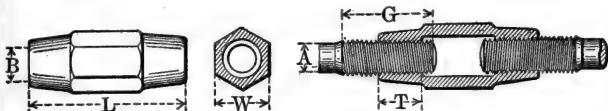
| Diameter of Screw. B | Diameter of Bar. | Side of Square Bar. | L | T | A | E | F | H | G |
|-------------------------|---------------------------------|---------------------------------|------------------|-----------------|---------|-----------------|-----------------|-----------------|-----------------|
| Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. |
| $\frac{3}{8}$ | | | $7\frac{1}{8}$ | $\frac{1}{8}$ | 6 | $\frac{1}{8}$ | $\frac{1}{8}$ | $1\frac{1}{8}$ | $\frac{1}{8}$ |
| $\frac{1}{2}$ | | | $7\frac{1}{4}$ | $\frac{1}{4}$ | 6 | $\frac{1}{4}$ | $\frac{1}{4}$ | $1\frac{1}{4}$ | $\frac{1}{4}$ |
| $\frac{5}{8}$ | | | $7\frac{1}{2}$ | $\frac{3}{4}$ | 6 | $\frac{3}{4}$ | $\frac{3}{4}$ | $1\frac{3}{4}$ | $\frac{3}{4}$ |
| $\frac{3}{4}$ | | | $7\frac{3}{4}$ | $1\frac{1}{8}$ | 6 | $1\frac{1}{8}$ | $1\frac{1}{8}$ | $1\frac{3}{4}$ | $\frac{3}{4}$ |
| $\frac{7}{8}$ | | | $7\frac{7}{8}$ | $1\frac{1}{4}$ | 6 | $1\frac{1}{4}$ | $1\frac{1}{4}$ | $1\frac{7}{8}$ | $\frac{7}{8}$ |
| 1 | $\frac{1}{2}$ and $\frac{3}{4}$ | $\frac{1}{2}$ | $8\frac{1}{4}$ | $1\frac{1}{8}$ | 6 | $1\frac{1}{8}$ | $1\frac{1}{8}$ | 2 | $\frac{1}{8}$ |
| $1\frac{1}{8}$ | $\frac{1}{2}$ and $\frac{3}{4}$ | $\frac{1}{2}$ and $\frac{1}{4}$ | $8\frac{1}{2}$ | $1\frac{1}{4}$ | 6 | $1\frac{1}{4}$ | $1\frac{1}{4}$ | $2\frac{1}{4}$ | 1 |
| $1\frac{1}{4}$ | $\frac{1}{2}$ and $\frac{3}{4}$ | $\frac{1}{2}$ and $\frac{1}{4}$ | 9 | $1\frac{1}{2}$ | 6 | $1\frac{1}{2}$ | $1\frac{1}{2}$ | $2\frac{1}{2}$ | $1\frac{1}{4}$ |
| $1\frac{1}{2}$ | $\frac{1}{2}$ and $\frac{3}{4}$ | $\frac{1}{2}$ and $\frac{1}{4}$ | $9\frac{1}{4}$ | $1\frac{3}{4}$ | 6 | $1\frac{3}{4}$ | $1\frac{3}{4}$ | $2\frac{3}{4}$ | $1\frac{1}{2}$ |
| $1\frac{3}{4}$ | $\frac{1}{2}$ and $\frac{3}{4}$ | $\frac{1}{2}$ and $\frac{1}{4}$ | $9\frac{1}{2}$ | $1\frac{7}{8}$ | 6 | $1\frac{7}{8}$ | $1\frac{7}{8}$ | $2\frac{7}{8}$ | $1\frac{3}{4}$ |
| $1\frac{7}{8}$ | $\frac{1}{2}$ and $\frac{3}{4}$ | $\frac{1}{2}$ and $\frac{1}{4}$ | $10\frac{1}{8}$ | $2\frac{1}{8}$ | 6 | $2\frac{1}{8}$ | $2\frac{1}{8}$ | $3\frac{1}{8}$ | $1\frac{7}{8}$ |
| 2 | $\frac{1}{2}$ and $\frac{3}{4}$ | $\frac{1}{2}$ and $\frac{1}{4}$ | $10\frac{1}{4}$ | $2\frac{1}{4}$ | 6 | $2\frac{1}{4}$ | $2\frac{1}{4}$ | $3\frac{1}{4}$ | $1\frac{3}{4}$ |
| $2\frac{1}{8}$ | $\frac{1}{2}$ and $\frac{3}{4}$ | $\frac{1}{2}$ and $\frac{1}{4}$ | $10\frac{1}{2}$ | $2\frac{1}{2}$ | 6 | $2\frac{1}{2}$ | $2\frac{1}{2}$ | $3\frac{1}{2}$ | $1\frac{1}{2}$ |
| $2\frac{1}{4}$ | $\frac{1}{2}$ and $\frac{3}{4}$ | $\frac{1}{2}$ and $\frac{1}{4}$ | $10\frac{3}{4}$ | $2\frac{3}{4}$ | 6 | $2\frac{3}{4}$ | $2\frac{3}{4}$ | $3\frac{3}{4}$ | $1\frac{1}{4}$ |
| $2\frac{1}{2}$ | $\frac{1}{2}$ and $\frac{3}{4}$ | $\frac{1}{2}$ and $\frac{1}{4}$ | $11\frac{1}{8}$ | $2\frac{1}{8}$ | 6 | $2\frac{1}{8}$ | $2\frac{1}{8}$ | $3\frac{1}{8}$ | $1\frac{3}{8}$ |
| $2\frac{3}{4}$ | $\frac{1}{2}$ and $\frac{3}{4}$ | $\frac{1}{2}$ and $\frac{1}{4}$ | $11\frac{1}{4}$ | $2\frac{1}{4}$ | 6 | $2\frac{1}{4}$ | $2\frac{1}{4}$ | $3\frac{1}{4}$ | $1\frac{1}{4}$ |
| $2\frac{7}{8}$ | $\frac{1}{2}$ and $\frac{3}{4}$ | $\frac{1}{2}$ and $\frac{1}{4}$ | $11\frac{1}{2}$ | $2\frac{1}{2}$ | 6 | $2\frac{1}{2}$ | $2\frac{1}{2}$ | $3\frac{1}{2}$ | $1\frac{1}{2}$ |
| 3 | $\frac{1}{2}$ and $\frac{3}{4}$ | $\frac{1}{2}$ and $\frac{1}{4}$ | 12 | 3 | 6 | 3 | 3 | $3\frac{1}{2}$ | $1\frac{1}{2}$ |
| $3\frac{1}{8}$ | $\frac{1}{2}$ and $\frac{3}{4}$ | $\frac{1}{2}$ and $\frac{1}{4}$ | $12\frac{1}{8}$ | $3\frac{1}{8}$ | 6 | $3\frac{1}{8}$ | $3\frac{1}{8}$ | $3\frac{1}{8}$ | $1\frac{1}{8}$ |
| $3\frac{1}{4}$ | $\frac{1}{2}$ and $\frac{3}{4}$ | $\frac{1}{2}$ and $\frac{1}{4}$ | $12\frac{1}{4}$ | $3\frac{1}{4}$ | 6 | $3\frac{1}{4}$ | $3\frac{1}{4}$ | $3\frac{1}{4}$ | $1\frac{1}{4}$ |
| $3\frac{1}{2}$ | $\frac{1}{2}$ and $\frac{3}{4}$ | $\frac{1}{2}$ and $\frac{1}{4}$ | $12\frac{1}{2}$ | $3\frac{1}{2}$ | 6 | $3\frac{1}{2}$ | $3\frac{1}{2}$ | $3\frac{1}{2}$ | $1\frac{1}{2}$ |
| $3\frac{3}{4}$ | $\frac{1}{2}$ and $\frac{3}{4}$ | $\frac{1}{2}$ and $\frac{1}{4}$ | $13\frac{1}{8}$ | $3\frac{3}{8}$ | 6 | $3\frac{3}{8}$ | $3\frac{3}{8}$ | $3\frac{3}{8}$ | $1\frac{3}{8}$ |
| 4 | $\frac{1}{2}$ and $\frac{3}{4}$ | $\frac{1}{2}$ and $\frac{1}{4}$ | $13\frac{1}{4}$ | $3\frac{1}{4}$ | 6 | $3\frac{1}{4}$ | $3\frac{1}{4}$ | $3\frac{1}{4}$ | $1\frac{1}{4}$ |
| $4\frac{1}{8}$ | $\frac{1}{2}$ and $\frac{3}{4}$ | $\frac{1}{2}$ and $\frac{1}{4}$ | $13\frac{1}{2}$ | $3\frac{1}{2}$ | 6 | $3\frac{1}{2}$ | $3\frac{1}{2}$ | $3\frac{1}{2}$ | $1\frac{1}{2}$ |
| $4\frac{1}{4}$ | $\frac{1}{2}$ and $\frac{3}{4}$ | $\frac{1}{2}$ and $\frac{1}{4}$ | $13\frac{3}{4}$ | $3\frac{3}{4}$ | 6 | $3\frac{3}{4}$ | $3\frac{3}{4}$ | $3\frac{3}{4}$ | $1\frac{3}{4}$ |
| $4\frac{1}{2}$ | $\frac{1}{2}$ and $\frac{3}{4}$ | $\frac{1}{2}$ and $\frac{1}{4}$ | $14\frac{1}{8}$ | $4\frac{1}{8}$ | 6 | $4\frac{1}{8}$ | $4\frac{1}{8}$ | $4\frac{1}{8}$ | $1\frac{7}{8}$ |
| $4\frac{3}{4}$ | $\frac{1}{2}$ and $\frac{3}{4}$ | $\frac{1}{2}$ and $\frac{1}{4}$ | $14\frac{1}{4}$ | $4\frac{1}{4}$ | 6 | $4\frac{1}{4}$ | $4\frac{1}{4}$ | $4\frac{1}{4}$ | $1\frac{3}{4}$ |
| 5 | $\frac{1}{2}$ and $\frac{3}{4}$ | $\frac{1}{2}$ and $\frac{1}{4}$ | $14\frac{3}{4}$ | $4\frac{3}{4}$ | 6 | $4\frac{3}{4}$ | $4\frac{3}{4}$ | $4\frac{3}{4}$ | $1\frac{1}{4}$ |
| | $\frac{1}{2}$ and $\frac{3}{4}$ | $\frac{1}{2}$ and $\frac{1}{4}$ | 15 | $4\frac{1}{2}$ | 6 | $4\frac{1}{2}$ | $4\frac{1}{2}$ | $4\frac{1}{2}$ | $1\frac{1}{2}$ |
| | $\frac{1}{2}$ and $\frac{3}{4}$ | $\frac{1}{2}$ and $\frac{1}{4}$ | 15 $\frac{1}{4}$ | $4\frac{1}{4}$ | 6 | $4\frac{1}{4}$ | $4\frac{1}{4}$ | $4\frac{1}{4}$ | $1\frac{1}{4}$ |
| | $\frac{1}{2}$ and $\frac{3}{4}$ | $\frac{1}{2}$ and $\frac{1}{4}$ | 15 $\frac{1}{2}$ | $4\frac{1}{2}$ | 6 | $4\frac{1}{2}$ | $4\frac{1}{2}$ | $4\frac{1}{2}$ | $1\frac{1}{2}$ |
| | $\frac{1}{2}$ and $\frac{3}{4}$ | $\frac{1}{2}$ and $\frac{1}{4}$ | 16 $\frac{1}{2}$ | $5\frac{1}{4}$ | 6 | $5\frac{1}{4}$ | $5\frac{1}{4}$ | $5\frac{1}{4}$ | $1\frac{3}{4}$ |
| | $\frac{1}{2}$ and $\frac{3}{4}$ | $\frac{1}{2}$ and $\frac{1}{4}$ | 17 $\frac{1}{4}$ | $5\frac{1}{4}$ | 6 | $5\frac{1}{4}$ | $5\frac{1}{4}$ | $5\frac{1}{4}$ | $1\frac{3}{4}$ |
| | $\frac{1}{2}$ and $\frac{3}{4}$ | $\frac{1}{2}$ and $\frac{1}{4}$ | 17 $\frac{1}{2}$ | $5\frac{1}{2}$ | 6 | $5\frac{1}{2}$ | $5\frac{1}{2}$ | $5\frac{1}{2}$ | $1\frac{1}{2}$ |
| | $\frac{1}{2}$ and $\frac{3}{4}$ | $\frac{1}{2}$ and $\frac{1}{4}$ | 18 | 6 | 6 | 6 | 6 | 6 | 6 |
| | $\frac{1}{2}$ and $\frac{3}{4}$ | $\frac{1}{2}$ and $\frac{1}{4}$ | 21 $\frac{1}{2}$ | 6 $\frac{1}{4}$ | 9 | 5 | 5 | 5 | 5 |
| | $\frac{1}{2}$ and $\frac{3}{4}$ | $\frac{1}{2}$ and $\frac{1}{4}$ | 22 $\frac{1}{2}$ | 6 $\frac{1}{2}$ | 9 | 5 $\frac{1}{2}$ | 5 $\frac{1}{2}$ | 5 $\frac{1}{2}$ | 5 $\frac{1}{2}$ |
| | $\frac{1}{2}$ and $\frac{3}{4}$ | $\frac{1}{2}$ and $\frac{1}{4}$ | 23 $\frac{1}{2}$ | 7 $\frac{1}{4}$ | 9 | 5 $\frac{1}{2}$ | 5 $\frac{1}{2}$ | 5 $\frac{1}{2}$ | 5 $\frac{1}{2}$ |
| | $\frac{1}{2}$ and $\frac{3}{4}$ | $\frac{1}{2}$ and $\frac{1}{4}$ | 24 | 7 $\frac{1}{2}$ | 9 | 5 $\frac{1}{2}$ | 5 $\frac{1}{2}$ | 5 $\frac{1}{2}$ | 5 $\frac{1}{2}$ |

Standard Lengths, 6, 9, 12, 15, 18, 24, 36, 48 and 72 inches between heads (A) for all sizes.

Lengths of Upset Ends shown on pages 372 to 375 inclusive are those best adapted for use with Turnbuckles of Standard Lengths, as above.

Dimensions E, F, G and H depend upon the specifications of the Bars with which the Turnbuckles are to be used.

RIGHT AND LEFT NUTS.

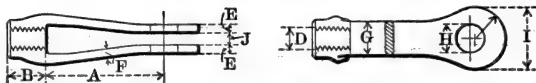


| Diameter of Screw. | Length of Upset. | Diameter of Bar. | Side of Square Bar. | Length of Nut. | Length of Thread. | Diameter of Hex. | Weight of | |
|--------------------|------------------|------------------------------------|-----------------------------------|-----------------|-------------------|------------------|-----------------|-----------------------------|
| | | | | | | | One Nut. | One Nut and Two Screw Ends. |
| B | G | A | A | L | T | W | Pounds. | Pounds. |
| Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | | |
| Ordinary Lengths. | | | | | | | | |
| $\frac{7}{8}$ | $4\frac{1}{2}$ | $\frac{5}{8}$ and $\frac{3}{4}$ | $\frac{9}{16}$ and $1\frac{1}{8}$ | 6 | $1\frac{7}{16}$ | $1\frac{5}{8}$ | $1\frac{3}{4}$ | $4\frac{1}{2}$ |
| 1 | $4\frac{1}{2}$ | $1\frac{1}{8}$ and $\frac{3}{4}$ | $\frac{3}{8}$ and $1\frac{1}{8}$ | 6 | $1\frac{7}{16}$ | $1\frac{5}{8}$ | $1\frac{3}{4}$ | $4\frac{1}{2}$ |
| $1\frac{1}{8}$ | $4\frac{1}{2}$ | $1\frac{1}{8}$ | $\frac{3}{8}$ | $6\frac{1}{2}$ | $1\frac{7}{16}$ | 2 | 3 | $7\frac{1}{2}$ |
| $1\frac{1}{4}$ | $4\frac{1}{2}$ | " | $\frac{3}{8}$ | $6\frac{1}{2}$ | $1\frac{7}{16}$ | 2 | 3 | $7\frac{1}{2}$ |
| $1\frac{3}{8}$ | 5 | $1\frac{1}{8}$ " $1\frac{1}{8}$ | 1 " $1\frac{5}{8}$ | 7 | $1\frac{7}{8}$ | $2\frac{3}{8}$ | $4\frac{3}{4}$ | $11\frac{1}{2}$ |
| $1\frac{1}{2}$ | 5 | $1\frac{1}{8}$ " $1\frac{1}{8}$ | 1 " $1\frac{5}{8}$ | 7 | $1\frac{7}{8}$ | $2\frac{3}{8}$ | $4\frac{3}{4}$ | $11\frac{1}{2}$ |
| $1\frac{3}{4}$ | $5\frac{1}{4}$ | $1\frac{1}{4}$ " $1\frac{3}{8}$ | $1\frac{1}{16}$ " $1\frac{1}{8}$ | $7\frac{1}{2}$ | $2\frac{1}{16}$ | $2\frac{3}{8}$ | $6\frac{3}{4}$ | $16\frac{1}{2}$ |
| $1\frac{7}{8}$ | $5\frac{1}{4}$ | $1\frac{5}{16}$ " $1\frac{3}{8}$ | $1\frac{3}{16}$ " $1\frac{1}{8}$ | $7\frac{1}{2}$ | $2\frac{1}{16}$ | $2\frac{3}{8}$ | $6\frac{3}{4}$ | $16\frac{1}{2}$ |
| 2 | $5\frac{1}{2}$ | $1\frac{7}{16}$ " $1\frac{9}{16}$ | $1\frac{1}{4}$ " $1\frac{5}{8}$ | 8 | $2\frac{1}{8}$ | $3\frac{1}{8}$ | $9\frac{1}{4}$ | $23\frac{1}{4}$ |
| $2\frac{1}{4}$ | $5\frac{1}{2}$ | $1\frac{9}{16}$ " $1\frac{9}{16}$ | $1\frac{3}{8}$ " $1\frac{1}{2}$ | 8 | $2\frac{1}{8}$ | $3\frac{1}{8}$ | $9\frac{1}{4}$ | $23\frac{1}{4}$ |
| $2\frac{1}{2}$ | $5\frac{1}{2}$ | $1\frac{11}{16}$ " $1\frac{9}{16}$ | $1\frac{7}{16}$ " $1\frac{1}{2}$ | $8\frac{1}{2}$ | $2\frac{1}{8}$ | $3\frac{1}{8}$ | $12\frac{1}{2}$ | $31\frac{1}{2}$ |
| $2\frac{3}{4}$ | $5\frac{1}{2}$ | $1\frac{13}{16}$ " $1\frac{9}{16}$ | $1\frac{9}{16}$ " $1\frac{1}{2}$ | $8\frac{1}{2}$ | $2\frac{1}{8}$ | $3\frac{1}{8}$ | $12\frac{1}{2}$ | $31\frac{1}{2}$ |
| $2\frac{7}{8}$ | 6 | $1\frac{7}{8}$ " 2 | $1\frac{5}{8}$ " $1\frac{1}{2}$ | 9 | $2\frac{3}{4}$ | $3\frac{7}{8}$ | $16\frac{3}{4}$ | $41\frac{1}{4}$ |
| $2\frac{1}{2}$ | 6 | $1\frac{15}{16}$ " 2 | $1\frac{3}{4}$ " $1\frac{7}{8}$ | 9 | $2\frac{3}{4}$ | $3\frac{7}{8}$ | $16\frac{3}{4}$ | $41\frac{1}{4}$ |
| $2\frac{3}{4}$ | $6\frac{1}{4}$ | $2\frac{1}{16}$ " $2\frac{1}{8}$ | $1\frac{3}{8}$ " $1\frac{7}{8}$ | $9\frac{1}{2}$ | $2\frac{5}{16}$ | $4\frac{1}{4}$ | $21\frac{1}{2}$ | $53\frac{1}{2}$ |
| $2\frac{7}{8}$ | $6\frac{1}{4}$ | $2\frac{3}{16}$ " $2\frac{1}{8}$ | $1\frac{5}{16}$ " $1\frac{7}{8}$ | $9\frac{1}{2}$ | $2\frac{5}{16}$ | $4\frac{1}{4}$ | $21\frac{1}{2}$ | $53\frac{1}{2}$ |
| $2\frac{1}{2}$ | $6\frac{1}{2}$ | $2\frac{1}{4}$ " $2\frac{5}{16}$ | 2 " $2\frac{1}{16}$ | 10 | $3\frac{3}{16}$ | $4\frac{5}{8}$ | $26\frac{1}{2}$ | $66\frac{1}{2}$ |
| 3 | $6\frac{1}{2}$ | $2\frac{5}{8}$ " $2\frac{5}{8}$ | $2\frac{1}{8}$ " $2\frac{1}{16}$ | 10 | $3\frac{3}{16}$ | $4\frac{5}{8}$ | $26\frac{1}{2}$ | $66\frac{1}{2}$ |
| $3\frac{1}{4}$ | $6\frac{3}{4}$ | $2\frac{9}{16}$ " $2\frac{5}{8}$ | $2\frac{5}{16}$ " $2\frac{1}{16}$ | $10\frac{1}{2}$ | $3\frac{3}{8}$ | 5 | 32 | 81 |
| $3\frac{1}{2}$ | 7 | $2\frac{11}{16}$ " $2\frac{5}{8}$ | $2\frac{3}{8}$ " $2\frac{1}{16}$ | 11 | $3\frac{3}{8}$ | $5\frac{3}{8}$ | $38\frac{1}{4}$ | $97\frac{1}{4}$ |
| $3\frac{3}{4}$ | $7\frac{1}{4}$ | 3 " $2\frac{11}{16}$ | $2\frac{1}{2}$ " $2\frac{1}{16}$ | $11\frac{1}{2}$ | $3\frac{1}{2}$ | $5\frac{3}{4}$ | 45 | 116 |
| 4 | $7\frac{1}{2}$ | $3\frac{1}{4}$ " $2\frac{7}{8}$ | $2\frac{7}{8}$ " $2\frac{1}{8}$ | 12 | $4\frac{1}{16}$ | 6 | $53\frac{1}{2}$ | 138 |
| Extra Lengths. | | | | | | | | |
| $1\frac{1}{4}$ | $4\frac{3}{4}$ | $\frac{7}{8}$ " $1\frac{5}{8}$ | $\frac{1}{2}$ " $1\frac{1}{8}$ | 12 | $2\frac{1}{8}$ | 2 | | |
| $1\frac{3}{8}$ | $4\frac{3}{4}$ | $\frac{1}{2}$ " $1\frac{3}{8}$ | $\frac{3}{4}$ " $1\frac{1}{8}$ | $8\frac{1}{2}$ | $1\frac{5}{8}$ | 2 | 4 | $9\frac{1}{2}$ |
| $1\frac{1}{2}$ | $4\frac{3}{4}$ | $\frac{1}{2}$ " $1\frac{3}{8}$ | $\frac{3}{4}$ " $1\frac{1}{8}$ | $8\frac{1}{2}$ | $1\frac{5}{8}$ | 2 | 4 | $9\frac{1}{2}$ |
| $1\frac{3}{4}$ | 5 | 1 " $1\frac{1}{8}$ | $\frac{7}{8}$ " $1\frac{5}{8}$ | 9 | $1\frac{7}{8}$ | $2\frac{3}{8}$ | $6\frac{1}{4}$ | $15\frac{1}{4}$ |
| $1\frac{1}{2}$ | 5 | $1\frac{1}{8}$ " $1\frac{1}{8}$ | 1 " $1\frac{5}{8}$ | 9 | $1\frac{7}{8}$ | $2\frac{3}{8}$ | $6\frac{1}{4}$ | $15\frac{1}{4}$ |
| $1\frac{3}{8}$ | $5\frac{1}{4}$ | $1\frac{1}{4}$ " $1\frac{1}{8}$ | $1\frac{1}{16}$ " $1\frac{1}{8}$ | $9\frac{1}{2}$ | $2\frac{1}{16}$ | $2\frac{3}{4}$ | $8\frac{3}{4}$ | $21\frac{1}{2}$ |
| $1\frac{1}{4}$ | $5\frac{1}{4}$ | $1\frac{5}{16}$ " $1\frac{3}{8}$ | $1\frac{3}{16}$ " $1\frac{1}{8}$ | $9\frac{1}{2}$ | $2\frac{1}{16}$ | $2\frac{3}{4}$ | $8\frac{3}{4}$ | $21\frac{1}{2}$ |
| $1\frac{3}{4}$ | $5\frac{1}{2}$ | $1\frac{7}{16}$ " $1\frac{3}{8}$ | $1\frac{1}{2}$ " $1\frac{5}{8}$ | 10 | $2\frac{1}{8}$ | $3\frac{1}{8}$ | $12\frac{1}{4}$ | $29\frac{3}{4}$ |
| 2 | $5\frac{1}{2}$ | $1\frac{9}{16}$ " $1\frac{3}{8}$ | $1\frac{3}{8}$ " $1\frac{1}{8}$ | 10 | $2\frac{1}{8}$ | $3\frac{1}{8}$ | $12\frac{1}{4}$ | $29\frac{3}{4}$ |

For Details of Upset Ends, see pages 372 to 375 inclusive.

Length of Upset Ends for use with Right and Left Nuts may be made one inch shorter than the dimensions given in column "G" above.

CLEVISES.

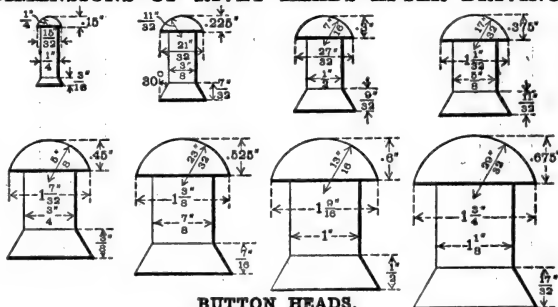


The Cleveland City Forge and Iron Co.

| Diameter of Screw. | Length of Fork. | Length of Thread. | Diameter of Pin in Inches. | | | | | | | | | | | | Dimensions to be used with Specified Diameters I. | | | |
|--------------------|-----------------|-------------------|----------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|---|-------|-------|-------|
| | | | 1 | 1 1/4 | 1 1/2 | 1 3/4 | 2 | 2 1/4 | 2 1/2 | 2 3/4 | 3 | 3 1/4 | 3 1/2 | 3 3/4 | I | G | F | E |
| D | A | B | Diameter I in Inches. | | | | | | | | | | | | I | G | F | E |
| Ins. | Ins. | Ins. | Ins. | Ins. | Ins. | Ins. | Ins. | Ins. | Ins. | Ins. | Ins. | Ins. | Ins. | Ins. | Ins. | Ins. | Ins. | Ins. |
| 3/4 | 5 1/2 | 1 1/8 | 2 3/4 | 2 3/4 | 2 3/4 | 3 | ... | ... | ... | ... | ... | ... | ... | ... | 2 3/4 | 1 1/2 | 1/2 | 1 1/2 |
| 7/8 | 5 1/2 | 1 3/8 | 2 3/4 | 2 3/4 | 3 | 3 | ... | ... | ... | ... | ... | ... | ... | ... | 3 | 1 5/8 | 1/2 | 1 1/2 |
| 1 | 6 | 1 1/2 | 2 3/4 | 2 3/4 | 3 | 3 1/4 | ... | ... | ... | ... | ... | ... | ... | ... | 3 1/4 | 1 3/4 | 3/4 | 1 1/2 |
| 1 1/8 | 6 | 1 5/8 | ... | 2 3/4 | 3 | 3 1/4 | 3 1/2 | ... | ... | ... | ... | ... | ... | ... | 3 1/2 | 1 7/8 | 3/4 | 1 1/2 |
| 1 1/4 | 6 1/2 | 1 7/8 | ... | 3 | 3 1/4 | 3 1/2 | 3 3/4 | ... | ... | ... | ... | ... | ... | ... | 3 3/4 | 2 | 5/8 | 1 1/2 |
| 1 1/2 | 6 1/2 | 2 1/8 | ... | 3 1/4 | 3 1/2 | 3 3/4 | 4 | 4 3/8 | 4 3/4 | 4 3/8 | 4 3/4 | ... | ... | ... | 4 | 2 1/8 | 5/8 | 1 1/2 |
| 1 3/4 | 7 | 2 1/4 | ... | ... | 3 3/4 | 4 | 4 3/8 | 4 3/4 | 4 3/8 | 4 3/4 | 5 1/4 | ... | ... | ... | 4 3/8 | 2 1/4 | 1 1/2 | 1 1/2 |
| 1 5/8 | 7 | 2 1/2 | ... | ... | ... | 4 3/8 | 4 3/4 | 4 3/8 | 4 3/4 | 5 1/4 | 5 1/4 | ... | ... | ... | 4 3/4 | 2 1/2 | 1 1/2 | 1 1/2 |
| 1 7/8 | 8 | 2 3/8 | ... | ... | ... | 4 3/4 | 5 1/4 | 5 1/4 | 5 1/4 | 5 1/4 | 5 1/4 | 6 1/4 | 6 1/4 | ... | 5 1/4 | 2 3/4 | 1 1/2 | 1 1/2 |
| 2 | 9 | 3 | ... | ... | ... | 5 1/4 | 5 1/4 | 5 1/4 | 5 1/4 | 5 1/4 | 5 1/4 | 6 1/4 | 6 1/4 | ... | 5 3/4 | 3 | 1 1/2 | 1 1/2 |
| 2 1/8 | 9 | 3 1/4 | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | 6 1/4 | 3 1/4 | 1 1/2 | 1 1/2 |
| 2 1/4 | 10 | 3 1/2 | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | 6 3/4 | 4 | 1 1/2 | 1 1/2 |
| 2 3/8 | 10 | 3 3/4 | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | 7 | 4 1/4 | 1 1/2 | 1 1/2 |
| 2 1/2 | 10 | 3 3/4 | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | 7 1/4 | 4 1/4 | 1 1/2 | 1 1/2 |
| 2 5/8 | 10 | 4 | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | 7 1/2 | 4 1/4 | 1 1/2 | 1 1/2 |
| 2 3/4 | 12 | 4 1/4 | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | 8 | 4 | 1 1/2 | 1 1/2 |
| 2 7/8 | 12 | 4 1/4 | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | 8 1/4 | 4 1/4 | 1 1/2 | 1 1/2 |
| 3 | 12 | 4 1/2 | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | 8 1/2 | 4 1/2 | 1 1/2 | 1 1/2 |

Dimension "H" is usually $\frac{1}{8}$ " larger than diameter of pin and "J" is made to suit the thickness of the pin plate. The above Clevises are designed for use with medium steel rods of 60000 to 68000 pounds tensile strength per square inch. All clevis nuts with diameter "I" 8 inches or larger dimension "A" will be 12 inches.

DIMENSIONS OF RIVET HEADS AFTER DRIVING.



BUTTON HEADS.

Height of Head = $\frac{1}{16}$ × Diameter of Rivet. Radius of Head = $\frac{3}{4}$ Diameter of Rivet + $\frac{1}{16}$ ".

COUNTERSUNK HEADS.

Diameter of Countersunk Head same as Button Head. Angle of Countersink = 30°. In figuring Clearances for Rivet Heads allow for Heights as follows: $\frac{5}{16}$ " for $\frac{3}{4}$ " rivets, $\frac{3}{16}$ " for $\frac{1}{2}$ " rivets. All dimensions in inches.

WEIGHTS, DIMENSIONS AND SAFE LOADS OF CHAINS.

As given by Standard Manufacturers.

| Common Coll. | | | | | Crane. | | | | Stud Link. | | | | |
|----------------|------------------------|-----------------|----------------|------------------------------|----------------------------|-----------------|----------------|------------------------------|----------------------------|-----------------|----------------|------------------------------|----------------------------|
| Size. | Thickness of Link Bar. | Length of Link. | Width of Link. | Approximate Weight per Foot. | Safe Load in Thousand Lbs. | Length of Link. | Width of Link. | Approximate Weight per Foot. | Safe Load in Thousand Lbs. | Length of Link. | Width of Link. | Approximate Weight per Foot. | Safe Load in Thousand Lbs. |
| Ins. | Ins. | Ins. | Lbs. | | | Ins. | Ins. | Lbs. | | Ins. | Ins. | Lbs. | |
| $\frac{1}{8}$ | $\frac{1}{8}$ | $1\frac{3}{8}$ | $\frac{1}{8}$ | .46 | .5 | | | | | | | | |
| $\frac{1}{4}$ | $\frac{1}{4}$ | $1\frac{1}{2}$ | $1\frac{1}{4}$ | .75 | .8 | | | | | | | | |
| $\frac{3}{8}$ | $\frac{3}{8}$ | $1\frac{3}{4}$ | $1\frac{1}{2}$ | 1.10 | 1.3 | | | | | | | | |
| $\frac{1}{2}$ | $\frac{1}{2}$ | $2\frac{1}{8}$ | $1\frac{3}{4}$ | 1.55 | 1.8 | | | | | | | | |
| $\frac{5}{8}$ | $\frac{5}{8}$ | $2\frac{1}{4}$ | $1\frac{1}{2}$ | 2.00 | 2.3 | | | | | | | | |
| $\frac{3}{4}$ | $\frac{3}{4}$ | $2\frac{1}{2}$ | $1\frac{7}{8}$ | 2.60 | 3.3 | | | | | 3 | $1\frac{3}{4}$ | 2.3 | 4.8 |
| $\frac{7}{8}$ | $\frac{7}{8}$ | $2\frac{3}{8}$ | $2\frac{1}{8}$ | 3.25 | 4.0 | $3\frac{1}{8}$ | $2\frac{1}{8}$ | 4.0 | 6.9 | $3\frac{3}{8}$ | 2 | 3.0 | 5.9 |
| 1 | 1 | $3\frac{3}{8}$ | $2\frac{1}{4}$ | 4.00 | 4.8 | | | | | $3\frac{3}{4}$ | $2\frac{1}{4}$ | 4.0 | 6.3 |
| $1\frac{1}{8}$ | $1\frac{1}{8}$ | | | | | | | | | 4 | $2\frac{1}{2}$ | 4.8 | 8.5 |
| $1\frac{1}{4}$ | $1\frac{1}{4}$ | $3\frac{7}{8}$ | $2\frac{1}{2}$ | 5.90 | 6.8 | $3\frac{5}{8}$ | $2\frac{1}{2}$ | 6.3 | 9.6 | $4\frac{3}{8}$ | $2\frac{3}{4}$ | 5.7 | 10.1 |
| $1\frac{1}{2}$ | $1\frac{1}{2}$ | $4\frac{1}{8}$ | $3\frac{1}{8}$ | 8.0 | 9.3 | $4\frac{1}{8}$ | $2\frac{3}{8}$ | 8.0 | 13.5 | $4\frac{3}{4}$ | 3 | 6.7 | 11.9 |
| $1\frac{3}{4}$ | $1\frac{3}{4}$ | | | | | | | | | 5 | $3\frac{1}{4}$ | 7.3 | 14.0 |
| 2 | 2 | | | | | | | | | $5\frac{3}{8}$ | $3\frac{1}{2}$ | 8.5 | 15.8 |
| $2\frac{1}{8}$ | $2\frac{1}{8}$ | 5 | $3\frac{5}{8}$ | 10.0 | 12.0 | $4\frac{3}{4}$ | $3\frac{1}{4}$ | 10.0 | 17.0 | $5\frac{7}{8}$ | $3\frac{3}{4}$ | 9.8 | 18.0 |
| $2\frac{1}{4}$ | $2\frac{1}{4}$ | $5\frac{1}{2}$ | 4 | 13.0 | 14.5 | $5\frac{1}{4}$ | $3\frac{3}{4}$ | 13.0 | 21.5 | $6\frac{1}{2}$ | $4\frac{1}{8}$ | 12.5 | 22.8 |
| $2\frac{3}{8}$ | $2\frac{3}{8}$ | $6\frac{1}{8}$ | $4\frac{3}{8}$ | 15.0 | 19.5 | $5\frac{7}{8}$ | $4\frac{1}{8}$ | 16.0 | 27.0 | $7\frac{1}{8}$ | $4\frac{1}{2}$ | 15.2 | 28.1 |
| $2\frac{1}{2}$ | $2\frac{1}{2}$ | | | | | $6\frac{1}{4}$ | $4\frac{3}{8}$ | 19.0 | 31.0 | $7\frac{3}{4}$ | $4\frac{7}{8}$ | 18.8 | 34.0 |
| $2\frac{7}{8}$ | $2\frac{7}{8}$ | | | | | | | | | | | | |
| 3 | 3 | | | | | $7\frac{1}{8}$ | 5 | 23.0 | 36.0 | $8\frac{1}{2}$ | $5\frac{3}{8}$ | 22.0 | 40.5 |
| $3\frac{1}{8}$ | $3\frac{1}{8}$ | | | | | $7\frac{3}{8}$ | $5\frac{1}{2}$ | 28.0 | 41.5 | $9\frac{1}{4}$ | $5\frac{7}{8}$ | 26.0 | 47.5 |
| $3\frac{1}{4}$ | $3\frac{1}{4}$ | | | | | $8\frac{1}{8}$ | $5\frac{7}{8}$ | 31.0 | 44.8 | 10 | $6\frac{1}{4}$ | 29.2 | 55.1 |
| $3\frac{3}{8}$ | $3\frac{3}{8}$ | | | | | $9\frac{1}{8}$ | $6\frac{3}{8}$ | 35.0 | 51.3 | $10\frac{1}{2}$ | $6\frac{3}{4}$ | 34.2 | 63.3 |
| $3\frac{1}{2}$ | $3\frac{1}{2}$ | | | | | | | | | | | | |
| $3\frac{3}{4}$ | $3\frac{3}{4}$ | | | | | $10\frac{1}{4}$ | $6\frac{3}{4}$ | 40.0 | 58.3 | $11\frac{1}{8}$ | $7\frac{1}{4}$ | 40.0 | 72.0 |
| 4 | 4 | | | | | $10\frac{3}{8}$ | $7\frac{1}{8}$ | 47.0 | 65.8 | 12 | $7\frac{3}{4}$ | 44.2 | 81.3 |
| $4\frac{1}{8}$ | $4\frac{1}{8}$ | | | | | $11\frac{1}{8}$ | $7\frac{3}{8}$ | 53.0 | 73.7 | 13 | $8\frac{1}{4}$ | 50.0 | 91.1 |
| $4\frac{1}{4}$ | $4\frac{1}{4}$ | | | | | 12 | 8 | 58.5 | 82.0 | $13\frac{1}{2}$ | $8\frac{3}{4}$ | 54.2 | 101.5 |
| $4\frac{3}{8}$ | $4\frac{3}{8}$ | | | | | $12\frac{5}{8}$ | $8\frac{3}{8}$ | 65.0 | 90.9 | 14 | 9 | 60.0 | 112.5 |

Safe Loads based on one-half Proof Test, or one-fourth of the approximate breaking load of chain.

BRIDGE PINS, NUTS AND PILOT NUTS.

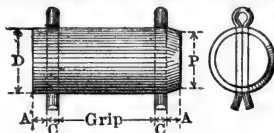


All Threads 8 per inch.

| Nominal Diameter of Pin. | Turned Diameter of Pin. | Diameter of Thread. | Short Diameter of Nut. | Long Diameter of Nut. | Diameter of Holes in Eye Bars. |
|--------------------------|-------------------------|---------------------|------------------------|-----------------------|--------------------------------|
| Inches. | D | F | A | G | |
| 1 1/2 | 1 7/8 | 1 1/4 | 2 | 2 1/8 | D + 1/8 |
| 1 3/4 | 1 7/8 | 1 1/2 | 2 1/2 | 2 7/8 | " + 1/8 |
| 2 | 1 7/8 | 1 1/2 | 2 1/2 | 2 7/8 | " + 1/8 |
| 2 1/4 | 2 1/8 | 1 1/2 | 3 | 3 1/2 | " + 1/8 |
| 2 1/2 | 2 1/8 | 2 | 3 | 3 1/2 | " + 1/8 |
| 2 3/4 | 2 1/8 | 2 | 3 1/2 | 4 1/4 | " + 1/8 |
| 3 | 2 1/8 | 2 | 3 1/2 | 4 1/4 | " + 1/8 |
| 3 1/4 | 3 1/8 | 2 1/8 | 4 | 4 1/4 | " + 1/8 |
| 3 1/2 | 3 1/8 | 2 1/8 | 4 | 4 1/4 | " + 1/8 |
| 3 3/4 | 3 1/8 | 2 3/4 | 4 1/2 | 5 1/8 | " + 1/8 |
| 4 | 3 1/8 | 3 | 4 1/2 | 5 1/8 | " + 1/8 |
| 4 1/4 | 4 1/8 | 3 1/2 | 5 | 5 1/8 | " + 1/8 |
| 4 1/2 | 4 1/8 | 3 1/2 | 5 | 5 1/8 | " + 1/8 |
| 4 3/4 | 4 1/8 | 4 | 5 1/2 | 6 3/8 | " + 1/8 |
| 5 | 4 1/8 | 4 | 5 1/2 | 6 3/8 | " + 1/8 |
| 5 1/4 | 5 1/8 | 4 | 6 | 6 1/4 | " + 1/8 |
| 5 1/2 | 5 1/8 | 4 | 6 | 6 1/4 | " + 1/8 |
| 5 3/4 | 5 1/8 | 4 | 6 1/2 | 7 1/2 | " + 1/8 |
| 6 | 5 1/8 | 4 | 6 1/2 | 7 1/2 | " + 1/8 |
| 6 1/4 | 6 3/8 | 4 | 7 | 8 1/8 | " + 1/8 |
| 6 1/2 | 6 3/8 | 4 | 7 | 8 1/8 | " + 1/8 |
| 6 3/4 | 6 3/8 | 4 | 7 1/2 | 8 1/4 | " + 1/8 |
| 7 | 6 3/8 | 4 | 7 1/2 | 8 1/4 | " + 1/8 |

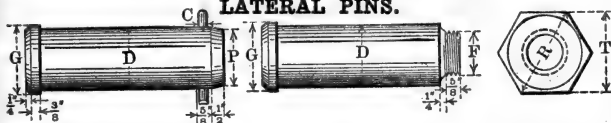
Allow 1/8" excess for each eye bar packed on the pin.

COLD ROLLED STEEL COTTER PINS.



Dimensions of Pin in Inches.

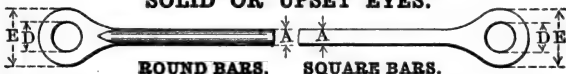
| Diameter of Pin. | D | 1 | 1 1/4 | 1 1/2 | 1 3/4 | 2 | 2 1/4 | 2 1/2 | 2 3/4 | 3 | 3 1/4 | 3 1/2 | 3 3/4 | 4 |
|----------------------------|---|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Diameter of Reduced Point. | P | 7/8 | 1 1/8 | 1 1/4 | 1 1/2 | 1 3/4 | 2 | 2 1/4 | 2 1/2 | 2 3/4 | 3 | 3 1/4 | 3 1/2 | 3 3/4 |
| Lengths of Ends. | A | 1 1/8 | 1 1/8 | 1 1/2 | 1 1/2 | 1 1/2 | 1 1/2 | 1 1/2 | 1 1/2 | 1 3/4 | 1 3/4 | 1 3/4 | 1 3/4 | 1 3/4 |
| Diameter of Cotter. | C | 1 1/8 | 1 1/8 | 1 1/8 | 1 1/8 | 1 3/8 | 1 3/8 | 1 3/8 | 1 3/8 | 1 1/2 | 1 1/2 | 1 1/2 | 1 1/2 | 1 1/2 |
| Diameter of Pin Hole. | | 1 1/8 | 1 1/8 | 1 1/8 | 1 1/8 | 1 3/8 | 1 3/8 | 1 3/8 | 1 3/8 | 1 1/2 | 1 1/2 | 1 1/2 | 1 1/2 | 1 1/2 |

LATERAL PINS.

| Rough Diameter of Pin. G | Nominal Diameter of Pin. N | Finished Diameter of Pin. D | Reduced Point. P | Short Diameter of Nut. T | Long Diameter of Nut. E | Diameter of Thread. F | Diameter of Cotter Pin. C |
|------------------------------------|--------------------------------------|---------------------------------------|----------------------------|------------------------------------|-----------------------------------|---------------------------------|-------------------------------------|
| Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inch. |
| 1½ | 1¼ | 1⅜ | 1 | 1⅝ | 1⅞ | 1 | 1 |
| 1¾ | 1½ | 1⅞ | 1¼ | 2 | 2¼ | 1¼ | " |
| 2 | 1¾ | 1⅞ | 1½ | 2½ | 2⅝ | 1½ | " |
| 2¼ | 2 | 1⅞ | 1¾ | 2½ | 2⅝ | 1½ | " |
| 2½ | 2¼ | 2⅜ | 2 | 2½ | 2⅝ | 1½ | ¾ |
| 2¾ | 2½ | 2⅞ | 2¼ | 3½ | 4⅜ | 2 | " |
| 3 | 2¾ | 2⅞ | 2½ | 3½ | 4⅜ | 2 | " |
| 3½ | 3 | 2⅞ | 2¾ | 3½ | 4⅜ | 2 | " |
| 3¾ | 3¼ | 3⅜ | 3¼ | 4½ | 5⅜ | 2½ | " |
| 4 | 3¾ | 3⅞ | 3½ | 4½ | 5⅜ | 2½ | " |

$$D = G - \frac{1}{16}''.$$

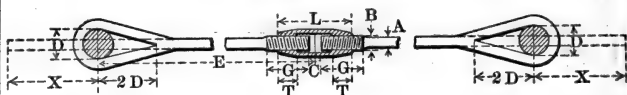
$$P = N - \frac{1}{4}''.$$

**COUNTER AND LATERAL RODS.
SOLID OR UPSET EYES.****ROUND BARS.****SQUARE BARS.**

| Diameter of Bar. A | Diameter of Largest Head. E | Diameter of Largest Pin. D | Add for One Head. | Side of Square Bar. A | Diameter of Largest Head. E | Diameter of Largest Pin. D | Add for One Head. |
|------------------------------|---------------------------------------|--------------------------------------|-------------------|---------------------------------|---------------------------------------|--------------------------------------|-------------------|
| Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. |
| ¾ | 2¼ | 1¼ | 9 | 1 | 4¼ | 2½ | 16 |
| 1 | 4¼ | 2½ | 18 | 1½ | 4¼ | 2½ | 14 |
| 1½ | 4¼ | 2½ | 16 | 1¼ | 5 | 2¾ | 18½ |
| 1¾ | 5 | 2¾ | 20½ | 1½ | 5 | 2¾ | 16½ |
| 1¾ | 5 | 2¾ | 18½ | 1½ | 5½ | 3 | 18 |
| 1½ | 5½ | 3 | 20 | 1½ | 5½ | 3 | 16½ |
| 1¾ | 5½ | 3 | 18½ | 1¾ | 6 | 3¼ | 18 |
| 1¾ | 6 | 3¼ | 21 | 1½ | 6 | 3¼ | 16½ |
| 1¾ | 6 | 3¼ | 19½ | 2 | 6½ | 3½ | 18½ |
| 2 | 6½ | 3½ | 21½ | 2½ | 6½ | 3½ | 17 |
| 2½ | 6½ | 3½ | 20 | 2½ | 7½ | 4 | 21½ |
| 2¼ | 7½ | 4 | 24½ | 2½ | 7½ | 4 | 19½ |
| 2½ | 7½ | 4 | 22¾ | 2½ | 8 | 4 | 22½ |
| 2½ | 8 | 4 | 25½ | 2½ | 8 | 4 | 21 |
| 2½ | 8 | 4 | 24 | 2¾ | 8 | 4 | 19½ |
| 2¾ | 8 | 4 | 22½ | 1½ | 5¼ | 3⅞ | 23 |
| | | | | 1¼ | 5½ | 3⅞ | 23 |
| | | | | 1½ | 5¾ | 3⅞ | 20 |
| | | | | 1½ | 6 | 3⅞ | 20 |
| | | | | 1½ | 3½ | 2¼ | |
| | | | | 1½ | 4½ | 2½ | 18 |

For details of upset screw ends for round and square bars see pages 372 to 375.

COUNTER AND LATERAL RODS. LOOP WELDED EYES.



Additional length of bar beyond center of pin required to make eye for square or round bars.

| Diameter or Side of Bar. Inches. | Diameter of Pin in Inches. | | | | | | | | | | |
|---|----------------------------|----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|
| | $\frac{3}{4}$ | 1 | $1\frac{1}{4}$ | $1\frac{1}{2}$ | $1\frac{3}{4}$ | 2 | $2\frac{1}{4}$ | $2\frac{1}{2}$ | $2\frac{3}{4}$ | 3 | $3\frac{1}{4}$ |
| $\frac{1}{8}$ | $5\frac{3}{4}$ | $6\frac{3}{4}$ | $7\frac{1}{2}$ | $8\frac{1}{2}$ | $9\frac{1}{2}$ | $10\frac{1}{4}$ | $11\frac{1}{4}$ | $12\frac{1}{4}$ | $13\frac{1}{4}$ | 14 | 15 |
| $\frac{1}{4}$ | $6\frac{1}{4}$ | $7\frac{1}{4}$ | 8 | 9 | 10 | $10\frac{3}{4}$ | $11\frac{3}{4}$ | $12\frac{3}{4}$ | $13\frac{3}{4}$ | $14\frac{1}{2}$ | $15\frac{1}{2}$ |
| $\frac{3}{8}$ | $6\frac{3}{4}$ | $7\frac{1}{2}$ | $8\frac{1}{2}$ | $9\frac{1}{2}$ | $10\frac{1}{4}$ | $11\frac{1}{4}$ | $12\frac{1}{4}$ | $13\frac{1}{4}$ | 14 | 15 | 16 |
| $\frac{1}{2}$ | | 8 | 9 | 10 | $10\frac{3}{4}$ | $11\frac{3}{4}$ | $12\frac{3}{4}$ | $13\frac{3}{4}$ | $14\frac{1}{2}$ | $15\frac{1}{2}$ | $16\frac{1}{2}$ |
| 1 | | $8\frac{1}{2}$ | $9\frac{1}{2}$ | $10\frac{1}{4}$ | $11\frac{1}{4}$ | $12\frac{1}{4}$ | $13\frac{1}{4}$ | 14 | 15 | 16 | $16\frac{1}{2}$ |
| $1\frac{1}{8}$ | | | 10 | $10\frac{3}{4}$ | $11\frac{3}{4}$ | $12\frac{3}{4}$ | $13\frac{3}{4}$ | $14\frac{1}{2}$ | $15\frac{1}{2}$ | $16\frac{1}{2}$ | $17\frac{1}{4}$ |
| $1\frac{1}{4}$ | | | $10\frac{1}{4}$ | $11\frac{1}{4}$ | $12\frac{1}{4}$ | $13\frac{1}{4}$ | 14 | 15 | 16 | $16\frac{3}{4}$ | $17\frac{3}{4}$ |
| $1\frac{3}{8}$ | | | | $11\frac{3}{4}$ | $12\frac{3}{4}$ | $13\frac{1}{2}$ | $14\frac{1}{2}$ | $15\frac{1}{2}$ | $16\frac{1}{2}$ | $17\frac{1}{4}$ | $18\frac{1}{4}$ |
| $1\frac{1}{2}$ | | | | $12\frac{1}{4}$ | $13\frac{1}{4}$ | 14 | 15 | 16 | $16\frac{3}{4}$ | $17\frac{3}{4}$ | $18\frac{3}{4}$ |
| $1\frac{5}{8}$ | | | | | $13\frac{1}{2}$ | $14\frac{1}{2}$ | $15\frac{1}{2}$ | $16\frac{1}{2}$ | $17\frac{1}{4}$ | $18\frac{1}{4}$ | $19\frac{1}{4}$ |
| $1\frac{3}{4}$ | | | | | 14 | 15 | 16 | $16\frac{3}{4}$ | $17\frac{3}{4}$ | $18\frac{3}{4}$ | $19\frac{3}{4}$ |
| $1\frac{7}{8}$ | | | | | | $15\frac{1}{2}$ | $16\frac{1}{2}$ | $17\frac{1}{4}$ | $18\frac{1}{4}$ | $19\frac{1}{4}$ | 20 |
| 2 | | | | | | 16 | $16\frac{3}{4}$ | $17\frac{3}{4}$ | $18\frac{3}{4}$ | $19\frac{1}{2}$ | $20\frac{1}{2}$ |
| $2\frac{1}{8}$ | | | | | | | $17\frac{1}{4}$ | $18\frac{1}{4}$ | $19\frac{1}{4}$ | $20\frac{1}{4}$ | 21 |
| $2\frac{1}{4}$ | | | | | | | 18 | $18\frac{3}{4}$ | $19\frac{3}{4}$ | $20\frac{3}{4}$ | $21\frac{1}{2}$ |
| $2\frac{3}{8}$ | | | | | | | | $19\frac{1}{4}$ | $20\frac{1}{4}$ | $21\frac{1}{4}$ | 22 |
| $2\frac{1}{2}$ | | | | | | | | $19\frac{3}{4}$ | $20\frac{3}{4}$ | $21\frac{3}{4}$ | $22\frac{3}{4}$ |
| $2\frac{5}{8}$ | | | | | | | | | $21\frac{1}{4}$ | $22\frac{1}{4}$ | $23\frac{1}{4}$ |
| $2\frac{3}{4}$ | | | | | | | | | $21\frac{3}{4}$ | $22\frac{3}{4}$ | $23\frac{3}{4}$ |
| $2\frac{7}{8}$ | | | | | | | | | | $23\frac{1}{4}$ | $24\frac{1}{4}$ |
| 3 | | | | | | | | | | $23\frac{3}{4}$ | $24\frac{3}{4}$ |
| $3\frac{1}{8}$ | | | | | | | | | | | $25\frac{1}{4}$ |
| $3\frac{1}{4}$ | | | | | | | | | | | $25\frac{1}{2}$ |

Length in inches beyond center of pin required to form one eye = X.

FORMULÆ: When $\frac{A}{2} = \text{or } < 1$

$X = 3.7 [D + A] + 1$

When $\frac{A}{2} > 1$

$X = 3.7 [D + A] + \frac{A}{2}$

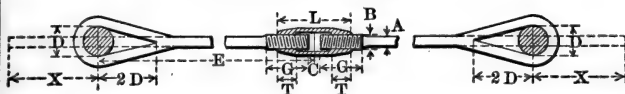
A = Side or Diameter of Bar.

D = Diameter of Pin.

Length of bar including amount required to form one eye = $E - \frac{1}{2} C + X$.

COUNTER AND LATERAL RODS.

LOOP WELDED EYES.



Additional length of bar beyond center of pin required to make eye for square or round bars.

| Diameter or Side of Bar. Inches. | Diameter of Pin in Inches. | | | | | | | | | | |
|---|----------------------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| | 3½ | 3¾ | 4 | 4½ | 4¾ | 4¾ | 5 | 5½ | 5¾ | 5¾ | 6 |
| ½ | 16 | 16¾ | 17¾ | 18¾ | 19¾ | 20¾ | 21¾ | 22¾ | 23¾ | 24¾ | 25¾ |
| ¾ | 16½ | 17¼ | 18¼ | 19¼ | 20 | 21 | 22 | 22¾ | 23¾ | 24¾ | 25¾ |
| 1 | 16¾ | 17¾ | 18¾ | 19¾ | 20¾ | 21¾ | 22¾ | 23¾ | 24¾ | 25¾ | 26 |
| 1¼ | 17¼ | 18¼ | 19¼ | 20 | 21 | 22 | 22¾ | 23¾ | 24¾ | 25¾ | 26½ |
| 1½ | 17¾ | 18¾ | 19¾ | 20¾ | 21¾ | 22¾ | 23¾ | 24¾ | 25¾ | 26½ | 27 |
| 1¾ | 18¼ | 19¼ | 20 | 21 | 22 | 22¾ | 23¾ | 24¾ | 25¾ | 26½ | 27½ |
| 2 | 18¾ | 19¾ | 20¾ | 21¾ | 22¾ | 23¾ | 24¾ | 25¾ | 26½ | 27½ | 28 |
| 2¼ | 19¼ | 20 | 21 | 22 | 22¾ | 23¾ | 24¾ | 25¾ | 26½ | 27½ | 28½ |
| 2½ | 19¾ | 20¾ | 21¾ | 22¾ | 23¾ | 24¾ | 25¾ | 26½ | 27½ | 28½ | 29 |
| 2¾ | 20 | 21 | 22 | 22¾ | 23¾ | 24¾ | 25¾ | 26½ | 27½ | 28½ | 29½ |
| 3 | 20½ | 21½ | 22½ | 23½ | 24½ | 25½ | 26½ | 27½ | 28½ | 29½ | 30 |
| 3¼ | 21 | 22 | 22¾ | 23¾ | 24¾ | 25¾ | 26½ | 27½ | 28½ | 29½ | 30½ |
| 3½ | 21½ | 22½ | 23½ | 24½ | 25½ | 26½ | 27½ | 28½ | 29½ | 30½ | 31 |
| 3¾ | 22 | 23 | 23¾ | 24¾ | 25¾ | 26½ | 27½ | 28½ | 29½ | 30½ | 31½ |
| 4 | 22½ | 23½ | 24½ | 25½ | 26½ | 27½ | 28½ | 29½ | 30½ | 31½ | 32 |
| 4¼ | 23 | 24 | 25 | 25¾ | 26¾ | 27¾ | 28¾ | 29¾ | 30¾ | 31¾ | 32½ |
| 4½ | 23½ | 24½ | 25½ | 26½ | 27½ | 28½ | 29½ | 30½ | 31½ | 32½ | 33 |
| 4¾ | 24 | 25 | 26 | 26¾ | 27¾ | 28¾ | 29¾ | 30¾ | 31¾ | 32¾ | 33½ |
| 5 | 24½ | 25½ | 26½ | 27½ | 28½ | 29½ | 30½ | 31½ | 32½ | 33½ | 34 |
| 5¼ | 25 | 26 | 27 | 28 | 28¾ | 29¾ | 30¾ | 31¾ | 32¾ | 33¾ | 34½ |
| 5½ | 25½ | 26½ | 27½ | 28½ | 29½ | 30½ | 31½ | 32½ | 33½ | 34½ | 35 |
| 5¾ | 26 | 27 | 28 | 29 | 30 | 31 | 32 | 33 | 34 | 35 | 36 |
| 6 | 26½ | 27½ | 28½ | 29½ | 30½ | 31½ | 32½ | 33½ | 34½ | 35½ | 36½ |
| 6¼ | 27 | 28 | 29 | 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 |

For additional length required to form upset end and details of same see tables of Upset Ends, pages 372 to 375 inclusive.

For details of Turnbuckles, see page 378.

For details of Right and Left Nuts, see page 379.

MISCELLANEOUS STEEL WIRE NAILS.

Approximate Number per Pound.

| Washburn & Moen Gauge. | Diameter in Inches. | Length in Inches. | | | | | | | | | | |
|------------------------------|------------------------|-------------------|---------------|---------------|---------------|---------------|---------------|---------------|-------|----------------|----------------|----------------|
| | | $\frac{3}{16}$ | $\frac{1}{4}$ | $\frac{3}{8}$ | $\frac{1}{2}$ | $\frac{5}{8}$ | $\frac{3}{4}$ | $\frac{7}{8}$ | 1 | $1\frac{1}{8}$ | $1\frac{1}{4}$ | $1\frac{1}{2}$ |
| 000 | .362 | | | | | | | | | | 28 | 23 |
| 00 | .331 | | | | | | | | | | 33 | 27 |
| 0 | .307 | | | | | | | | | | 38 | 32 |
| 1 | .283 | | | | | | | | 57 | 50 | 45 | 38 |
| 2 | .263 | | | | | | | | 65 | 58 | 52 | 44 |
| 3 | .244 | | | | | | 100 | 87 | 76 | 67 | 60 | 50 |
| 4 | .225 | | | | | | 120 | 104 | 90 | 80 | 72 | 60 |
| 5 | .207 | | | | 211 | 169 | 141 | 121 | 106 | 94 | 85 | 71 |
| 6 | .192 | | | | 247 | 197 | 164 | 141 | 123 | 111 | 99 | 82 |
| 7 | .177 | | | | 299 | 239 | 200 | 171 | 149 | 133 | 120 | 100 |
| 8 | .162 | | | | 345 | 275 | 229 | 197 | 172 | 153 | 137 | 115 |
| 9 | .148 | | | | 414 | 331 | 276 | 236 | 207 | 184 | 165 | 138 |
| 10 | .135 | | | 663 | 496 | 397 | 333 | 283 | 248 | 220 | 198 | 165 |
| 11 | .120 | | | 837 | 628 | 502 | 418 | 359 | 314 | 279 | 251 | 209 |
| 12 | .105 | | | 1096 | 822 | 658 | 548 | 469 | 411 | 365 | 329 | 274 |
| 13 | .092 | | | 1429 | 1072 | 857 | 714 | 613 | 536 | 476 | 429 | 357 |
| 14 | .080 | | 2840 | 1893 | 1420 | 1136 | 947 | 811 | 710 | 631 | 568 | 473 |
| 15 | .072 | | 3504 | 2336 | 1752 | 1402 | 1168 | 1001 | 876 | 778 | 701 | 584 |
| 16 | .063 | | 4571 | 3048 | 2280 | 1828 | 1523 | 1305 | 1143 | 1015 | 913 | 761 |
| 17 | .054 | | 6233 | 4156 | 3116 | 2495 | 2077 | 1781 | 1558 | 1385 | 1246 | 1038 |
| 18 | .047 | | 8276 | 5517 | 4138 | 3310 | 2758 | 2364 | 2069 | 1839 | 1655 | 1379 |
| 19 | .041 | | 10668 | 7112 | 5334 | 4267 | 3556 | 2933 | 2667 | 2370 | 2133 | 1778 |
| 20 | .035 | 20000 | 15000 | 10000 | 7500 | 6000 | 5000 | 4400 | 3750 | 3333 | 3000 | |
| 21 | .032 | 23702 | 17777 | 11850 | 8888 | 7111 | 5926 | 5079 | 4444 | | | |
| 22 | .028 | 30476 | 22856 | 15237 | 11428 | 9143 | 7618 | | | | | |

| Washburn & Moen Gauge. | Diameter in Inches. | Length in Inches. | | | | | | | | | | | | | | |
|------------------------------|------------------------|-------------------|-----|-----------------|-----------------|-----------------|-----|-----------------|-----|-----------------|----|-------------------|----|-----------------|-----------------|-----------------|
| | | 1 $\frac{3}{4}$ | 2 | 2 $\frac{1}{4}$ | 2 $\frac{1}{2}$ | 2 $\frac{3}{4}$ | 3 | 3 $\frac{1}{2}$ | 4 | 4 $\frac{1}{2}$ | 5 | 6 | 7 | 8 | 9 | 10 |
| 000 | .362 | 20 | 17 | 16 | 14 | 13 | 12 | 10 | 9 | 8 | 7 | 6 | 5 | 4 $\frac{1}{2}$ | 4 | 3 $\frac{1}{2}$ |
| 00 | .331 | 23 | 20 | 18 | 16 | 15 | 14 | 12 | 10 | 9 | 8 | 7 | 6 | 5 | 4 $\frac{1}{2}$ | 4 |
| 0 | .307 | 27 | 24 | 21 | 19 | 17 | 16 | 14 | 12 | 10 | 9 | 8 | 7 | 6 | 5 | 4 $\frac{1}{2}$ |
| 1 | .283 | 32 | 28 | 25 | 23 | 21 | 19 | 16 | 14 | 13 | 11 | 10 | 8 | 7 | 6 | 5 $\frac{1}{2}$ |
| 2 | .263 | 37 | 32 | 29 | 26 | 24 | 22 | 19 | 16 | 14 | 13 | 11 | 9 | 8 | 7 | 6 $\frac{1}{2}$ |
| 3 | .244 | 43 | 38 | 34 | 30 | 28 | 25 | 22 | 19 | 17 | 15 | 13 | 11 | 10 | 8 | 7 $\frac{1}{2}$ |
| 4 | .225 | 51 | 45 | 40 | 36 | 33 | 30 | 26 | 23 | 20 | 18 | 15 | 13 | 11 | 10 | 9 |
| 5 | .207 | 60 | 53 | 47 | 42 | 39 | 35 | 30 | 26 | 24 | 21 | 18 | 15 | | | |
| 6 | .192 | 71 | 62 | 55 | 50 | 45 | 41 | 35 | 31 | 28 | 25 | 21 | 18 | | | |
| 7 | .177 | 85 | 75 | 67 | 60 | 54 | 50 | 43 | 37 | 33 | 30 | 25 | | | | |
| 8 | .162 | 98 | 86 | 76 | 69 | 62 | 57 | 49 | 43 | 39 | 35 | 29 | | | | |
| 9 | .148 | 118 | 103 | 92 | 82 | 75 | 69 | 59 | 52 | 46 | 41 | | | | | |
| 10 | .135 | 142 | 124 | 110 | 99 | 90 | 83 | 71 | 62 | 55 | 50 | | | | | |
| 11 | .120 | 179 | 157 | 139 | 125 | 114 | 105 | 90 | 79 | 70 | | W. & M. Gauge. | | 11 | 12 | |
| 12 | .105 | 235 | 204 | 182 | 164 | 149 | 137 | 117 | 103 | | | | | | | |
| 13 | .092 | 306 | 268 | 238 | 214 | 195 | 178 | 153 | | | | | | | | |
| 14 | .080 | 406 | 350 | 315 | 284 | 258 | 236 | | | | | | | | | |
| 15 | .072 | 500 | 438 | 389 | 350 | | | | | | | | | | | |
| 16 | .063 | 653 | 571 | 508 | | | | | | | | | | | | |
| 17 | .054 | 890 | 779 | | | | | | | | | | | | | |
| 18 | .047 | 1182 | | | | | | | | | | | | | | |
| | | | | | | | | | | | | 000 | | 3 $\frac{1}{4}$ | | 3 |
| | | | | | | | | | | | | 00 | | 3 $\frac{3}{4}$ | | 3 $\frac{1}{4}$ |
| | | | | | | | | | | | | 0 | | 4 $\frac{1}{4}$ | | 4 |
| | | | | | | | | | | | | 1 | | 5 | | 4 $\frac{1}{2}$ |
| | | | | | | | | | | | | 2 | | 6 | | 5 $\frac{1}{2}$ |

These approximate numbers are an average only, and the figures given may be varied either way, by changes in the dimensions of heads or points. Brads and no-head nails will have more to the pound than table shows, and large or thick-headed nails will have less.

CUT STEEL NAILS AND SPIKES.**Sizes, Lengths, and Approximate Number per Pound.**

| Sizes. | Length. Inches. | Common. | Clinch. | Finishing. | Casing and Box. | Fencing. | Spiques. |
|--------|--------------------|---------|---------|------------|--------------------|----------|----------|
| 2d | 1 | 740 | 400 | 1100 | | | |
| 3d | 1½ | 460 | 260 | 880 | | | |
| 4d | 1½ | 280 | 180 | 530 | 420 | | |
| 5d | 1¾ | 210 | 125 | 350 | 300 | 100 | |
| 6d | 2 | 160 | 100 | 300 | 210 | 80 | |
| 7d | 2¼ | 120 | 80 | 210 | 180 | 60 | |
| 8d | 2½ | 88 | 68 | 168 | 130 | 52 | |
| 9d | 2¾ | 73 | 52 | 130 | 107 | 38 | |
| 10d | 3 | 60 | 48 | 104 | 88 | 26 | |
| 12d | 3¼ | 46 | 40 | 96 | 70 | 20 | |
| 16d | 3½ | 33 | 34 | 86 | 52 | 18 | 17 |
| 20d | 4 | 23 | 24 | 76 | 38 | 16 | 14 |
| 25d | 4¼ | 20 | | | | | |
| 30d | 4½ | 16½ | | | 30 | | 11 |
| 40d | 5 | 12 | | | 26 | | 9 |
| 50d | 5½ | 10 | | | 20 | | 7½ |
| 60d | 6 | 8 | | | 16 | | 6 |
| | 6½ | | | | | | 5½ |
| | 7 | | | | | | 5 |

| Sizes. | Length. Inches. | Barrel. | Light Barrel. | Slating. | Sizes. | Length. Inches. | Flat Grip. Fine. | Edge Grip. Fine. |
|--------|--------------------|---------|------------------|----------|----------|--------------------|---------------------|---------------------|
| | 5⁄8 | 750 | | | | ¾ | 1462 | |
| | ¾ | 600 | | | | 7⁄8 | 1300 | |
| | 7⁄8 | 500 | | | 2d | 1 | 1100 | 960 |
| 2d | 1 | 450 | | 340 | 3d | 1½ | 800 | 750 |
| | 1½ | 310 | 400 | | 4d | 1¾ | 650 | 600 |
| 3d | 1¼ | 280 | 304 | 280 | Tobacco. | | Brads. | Shingle. |
| | 1¾ | 210 | | | | | | |
| 4d | 1½ | 190 | 224 | 220 | 130 | | | |
| 5d | 1¾ | | | 180 | | | | |
| 6d | 2 | | | | 97 | | 120 | |
| 7d | 2¼ | | | | 85 | | 94 | |
| 8d | 2½ | | | | 68 | | 74 | 90 |
| 9d | 2¾ | | | | 58 | | 62 | 72 |
| 10d | 3 | | | | 48 | | 50 | 60 |
| 12d | 3¼ | | | | | | 40 | |
| 16d | 3½ | | | | | | 27 | |

SQUARE BOAT SPIKES.

Approximate Number in a Keg of 200 Pounds.

| Size. Inch. | Length of Spike—Inches. | | | | | | | | | | | |
|----------------|-------------------------|-------|-------|-------|-------|-----|-----|-----|-----|-----|-----|-----|
| | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 14 | 16 |
| $\frac{1}{4}$ | 3000 | 2375 | 2050 | 1825 | | | | | | | | |
| $\frac{5}{16}$ | 1660 | 1360 | 1230 | 1175 | 990 | 880 | | | | | | |
| $\frac{3}{8}$ | 1320 | 1140 | 940 | 800 | 650 | 600 | 525 | 475 | | | | |
| $\frac{7}{16}$ | | | | 600 | 590 | 510 | 400 | 360 | 320 | 280 | | |
| $\frac{1}{2}$ | | | | 450 | 375 | 335 | 300 | 275 | 260 | 240 | | |
| $\frac{5}{8}$ | | | | | | 260 | 240 | 220 | 205 | 190 | 175 | 160 |

WROUGHT SPIKES.

Approximate Number in a Keg of 150 Pounds.

| Size. Inch. | Length of Spike—Inches. | | | | | | | | | | | |
|----------------|-------------------------|------|------|------|------|------|------|-----|-----|-----|-----|-----|
| | 3 | 3½ | 4 | 4½ | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
| $\frac{1}{4}$ | 2250 | 1890 | 1650 | 1464 | 1380 | 1292 | 1161 | | | | | |
| $\frac{5}{16}$ | | 1208 | 1135 | 1064 | 930 | 868 | 662 | 635 | 573 | | | |
| $\frac{3}{8}$ | | | | | 742 | 570 | 482 | 455 | 424 | 391 | | |
| $\frac{7}{16}$ | | | | | | | 445 | 384 | 300 | 270 | 249 | 236 |
| $\frac{1}{2}$ | | | | | | | 306 | 256 | 240 | 222 | 203 | 180 |

WOOD SCREWS.

| Size Num- ber. | Diam- eter. Inch. | Size Num- ber. | Diam- eter. Inch. | Size Num- ber. | Diam- eter. Inch. | Size Num- ber. | Diam- eter. Inch. | Size Num- ber. | Diam- eter. Inch. | Size Num- ber. | Diam- eter. Inch. |
|----------------------|-------------------------|----------------------|-------------------------|----------------------|-------------------------|----------------------|-------------------------|----------------------|-------------------------|----------------------|-------------------------|
| 0 | .056 | 5 | .122 | 10 | .188 | 15 | .255 | 20 | .321 | 25 | .387 |
| 1 | .069 | 6 | .135 | 11 | .201 | 16 | .268 | 21 | .334 | 26 | .401 |
| 2 | .082 | 7 | .149 | 12 | .215 | 17 | .281 | 22 | .347 | 27 | .414 |
| 3 | .096 | 8 | .162 | 13 | .228 | 18 | .293 | 23 | .361 | 28 | .427 |
| 4 | .109 | 9 | .175 | 14 | .241 | 19 | .308 | 24 | .374 | 29 | .440 |
| | | | | | | | | | | 30 | .453 |

RAILROAD SPIKES.

| Size Measured. Under Head. Inches. | Average Number per Keg of 200 Pounds | Quantity of Spikes per Mile of Single Track. Ties 2 feet c. to c. 4 Spikes per Tie. | | Rail Used. Weight per Yard. Pounds. |
|--|--|---|-----------------|---|
| | | Pounds. | Kgs. | |
| $5\frac{1}{2} \times \frac{5}{8}$ | 300 | 7040 | $35\frac{1}{5}$ | 75 to 100 |
| $5\frac{1}{2} \times \frac{9}{16}$ | 375 | 5870 | $29\frac{1}{3}$ | 45 " 75 |
| $5 \times \frac{9}{16}$ | 400 | 5170 | 26 | 40 " 56 |
| $5 \times \frac{1}{2}$ | 450 | 4660 | $23\frac{1}{3}$ | 35 " 40 |
| $4\frac{1}{2} \times \frac{1}{2}$ | 530 | 3960 | 20 | 30 " 35 |
| $4 \times \frac{1}{2}$ | 600 | 3520 | $17\frac{2}{3}$ | 25 " 35 |
| $4\frac{1}{2} \times \frac{7}{16}$ | 680 | 3110 | $15\frac{1}{2}$ | 20 " 30 |
| $4 \times \frac{7}{16}$ | 720 | 2910 | $14\frac{3}{4}$ | 20 " 30 |
| $3\frac{1}{2} \times \frac{7}{16}$ | 900 | 2350 | 11 | 16 " 25 |
| $4 \times \frac{3}{8}$ | 1000 | 2090 | $10\frac{1}{2}$ | 16 " 25 |
| $3\frac{1}{2} \times \frac{3}{8}$ | 1190 | 1780 | 9 | 16 " 20 |
| $3 \times \frac{3}{8}$ | 1240 | 1710 | $8\frac{1}{2}$ | 16 " 20 |
| $2\frac{1}{2} \times \frac{3}{8}$ | 1342 | 1575 | $7\frac{7}{8}$ | 12 " 16 |

DIMENSIONS, WEIGHTS AND PROPERTIES OF STANDARD PIPE.

| Diameter in Inches. | | | Weight per Foot. Pounds. | Moment of Inertia. Inches. ⁴ | Section Modulus. Inches. ³ | Radius of Gyration. Inches. |
|---------------------|-----------|-----------|------------------------------------|--|---|--|
| Nominal. | External. | Internal. | | | | |

BLACK OR GALVANIZED STANDARD WEIGHT PIPE.

| | | | | | | |
|----------------|--------|--------|--------|-------|------|------|
| $\frac{1}{8}$ | .405 | .269 | .244 | .001 | .005 | .12 |
| $\frac{1}{4}$ | .540 | .364 | .424 | .003 | .012 | .16 |
| $\frac{3}{8}$ | .675 | .493 | .567 | .007 | .022 | .21 |
| $\frac{1}{2}$ | .840 | .622 | .850 | .017 | .041 | .26 |
| $\frac{3}{4}$ | 1.050 | .824 | 1.130 | .037 | .071 | .33 |
| 1 | 1.315 | 1.049 | 1.678 | .09 | .13 | .42 |
| $1\frac{1}{4}$ | 1.660 | 1.380 | 2.272 | .19 | .23 | .54 |
| $1\frac{1}{2}$ | 1.900 | 1.610 | 2.717 | .31 | .36 | .62 |
| 2 | 2.375 | 2.067 | 3.652 | .67 | .56 | .79 |
| $2\frac{1}{2}$ | 2.875 | 2.469 | 5.793 | 1.53 | 1.06 | .95 |
| 3 | 3.500 | 3.068 | 7.575 | 3.02 | 1.72 | 1.16 |
| $3\frac{1}{2}$ | 4.000 | 3.548 | 9.109 | 4.79 | 2.39 | 1.34 |
| 4 | 4.500 | 4.026 | 10.790 | 7.23 | 3.21 | 1.51 |
| $4\frac{1}{2}$ | 5.000 | 4.506 | 12.538 | 10.4 | 4.2 | 1.68 |
| 5 | 5.563 | 5.047 | 14.617 | 15.2 | 5.5 | 1.88 |
| 6 | 6.625 | 6.065 | 18.974 | 28.1 | 8.5 | 2.25 |
| 7 | 7.625 | 7.023 | 23.544 | 46.5 | 12.2 | 2.59 |
| 8 | 8.625 | 8.071 | 24.696 | 63.4 | 14.7 | 3.31 |
| 8 | 8.625 | 7.981 | 28.554 | 72.5 | 16.8 | 2.94 |
| 9 | 9.625 | 8.941 | 33.907 | 107.6 | 22.4 | 3.28 |
| 10 | 10.750 | 10.192 | 31.201 | 125.9 | 23.4 | 3.70 |
| 10 | 10.750 | 10.020 | 40.483 | 160.9 | 29.9 | 3.67 |
| 10 | 10.750 | 10.136 | 34.240 | 137.1 | 25.5 | 3.69 |
| 11 | 11.750 | 11.000 | 45.557 | 217.0 | 36.9 | 4.02 |
| 12 | 12.750 | 12.090 | 43.773 | 248.5 | 40.0 | 3.91 |
| 12 | 12.750 | 12.000 | 49.562 | 285.4 | 44.7 | 4.38 |
| 13 | 14.00 | 13.25 | 54.568 | 372.8 | 53.3 | 4.82 |
| 14 | 15.00 | 14.25 | 58.573 | 461.0 | 61.5 | 5.23 |
| 15 | 16.00 | 15.25 | 62.579 | 562.0 | 70.3 | 5.53 |

STANDARD EXTRA STRONG PIPE.

| | | | | | | |
|---------------|-------|------|-------|------|------|-----|
| $\frac{1}{8}$ | .405 | .215 | .314 | .001 | .006 | .11 |
| $\frac{1}{4}$ | .540 | .302 | .535 | .004 | .014 | .15 |
| $\frac{3}{8}$ | .675 | .423 | .738 | .009 | .026 | .20 |
| $\frac{1}{2}$ | .840 | .546 | 1.087 | .020 | .048 | .25 |
| $\frac{3}{4}$ | 1.050 | .742 | 1.473 | .045 | .085 | .32 |

DIMENSIONS, WEIGHTS AND PROPERTIES OF STANDARD PIPE (CONTINUED).

| Diameter in Inches. | | | Weight per Foot. Pounds. | Moment of Inertia. Inches. ⁴ | Section Modulus. Inches. ³ | Radius of Gyration. Inches. |
|---|-----------|-----------|------------------------------------|--|---|--|
| Nominal. | External. | Internal. | | | | |
| STANDARD EXTRA STRONG PIPE (CONTINUED). | | | | | | |
| 1 | 1.315 | .957 | 2.171 | .11 | .16 | .41 |
| 1½ | 1.660 | 1.278 | 2.996 | .24 | .29 | .52 |
| 1½ | 1.900 | 1.500 | 3.631 | .39 | .46 | .61 |
| 2 | 2.375 | 1.939 | 5.022 | .87 | .73 | .77 |
| 2½ | 2.875 | 2.323 | 7.661 | 1.92 | 1.34 | .92 |
| 3 | 3.500 | 2.900 | 10.252 | 3.89 | 2.23 | 1.14 |
| 3½ | 4.000 | 3.364 | 12.505 | 6.28 | 3.14 | 1.29 |
| 4 | 4.500 | 3.826 | 14.983 | 9.6 | 4.3 | 1.48 |
| 4½ | 5.000 | 4.290 | 17.611 | 14.1 | 5.6 | 1.65 |
| 5 | 5.563 | 4.813 | 20.778 | 20.7 | 7.4 | 1.84 |
| 6 | 6.625 | 5.761 | 28.573 | 40.5 | 12.2 | 2.19 |
| 7 | 7.625 | 6.625 | 38.048 | 71.4 | 18.7 | 2.53 |
| 8 | 8.625 | 7.625 | 43.388 | 105.7 | 24.5 | 2.88 |
| 9 | 9.625 | 8.625 | 48.728 | 149.4 | 31.0 | 3.23 |
| 10 | 10.750 | 9.75 | 54.735 | 212.0 | 39.3 | 3.63 |
| 11 | 11.750 | 10.75 | 60.075 | 280.1 | 47.7 | 3.98 |
| 12 | 12.750 | 11.75 | 65.415 | 360.7 | 56.6 | 4.33 |

STANDARD DOUBLE EXTRA STRONG PIPE.

| | | | | | | |
|----|-------|-------|--------|-------|------|------|
| 1½ | .840 | .252 | 1.714 | .024 | .058 | .22 |
| 1½ | 1.050 | .434 | 2.440 | .058 | .110 | .28 |
| 1 | 1.315 | .599 | 3.659 | .14 | .21 | .36 |
| 1½ | 1.660 | .896 | 5.214 | .34 | .41 | .47 |
| 1½ | 1.900 | 1.100 | 6.408 | .57 | .67 | .55 |
| 2 | 2.375 | 1.503 | 9.029 | 1.31 | 1.10 | .70 |
| 2½ | 2.875 | 1.771 | 13.695 | 2.87 | 2.00 | .84 |
| 3 | 3.500 | 2.300 | 18.583 | 6.0 | 3.4 | 1.05 |
| 3½ | 4.000 | 2.728 | 22.850 | 9.8 | 4.9 | 1.21 |
| 4 | 4.500 | 3.152 | 27.541 | 15.3 | 6.8 | 1.37 |
| 4½ | 5.000 | 3.580 | 32.530 | 22.6 | 9.0 | 1.54 |
| 5 | 5.563 | 4.063 | 38.552 | 33.7 | 12.3 | 1.72 |
| 6 | 6.625 | 4.897 | 53.160 | 66.3 | 20.0 | 2.08 |
| 7 | 7.625 | 5.875 | 62.079 | 107.5 | 28.2 | 2.41 |
| 8 | 8.625 | 6.875 | 72.424 | 162.0 | 37.6 | 2.76 |

WROUGHT IRON WELDED STEAM, GAS AND WATER PIPE.

| Nominal. Inches. | DIAMETER. | | Thickness. Inches. | Weight per Foot. Pounds. | CIRCUMFERENCE. | | Lineal Feet to 1 Sq. Ft. Surface. | |
|---------------------|--------------------|---------------------|-----------------------|--------------------------------|----------------------|----------------------|--------------------------------------|---------------------|
| | Inside. Inches. | Outside. Inches. | | | Internal. Inches. | External. Inches. | Inside. Inches. | Outside. Inches. |
| $\frac{1}{8}$ | .269 | .405 | .088 | .244 | .85 | 1.27 | 14.13 | 9.45 |
| $\frac{1}{4}$ | .364 | .540 | .088 | .424 | 1.14 | 1.70 | 10.52 | 7.06 |
| $\frac{3}{8}$ | .493 | .675 | .091 | .567 | 1.55 | 2.12 | 7.74 | 5.66 |
| $\frac{1}{2}$ | .622 | .840 | .109 | .850 | 1.95 | 2.64 | 6.15 | 4.55 |
| $\frac{3}{4}$ | .824 | 1.050 | .113 | 1.130 | 2.59 | 3.30 | 4.63 | 3.64 |
| 1 | 1.049 | 1.315 | .133 | 1.678 | 3.30 | 4.13 | 3.64 | 2.91 |
| $1\frac{1}{4}$ | 1.380 | 1.660 | .140 | 2.272 | 4.34 | 5.22 | 2.77 | 2.30 |
| $1\frac{1}{2}$ | 1.610 | 1.900 | .145 | 2.717 | 5.06 | 5.97 | 2.37 | 2.01 |
| 2 | 2.067 | 2.375 | .154 | 3.652 | 6.49 | 7.46 | 1.85 | 1.61 |
| $2\frac{1}{2}$ | 2.469 | 2.875 | .203 | 5.793 | 7.76 | 9.03 | 1.55 | 1.33 |
| 3 | 3.068 | 3.500 | .216 | 7.575 | 9.64 | 11.00 | 1.24 | 1.09 |
| $3\frac{1}{2}$ | 3.548 | 4.000 | .226 | 9.109 | 11.15 | 12.57 | 1.08 | .95 |
| 4 | 4.026 | 4.500 | .237 | 10.790 | 12.65 | 14.14 | .95 | .85 |
| $4\frac{1}{2}$ | 4.506 | 5.000 | .247 | 12.538 | 14.16 | 15.71 | .85 | .76 |
| 5 | 5.047 | 5.563 | .258 | 14.617 | 15.86 | 17.48 | .76 | .69 |
| 6 | 6.065 | 6.625 | .280 | 18.974 | 19.05 | 20.81 | .63 | .58 |
| 7 | 7.023 | 7.625 | .301 | 23.544 | 22.06 | 23.95 | .54 | .50 |
| 8 | 8.071 | 8.625 | .277 | 24.696 | 25.36 | 27.10 | .47 | .44 |
| 8 | 7.981 | 8.625 | .322 | 28.554 | 25.07 | 27.10 | .48 | .44 |
| 9 | 8.941 | 9.625 | .342 | 33.907 | 28.09 | 30.24 | .43 | .40 |
| 10 | 10.192 | 10.750 | .279 | 31.201 | 32.02 | 33.77 | .37 | .36 |
| 10 | 10.136 | 10.750 | .307 | 34.240 | 31.84 | 33.77 | .38 | .36 |
| 10 | 10.020 | 10.750 | .365 | 40.483 | 31.48 | 33.77 | .38 | .36 |
| 11 | 11.000 | 11.750 | .375 | 45.557 | 34.56 | 36.91 | .35 | .33 |
| 12 | 12.090 | 12.750 | .330 | 43.773 | 37.98 | 40.06 | .32 | .30 |
| 12 | 12.000 | 12.750 | .375 | 49.562 | 37.70 | 40.06 | .32 | .30 |
| 13 | 13.250 | 14.000 | .375 | 54.568 | 41.63 | 43.98 | .29 | .27 |
| 14 | 14.250 | 15.000 | .375 | 58.573 | 44.77 | 47.12 | .27 | .25 |
| 15 | 15.250 | 16.000 | .375 | 62.579 | 47.91 | 50.27 | .25 | .24 |

| Nominal Diameter. Inches. | AREA. | | Lineal Feet containing 1 Cubic Foot. | No. of Threads per Inch. | Contents to 1 Lineal Foot. Gallons. | COUPLINGS FOR PIPE. | |
|---------------------------------|--------------------------|--------------------------|--|--------------------------------|---|--------------------------|--------------------|
| | Internal. Sq. Inches. | External. Sq. Inches. | | | | Outside Diam. Inches. | Length. Inches. |
| $\frac{1}{8}$ | .06 | .13 | 2540.00 | 27 | .003 | .59 | .81 |
| $\frac{1}{4}$ | .10 | .23 | 1384.00 | 18 | .005 | .72 | .94 |
| $\frac{3}{8}$ | .19 | .36 | 754.40 | 18 | .010 | .84 | 1.06 |
| $\frac{1}{2}$ | .30 | .55 | 473.90 | 14 | .016 | 1.00 | 1.31 |
| $\frac{3}{4}$ | .53 | .87 | 270.00 | 14 | .028 | 1.33 | 1.56 |
| 1 | .87 | 1.35 | 166.60 | $11\frac{1}{2}$ | .045 | 1.56 | 1.81 |
| $1\frac{1}{4}$ | 1.50 | 2.16 | 96.28 | $11\frac{1}{2}$ | .078 | 1.95 | 2.13 |
| $1\frac{1}{2}$ | 2.04 | 2.84 | 70.73 | $11\frac{1}{2}$ | .106 | 2.22 | 2.38 |
| 2 | 3.35 | 4.43 | 42.91 | $11\frac{1}{2}$ | .174 | 2.75 | 2.63 |
| $2\frac{1}{2}$ | 4.78 | 6.49 | 30.08 | 8 | .249 | 3.28 | 2.88 |
| 3 | 7.38 | 9.62 | 19.48 | 8 | .380 | 3.94 | 3.13 |
| $3\frac{1}{2}$ | 9.88 | 12.57 | 14.57 | 8 | .514 | 4.44 | 3.63 |
| 4 | 12.72 | 15.90 | 11.31 | 8 | .661 | 5.00 | 3.63 |
| $4\frac{1}{2}$ | 15.93 | 19.63 | 9.03 | 8 | .828 | 5.50 | 3.63 |
| 5 | 19.99 | 24.30 | 7.20 | 8 | 1.040 | 6.22 | 4.13 |
| 6 | 28.87 | 34.47 | 4.98 | 8 | 1.500 | 7.31 | 4.13 |
| 7 | 38.71 | 45.66 | 3.72 | 8 | 2.010 | 8.31 | 4.13 |
| 8 | 51.16 | 58.43 | 2.82 | 8 | 2.660 | 9.31 | 4.63 |
| 8 | 50.03 | 58.43 | 2.88 | 8 | 2.610 | 9.31 | 4.63 |
| 9 | 62.79 | 72.76 | 2.29 | 8 | 3.260 | 10.38 | 5.13 |
| 10 | 81.47 | 90.76 | 1.77 | 8 | 4.230 | 11.66 | 6.13 |
| 10 | 80.33 | 90.76 | 1.78 | 8 | 4.190 | 11.66 | 6.13 |
| 10 | 78.86 | 90.76 | 1.83 | 8 | 4.100 | 11.66 | 6.13 |
| 11 | 95.03 | 108.43 | 1.52 | 8 | 4.940 | 12.66 | 6.13 |
| 12 | 114.63 | 127.68 | 1.25 | 8 | 5.960 | 13.88 | 6.13 |
| 12 | 113.10 | 127.68 | 1.27 | 8 | 5.880 | 13.88 | 6.13 |
| 13 | 137.89 | 153.94 | 1.04 | 8 | 7.160 | 15.06 | 6.13 |
| 14 | 159.48 | 176.71 | .90 | 8 | 8.280 | 16.38 | 6.13 |
| 15 | 182.65 | 201.06 | .79 | 8 | 9.490 | 17.38 | 6.13 |

MANUFACTURERS' STANDARD SPECIFICATIONS.

REVISED APRIL 22, 1919

STRUCTURAL STEEL.**Grades.**

1. These specifications cover three classes of structural steel, namely:

Class A steel, to be used for railway bridges and ships.

Class B steel, to be used for buildings, highway bridges, train sheds and similar structures.

Class C steel, to be used for structural rivets.

I. MANUFACTURE.**Process.**

2. Steel for Classes A and C shall be made by the open-hearth process. Steel for Class B may be made either by the open-hearth or by the Bessemer process.

II. CHEMICAL PROPERTIES AND TESTS.**Chemical Composition.**

3. The steel shall conform to the following requirements as to chemical composition:

| Elements Considered. | Class A Steel. | Class B Steel. | Class C Steel. |
|------------------------------|----------------|----------------|----------------|
| Phosphorus, max., per cent.: | | | |
| Basic open hearth..... | 0.04 | 0.06 | 0.04 |
| Acid open hearth..... | 0.06 | 0.08 | 0.04 |
| Bessemer..... | | 0.10 | |
| Sulphur, max., per cent..... | 0.06 | | 0.05 |

Ladle Analyses.

4. To determine whether the material conforms to the requirements specified in section 3, an analysis shall be made by the manufacturer from a test ingot taken during the pouring of each melt. A copy of this analysis shall be given to the purchaser or his representative, if requested.

Check Analyses.

5. A check analysis of Class A and Class C steel may be made by the purchaser from finished material representing each melt, in which case an excess of 25 per cent. above the requirements specified in section 3 shall be allowed.

III. PHYSICAL PROPERTIES AND TESTS.**Tension Tests.**

6. The steel shall conform to the following requirements as to tensile properties:

| Properties Considered. | Class A Steel. | Class B Steel. | Class C Steel. |
|--|--------------------------|--------------------------|-------------------------|
| Tensile strength, lb. per sq. in. | 55,000-65,000 | 55,000-65,000* | 46,000-56,000 |
| Yield point, minimum, lb. per sq. in. | 0.5 tens. str. | 0.5 tens. str. | 0.5 tens. str. |
| Elongation in 8 in., min., per cent. | 1,400,000† tens. str. | 1,400,000† tens. str. | 1,400,000 tens. str. |
| Elongation in 2 in., min., per cent. (Fig. 2)..... | 22 | 22 | |

* See section 8. † See section 9.

Yield Point.

7. The yield point shall be determined by the drop of the beam of the testing machine.

Modification in Tensile Strength.

8. Class B steel may have tensile strength up to 70,000 lb. maximum, provided the elongation is not less than the percentage required for 65,000 lb. tensile strength.

Modifications in Elongation.

9. (a) For material over $\frac{3}{4}$ in. in thickness, a deduction of 1 from the percentage of elongation in 8 in. specified for Classes A and B in section 6 shall be made for each increase of $\frac{1}{8}$ in. in thickness above $\frac{3}{4}$ in., to a minimum of 18 per cent.

(b) For material under $\frac{5}{8}$ in. in thickness, a deduction of 2.5 from the percentage of elongation in 8 in. specified for Classes A and B in section 6 shall be made for each decrease of $\frac{1}{16}$ in. in thickness below $\frac{5}{8}$ in.

Character of Fracture.

10. All broken tension test specimens shall show a silky fracture.

Bend Tests.

11. (a) The test specimen for plates, shapes and bars shall bend cold through 180 deg. without fracture on the outside of the bent portion, as follows: For material $\frac{3}{4}$ in. and under in thickness, flat on itself; for material over $\frac{3}{4}$ in. up to $1\frac{1}{4}$ in. in thickness, around a pin the diameter of which is equal to $1\frac{1}{2}$ times the thickness of the specimen; and for material over $1\frac{1}{4}$ in. in thickness, around a pin the diameter of which is equal to twice the thickness of the specimen.

(b) The test specimen for pins and rollers shall bend cold through 180 deg. around a 1-in. pin without fracture on the outside of the bent portion.

(c) A rivet rod shall bend cold through 180 deg. flat on itself without fracture on the outside of the bent portion.

(d) Bend tests may be made by pressure or by blows.

Test Specimens.

12. (a) Tension and bend test specimens shall be taken from the finished rolled or forged product, and shall not be annealed or otherwise treated, except as specified in section 13.

(b) Tension and bend test specimens for plates, shapes and bars, except as specified in paragraph (c), shall be of the full thickness of material as rolled, and with both edges milled to the form and dimensions shown in Fig. 1, or may have both edges parallel.

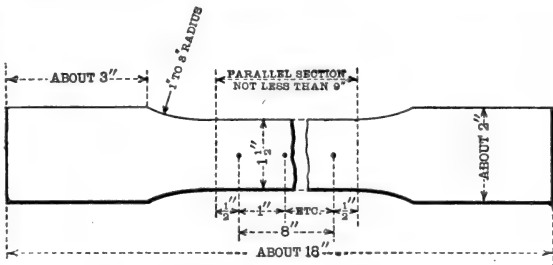


FIG. 1.

(c) Tension and bend test specimens for plates and bars (except eye-bar flats) over 1½ in. in thickness or diameter may be turned or planed to a diameter or thickness of at least ¾ in. for a length of at least 9 in.

(d) Tension and bend test specimens for pins and rollers shall be taken parallel to the axis, 1 in. from the surface of the bar. Tension test specimens shall be of the form and dimensions shown in Fig. 2. Bend test specimens shall be 1 in. by $\frac{1}{2}$ in. in section.

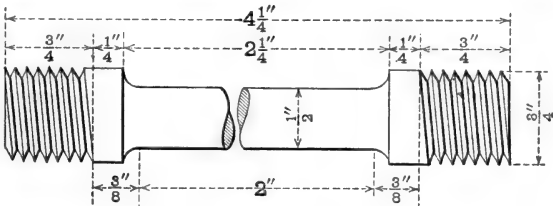


FIG. 2.

(e) Rivet bars shall be tested in full-size section as rolled.

Annealed Specimens.

13. Test specimens for material which is to be annealed or otherwise treated before use shall be cut from properly annealed or similarly treated short lengths of the full section of the piece.

Number of Tests.

14. (a) At least one tension test and one bend test shall be made from each melt. If material from one melt differs $\frac{3}{8}$ in. or more in thickness, tests shall be made from both the thickest and the thinnest material rolled.

(b) If any test specimen develops flaws, or if an 8-in. tension test specimen breaks outside the middle third of the gage length, or if a 2-in. tension test specimen breaks outside the gage length, it may be discarded and another specimen substituted therefor.

(c) Material intended for fillers or ornamental purposes will not be subject to test.

IV. PERMISSIBLE VARIATIONS IN WEIGHT AND GAGE.**Permissible Variations.**

15. (a) The sectional area or weight of each structural shape and of each rolled-edge plate up to and including 36 inches in width shall not vary more than 2.5 per cent. from theoretical or specified amounts.

(b) The thickness or weight of each universal plate over 36 in. in width, and of each sheared plate, shall conform to the schedules of permissible variations for sheared plates, Manufacturers' Standard Practice, appended to these specifications.

(c) The weights of angles, tees, zees and channels of bar sizes, and the dimensions of rounds, squares, hexagons and flats, shall conform to the Manufacturers' Standard Practice governing the allowable variations in size and weight of hot-rolled bars.

V. FINISH.**Finish.**

16. The finished material shall be free from injurious defects and shall have a workmanlike finish.

VI. MARKING.**Marking.**

17. The name of the manufacturer and the melt number shall be legibly marked, stamped or rolled upon all finished material, except that each pin and roller shall be stamped on the end. Rivet and lattice steel and other small pieces may be shipped in securely fastened bundles, with the above marks legibly stamped on attached metal tags. Test specimens shall have their melt numbers plainly marked or stamped.

VII. INSPECTION AND REJECTION.**Inspection.**

18. The inspector representing the purchaser shall have free entry, at all times while work on the contract of the purchaser is being performed, to all parts of the manufacturer's works which concern the manufacture of the

material ordered. The manufacturer shall afford the inspector, free of cost, all reasonable facilities to satisfy him that the material is being furnished in accordance with these specifications. All tests and inspection shall be made at the place of manufacture prior to shipment, and shall be so conducted as not to interfere unnecessarily with the operation of the works.

Rejection.

19. Material which, subsequent to the above tests at the mills and its acceptance there, develops weak spots, brittleness, cracks or other imperfections, or is found to have injurious defects, may be rejected at the shop, and shall then be replaced by the manufacturer at his own cost.

BOILER STEEL.

Grades.

1. There shall be three grades of steel for boilers, namely: flange, firebox, and boiler rivet.

I. MANUFACTURE.

Process.

2. The steel shall be made by the open-hearth process.

II. CHEMICAL PROPERTIES AND TESTS.

Chemical Composition.

3. The steel shall conform to the following requirements as to chemical composition:

| Elements Considered. | Flange Steel. | Firebox Steel. | Boiler Rivet Steel. |
|------------------------------|---------------|----------------|---------------------|
| Manganese, per cent..... | 0.30 to 0.60 | 0.30 to 0.50 | 0.30 to 0.50 |
| Phosphorus, max., per cent.: | | | |
| Basic..... | 0.04 | 0.035 | 0.04 |
| Acid..... | 0.05 | 0.04 | 0.04 |
| Sulphur, max., per cent..... | 0.05 | 0.04 | 0.045 |

Ladle Analyses.

4. To determine whether the material conforms to the requirements specified in section 3, an analysis shall be made by the manufacturer from a test ingot taken during the pouring of each melt. A copy of this analysis shall be given to the purchaser or his representative.

Check Analyses.

5. A check analysis may be made by the purchaser from a broken tension test specimen representing each plate as rolled, and this analysis shall conform to the requirements specified in section 3.

III. PHYSICAL PROPERTIES AND TESTS.

Tension Tests.

6. The steel shall conform to the following requirements as to tensile properties:

| Properties Considered. | Flange Steel. | Firebox Steel. | Boiler Rivet Steel. |
|--|---------------------------------|---------------------------------|--------------------------------|
| Tensile strength, lb. per sq. in..... | 55,000-65,000 | 52,000- 60,000 | 45,000-55,000 |
| Yield point, min., lb. per sq. in..... | 0.5 tens. str. | 0.5 tens. str. | 0.5 tens. str. |
| Elongation in 8 in., min., per cent..... | <u>1,450,000*</u> tens. str. | <u>1,450,000*</u> tens. str. | <u>1,450,000</u> tens. str. |

* See section 8.

Yield Point.

7. The yield point shall be determined by the drop of the beam of the testing machine.

Modifications in Elongation.

8. (a) For plates over $\frac{3}{4}$ in. in thickness, a deduction of 0.5 from the specified percentage of elongation will be allowed for each increase of $\frac{1}{8}$ in. in thickness above $\frac{3}{4}$ in., to a minimum of 20 per cent.

(b) For plates under $\frac{1}{8}$ in. in thickness, a deduction of 2.5 from the percentage of elongation specified in section 6 shall be made for each decrease of $\frac{1}{8}$ in. in thickness below $\frac{1}{8}$ in.

Bend Tests.

9. (a) Cold-bend tests shall be made on the material as rolled.

(b) Quench-bend test specimens, before bending, shall be heated to a light cherry red as seen in the dark (about 1200 deg. F.), and quenched in water the temperature of which is about 80 deg. F.

(c) Specimens for cold-bend and quench-bend tests of flange and firebox steel shall bend through 180 deg. without fracture on the outside of the bent portion, as follows: For material $\frac{3}{4}$ in. and under in thickness, flat on themselves; for material over $\frac{3}{4}$ in. up to $1\frac{1}{4}$ in. in thickness, around a pin the diameter of which is equal to the thickness of the specimen; and for material over $1\frac{1}{4}$ in. in thickness, around a pin the diameter of which is equal to $1\frac{1}{2}$ times the thickness of the specimen.

(d) Specimens for cold-bend and quench-bend tests of boiler rivet steel shall bend cold through 180 deg. flat on themselves without fracture on the outside of the bent portion.

(e) Bend tests may be made by pressure or by blows.

Test Specimens.

10. (a) Tension and bend test specimens for plates shall be taken from the finished product, and shall be of the full thickness of material as rolled. Tension test specimens shall be of the form and dimensions shown in Fig. 1. Bend test specimens shall be $1\frac{1}{2}$ in. to $2\frac{1}{2}$ in. wide, and shall have the sheared edges milled or planed.

(b) The tension and bend test specimens for rivet bars shall be of the full-size section of material as rolled.

Number of Tests.

11. (a) One tension, one cold-bend, and one quench-bend test shall be made from each plate as rolled.

(b) Two tension, two cold-bend, and two quench-bend tests shall be made for each melt of rivet steel.

(c) If any test specimen develops flaws, or if a tension test specimen breaks outside the middle third of the gage length, it may be discarded and another specimen substituted therefor.

IV. PERMISSIBLE VARIATIONS IN WEIGHT AND GAGE.**Permissible Variations.**

12. (a) The thickness or weight of each sheared plate shall conform to the schedule of permissible variations, Manufacturers' Standard Practice, appended to these specifications.

(b) The dimensions of rivet bars shall conform to the Manufacturers' Standard Practice governing allowable variations in the size of hot-rolled bars.

V. FINISH.**Finish.**

13. The finished material shall be free from injurious defects and shall have a workmanlike finish.

VI. MARKING.**Marking.**

14. The melt or slab number, name of the manufacturer, grade, and the minimum tensile strength for its grade as specified in section 6 shall be legibly stamped on each plate. The melt or slab number shall be legibly stamped on each test specimen representing that melt or slab.

VII. INSPECTION AND REJECTION.**Inspection.**

15. The inspector representing the purchaser shall have free entry, at all times while work on the contract of the purchaser is being performed, to all parts of the manufacturer's works which concern the manufacture of the material ordered. The manufacturer shall afford the inspector, free of cost, all reasonable facilities to satisfy him that the material is being furnished in accordance with these specifications. All tests and inspection shall be made at the place of manufacture prior to shipment, and shall be so conducted as not to interfere unnecessarily with the operation of the works.

Rejection.

16. Material which, subsequent to the above tests at the mills and its acceptance there, develops weak spots, brittleness, cracks or other imperfections, or is found to have injurious defects, may be rejected at the shop, and shall then be replaced by the manufacturer at his own cost.

MANUFACTURERS' STANDARD PRACTICE.**PERMISSIBLE VARIATIONS IN WEIGHT AND THICKNESS
OF SHEARED PLATES.****WHEN ORDERED TO WEIGHT.**

One cubic inch of rolled steel is assumed to weigh 0.2833 pound.

When ordered to weight per square foot, the weight of each lot* in each shipment shall not vary from the weight ordered more than the amount given in the following table:

| Ordered Weight Lbs. per Sq. Ft. | Permissible Variations in Average Weights per Square Foot of Plates for Widths Given, Expressed in Percentages of Ordered Weights. | | | | | | | | | |
|------------------------------------|---|--------|------------------------------------|--------|------------------------------------|--------|------------------------------------|--------|------------------------------------|--------|
| | Under 48 In. | | 48 in. incl. to 60 in. excl. | | 60 in. incl. to 72 in. excl. | | 72 in. incl. to 84 in. excl. | | 84 in. incl. to 96 in. excl. | |
| | Over. | Under. | Over. | Under. | Over. | Under. | Over. | Under. | Over. | Under. |
| Under 5 | 5 | 3 | 5.5 | 3 | 6 | 3 | 7 | 3 | | |
| 5 incl. to 7.5 excl. | 4.5 | 3 | 5 | 3 | 5.5 | 3 | 6 | 3 | | |
| 7.5 " " 10 " | 4 | 3 | 4.5 | 3 | 5 | 3 | 5.5 | 3 | 6 | 3 |
| 10 " " 12.5 " | 3.5 | 2.5 | 4 | 3 | 4.5 | 3 | 5 | 3 | 5.5 | 3 |
| 12.5 " " 15 " | 3 | 2.5 | 3.5 | 2.5 | 4 | 3 | 4.5 | 3 | 5 | 3 |
| 15 " " 17.5 " | 2.5 | 2.5 | 3 | 2.5 | 3.5 | 2.5 | 4 | 3 | 4.5 | 3 |
| 17.5 " " 20 " | 2.5 | 2 | 2.5 | 2.5 | 3 | 2.5 | 3.5 | 2.5 | 4 | 3 |
| 20 " " 25 " | 2 | 2 | 2.5 | 2 | 2.5 | 2.5 | 3 | 2.5 | 3.5 | 2.5 |
| 25 " " 30 " | 2 | 2 | 2 | 2 | 2.5 | 2 | 2.5 | 2.5 | 3 | 2.5 |
| 30 " " 40 " | 2 | 2 | 2 | 2 | 2 | 2 | 2.5 | 2 | 2.5 | 2.5 |
| 40 or over | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2.5 | 2 |

NOTE:—The weight per square foot of individual plates shall not vary from the ordered weight by more than $1\frac{1}{2}$ times the amount given in this table.

* The term "lot" applied to this table means all of the plates of each group width and group weight.

MANUFACTURERS' STANDARD PRACTICE.**PERMISSIBLE VARIATIONS IN WEIGHT AND THICKNESS
OF SHEARED PLATES.****WHEN ORDERED TO WEIGHT.**

One cubic inch of rolled steel is assumed to weigh 0.2833 pound.

When ordered to weight per square foot, the weight of each lot* in each shipment shall not vary from the weight ordered more than the amount given in the following table:

| Permissible Variations in Average Weights per Square Foot of Plates for Widths Given, Expressed in Percentages of Ordered Weights. | | | | | | | | Ordered Weight Lbs. per Sq. Ft. |
|---|--------|--------------------------------------|--------|--------------------------------------|--------|---------------------|--------|--|
| 96 in. incl. to 108 in. excl. | | 108 in. incl. to 120 in. excl. | | 120 in. incl. to 132 in. excl. | | 132 in. or over. | | |
| Over. | Under. | Over. | Under. | Over. | Under. | Over. | Under. | |
| | | | | | | | | Under 5 |
| | | | | | | | | 5 incl. to 7.5 excl. |
| 7 | 3 | 8 | 3 | | | | | 7.5 " " 10 " |
| 6 | 3 | 7 | 3 | 8 | 3 | 9 | 3 | 10 " " 12.5 " |
| 5.5 | 3 | 6 | 3 | 7 | 3 | 8 | 3 | 12.5 " " 15 " |
| 5 | 3 | 5.5 | 3 | 6 | 3 | 7 | 3 | 15 " " 17.5 " |
| 4.5 | 3 | 5 | 3 | 5.5 | 3 | 6 | 3 | 17.5 " " 20 " |
| 4 | 3 | 4.5 | 3 | 5 | 3 | 5.5 | 3 | 20 " " 25 " |
| 3.5 | 3 | 4 | 3 | 4.5 | 3 | 5 | 3 | 25 " " 30 " |
| 3 | 2.5 | 3.5 | 3 | 4 | 3 | 4.5 | 3 | 30 " " 40 " |
| 2.5 | 2.5 | 3 | 2.5 | 3.5 | 3 | 4 | 3 | 40 or over |

NOTE:—The weight per square foot of individual plates shall not vary from the ordered weight by more than $1\frac{1}{2}$ times the amount given in this table.

* The term "lot" applied to this table means all of the plates of each group width and group weight.

MANUFACTURERS' STANDARD PRACTICE.

PERMISSIBLE VARIATIONS IN WEIGHT AND THICKNESS OF SHEARED PLATES (CONTINUED).

WHEN ORDERED TO THICKNESS.

One cubic inch of rolled steel is assumed to weigh 0.2833 pound.

When ordered to thickness, the thickness of each plate shall not vary more than 0.01 inch under that ordered. The overweight of each lot* in each shipment shall not exceed the amount given in the following table:

| Ordered Thickness Inch. | Permissible Excess in Average Weights Per Square Foot of Plates for Widths Given, Expressed in Percentages of Nominal Weights. | | | | | | | | |
|---|---|---------------------------------------|---------------------------------------|---------------------------------------|---------------------------------------|--|---|---|-----------------------|
| | Under 48 in. | 48 in. incl. to 60 in. excl. | 60 in. incl. to 72 in. excl. | 72 in. incl. to 84 in. excl. | 84 in. incl. to 96 in. excl. | 96 in. incl. to 108 in. excl. | 108 in. incl. to 120 in. excl. | 120 in. incl. to 132 in. excl. | 132 in. or over |
| Under $\frac{1}{8}$ | 9 | 10 | 12 | 14 | | | | | |
| $\frac{1}{8}$ incl. to $\frac{3}{16}$ excl. | 8 | 9 | 10 | 12 | | | | | |
| $\frac{3}{16}$ " " $\frac{1}{4}$ " | 7 | 8 | 9 | 10 | 12 | | | | |
| $\frac{1}{4}$ " " $\frac{5}{16}$ " | 6 | 7 | 8 | 9 | 10 | 12 | 14 | 16 | 19 |
| $\frac{5}{16}$ " " $\frac{3}{8}$ " | 5 | 6 | 7 | 8 | 9 | 10 | 12 | 14 | 17 |
| $\frac{3}{8}$ " " $\frac{7}{16}$ " | 4.5 | 5 | 6 | 7 | 8 | 9 | 10 | 12 | 15 |
| $\frac{7}{16}$ " " $\frac{1}{2}$ " | 4 | 4.5 | 5 | 6 | 7 | 8 | 9 | 10 | 13 |
| $\frac{1}{2}$ " " $\frac{5}{8}$ " | 3.5 | 4 | 4.5 | 5 | 6 | 7 | 8 | 9 | 11 |
| $\frac{5}{8}$ " " $\frac{3}{4}$ " | 3 | 3.5 | 4 | 4.5 | 5 | 6 | 7 | 8 | 9 |
| $\frac{3}{4}$ " " 1 " | 2.5 | 3 | 3.5 | 4 | 4.5 | 5 | 6 | 7 | 8 |
| 1 or over | 2.5 | 2.5 | 3 | 3.5 | 4 | 4.5 | 5 | 6 | 7 |

* The term "lot" applied to this table means all of the plates of each group width and group thickness.

WOODEN BEAMS AND COLUMNS.

The results of a series of studies of wooden beams and columns of various kinds of American timber are contained in the Proceedings of the Fifth Annual Convention of the Association of Railway Superintendents of Bridges and Buildings, October, 1895, at which the Committee on Strength of Bridge and Trestle Timbers presented a report, portions of which have been used in preparing certain of the tables on the following pages, but as noted thereon the arrangement and values in many cases have been modified by later information from various sources.

The publications of the Forestry Division of the United States Department of Agriculture, Bulletins Nos. 8 and 12, and Circular No. 15, contain reports of tests of American woods, and deductions drawn therefrom. Extracts and tables from these reports are given on the following pages.

The tables of safe loads for wooden beams and tables of strength of wooden columns given on the following pages have been specially calculated for this book, using the information regarding the properties of the various species contained in the reports above referred to, as modified in some cases by later data.

In order that information on this subject will be more complete, tables are given herein showing structural timber stress values, as published in the United States Forestry Service Bulletin, No. 108, and also those recommended by the American Railway Engineering and Maintenance of Way Association, Bulletin No. 107.

Explanation of the Tables of Safe Loads in Pounds, Uniformly Distributed, for Rectangular Wooden Beams One Inch Thick, Pages 416 to 421 Inclusive.

General.

For convenience in use, three of these tables have been prepared from which the safe loads of the various species can be obtained, either directly or by proportion as stated in the footnotes.

The values given in the tables are the safe loads in pounds uniformly distributed, including the weight of the beam itself, for rectangular beams one inch thick for spans from four to forty feet and for depths from four to twenty-four inches. The safe load for a beam of any thickness may be found by multiplying the values given in the tables by the thickness of the beam in inches.

The last column of each of the three Tables of Safe Loads for

Rectangular Wooden Beams gives a coefficient of deflection, by means of which the deflection for any beam may be obtained, corresponding to the given span and safe load, by dividing the coefficient by the depth of the beam in inches, which will give approximately the deflection in inches under the given conditions.

In each table the deflection coefficient is given for only one species of wood, as shown, but the deflections for other species may be obtained from these by proportion as explained hereafter.

For the reason that wood has no well-defined limit or modulus of elasticity the deflections obtained by the use of the coefficients are only approximate and will vary, according to the moisture content of the wood and the character of the loading. The deflections thus obtained are, therefore, useful only as a general indication of the amount of bending to be expected under the given conditions and are not exact as in the case of materials like steel, which has a well-defined limit and modulus of elasticity.*

The safe loads for other species of woods than those stated in the headings of the tables may be obtained from those given, by direct proportion, dependent upon the ratio of their allowable unit stress as compared with that for which the table is figured, as stated in the foot-notes at the bottom of the tables.

* NOTE.—“A series of tests, undertaken at the College of Forestry at Cornell University, seems to demonstrate that, at least in coniferous wood, a definite elastic limit for any particular piece can be easily shown, and, that it coincides with the theoretically calculated elastic limit upon the bases of compression tests and their application, according to Neely's formula.”

Explanation of the Table of Safe Loads for Rectangular Beams of White Pine, Cedar, Spruce or Eastern Fir.

The values for the various species of woods, which are included in this table are calculated for an allowable fibre stress, for flexure, of 700 pounds per square inch.

The deflection coefficients are given for white pine and are based upon a modulus of elasticity of 1 000 000 pounds per square inch.

The lower dotted line crossing the table indicates the limits of spans for which the deflection will exceed $\frac{1}{360}$ of the span for the kind of wood for which the deflection coefficient is given. For spans below the line the safe loads given in the tables will produce a deflection greater than $\frac{1}{360}$ of the span, while those above the line will produce less than this, which is the usual limit of deflection in order to prevent cracking of plastered ceilings. Similarly,

the upper dotted line indicates the limit of deflection for the kind of wood for which the deflection coefficient is given, corresponding to a modulus of elasticity of 500 000 pounds per square inch, which should be considered in cases where the deflection should be more closely limited.

The coefficients of deflection for Cedar corresponding to moduli of 700 000 and 350 000 may be obtained by multiplying those of the table by $\frac{1}{2}$ and $\frac{3}{4}$ respectively, and for Spruce and Eastern Fir corresponding to moduli of 1 200 000 and 600 000 by multiplying those of the table by $\frac{2}{3}$ and $\frac{1}{2}$ respectively.

The full zig-zag line in the table gives the limits of the safe loads corresponding to the allowable shearing stress along the neutral axis of the beam. The safe loads above the line, which are based upon the extreme fibre strains, will produce shearing stresses along the axis or with the grain in excess of that allowable, which, in the case of White Pine and the other woods of this table, is 100 pounds per square inch.

The position of this line, which indicates the limit of safe loads for shearing along the neutral axis, was determined by the aid of the following formula:

$$W = \frac{4bds}{3}$$

in which

W = safe load in pounds uniformly distributed.

d = depth of beam in inches.

b = breadth of beam in inches.

s = allowable shear in the direction of the grain in pounds per square inch.

Explanation of the Table of Safe Loads for Rectangular Beams of Short-leaf Yellow Pine.

The table is calculated for an allowable fibre stress, for flexure, of 1 000 pounds per square inch.

The deflection coefficients are figured for a modulus of elasticity of 1 200 000 pounds per square inch, but may be used for other moduli, after obtaining the corresponding coefficients by proportion as heretofore explained.

The lower dotted line across the table indicates the limits of spans for which the safe load will produce deflections greater than

$\frac{1}{360}$ of the length of the beam. Values above the line will give less deflection than this, and those below will give greater, based on a modulus of 1 200 000 pounds per square inch. Similarly, the upper dotted line indicates the limit of deflection corresponding to a modulus of elasticity of 600 000 pounds per square inch.

The full zig-zag line across the table indicates the limiting spans and loads based on the allowable intensity of shearing stress along the neutral axis of the beam. The values above the full zig-zag line correspond to shearing stresses greater than the allowable stress in the direction of the grain for Short-leaf Yellow Pine, while those below the line correspond to shearing stresses less than that allowable, which, in this case, is assumed to be 100 pounds per square inch.

Explanation of Tables of Safe Loads for Rectangular Beams of White Oak and Long-leaf Yellow Pine.

This table is computed for an allowable fibre stress of 1 200 pounds per square inch, for flexure, and the deflection coefficients are calculated for a modulus of elasticity of 1 500 000 pounds per square inch.

The limit for a deflection of $\frac{1}{360}$ of the span is indicated by the lower dotted zig-zag line on the tables, the values below which correspond to deflections greater than, and those above to deflections less than, the limiting deflections. The upper dotted zig-zag line similarly indicates the limits of deflection for a modulus of elasticity of 750 000 pounds per square inch.

The lower full zig-zag line indicates the limit of allowable shearing stress along the axis corresponding to the allowable intensity, for Yellow Pine, of 150 pounds per square inch.

Similarly, the upper full zig-zag line indicates the limits for shearing along the axis for White Oak based on an allowable intensity of 200 pounds per square inch.

BEARING AT POINTS OF SUPPORT.

Care should be taken in designing to provide sufficient bearing at the points of support so that the allowable intensity of compression across the grain, as given in the tables on pages 409 to 415, is not exceeded.

This may be obtained, where necessary, by the use of corbels or bearing plates of harder wood arranged so as to give a large bearing area against the softer beam.

The following statements are made in Bulletin No. 12, U. S. Department of Agriculture, Division of Forestry:

RECOMMENDED PRACTICE.

"Since the strength of timber varies very greatly with the moisture contents (see Bulletin 8 of the Forestry Division), the economical designing of such structures will necessitate their being separated into groups according to the maximum moisture contents in use.

MOISTURE CLASSIFICATION.

"Class A (moisture contents, 18 per cent.)—Structures freely exposed to the weather, such as railway trestles, uncovered bridges, etc.

"Class B (moisture contents, 15 per cent.)—Structures under roof but without side shelter, freely exposed to outside air, but protected from rain, such as roof trusses of open shops and sheds, covered bridges over streams, etc.

"Class C (moisture contents, 12 per cent.)—Structures in buildings unheated, but more or less protected from outside air, such as roof trusses of barns, enclosed shops and sheds, etc.

"Class D (moisture contents, 10 per cent.)—Structures in buildings at all times protected from the outside air, heated in the winter, such as roof trusses in houses, halls, churches, etc.

"For long-leaf pine add to all the values given in the tables, except those for moduli of elasticity, tension and shearing, for Class B, 15 per cent.; for Class C, 40 per cent.; and for Class D, 55 per cent. For the other species add to these values, for Class B, 8 per cent.; for Class C, 18 per cent., and for Class D, 25 per cent."

Based upon the above classification of structures, the two following tables have been figured to facilitate calculations of allowable loads for wooden beams and columns.

Proportion of the Values given in the "Tables of Safe Loads for Wooden Beams," Pages 416 to 421 inclusive, to be used in order to obtain the Safe Loads for the various classes of structures referred to above.

| Classes. | Yellow Pine. | All Others. |
|--------------|--------------|-------------|
| Class A..... | 1.00 | 1.00 |
| Class B..... | 1.15 | 1.08 |
| Class C..... | 1.40 | 1.18 |
| Class D..... | 1.55 | 1.25 |

Safety Factors to be applied to the Values given in the Table of "Strength of Solid Wooden Columns," Pages 422 and 423, in order to obtain the Safe Loads for the various classes of structures referred to above.

| Classes. | Yellow Pine. | All Others. |
|--------------|--------------|-------------|
| Class A..... | 0.20 | 0.20 |
| Class B..... | 0.23 | 0.22 |
| Class C..... | 0.28 | 0.24 |
| Class D..... | 0.31 | 0.25 |

**SPECIFIC GRAVITY AND WEIGHT PER FOOT
FOR VARIOUS KINDS OF TIMBER.**

| Name of Wood. | Specific Gravity. | Weight per Cubic Foot. | Weight per Foot, Board Measure. |
|--|-------------------|------------------------|---------------------------------|
| White Oak..... | 0.80 | 49.94 | 4.16 |
| White Pine..... | 0.38 | 23.72 | 1.98 |
| Southern Long-leaf or Georgia Yellow Pine..... | 0.61 | 38.08 | 3.17 |
| Douglas Fir..... | 0.51 | 31.84 | 2.65 |
| Short-leaf Yellow Pine..... | 0.51 | 31.84 | 2.65 |
| Red Pine (Norway Pine)..... | 0.50 | 31.21 | 2.60 |
| Spruce and Eastern Fir..... | 0.40 | 24.97 | 2.08 |
| Hemlock..... | 0.40 | 24.97 | 2.08 |
| Cypress..... | 0.46 | 28.72 | 2.39 |
| Cedar..... | 0.37 | 23.10 | 1.93 |
| Chestnut..... | 0.66 | 41.20 | 3.43 |
| California Redwood..... | 0.39 | 24.16 | 2.01 |
| California Spruce..... | 0.40 | 24.97 | 2.08 |

The specific gravities and weights given above are the averages of a large number of determinations by various authorities, for woods containing less than 15 per cent. of moisture or such as are commercially known as dry timber. The weights of green or unseasoned woods will be from 20 to 40 per cent. greater than those given in the above table.

SAFE UNIT STRESSES FOR TIMBER.

RECOMMENDED IN BULLETIN NO. 12, U. S. DEPARTMENT OF
AGRICULTURE, DIVISION OF FORESTRY.

Safe Unit Stresses at 18% Moisture.

| Species. | Modulus of Strength at Rupture per Square Inch. | Modulus of Elasticity per Square Inch. | Elastic Resilience per Cubic Inch. | Crushing Strength Endwise per Square Inch. | Crushing Strength Across the Grain per Square Inch. | Tensile Strength per Square Inch. | Shearing Strength per Square Inch. |
|---|---|--|--|--|---|---|--|
| | Lbs. | Lbs. | Lbs. | Lbs. | Lbs. | Lbs. | Lbs. |
| Long-leaf Pine (<i>Pinus palustris</i>) D | 1550 | 720000 | 1.30 | 1000 | 215 | 12000 | 125 |
| Short-leaf Pine (<i>Pinus echinata</i>) D..... | 1300 | 600000 | 1.30 | 840 | 215 | 9000 | 100 |
| White Pine (<i>Pinus strobus</i>)..... | 880 | 435000 | 1.00 | 700 | 147 | 7000 | 75 |
| Norway Pine (<i>Pinus resinosa</i>)..... | 1090 | 566000 | | 760 | 143 | | |
| Colorado Pine (<i>Pinus ponderosa</i>)..... | 980 | 444000 | | 630 | 180 | | |
| Douglas Fir (<i>Pseudotsuga douglasii</i>)..... | 1320 | 690000 | | 880 | 167 | | |
| Redwood (<i>Sequoia sempervirens</i>)..... | *1440 | †226000 | | 650 | 115 | | |
| Red Cedar (<i>Juniperus virginiana</i>)..... | 1000 | 335000 | | 700 | 250 | | |
| Bald Cypress (<i>Taxodium distichum</i>) D... | 1000 | 450000 | 1.10 | 675 | 120 | 6000 | 60 |
| White Oak (<i>Quercus alba</i>) D..... | 1200 | 550000 | 1.25 | 800 | 400 | 10000 | 200 |
| Factor of Safety..... | 5 | 2 | 1 | 5 | 3 | 1 | 4 |

The values marked "D" were obtained from experiments made by the Forestry Division. The other values were obtained from various sources, chiefly the 10th Census Report, but so modified as to give results comparable with Forestry Division values. To arrive at true average values of strength multiply safe loads by factor of safety given in each column. The value for resilience and tensile strength are the ultimate values. The former is practically never used in designing. The latter is a factor impossible to develop in practice, since the piece will always fail in some other way, usually by shearing.

The crushing strength across the grain in above is based upon a crushing of 3 per cent. of the cross sectional height of the piece.

* This value is certainly too large.

† " " " " " small.—Ed.

AVERAGE TESTED STRENGTH VALUES OF STRUCTURAL TIMBERS WITH ORDINARY DEFECTS.

| Kind of Timber. | Condition. | Average Moisture Content. | Bending. | |
|---|--------------|---------------------------------|--|---------------------------|
| | | | Fibre Stress at Elastic Limit. | Modulus of Rupture. |
| | | Per Cent. | Lbs. per Sq. In. | Lbs. per Sq. In. |
| Long-leaf Pine (Pinus Palustris). | Green..... | 27.6 | 3734 | 6140 |
| | Air Seasoned | 19.2 | 3691 | 5749 |
| Douglas Fir (Pseudo- tsuga Taxifolia). | Green..... | 33.2 | 3968 | 5983 |
| | Air Seasoned | 17.3 | 4563 | 6372 |
| Short-leaf Pine (Pinus Echinata). | Green..... | 46.4 | 3237 | 5548 |
| | Air Seasoned | 15.9 | 4675 | 6573 |
| Western Larch (Larix Occidentalis). | Green..... | 51.3 | 3324 | 4948 |
| | Air Seasoned | 17.9 | 3503 | 5856 |
| Loblolly Pine (Pinus Taeda). | Green..... | 34.4 | 3040 | 5084 |
| | Air Seasoned | 17.9 | 3517 | 6118 |
| Tamarack (Larix Lari- cina). | Green..... | 42.0 | 2813 | 4556 |
| | Air Seasoned | 21.5 | 3730 | 5498 |
| Western Hemlock (Tsuga Heterophylla). | Green..... | 47.6 | 3516 | 5296 |
| | Air Seasoned | 17.7 | 4398 | 6420 |
| Redwood (Sequoia Sem- pervirens). | Green..... | 87.5 | 3760 | 4472 |
| | Air Seasoned | 20.9 | 3442 | 3891 |
| Norway Pine (Pinus Resinosa). | Green..... | 49.0 | 2492 | 3864 |
| | Air Seasoned | 15.7 | 4069 | 6054 |

The above table presents the average results of an extensive series of tests on structural timbers as conducted by the United States Forestry Service and published in Bulletin No. 108, issued September 23, 1912. Many engineering handbooks and other publications dealing with timber quote results of tests made only on small thoroughly seasoned specimens, free from defects. Such values may be from one and one-half to two times as high as stresses developed in large timbers and joists.

The above tabulations, with the exception of those in final column headed "Shear," are based upon tests of structural size timbers having such defects as are ordinarily to be found. The "Shear" column values, owing to the method of testing, were obtained from small specimens and it will be seen that the shearing stresses developed are much higher than the calculated shearing stresses in beams that failed by horizontal shear. The difference is doubtless due to the fact that on account of checks and shakes, the actual area resisting shear is likely to be much less than the calculated area used in the formula for horizontal shear. Since large timbers almost invariably form checks during seasoning, it is not safe, in designing timber beams, to use shearing stresses higher than those determined for beams that failed in horizontal shear.

AVERAGE TESTED STRENGTH VALUES OF STRUCTURAL TIMBERS WITH ORDINARY DEFECTS.

| Bending. | | Compression. | | | | Shear. |
|------------------------------|-----------------------|--|---|------------------------------|--|---|
| Modulus of Elasticity. | *Horizontal Shear. | Parallel to Grain. | | | Perpendicular to Grain. | Shearing Strength (Small Specimens). |
| | | Crushing Strength at Elastic Limit. | Crushing Strength at Maximum Load. | Modulus of Elasticity. | Crushing Strength at Elastic Limit. | |
| 1000 Lbs. per Sq. In. | Lbs. per Sq. In. | Lbs. per Sq. In. | Lbs. per Sq. In. | 1000 Lbs. per Sq. In. | Lbs. per Sq. In. | Lbs. per Sq. In. |
| 1463 | 353 | 3480 | 4800 | | 568 | 973 |
| 1705 | 272 | 3480 | 4800 | | 572 | 984 |
| 1517 | 166 | 2770 | 3495 | 1414 | 570 | 765 |
| 1549 | 221 | 3271 | 4258 | 1038 | 639 | 822 |
| 1473 | 332 | 2460 | 3435 | 1548 | 351 | 704 |
| 1726 | 364 | 4070 | 6030 | 1951 | 796 | 1135 |
| 1301 | 288 | 2675 | 3510 | 1575 | 456 | 700 |
| 1487 | 340 | | 5746 | | 597 | 905 |
| 1387 | 335 | 2050 | 2940 | 548 | 500 | 630 |
| 1487 | 434 | 3011 | 4292 | 1206 | 655 | 1115 |
| 1220 | 261 | 2400 | 3230 | 1373 | | 668 |
| 1341 | 299 | 3349 | 4320 | 1351 | | 879 |
| 1445 | 288 | 2905 | 3355 | 1617 | 434 | 630 |
| 1737 | 307 | 4840 | 5814 | 2140 | 473 | 924 |
| 1042 | 302 | 3194 | 3882 | 1240 | 434 | 742 |
| 890 | | | 4276 | | 525 | 671 |
| 1133 | 232 | 2065 | 2555 | 1002 | | 589 |
| 1418 | 278 | 3047 | 4228 | 1367 | | 1145 |

* Only those pieces which failed first by horizontal shear are included in this column.

The averages for the bending tests are the results of tests on timbers ranging in cross section from 4 by 10 inches to 8 by 16 inches, over a 15-ft. span.

A comparison of the results of tests on air seasoned material with those on green material shows that, in general, all of the mechanical properties are increased by seasoning. Increase in strength of wood fibre, due to drying, is, in the case of large timbers, largely offset by a weakening of the timber due to the formation of checks. If the moisture content of a seasoned timber is increased, it loses strength rapidly, and if thoroughly soaked with water will become slightly weaker than when green. On this account, it is not safe in practice to depend upon any increase of strength in timbers, due to seasoning. When, however, large beams are seasoned with ordinary care, it is safe to assume that they are not weaker than when green.

UNIT STRESSES FOR STRUCTURAL TIMBER.

(Expressed in Pounds per Square Inch.)

| Kind of Timber. | Bending. | | | Shearing. | | | |
|--------------------|-----------------------|--------------|-------------------------------------|--------------------|--------------|------------------------------|--------------|
| | Extreme Fibre Stress. | | Modulus of Elasticity in Thousands. | Parallel to Grain. | | Longitudinal Shear in Beams. | |
| | Average Ultimate. | Safe Stress. | | Average Ultimate. | Safe Stress. | Average Ultimate. | Safe Stress. |
| Douglas Fir..... | 6100 | 1200 | 1510 | 690 | 170 | 270 | 110 |
| Long-leaf Pine... | 6500 | 1300 | 1610 | 720 | 180 | 300 | 120 |
| Short-leaf Pine... | 5600 | 1100 | 1480 | 710 | 170 | 330 | 130 |
| White Pine..... | 4400 | 900 | 1130 | 400 | 100 | 180 | 70 |
| Spruce..... | 4800 | 1000 | 1310 | 600 | 150 | 170 | 70 |
| Norway Pine.... | 4200 | 800 | 1190 | *590 | 130 | 250 | 100 |
| Tamarack..... | 4600 | 900 | 1220 | 670 | 170 | 260 | 100 |
| Western Hemlock | 5800 | 1100 | 1480 | 630 | 160 | *270 | 100 |
| Redwood..... | 5000 | 900 | 800 | 300 | 80 | | |
| Bald Cypress.... | 4800 | 900 | 1150 | 500 | 120 | | |
| Red Cedar..... | 4200 | 800 | 800 | | | | |
| White Oak..... | 5700 | 1100 | 1150 | 840 | 210 | 270 | 110 |

NOTE.—These unit stresses are for a green condition of timber and are to * Partially air-dry.

The above table gives the ultimate and safe unit stress values for structural timber as adopted by the American Railway Engineering and Maintenance of Way Association, upon recommendation of their Committee on Wooden Bridges and Trestles, Convention of 1909; and published in the Association's "Bulletin No. 107," 1909, and "Manual," 1911.

They state that the working unit stresses given in this table are intended for railroad bridges and trestles. For highway bridges and trestles, the unit stresses may be increased twenty-five (25) per cent. For buildings and similar structures, in which the timber is protected from the weather and practically free from impact, the unit stresses may be increased fifty (50) per cent. To compute the deflection of a beam under long continued loading instead of that when the load is first applied, only fifty (50) per cent. of the corresponding modulus of elasticity given in the tables is to be employed.†

The safe unit stresses were determined by carefully considering both the average ultimate stresses, which represent the best results now available, as well as the unit stresses which have been in use in designing wooden bridges and trestles, and have been demonstrated by extensive practice to be safe.

† Timber has no well-defined modulus of elasticity.—Ed.

UNIT STRESSES FOR STRUCTURAL TIMBER.

(Expressed in Pounds per Square Inch.)

| Compression. | | | | | | Ratio of Length to Stringer Depth. |
|----------------------------|-----------------|-----------------------|-----------------|-------------------------------|---------------------------------------|---|
| Perpendicular to Grain. | | Parallel to Grain. | | Columns under 15 Diams. | Long Columns over 15 Diameters. | |
| Elastic Limit. | Safe Stress. | Average Ultimate. | Safe Stress. | Safe Stress. | Safe Stress. | |
| 630 | 310 | 3600 | 1200 | 900 | $1200 \left(1 - \frac{L}{60D}\right)$ | 10 |
| 520 | 260 | 3800 | 1300 | 980 | $1300 \left(\frac{L}{60D}\right)$ | 10 |
| 340 | 170 | 3400 | 1100 | 830 | $1100 \left(\frac{L}{60D}\right)$ | 10 |
| 290 | 150 | 3000 | 1000 | 750 | $1000 \left(\frac{L}{60D}\right)$ | 10 |
| 370 | 180 | 3200 | 1100 | 830 | $1100 \left(\frac{L}{60D}\right)$ | |
| | 150 | *2600 | 800 | 600 | $800 \left(\frac{L}{60D}\right)$ | |
| | 220 | *3200 | 1000 | 750 | $1000 \left(\frac{L}{60D}\right)$ | |
| 440 | 220 | 3500 | 1200 | 900 | $1200 \left(\frac{L}{60D}\right)$ | |
| 400 | 150 | 3300 | 900 | 680 | $900 \left(\frac{L}{60D}\right)$ | |
| 340 | 170 | 3900 | 1100 | 830 | $1100 \left(\frac{L}{60D}\right)$ | |
| 470 | 230 | 2800 | 900 | 680 | $900 \left(\frac{L}{60D}\right)$ | |
| 920 | 450 | 3500 | 1300 | 980 | $1300 \left(\frac{L}{60D}\right)$ | 12 |

be used without increasing the live load stresses for impact.

L = length in inches.

D = least side or diameter in inches.

The relation between the strength of the lowest 10 per cent. group of tests and the average strength for each series, the relation between the elastic limit and the ultimate strength, as well as the fact that the live load stresses are not to be increased for impact, are all to be taken into account in determining the general relation between the safe stress and the average ultimate stress; it being always remembered that it is more rational to relate the safe unit stress to the elastic limit of the material than to its ultimate strength.

As large columns not over 15 diameters in length may not develop more than 70 per cent. of the strength of short blocks, the column formulas are arranged to give approximately these relative values at the given limit of length when L, the length of the column in inches, equals 15 times its least diameter D, also expressed in inches.

It is expected that these unit stresses will be revised at intervals of a few years, whenever new results of timber tests are published, or when the experience of bridge engineers who have adapted them shall indicate that revision is desirable.

AVERAGE ULTIMATE BREAKING UNIT

| Kind of Timber. | Tension. | |
|--|-------------|---------------|
| | With Grain. | Across Grain. |
| White Oak..... | 12000 | 2000 |
| White Pine..... | 7000 | 500 |
| Southern Long-leaf or Georgia Yellow Pine..... | 12000 | 600 |
| Douglas Fir..... | 8000 | |
| Short-leaf Yellow Pine..... | 9000 | 500 |
| Red Pine (Norway Pine)..... | 8000 | 500 |
| Spruce and Eastern Fir..... | 8000 | 500 |
| Hemlock..... | 8000 | |
| Cypress..... | 6000 | |
| Cedar..... | 7000 | |
| Chestnut..... | 8500 | |
| California Redwood..... | 7000 | |
| California Spruce..... | | |

AVERAGE SAFE ALLOWABLE WORKING UNIT

| Kind of Timber. | Tension. | |
|--|-------------|---------------|
| | With Grain. | Across Grain. |
| Factor of Safety. | Ten. | Ten. |
| White Oak..... | 1200 | 200 |
| White Pine..... | 700 | 50 |
| Southern Long-leaf or Georgia Yellow Pine..... | 1200 | 60 |
| Douglas Fir..... | 800 | |
| Short-leaf Yellow Pine..... | 900 | 50 |
| Red Pine (Norway Pine)..... | 800 | 50 |
| Spruce and Eastern Fir..... | 800 | 50 |
| Hemlock..... | 600 | |
| Cypress..... | 600 | |
| Cedar..... | 700 | |
| Chestnut..... | 850 | |
| California Redwood..... | 700 | |
| California Spruce..... | | |

The above tables are based on those recommended by the committee on intendents of Bridges and Buildings at their Fifth Annual Convention in by later data from various sources.

STRESSES, IN POUNDS PER SQUARE INCH.

| Compression. | | | Transverse. | | Shearing. | |
|--------------|-------------------------|---------------|-----------------------|------------------------|-------------|---------------|
| With Grain. | | Across Grain. | Extreme Fibre Stress. | Modulus of Elasticity. | With Grain. | Across Grain. |
| End Bearing. | Columns Under 15 Diams. | | | | | |
| 7000 | 5000 | 2000 | 7000 | 1500000 | 800 | 4000 |
| 5500 | 3500 | 700 | 4000 | 1000000 | 400 | 2000 |
| 7000 | 5000 | 1400 | 7000 | 1500000 | 600 | 5000 |
| 5700 | 4500 | 800 | 5000 | 1400000 | 500 | |
| 6000 | 4500 | 1000 | 6000 | 1200000 | 400 | 4000 |
| 5000 | 4000 | 800 | 5000 | 1130000 | | |
| 6000 | 4000 | 700 | 4000 | 1200000 | 400 | 3000 |
| | 4000 | 600 | 3500 | 900000 | 350 | 2500 |
| 5000 | 4000 | 700 | 5000 | 900000 | | |
| 5500 | 3500 | 700 | 4000 | 700000 | 400 | 1500 |
| | 4000 | 900 | 5000 | 1000000 | 600 | 2000 |
| | 4000 | 600 | 4500 | 700000 | 400 | |
| | 4000 | | 5000 | 1200000 | | |

STRESSES, IN POUNDS PER SQUARE INCH.

| Compression. | | | Transverse. | | Shearing. | |
|--------------|-------------------------|---------------|-----------------------|------------------------|-------------|---------------|
| With Grain. | | Across Grain. | Extreme Fibre Stress. | Modulus of Elasticity. | With Grain. | Across Grain. |
| End Bearing. | Columns Under 15 Diams. | | | | | |
| Five. | Five. | Four. | Six. | Two. | Four. | Four. |
| 1400 | 1000 | 500 | 1200 | 750000 | 200 | 1000 |
| 1100 | 700 | 200 | 700 | 500000 | 100 | 500 |
| 1400 | 1000 | 350 | 1200 | 750000 | 150 | 1250 |
| 1100 | 900 | 200 | 800 | 750000 | 130 | |
| 1200 | 900 | 250 | 1000 | 600000 | 100 | 1000 |
| 1000 | 800 | 200 | 800 | 565000 | | |
| 1200 | 800 | 200 | 700 | 600000 | 100 | 750 |
| | 800 | 150 | 600 | 450000 | 100 | 600 |
| 1000 | 800 | 200 | 800 | 450000 | | |
| 1100 | 700 | 200 | 700 | 350000 | 100 | 400 |
| | 800 | 250 | 800 | 500000 | 150 | 500 |
| | 800 | 150 | 750 | 350000 | 100 | |
| | 800 | | 800 | 600000 | | |

"Strength of Bridge and Trestle Timbers" of the Association of Railway Super-October, 1895, but the arrangement and values in many cases are now modified

SAFE LOAD IN POUNDS FOR RECTANGULAR OF WHITE PINE, CEDAR

Allowable fibre stress 700 pounds per square inch. Safety factor 6.

Safe loads for other safety factors may be obtained as follows:

| Span in Feet. | Depth of Beam in Inches. | | | | | | | | | | | Deflection Coefficient for White Pine V |
|---------------------|--------------------------|-----|-----|-----|------|------|------|------|------|------|------|--|
| | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | |
| 4 | 311 | 486 | 700 | 953 | 1244 | 1575 | 1944 | 2352 | 2800 | 3286 | 3811 | .34 |
| 5 | 249 | 389 | 560 | 762 | 996 | 1260 | 1556 | 1882 | 2240 | 2629 | 3049 | .53 |
| 6 | 207 | 324 | 467 | 635 | 830 | 1050 | 1296 | 1569 | 1867 | 2191 | 2541 | .76 |
| 7 | 178 | 278 | 400 | 544 | 711 | 900 | 1111 | 1344 | 1600 | 1878 | 2178 | 1.03 |
| 8 | 156 | 243 | 350 | 476 | 622 | 788 | 972 | 1176 | 1400 | 1643 | 1906 | 1.34 |
| 9 | 138 | 216 | 311 | 423 | 553 | 700 | 864 | 1046 | 1244 | 1460 | 1694 | 1.70 |
| 10 | 124 | 194 | 280 | 381 | 498 | 630 | 778 | 941 | 1120 | 1314 | 1524 | 2.10 |
| 11 | 113 | 177 | 255 | 346 | 453 | 573 | 707 | 856 | 1018 | 1195 | 1386 | 2.54 |
| 12 | 103 | 162 | 233 | 318 | 415 | 525 | 648 | 784 | 933 | 1095 | 1270 | 3.02 |
| 13 | 96 | 150 | 215 | 293 | 383 | 485 | 598 | 724 | 862 | 1011 | 1173 | 3.55 |
| 14 | 89 | 139 | 200 | 272 | 356 | 450 | 556 | 672 | 800 | 939 | 1089 | 4.12 |
| 15 | 83 | 130 | 187 | 254 | 332 | 420 | 519 | 627 | 747 | 876 | 1016 | 4.73 |
| 16 | 78 | 122 | 175 | 238 | 311 | 394 | 486 | 588 | 700 | 821 | 953 | 5.38 |
| 17 | 73 | 114 | 165 | 224 | 293 | 371 | 458 | 554 | 659 | 773 | 897 | 6.07 |
| 18 | 69 | 108 | 156 | 212 | 277 | 350 | 432 | 523 | 622 | 730 | 847 | 6.80 |
| 19 | 65 | 102 | 147 | 201 | 262 | 332 | 409 | 495 | 589 | 692 | 802 | 7.58 |
| 20 | | 97 | 140 | 191 | 249 | 315 | 389 | 471 | 560 | 657 | 762 | 8.40 |
| 21 | | 93 | 133 | 182 | 237 | 300 | 370 | 448 | 533 | 626 | 726 | 9.26 |
| 22 | | 88 | 127 | 173 | 226 | 286 | 354 | 428 | 509 | 597 | 693 | 10.16 |
| 23 | | 85 | 122 | 166 | 216 | 274 | 338 | 409 | 487 | 572 | 663 | 11.11 |
| 24 | | | 117 | 159 | 207 | 263 | 324 | 392 | 467 | 548 | 635 | 12.10 |
| 25 | | | 112 | 152 | 199 | 252 | 311 | 376 | 448 | 526 | 610 | 13.13 |
| 26 | | | 108 | 147 | 191 | 242 | 299 | 362 | 431 | 506 | 586 | 14.20 |
| 27 | | | 104 | 141 | 184 | 233 | 288 | 349 | 415 | 487 | 565 | 15.31 |
| 28 | | | 100 | 136 | 178 | 225 | 278 | 336 | 400 | 469 | 544 | 16.46 |
| 29 | | | 97 | 131 | 172 | 217 | 268 | 325 | 386 | 453 | 526 | 17.66 |
| 30 | | | 93 | 127 | 166 | 210 | 259 | 314 | 373 | 438 | 508 | 18.90 |
| 31 | | | 90 | 123 | 161 | 203 | 251 | 304 | 361 | 424 | 492 | 20.18 |
| 32 | | | 88 | 119 | 156 | 197 | 243 | 294 | 350 | 411 | 476 | 21.50 |
| 33 | | | 85 | 115 | 151 | 191 | 236 | 285 | 339 | 398 | 462 | 22.87 |
| 34 | | | | 112 | 146 | 185 | 229 | 277 | 329 | 387 | 448 | 24.28 |
| 35 | | | | 109 | 142 | 180 | 222 | 269 | 320 | 376 | 436 | 25.73 |

**UNIFORMLY DISTRIBUTED
BEAMS ONE INCH THICK
AND SPRUCE OR EASTERN FIR.**

Modulus of rupture 4 200 pounds per square inch.

New safe load = Safe load from table $\times \frac{6}{\text{New factor}}$.

| Span in Feet. | Depth of Beam in Inches. | | | | | | | | | | Deflection Coefficient for White Pine V |
|---------------------|--------------------------|------|------|------|------|------|------|------|------|------|--|
| | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | |
| 9 | 1944 | 2212 | 2498 | 2800 | 3120 | 3457 | 3811 | 4183 | 4571 | 4978 | 1.70 |
| 10 | 1750 | 1991 | 2248 | 2520 | 2808 | 3111 | 3430 | 3764 | 4114 | 4480 | 2.10 |
| 11 | 1601 | 1810 | 2044 | 2291 | 2552 | 2828 | 3118 | 3422 | 3740 | 4073 | 2.54 |
| 12 | 1458 | 1659 | 1873 | 2100 | 2340 | 2593 | 2858 | 3137 | 3428 | 3733 | 3.02 |
| 13 | 1346 | 1531 | 1729 | 1938 | 2160 | 2393 | 2638 | 2896 | 3165 | 3446 | 3.55 |
| 14 | 1250 | 1422 | 1606 | 1800 | 2056 | 2222 | 2450 | 2689 | 2939 | 3200 | 4.12 |
| 15 | 1167 | 1328 | 1499 | 1680 | 1872 | 2074 | 2287 | 2510 | 2743 | 2987 | 4.73 |
| 16 | 1094 | 1244 | 1405 | 1575 | 1755 | 1944 | 2144 | 2353 | 2571 | 2800 | 5.38 |
| 17 | 1029 | 1171 | 1322 | 1482 | 1652 | 1830 | 2018 | 2214 | 2420 | 2635 | 6.07 |
| 18 | 972 | 1106 | 1249 | 1400 | 1560 | 1728 | 1906 | 2091 | 2286 | 2489 | 6.80 |
| 19 | 921 | 1048 | 1183 | 1326 | 1478 | 1637 | 1805 | 1981 | 2165 | 2358 | 7.58 |
| 20 | 875 | 996 | 1124 | 1260 | 1404 | 1556 | 1715 | 1882 | 2057 | 2240 | 8.40 |
| 21 | 833 | 948 | 1070 | 1200 | 1337 | 1481 | 1633 | 1793 | 1959 | 2133 | 9.26 |
| 22 | 795 | 905 | 1022 | 1145 | 1276 | 1414 | 1559 | 1711 | 1870 | 2036 | 10.16 |
| 23 | 761 | 866 | 977 | 1096 | 1221 | 1353 | 1491 | 1637 | 1789 | 1948 | 11.11 |
| 24 | 729 | 830 | 937 | 1050 | 1170 | 1296 | 1429 | 1569 | 1714 | 1867 | 12.10 |
| 25 | 700 | 796 | 899 | 1008 | 1123 | 1244 | 1372 | 1506 | 1645 | 1792 | 13.13 |
| 26 | 673 | 766 | 865 | 969 | 1080 | 1197 | 1319 | 1448 | 1582 | 1723 | 14.20 |
| 27 | 648 | 737 | 833 | 933 | 1040 | 1152 | 1270 | 1394 | 1524 | 1659 | 15.31 |
| 28 | 625 | 711 | 803 | 900 | 1003 | 1111 | 1225 | 1344 | 1469 | 1600 | 16.46 |
| 29 | 603 | 687 | 775 | 869 | 968 | 1073 | 1183 | 1298 | 1419 | 1545 | 17.66 |
| 30 | 583 | 664 | 749 | 840 | 936 | 1037 | 1143 | 1255 | 1371 | 1493 | 18.90 |
| 31 | 565 | 642 | 725 | 813 | 906 | 1004 | 1106 | 1214 | 1327 | 1445 | 20.18 |
| 32 | 547 | 622 | 703 | 787 | 877 | 972 | 1072 | 1176 | 1286 | 1400 | 21.50 |
| 33 | 534 | 603 | 681 | 764 | 850 | 943 | 1039 | 1141 | 1247 | 1358 | 22.87 |
| 34 | 515 | 586 | 661 | 741 | 826 | 915 | 1009 | 1107 | 1210 | 1318 | 24.28 |
| 35 | 500 | 569 | 642 | 720 | 802 | 889 | 980 | 1076 | 1176 | 1280 | 25.73 |
| 36 | 486 | 553 | 624 | 700 | 780 | 864 | 953 | 1046 | 1143 | 1244 | 27.22 |
| 37 | 473 | 538 | 608 | 681 | 759 | 841 | 927 | 1017 | 1112 | 1211 | 28.75 |
| 38 | 460 | 524 | 592 | 663 | 739 | 819 | 903 | 991 | 1083 | 1179 | 30.32 |
| 39 | 449 | 511 | 576 | 646 | 720 | 798 | 880 | 965 | 1055 | 1149 | 31.94 |
| 40 | 438 | 498 | 562 | 630 | 702 | 778 | 858 | 941 | 1029 | 1120 | 33.60 |

SAFE LOADS IN POUNDS FOR RECTANGULAR OF SHORT-LEAF

Allowable fibre stress 1 000 pounds per square inch. Safety factor 6.

Safe loads for other safety factors may be obtained as follows:

| Span in Feet. | Depth of Beam in Inches. | | | | | | | | | | | Deflection Coefficient V |
|---------------------|--------------------------|-----|------|------|------|------|------|------|------|------|------|--------------------------------|
| | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | |
| 4 | 444 | 694 | 1000 | 1361 | 1778 | 2250 | 2778 | 3361 | 4000 | 4694 | 5444 | .40 |
| 5 | 356 | 556 | 800 | 1039 | 1422 | 1800 | 2222 | 2689 | 3200 | 3756 | 4356 | .63 |
| 6 | 296 | 463 | 667 | 907 | 1185 | 1500 | 1852 | 2241 | 2667 | 3130 | 3630 | .90 |
| 7 | 254 | 397 | 571 | 778 | 1016 | 1286 | 1587 | 1921 | 2286 | 2683 | 3111 | 1.23 |
| 8 | 222 | 347 | 500 | 681 | 889 | 1125 | 1389 | 1681 | 2000 | 2347 | 2722 | 1.60 |
| 9 | 198 | 309 | 444 | 605 | 790 | 1000 | 1235 | 1494 | 1778 | 2086 | 2420 | 2.03 |
| 10 | 178 | 278 | 400 | 544 | 711 | 900 | 1111 | 1344 | 1600 | 1878 | 2178 | 2.50 |
| 11 | 162 | 253 | 364 | 495 | 646 | 818 | 1010 | 1222 | 1455 | 1707 | 1980 | 3.03 |
| 12 | 148 | 231 | 333 | 454 | 593 | 750 | 926 | 1120 | 1333 | 1565 | 1815 | 3.60 |
| 13 | 137 | 214 | 308 | 419 | 547 | 692 | 855 | 1034 | 1231 | 1444 | 1675 | 4.23 |
| 14 | 127 | 198 | 286 | 389 | 508 | 643 | 794 | 960 | 1143 | 1341 | 1556 | 4.90 |
| 15 | 119 | 185 | 267 | 363 | 474 | 600 | 741 | 896 | 1067 | 1252 | 1452 | 5.63 |
| 16 | 111 | 174 | 250 | 340 | 444 | 563 | 694 | 840 | 1000 | 1174 | 1361 | 6.40 |
| 17 | 105 | 163 | 235 | 320 | 418 | 529 | 654 | 791 | 941 | 1105 | 1281 | 7.23 |
| 18 | 99 | 154 | 222 | 302 | 395 | 500 | 617 | 747 | 889 | 1043 | 1210 | 8.10 |
| 19 | 94 | 146 | 211 | 287 | 374 | 474 | 585 | 708 | 842 | 988 | 1146 | 9.03 |
| 20 | 89 | 139 | 200 | 272 | 356 | 450 | 556 | 672 | 800 | 939 | 1089 | 10.00 |
| 21 | 85 | 132 | 190 | 259 | 339 | 429 | 529 | 640 | 762 | 894 | 1037 | 11.03 |
| 22 | 81 | 126 | 182 | 247 | 323 | 409 | 505 | 611 | 727 | 854 | 990 | 12.10 |
| 23 | 77 | 121 | 174 | 237 | 309 | 391 | 483 | 585 | 696 | 816 | 947 | 13.23 |
| 24 | | 116 | 162 | 227 | 296 | 375 | 463 | 560 | 667 | 782 | 907 | 14.40 |
| 25 | | 111 | 160 | 218 | 284 | 360 | 444 | 538 | 640 | 751 | 871 | 15.63 |
| 26 | | 107 | 154 | 209 | 274 | 346 | 427 | 517 | 615 | 722 | 838 | 16.90 |
| 27 | | 103 | 148 | 202 | 263 | 333 | 412 | 498 | 593 | 695 | 807 | 18.23 |
| 28 | | 99 | 143 | 194 | 254 | 321 | 397 | 480 | 571 | 671 | 778 | 19.60 |
| 29 | | | 138 | 188 | 245 | 310 | 383 | 464 | 552 | 648 | 751 | 21.03 |
| 30 | | | 133 | 181 | 237 | 300 | 370 | 448 | 533 | 626 | 726 | 22.50 |
| 31 | | | 129 | 176 | 229 | 290 | 358 | 434 | 516 | 606 | 703 | 24.03 |
| 32 | | | 125 | 170 | 222 | 281 | 347 | 420 | 500 | 587 | 681 | 25.60 |
| 33 | | | 121 | 165 | 215 | 273 | 337 | 407 | 485 | 569 | 660 | 27.23 |
| 34 | | | 118 | 160 | 209 | 265 | 327 | 395 | 471 | 552 | 641 | 28.90 |
| 35 | | | 114 | 156 | 203 | 257 | 317 | 384 | 457 | 537 | 602 | 30.63 |

Safe loads for any fibre stress may be readily obtained from this table by proportion.

UNIFORMLY DISTRIBUTED, BEAMS ONE INCH THICK, YELLOW PINE.

Modulus of rupture 6 000 pounds per square inch.

New safe load = Safe load from table $\times \frac{6}{\text{New factor}}$.

| Span in Feet. | Depth of Beam in Inches. | | | | | | | | | | Deflection Coefficient V |
|---------------------|--------------------------|------|------|------|------|------|------|------|------|------|---------------------------------------|
| | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | |
| 9 | 2778 | 3160 | 3568 | 4000 | 4457 | 4938 | 5444 | 5975 | 6531 | 7111 | 2.03 |
| 10 | 2500 | 2844 | 3211 | 3600 | 4011 | 4444 | 4900 | 5378 | 5878 | 6400 | 2.50 |
| 11 | 2273 | 2586 | 2919 | 3273 | 3646 | 4040 | 4455 | 4889 | 5343 | 5818 | 3.03 |
| 12 | 2083 | 2370 | 2676 | 3000 | 3343 | 3704 | 4083 | 4481 | 4898 | 5333 | 3.60 |
| 13 | 1923 | 2188 | 2470 | 2769 | 3085 | 3419 | 3769 | 4137 | 4521 | 4923 | 4.23 |
| 14 | 1786 | 2032 | 2294 | 2571 | 2865 | 3175 | 3500 | 3841 | 4198 | 4571 | 4.90 |
| 15 | 1667 | 1896 | 2141 | 2400 | 2674 | 2963 | 3267 | 3585 | 3919 | 4267 | 5.63 |
| 16 | 1563 | 1778 | 2007 | 2250 | 2507 | 2778 | 3062 | 3361 | 3674 | 4000 | 6.40 |
| 17 | 1471 | 1673 | 1889 | 2118 | 2359 | 2614 | 2882 | 3163 | 3458 | 3765 | 7.23 |
| 18 | 1389 | 1580 | 1789 | 2000 | 2228 | 2469 | 2722 | 2988 | 3265 | 3556 | 8.10 |
| 19 | 1316 | 1497 | 1690 | 1895 | 2111 | 2339 | 2579 | 2830 | 3094 | 3368 | 9.03 |
| 20 | 1250 | 1422 | 1606 | 1800 | 2006 | 2222 | 2450 | 2689 | 2939 | 3200 | 10.00 |
| 21 | 1190 | 1354 | 1529 | 1714 | 1910 | 2116 | 2333 | 2561 | 2799 | 3048 | 11.03 |
| 22 | 1136 | 1293 | 1460 | 1636 | 1823 | 2020 | 2227 | 2444 | 2672 | 2909 | 12.10 |
| 23 | 1087 | 1237 | 1396 | 1565 | 1744 | 1932 | 2130 | 2338 | 2556 | 2783 | 13.23 |
| 24 | 1042 | 1185 | 1338 | 1500 | 1671 | 1852 | 2042 | 2241 | 2449 | 2667 | 14.40 |
| 25 | 1000 | 1138 | 1284 | 1440 | 1604 | 1778 | 1960 | 2131 | 2351 | 2560 | 15.63 |
| 26 | 962 | 1094 | 1235 | 1385 | 1543 | 1709 | 1885 | 2068 | 2261 | 2462 | 16.90 |
| 27 | 926 | 1053 | 1189 | 1333 | 1486 | 1646 | 1815 | 1992 | 2177 | 2370 | 18.23 |
| 28 | 893 | 1016 | 1147 | 1286 | 1433 | 1587 | 1750 | 1921 | 2099 | 2286 | 19.60 |
| 29 | 862 | 981 | 1107 | 1241 | 1383 | 1533 | 1690 | 1854 | 2027 | 2207 | 21.03 |
| 30 | 833 | 948 | 1070 | 1200 | 1337 | 1481 | 1633 | 1793 | 1959 | 2133 | 22.50 |
| 31 | 806 | 918 | 1036 | 1161 | 1294 | 1434 | 1581 | 1735 | 1896 | 2065 | 24.03 |
| 32 | 781 | 889 | 1003 | 1125 | 1253 | 1389 | 1531 | 1681 | 1837 | 2000 | 25.60 |
| 33 | 758 | 862 | 973 | 1091 | 1215 | 1347 | 1485 | 1630 | 1781 | 1939 | 27.23 |
| 34 | 735 | 837 | 944 | 1059 | 1180 | 1307 | 1441 | 1582 | 1728 | 1882 | 28.90 |
| 35 | 714 | 813 | 917 | 1029 | 1146 | 1270 | 1400 | 1537 | 1677 | 1829 | 30.63 |
| 36 | 694 | 780 | 894 | 1000 | 1114 | 1235 | 1361 | 1494 | 1633 | 1778 | 32.40 |
| 37 | 676 | 760 | 868 | 973 | 1084 | 1201 | 1324 | 1453 | 1589 | 1730 | 34.23 |
| 38 | 658 | 740 | 845 | 947 | 1056 | 1169 | 1289 | 1415 | 1547 | 1684 | 36.10 |
| 39 | 641 | 720 | 823 | 923 | 1028 | 1140 | 1256 | 1379 | 1507 | 1641 | 38.03 |
| 40 | 625 | 711 | 803 | 900 | 1003 | 1111 | 1225 | 1344 | 1469 | 1600 | 40.00 |

Safe loads for beams of California Redwood, $\frac{3}{4}$ of above.

SAFE LOADS IN POUNDS FOR RECTANGULAR OF WHITE OAK AND

Allowable fibre stress 1 200 pounds per square inch. Safety factor 6.

Safe loads for other safety factors may be obtained as follows:

| Span in Feet. | Depth of Beam in Inches. | | | | | | | | | | | Deflection Coefficient. V |
|---------------------|--------------------------|-----|------|------|------|------|------|------|------|------|------|---------------------------------|
| | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | |
| 4 | 533 | 833 | 1200 | 1633 | 2133 | 2700 | 3333 | 4033 | 4800 | 5633 | 6533 | .38 |
| 5 | 427 | 667 | 960 | 1307 | 1707 | 2160 | 2667 | 3227 | 3840 | 4507 | 5227 | .80 |
| 6 | 356 | 556 | 800 | 1089 | 1422 | 1800 | 2222 | 2689 | 3200 | 3756 | 4356 | .86 |
| 7 | 305 | 476 | 686 | 933 | 1219 | 1543 | 1905 | 2305 | 2743 | 3219 | 3733 | 1.18 |
| 8 | 267 | 417 | 600 | 817 | 1067 | 1350 | 1667 | 2017 | 2400 | 2817 | 3267 | 1.54 |
| 9 | 237 | 370 | 533 | 726 | 948 | 1200 | 1481 | 1793 | 2133 | 2504 | 2904 | 1.94 |
| 10 | 213 | 333 | 480 | 653 | 853 | 1080 | 1333 | 1613 | 1920 | 2253 | 2613 | 2.40 |
| 11 | 194 | 303 | 436 | 594 | 776 | 982 | 1212 | 1467 | 1745 | 2048 | 2376 | 2.90 |
| 12 | 178 | 278 | 400 | 544 | 711 | 900 | 1111 | 1344 | 1600 | 1878 | 2178 | 3.46 |
| 13 | 164 | 256 | 369 | 503 | 656 | 831 | 1026 | 1241 | 1477 | 1733 | 2010 | 4.06 |
| 14 | 152 | 238 | 343 | 467 | 610 | 771 | 952 | 1152 | 1371 | 1610 | 1867 | 4.70 |
| 15 | 142 | 222 | 320 | 436 | 569 | 720 | 889 | 1076 | 1280 | 1502 | 1742 | 5.40 |
| 16 | 133 | 208 | 300 | 408 | 533 | 675 | 833 | 1008 | 1200 | 1408 | 1633 | 6.14 |
| 17 | 125 | 196 | 282 | 384 | 502 | 635 | 784 | 949 | 1129 | 1325 | 1537 | 6.94 |
| 18 | 119 | 185 | 267 | 363 | 474 | 600 | 741 | 896 | 1067 | 1252 | 1452 | 7.78 |
| 19 | 112 | 175 | 253 | 344 | 449 | 568 | 702 | 849 | 1011 | 1186 | 1375 | 8.66 |
| 20 | 107 | 167 | 240 | 327 | 427 | 540 | 667 | 807 | 960 | 1127 | 1307 | 9.60 |
| 21 | 102 | 159 | 229 | 311 | 406 | 514 | 635 | 768 | 914 | 1073 | 1244 | 10.58 |
| 22 | 97 | 152 | 218 | 297 | 388 | 491 | 606 | 733 | 873 | 1024 | 1188 | 11.62 |
| 23 | 93 | 145 | 209 | 284 | 371 | 470 | 580 | 701 | 835 | 980 | 1136 | 12.70 |
| 24 | 89 | 139 | 200 | 272 | 356 | 450 | 556 | 672 | 800 | 939 | 1089 | 13.82 |
| 25 | 85 | 133 | 192 | 261 | 341 | 432 | 533 | 645 | 768 | 901 | 1045 | 15.00 |
| 26 | | 128 | 185 | 251 | 328 | 415 | 513 | 621 | 738 | 867 | 1005 | 16.22 |
| 27 | | 123 | 178 | 242 | 316 | 400 | 494 | 598 | 711 | 835 | 968 | 17.50 |
| 28 | | 119 | 171 | 233 | 305 | 386 | 476 | 576 | 686 | 805 | 933 | 18.82 |
| 29 | | 115 | 166 | 225 | 294 | 372 | 460 | 556 | 662 | 777 | 901 | 20.18 |
| 30 | | 111 | 160 | 218 | 284 | 360 | 444 | 538 | 640 | 751 | 871 | 21.60 |
| 31 | | 108 | 155 | 211 | 275 | 348 | 430 | 520 | 619 | 727 | 843 | 23.06 |
| 32 | | | 150 | 204 | 267 | 338 | 417 | 504 | 600 | 704 | 817 | 24.58 |
| 33 | | | 145 | 198 | 259 | 327 | 404 | 489 | 582 | 683 | 792 | 26.14 |
| 34 | | | 141 | 192 | 251 | 318 | 392 | 475 | 565 | 663 | 769 | 27.74 |
| 35 | | | 137 | 187 | 244 | 309 | 381 | 461 | 549 | 644 | 747 | 29.40 |

Safe loads for beams of Douglas Fir, Red Pine (Norway Pine), Cypress, Chestnut and California Spruce, $\frac{3}{4}$ of above.

UNIFORMLY DISTRIBUTED, BEAMS ONE INCH THICK, LONG-LEAF YELLOW PINE.

Modulus of rupture 7 200 pounds per square inch.

New safe load = Safe load from table $\times \frac{6}{\text{New factor}}$

| Span in Feet. | Depth of Beam in Inches. | | | | | | | | | | Deflection Coefficient V |
|---------------------|--------------------------|------|------|------|------|------|------|------|------|------|--------------------------------|
| | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | |
| 9 | 3333 | 3793 | 4281 | 4800 | 5348 | 5926 | 6533 | 7170 | 7837 | 8533 | 1.94 |
| 10 | 3000 | 3413 | 3853 | 4320 | 4813 | 5333 | 5880 | 6453 | 7053 | 7680 | 2.40 |
| 11 | 2727 | 3103 | 3503 | 3927 | 4376 | 4848 | 5355 | 5867 | 6412 | 6982 | 2.90 |
| 12 | 2500 | 2844 | 3211 | 3600 | 4011 | 4444 | 4900 | 5378 | 5878 | 6400 | 3.46 |
| 13 | 2308 | 2626 | 2964 | 3323 | 3703 | 4103 | 4523 | 4964 | 5426 | 5908 | 4.06 |
| 14 | 2143 | 2438 | 2752 | 3086 | 3438 | 3810 | 4200 | 4610 | 5038 | 5486 | 4.70 |
| 15 | 2000 | 2276 | 2569 | 2880 | 3209 | 3556 | 3920 | 4302 | 4702 | 5120 | 5.40 |
| 16 | 1875 | 2133 | 2408 | 2700 | 3008 | 3333 | 3675 | 4033 | 4433 | 4800 | 6.14 |
| 17 | 1765 | 2008 | 2267 | 2541 | 2831 | 3137 | 3459 | 3796 | 4149 | 4518 | 6.94 |
| 18 | 1667 | 1896 | 2141 | 2400 | 2674 | 2963 | 3267 | 3585 | 3819 | 4267 | 7.78 |
| 19 | 1579 | 1796 | 2027 | 2274 | 2533 | 2807 | 3095 | 3396 | 3712 | 4042 | 8.66 |
| 20 | 1500 | 1707 | 1927 | 2160 | 2407 | 2667 | 2940 | 3227 | 3527 | 3840 | 9.60 |
| 21 | 1429 | 1625 | 1835 | 2057 | 2292 | 2540 | 2800 | 3073 | 3359 | 3657 | 10.58 |
| 22 | 1364 | 1552 | 1752 | 1964 | 2188 | 2424 | 2678 | 2933 | 3206 | 3491 | 11.62 |
| 23 | 1304 | 1484 | 1675 | 1878 | 2093 | 2319 | 2557 | 2806 | 3067 | 3339 | 12.70 |
| 24 | 1250 | 1422 | 1606 | 1800 | 2006 | 2222 | 2450 | 2689 | 2939 | 3200 | 13.82 |
| 25 | 1200 | 1365 | 1541 | 1728 | 1925 | 2133 | 2352 | 2581 | 2821 | 3072 | 15.00 |
| 26 | 1154 | 1313 | 1482 | 1662 | 1851 | 2051 | 2262 | 2482 | 2713 | 2954 | 16.22 |
| 27 | 1111 | 1264 | 1427 | 1600 | 1783 | 1975 | 2178 | 2390 | 2612 | 2844 | 17.50 |
| 28 | 1071 | 1219 | 1376 | 1543 | 1719 | 1905 | 2100 | 2305 | 2519 | 2743 | 18.82 |
| 29 | 1034 | 1177 | 1329 | 1490 | 1660 | 1839 | 2028 | 2225 | 2432 | 2648 | 20.18 |
| 30 | 1000 | 1138 | 1284 | 1440 | 1604 | 1778 | 1960 | 2151 | 2351 | 2560 | 21.60 |
| 31 | 968 | 1101 | 1243 | 1394 | 1553 | 1720 | 1897 | 2082 | 2275 | 2477 | 23.06 |
| 32 | 938 | 1067 | 1204 | 1350 | 1504 | 1667 | 1838 | 2017 | 2217 | 2400 | 24.58 |
| 33 | 909 | 1034 | 1168 | 1309 | 1459 | 1616 | 1785 | 1956 | 2137 | 2327 | 26.14 |
| 34 | 882 | 1004 | 1133 | 1271 | 1416 | 1569 | 1729 | 1898 | 2075 | 2259 | 27.74 |
| 35 | 857 | 975 | 1101 | 1234 | 1375 | 1524 | 1680 | 1844 | 2013 | 2194 | 29.40 |
| 36 | 833 | 948 | 1070 | 1200 | 1337 | 1481 | 1633 | 1793 | 1959 | 2133 | 31.10 |
| 37 | 811 | 923 | 1041 | 1168 | 1301 | 1441 | 1589 | 1744 | 1906 | 2076 | 32.86 |
| 38 | 789 | 893 | 1014 | 1137 | 1267 | 1404 | 1547 | 1698 | 1856 | 2021 | 34.66 |
| 39 | 769 | 875 | 988 | 1108 | 1234 | 1368 | 1508 | 1655 | 1809 | 1969 | 36.50 |
| 40 | 750 | 853 | 963 | 1080 | 1203 | 1333 | 1470 | 1613 | 1763 | 1920 | 38.40 |

Safe loads for beams of Hemlock, $\frac{1}{2}$ of above.

STRENGTH OF SOLID WOODEN COLUMNS OF DIFFERENT KINDS OF TIMBER.

For various values of $\frac{l}{d}$.

l = length of column in inches. d = least diameter in inches.

BASED ON THE FORMULA OF THE U. S. DEPARTMENT OF AGRICULTURE, DIVISION OF FORESTRY.

$$P = F \times \frac{700 + 15c}{700 + 15c + c^2}$$

P = ultimate strength in pounds per square inch.

F = ultimate crushing strength of timber. $c = \frac{l}{d}$.

Values of F are those given in table on pages 414 and 415 herein.

| | Ultimate Strength in Pounds per Square Inch: | | | |
|---------------|---|---|---|-----------------------------|
| | White Oak and Southern Long-leaf or Georgia Yellow Pine. | Douglas Fir and Short-leaf Yellow Pine. | Red Pine (Norway Pine), Spruce or Eastern Fir, Hemlock, Cypress, Chestnut, California Redwood and Cali- fornia Spruce. | White Pine and Cedar. |
| F | 5000 | 4500 | 4000 | 3500 |
| $\frac{l}{d}$ | | | | |
| 2 | 4973 | 4475 | 3978 | 3481 |
| 3 | 4940 | 4446 | 3952 | 3458 |
| 4 | 4897 | 4407 | 3918 | 3428 |
| 5 | 4844 | 4359 | 3875 | 3391 |
| 6 | 4782 | 4304 | 3826 | 3347 |
| 7 | 4713 | 4242 | 3770 | 3299 |
| 8 | 4638 | 4174 | 3710 | 3247 |
| 9 | 4558 | 4102 | 3646 | 3190 |
| 10 | 4474 | 4026 | 3579 | 3132 |
| 11 | 4386 | 3948 | 3509 | 3070 |
| 12 | 4297 | 3867 | 3438 | 3008 |
| 13 | 4206 | 3785 | 3365 | 2944 |
| 14 | 4114 | 3703 | 3291 | 2880 |
| 15 | 4022 | 3620 | 3217 | 2815 |
| 16 | 3930 | 3537 | 3144 | 2751 |
| 17 | 3838 | 3455 | 3071 | 2687 |
| 18 | 3748 | 3373 | 2998 | 2624 |
| 19 | 3659 | 3293 | 2927 | 2561 |

For safety factors for various classes of structures to be used in connection with the above table, see p. 408.

STRENGTH OF SOLID WOODEN COLUMNS OF DIFFERENT KINDS OF TIMBER.

For various values of $\frac{l}{d}$.

l = length of column in inches. d = least diameter in inches.

BASED ON THE FORMULA OF THE U. S. DEPARTMENT OF AGRICULTURE, DIVISION OF FORESTRY.

$$P = F \times \frac{700 + 15c}{700 + 15c + c^3}$$

P = ultimate strength in pounds per square inch.

F = ultimate crushing strength of timber. $c = \frac{l}{d}$.

Values of F are those given in table on pages 414 and 415 herein.

| F | Ultimate Strength in Pounds per Square Inch. | | | |
|---------------|---|---|---|-----------------------------|
| | White Oak and Southern Long-leaf or Georgia Yellow Pine. | Douglas Fir and Short-leaf Yellow Pine. | Red Pine (Norway Pine), Spruce or Eastern Fir, Hemlock, Cypress, Chestnut, California Redwood and Cali- fornia Spruce. | White Pine and Cedar. |
| $\frac{l}{d}$ | 5000 | 4500 | 4000 | 3500 |
| 20 | 3571 | 3214 | 2857 | 2500 |
| 21 | 3486 | 3137 | 2788 | 2440 |
| 22 | 3402 | 3061 | 2721 | 2381 |
| 23 | 3320 | 2988 | 2656 | 2324 |
| 24 | 3240 | 2916 | 2592 | 2268 |
| 25 | 3162 | 2846 | 2529 | 2213 |
| 26 | 3086 | 2777 | 2469 | 2160 |
| 27 | 3013 | 2711 | 2410 | 2109 |
| 28 | 2941 | 2647 | 2353 | 2059 |
| 29 | 2872 | 2585 | 2298 | 2010 |
| 30 | 2805 | 2524 | 2244 | 1963 |
| 32 | 2677 | 2409 | 2142 | 1874 |
| 34 | 2557 | 2301 | 2046 | 1790 |
| 36 | 2445 | 2200 | 1956 | 1711 |
| 38 | 2340 | 2106 | 1872 | 1638 |
| 40 | 2241 | 2017 | 1793 | 1569 |
| 42 | 2149 | 1934 | 1719 | 1505 |
| 44 | 2063 | 1857 | 1650 | 1444 |
| 46 | 1982 | 1784 | 1586 | 1388 |
| 48 | 1907 | 1716 | 1525 | 1335 |
| 50 | 1835 | 1652 | 1468 | 1285 |

For safety factors for various classes of structures to be used in connection with the above table, see p. 408.

SPECIFIC GRAVITIES AND WEIGHTS OF VARIOUS SUBSTANCES.

| <p>The Basis for Specific Gravities is Pure Water at 62 Degrees Fah., Barometer 30 Inches.</p> <p>Weight of One Cubic Foot, 62.355 Pounds.</p> | | Average Specific Gravity. Water = 1. | Average Weight of One Cubic Foot. Pounds. |
|--|--|---|--|
| Acid, acetic, 90% | | 1.062 | 66.3 |
| " fluoric, 58% | | 1.20 | 75 |
| " muriatic (hydrochloric), 40% | | 1.20 | 75 |
| " nitric, 35% | | 1.217 | 76 |
| " phosphoric, 72% | | 1.558 | 97.2 |
| " sulphuric, 97% | | 1.841 | 115 |
| Air, atmospheric at 60 degrees F., under pressure of one atmosphere, or 14.7 pounds per square inch, weighs $\frac{1}{815}$ as much as water | | .00123 | .0765 |
| Alabaster | | | 160 |
| Alcohol, commercial | | .833 | 52 |
| Alder wood | | .68 | 42 |
| Alum | | .53 | 33 |
| Aluminum bronze, 10% | | 7.70 | 480 |
| " " 5% | | 8.26 | 516 |
| " nickel alloy, annealed | | 2.74 | 170.9 |
| " " cast | | 2.85 | 178.1 |
| " " rolled | | 2.76 | 172.1 |
| " pure, annealed | | 2.66 | 165.9 |
| " " cast | | 2.56 | 159.6 |
| " " rolled | | 2.68 | 167.1 |
| " wire | | 2.70 | 168 |
| " wrought | | 2.67 | 167 |
| Ammonia, liquid, 29% | | .897 | 56 |
| Anthracite, 1.3 to 1.84; of Penna., 1.3 to 1.7 | | 1.5 | 93.5 |
| " broken, of any size, loose | | | 52 to 57 |
| " moderately shaken | | | 56 to 60 |
| " heaped bushel, loose, 77 to 83 pounds | | | |
| " a ton loose occupies 40 to 43 cubic feet | | | |
| Antimony, cast | | 6.70 | 418 |
| " native | | 6.67 | 416 |
| Apple wood | | .76 | 47 |
| Arsenic | | 5.67 | 354 |
| Asbestos | | 2.40 | 149 |
| Ash, American white, dry (see note p. 433) | | .61 | 38 |
| " perfectly dry (see note p. 423) | | .752 | 47 |
| Ashes of soft coal, solidly packed | | | 40 to 45 |
| Asphaltum, 1 to 1.8 | | 1.4 | 87.3 |
| Bamboo wood | | .35 | 22 |
| Barley | | | 40 |
| Basalt | | 2.86 | 178 |
| Beech wood | | .73 | 46 |
| Beer, lager | | 1.034 | 64.5 |

SPECIFIC GRAVITIES AND WEIGHTS OF VARIOUS SUBSTANCES.

| The Basis for Specific Gravities is Pure Water at 62 Degrees Fah., Barometer 30 Inches. Weight of One Cubic Foot, 62.355 Pounds. | | Average Specific Gravity. Water=1. | Average Weight of One Cubic Foot. Pounds. |
|--|--|---|--|
| Beeswax..... | | .965 | 60.2 |
| Benzine..... | | | 50 |
| Birch wood..... | | .65 | 41 |
| Bismuth..... | | 9.78 | 611 |
| Bleaching powder..... | | | 31 |
| Bluestone..... | | | 150 |
| Borax..... | | | 110 |
| Boxwood..... | | .97 | 60 |
| Brass, cu. 67, zn. 33, cast..... | | 8.32 | 519 |
| “ high yellow plates..... | | 8.59 | 535 |
| “ Muntz metal..... | | 8.22 | 512 |
| “ Naval rolled..... | | 8.51 | 530 |
| “ sheet..... | | 8.46 | 527 |
| “ wire..... | | 8.56 | 533 |
| Brick, best pressed..... | | | 150 |
| “ common and hard..... | | | 125 |
| “ soft inferior..... | | | 100 |
| Brickwork, at 125 pounds per cubic foot, 1 cubic yard equals 1.507 tons, and 17.92 cubic feet equal 1 ton..... | | | |
| “ coarse, inferior, soft..... | | | 100 |
| “ medium quality..... | | | 125 |
| “ pressed brick, fine joints..... | | | 140 |
| Bronze, cu. 90, tin 10..... | | 8.67 | 541 |
| “ gun..... | | 8.75 | 546 |
| “ Tobin..... | | 8.38 | 523 |
| Butter..... | | .94 | 59 |
| Butternut wood..... | | .45 | 28 |
| Calcite..... | | | 170 |
| Calcium..... | | 1.57 | 98 |
| Camphor..... | | .99 | 61.7 |
| Caoutchouc..... | | .96 | 60 |
| Carbon..... | | 2.15 | 134 |
| Carpet..... | | | 12 |
| Caustic soda..... | | | 88 |
| Cedar, American..... | | .56 | 35 |
| Cement barrel, 15-30 pounds, average 20 pounds..... | | | |
| “ mortar, Portland, 1 : 2½..... | | | 135 |
| “ natural, per barrel, net, 282 pounds..... | | | |
| “ “ bag, net, 94 pounds..... | | | |
| “ Portland, loose..... | | | 88 to 92 |
| “ “ packed, as in barrels..... | | | 108 to 115 |
| “ “ per bag, net, 94 pounds..... | | | |

SPECIFIC GRAVITIES AND WEIGHTS OF VARIOUS SUBSTANCES.

| The Basis for Specific Gravities is Pure Water at 62 Degrees Fah., Barometer 30 Inches. Weight of One Cubic Foot, 62.355 Pounds. | | Average Specific Gravity. Water=1. | Average Weight of One Cubic Foot. Pounds. |
|--|------|---|--|
| Cement, Portland, per barrel, net, 376 pounds..... | | | 100 |
| " " standard proportioning..... | | | 178 |
| " set..... | 2.85 | | 156 |
| Chalk..... | 2.5 | | 15 to 30 |
| Charcoal of pines and oaks..... | | | 30 |
| Cheese..... | | | 42 |
| Cherry wood, perfectly dry (see note p. 433)..... | .672 | | 41 |
| Chestnut..... | .66 | | 425 |
| Chromium..... | 6.8 | | 63.4 |
| Cider..... | 1.02 | | 40 |
| Cinders (coal ashes and clinkers)..... | | | 550 |
| Cinnabar..... | 8.81 | | 45 |
| Citron..... | .73 | | 63 |
| Clay, dry in lump, loose..... | | | 150 |
| " hard, ordinary..... | 2.1 | | 119 |
| " potters', dry, 1.8 to 2.1..... | 1.9 | | |
| Coal, anthracite (see Anthracite). | | | |
| " bituminous, a heaped bushel, loose, 70 to 78..... | | | 47 to 52 |
| " " broken, of any size, loose..... | | | 51 to 56 |
| " " moderately shaken..... | | | 79 to 84 |
| " " solid, Cambria Co., Pa., 1.27-1.34..... | | | 84 |
| " " " 1.2 to 1.5..... | 1.35 | | 52 |
| " " 1 ton occupies 43 to 48 cubic feet..... | | | 83 |
| " lignite..... | .83 | | 546 |
| Cobalt..... | 8.77 | | 85 |
| Coke..... | 1.34 | | |
| " loose, a heaped bushel, 35 to 42..... | | | 23 to 32 |
| " " good quality..... | | | |
| " 1 ton occupies 80 to 97 cubic feet..... | | | |
| Concrete, cinder, with Portland cement..... | | | 112 |
| " conglomerate " "..... | | | 150 |
| " gravel " "..... | | | 150 |
| " limestone " "..... | | | 148 |
| " sandstone " "..... | | | 143 |
| " trap " "..... | | | 155 |
| " loose, unrammed, weighs 5 to 25% lighter, varying with consistency..... | | | |
| Copper, cast, 8.6 to 8.8..... | 8.7 | | 542 |
| " hammered..... | 8.93 | | 557 |
| " plates and sheets..... | 8.93 | | 557 |
| " pure..... | 8.82 | | 549 |
| " rolled, 8.8 to 9..... | 8.9 | | 555 |
| " wire..... | 8.89 | | 554 |
| " wrought..... | 8.9 | | 555 |
| Cork, dry (see note p. 433)..... | .24 | | 15 |

SPECIFIC GRAVITIES AND WEIGHTS OF VARIOUS SUBSTANCES.

| The Basis for Specific Gravities is Pure Water at 62 Degrees Fah., Barometer 30 Inches. Weight of One Cubic Foot, 62.355 Pounds. | | Average Specific Gravity. Water=1. | Average Weight of One Cubic Foot. Pounds. |
|--|--|---|--|
| Corn..... | | | 31 |
| Cornmeal..... | | | 37 |
| Corundum, pure, 3.8 to 4..... | | 3.9 | |
| Cotton goods..... | | | 11-33 |
| Crockery..... | | | 40 |
| Cypress wood..... | | .46 | 29 |
| Dogwood..... | | .76 | 47 |
| Dolomite..... | | | 180 |
| Earth, common loam, perfectly dry, loose..... | | | 72 to 80 |
| " " " " " shaken..... | | | 82 to 92 |
| " " " " " rammed..... | | | 90 to 100 |
| " " " slightly moist, loose..... | | | 70 to 76 |
| " " " more moist, loose..... | | | 66 to 68 |
| " " " " " shaken..... | | | 75 to 90 |
| " " " " " packed..... | | | 90 to 100 |
| " " " as soft flowing mud..... | | | 104 to 112 |
| " " " " " " well pressed..... | | | 110 to 120 |
| Ebonite..... | | 1.15 | 72 |
| Ebony wood, American..... | | 1.33 | 83 |
| " " Indian..... | | 1.21 | 75 |
| Eggs..... | | 1.09 | |
| Elder wood..... | | .70 | 44 |
| Elm wood, perfectly dry (see note p. 433)..... | | .56 | 35 |
| Fat—beef, hog and mutton..... | | .92 | 57 |
| Feldspar..... | | | 160 |
| Fir wood..... | | .55 | 34 |
| Flax..... | | | 90 |
| Flint..... | | 2.6 | 162 |
| Flour, compact..... | | | 40 |
| " loose..... | | | 30 |
| Gamboge..... | | 1.22 | 76 |
| Gasoline (motor)..... | | .71-.75 | 44 to 47 |
| Glass, common window..... | | 2.52 | 157 |
| " crown or plate..... | | | 160 |
| " crystal..... | | | 188 |
| " flint..... | | 3.70 | 230 |
| Glassware in boxes..... | | | 60 |
| Gneiss, common, 2.62 to 2.76..... | | 2.69 | 168 |

SPECIFIC GRAVITIES AND WEIGHTS OF VARIOUS SUBSTANCES.

| The Basis for Specific Gravities is Pure Water at 62 Degrees Fah., Barometer 30 Inches. Weight of One Cubic Foot, 62.355 Pounds. | | Average Specific Gravity. Water=1. | Average Weight of One Cubic Foot. Pounds. |
|--|-----------|---|--|
| Gneiss, in loose piles..... | | | 96 |
| Gold, cast, pure or 24-karat..... | 19.258 | | 1204 |
| " pure, hammered..... | 19.5 | | 1217 |
| " standard 22-k. (gold 11, copper 1)..... | 17.5 | | 1090 |
| Granite, solid..... | 2.72 | | 170 |
| " broken..... | | | 96 |
| " dressed..... | | | 165 |
| " rubble..... | | | 154 |
| " dry..... | | | 138 |
| Graphite..... | | | 130 |
| Gravel..... | | | 120 |
| " and sand..... | | | 90-130 |
| Greenstone, trap, 2.8 to 3.2..... | 3.00 | | 187 |
| Gum arabic..... | 1.45 | | 90 |
| Gum wood..... | .92 | | 57 |
| Gunpowder, loose..... | .90 | | 56 |
| " shaken..... | 1.00 | | 62.4 |
| " solid..... | 1.55-1.80 | | 97-113 |
| Gutta-percha..... | .98 | | 61 |
| Gypsum, plaster of Paris or stucco mixed with water into a stiff mass, such as mortar, set and dried out..... | | | 77 |
| " rock, natural, free from surface water, not calcined in block form..... | | | 140-145 |
| " crushed, not calcined, all to pass through 1-inch ring..... | | | 90-100 |
| " ground, 90% to pass through 100-mesh screen dried of all free moisture, not calcined, known as "land plaster"..... | | | 75-80 |
| " same, but calcined, known as "stucco" or "plaster of Paris"—loose..... | | | 55-65 |
| " well shaken down or in bins..... | | | 65-75 |
| Hackmatack wood (American larch) (tamarack)..... | .59 | | 37 |
| Hay, baled..... | | | 24 |
| Hazel wood..... | .60 | | 38 |
| Hemlock wood..... | .40 | | 25 |
| Hemp..... | | | 90 |
| Hickory wood, perfectly dry (see note p. 433)..... | .85 | | 53 |
| Holly wood..... | .76 | | 47 |
| Honey..... | 1.45 | | 91 |
| Hornbeam wood..... | .76 | | 47 |
| Hornblende..... | | | 190 |
| Human blood..... | 1.054 | | 65.7 |

SPECIFIC GRAVITIES AND WEIGHTS OF VARIOUS SUBSTANCES.

| <p>The Basis for Specific Gravities is Pure Water at 62 Degrees Fah., Barometer 30 Inches. Weight of One Cubic Foot, 62.355 Pounds.</p> | | Average Specific Gravity. Water=1. | Average Weight of One Cubic Foot. Pounds. |
|---|--|---|--|
| Hydrogen..... | | .00008 | .0052 |
| Ice, .917 to .922..... | | .92 | 57.4 |
| India rubber | | .93 | 58 |
| Indigo..... | | 1.01 | 63 |
| Iron, cast, 6.9 to 7.4..... | | 7.15 | 446 |
| " grey cast..... | | 7.08 | 442 |
| " " foundry, cold..... | | 7.21 | 450 |
| " " " molten..... | | 6.94 | 433 |
| " pure..... | | 7.86 | 491 |
| " white cast..... | | 7.65 | 477 |
| " wire..... | | 7.77 | 485 |
| " wrought..... | | 7.69 | 480 |
| Jasmine wood, Spanish..... | | .77 | 48 |
| Juniper wood..... | | .56 | 35 |
| Larch wood..... | | .56 | 35 |
| Lard..... | | .95 | 59 |
| Lead, cast..... | | 11.37 | 708 |
| " commercial..... | | 11.38 | 709.6 |
| " sheet..... | | 11.43 | 712 |
| Leather, dry..... | | .86 | 54 |
| " greased..... | | 1.02 | 64 |
| " in bales..... | | | 16-23 |
| Lignite..... | | | 80 |
| Lignum-vitæ wood (dry)..... | | .65-1.33 | 41 to 83 |
| Lime..... | | 1.03 | 64 |
| " quick..... | | 1.5 | 95 |
| " " ground, thoroughly shaken, per struck bushel 93¾ pounds..... | | | 75 |
| " " " well shaken, per struck bushel 80 pounds..... | | | 64 |
| Limestone and marble..... | | 2.6 | 164.4 |
| " broken..... | | 1.61 | 100 |
| " solid..... | | 2.70 | 168 |
| Linden wood | | .60 | 38 |
| Loam..... | | 1.23 | 77 |
| Locust wood, dry (see note p. 433)..... | | .71 | 44 |
| Logwood..... | | .91 | 57 |
| Lye..... | | | 110 |
| Magnesite..... | | | 190 |

SPECIFIC GRAVITIES AND WEIGHTS OF VARIOUS SUBSTANCES.

| The Basis for Specific Gravities is Pure Water at 62 Degrees Fah., Barometer 30 Inches. J Weight of One Cubic Foot, 62.355 Pounds. | | | Average Specific Gravity. Water=1. | Average Weight of One Cubic Foot. Pounds. |
|---|--|--|---|--|
| Magnesium..... | | | 1.74 | 109 |
| Mahogany wood, Spanish, dry (see note p. 433) | | | .85 | 53 |
| “ “ Honduras, dry (see note. p. 433)..... | | | .56 | 35 |
| Manganese..... | | | 8.00 | 500 |
| Maple wood, dry (see note p. 433)..... | | | .79 | 49 |
| Marble (see Limestone). | | | | |
| Marl..... | | | | 140 |
| Masonry debris | | | | 90 |
| “ of brickwork (see Brickwork). | | | | |
| “ “ granite or limestone, well dressed..... | | | | 165 |
| “ “ well-scabbled mortar rubble, about 1/5 of mass will be mortar | | | | 154 |
| “ “ “ well-scabbled dry rubble..... | | | | 138 |
| “ “ “ roughly scabbled mortar rubble, about 1/4 to 1/3 of mass will be mortar | | | | 150 |
| “ “ “ scabbled dry rubble..... | | | | 125 |
| “ “ sandstone, 1/8 less than granite..... | | | | |
| Mastic wood..... | | | .85 | 53 |
| Mercury, at 32° F..... | | | 13.62 | 849 |
| “ at 68° F..... | | | 13.5 | 846 |
| Mica, 2.75 to 3.1..... | | | 2.93 | 183 |
| Milk..... | | | 1.03 | 64.5 |
| Molybdenum..... | | | 8.50 | 532 |
| Mortar, hardened, 1.4 to 1.9..... | | | 1.65 | 103 |
| Muck (decayed vegetable matter, manure, etc.)..... | | | .92 | 57 |
| Mud, dry, close..... | | | | 80 to 110 |
| “ wet, moderately pressed | | | | 110 to 130 |
| “ “ fluid | | | | 104 to 120 |
| Mulberry wood..... | | | .73 | 46 |
| Nickel, cast..... | | | 8.29 | 516 |
| “ rolled..... | | | 8.69 | 541 |
| “ silver (52 cu.+26 zn.+22 ni.) | | | 8.44 | 527 |
| Nitrogen..... | | | .00125 | .0782 |
| Oak wood, heart of old..... | | | 1.17 | 73 |
| “ “ live, perfectly dry, .88-1.02 (see note p. 433) | | | .95 | 59.3 |
| “ “ red, black, perfectly dry | | | | 32 to 45 |
| “ “ white | | | .84 | 52 |
| Oats..... | | | | 27 |
| Oil—bone, colza, cylinder, engine, 500° fire test, mustard seed, neatsfoot, paraffin, rape seed, tallow | | | .90 | 56.2 |
| “ burning (kerosene), 150° and 300°..... | | | .83 | 51.7 |

SPECIFIC GRAVITIES AND WEIGHTS OF VARIOUS SUBSTANCES.

| The Basis for Specific Gravities is Pure Water at 62 Degrees Fah., Barometer 30 Inches. Weight of One Cubic Foot, 62.355 Pounds. | | Average Specific Gravity. Water=1. | Average Weight of One Cubic Foot. Pounds. |
|--|--|---|--|
| Oil, cotton seed | | .96 | 60.2 |
| “ gasoline (motor) | | .71-.75 | 44 to 49 |
| “ lard | | .92 | 57.4 |
| “ linseed | | .94 | 58.8 |
| “ mineral lubricating | | .91 | 57 |
| “ Navy sperm | | .87 | 54 |
| “ olive | | .91 | 57 |
| “ petroleum | | .88 | 55 |
| “ signal | | .85 | 53 |
| “ turpentine | | .87 | 54 |
| “ whale | | .93 | 58 |
| Oxygen | | .00143 | .0895 |
| Paper, calendered | | | 50-70 |
| “ strawboard newspaper | | | 33-44 |
| “ writing or wrapping | | | 70-90 |
| Paraffine | | .89 | 55.5 |
| Pear wood | | .66 | 41 |
| Peat | | | 50 |
| Petroleum | | .878 | 54.8 |
| Phosphate rock | | | 200 |
| Pine wood, white | | .40 | 25 |
| “ “ yellow, Northern | | .55 | 34 |
| “ “ “ Southern | | .72 | 45 |
| Pitch | | 1.15 | 71.7 |
| Plaster | | | 53 |
| “ of Paris (see Gypsum). | | | |
| Platinum | | 21.5 | 1342 |
| Plum wood | | .78 | 49 |
| Poplar wood, dry (see note p. 433) | | .47 | 29 |
| “ “ white Spanish | | .53 | 33 |
| Porcelain | | 2.40 | 149 |
| Potassium | | .87 | 54 |
| Potatoes, in pile | | | 45 |
| Proof spirit | | .93 | 58 |
| Pumice stone | | .63 | 39 |
| Quartz | | 2.65 | 165 |
| Rags in bales | | | 15-36 |
| Redwood | | .48 | 30 |
| Rope | | | 42 |
| Rosin | | 1.10 | 68.6 |

SPECIFIC GRAVITIES AND WEIGHTS OF VARIOUS SUBSTANCES.

| <p>The Basis for Specific Gravities is Pure Water at 62 Degrees Fah., Barometer 30 Inches. Weight of One Cubic Foot, 62.355 Pounds.</p> | | Average Specific Gravity. Water=1. | Average Weight of One Cubic Foot. Pounds. |
|---|-------|---|--|
| Rubber..... | | | 60 |
| Rubber goods..... | | | 95 |
| Rye..... | | | 50 |
| Salt, coarse (per struck bushel, Syracuse, N. Y., 56 lbs.)..... | | | 45 |
| Saltpetre..... | | | 68 |
| Sand, of pure quartz, perfectly dry and loose..... | | | 90 to 106 |
| " " " voids full of water..... | | | 118 to 129 |
| " " " very large and small grains, dry..... | | | 117 |
| Sandstone, dressed..... | | | 144 |
| " 2.1 to 2.73, 131 to 171..... | 2.41 | | 151 |
| " quarried and piled, 1 measure solid makes 1¾ (about) piled..... | | | 86 |
| Sassafras wood..... | .48 | | 30 |
| Shales, red or black, 2.4 to 2.8..... | 2.6 | | 162 |
| Silk..... | | | 8-32 |
| Silver..... | 10.5 | | 655 |
| Slag..... | | | 160 to 180 |
| " furnace, granulated..... | | | 53 |
| Slate, 2.7 to 2.9..... | 2.8 | | 175 |
| Snow, fresh-fallen..... | | | 5 to 12 |
| " moistened, compacted by rain..... | | | 15 to 50 |
| Soapstone, 2.65 to 2.8..... | 2.73 | | 170 |
| Soda ash..... | | | 62 |
| Sodium..... | .97 | | 61 |
| Spelter, 6.8 to 7.2..... | 7.00 | | 437.5 |
| Spermaceti..... | .94 | | 59 |
| Spruce wood..... | .50 | | 31.2 |
| " " old..... | .46 | | 28.7 |
| Starch..... | | | 95 |
| Starch (in barrels)..... | | | 23 |
| Steam at 212° F..... | .0006 | | .0368 |
| Steel..... | 7.85 | | 489.6 |
| Straw, baled..... | | | 24 |
| Sugar..... | 1.60 | | 100 |
| " stored..... | | | 42 |
| Sulphur..... | 2.00 | | 125 |
| Sumac wood..... | | | 39 |
| Sycamore wood, perfectly dry (see note p. 433)..... | .59 | | 37 |
| Talc..... | | | 170 |
| Tallow..... | .94 | | 58.6 |
| Tar..... | 1.15 | | 71.7 |

SPECIFIC GRAVITIES AND WEIGHTS OF VARIOUS SUBSTANCES.

| <p>The Basis for Specific Gravities is Pure Water at 62 Degrees Fah., Barometer 30 Inches.</p> <p>Weight of One Cubic Foot, 62.355 Pounds.</p> | | | Average Specific Gravity. Water=1. | Average Weight of One Cubic Foot. Pounds. |
|--|--|--|---|--|
| Teak wood..... | | | .82 | 51 |
| Tile (see page 69). | | | | |
| Tin, cast, 7.2 to 7.5..... | | | 7.35 | 459 |
| " pure..... | | | 7.29 | 455 |
| Tobacco..... | | | | 28 |
| Trap rock, compact..... | | | 3.02 | 188 |
| " in pile..... | | | | 190 |
| Tungsten..... | | | 19.1 | 1192 |
| Turf..... | | | .40 | 25 |
| Vanadium..... | | | 5.5 | 343 |
| Vapor, alcohol..... | | | .00198 | .122 |
| " turpentine spirits..... | | | .00615 | .378 |
| " water..... | | | .00077 | .047 |
| Vine wood..... | | | 1.33 | 83 |
| Vinegar..... | | | 1.08 | 67.4 |
| Walnut wood, black, perfectly dry (see note below)... | | | .61 | 38 |
| Water, pure rain, distilled, at 32° F., Bar. 30 inches..... | | | | 62.417 |
| " " " " " 62° F., " 30 " | | | 1 | 62.355 |
| " " " " " 212° F., " 30 " | | | | 59.7 |
| " sea, 1.026 to 1.030..... | | | 1.028 | 64.08 |
| Wax, bees..... | | | .97 | 61 |
| Wheat..... | | | | 39-44 |
| White metal (Babbitts)..... | | | 7.32 | 456 |
| Willow wood..... | | | .54 | 34 |
| Wine..... | | | .99 | 62 |
| Wool, in bales..... | | | | 15-22 |
| Woolen goods..... | | | | 13-22 |
| Yew wood..... | | | .79 | 49 |
| Zinc, cast..... | | | 6.86 | 428 |
| " pure..... | | | 7.15 | 446 |
| " rolled..... | | | 7.19 | 449 |

NOTE.—Green timbers usually weigh from one-fifth to nearly one-half more than dry; ordinary building timbers, tolerably seasoned, one-sixth more.

For specific gravities of woods not given in this table, see page 408.

STANDARD DECIMAL GAUGE.

| Standard Decimal Gauge in Inches. | Thickness in Fractions of an Inch. | Approximate Thickness in Millimetres. | Weight per Square Foot in Pounds, Avoirdupois. | |
|--|---|--|---|--|
| | | | IRON. Basis—480 Pounds per Cubic Foot. | STEEL. Basis—489.6 Pounds per Cubic Foot. |
| .002 | 1-500 | .05080010 | .08 | .0816 |
| .004 | 1-250 | .10160020 | .16 | .1632 |
| .006 | 3-500 | .15240030 | .24 | .2448 |
| .008 | 1-125 | .20320041 | .32 | .3264 |
| .010 | 1-100 | .25400051 | .40 | .4080 |
| .012 | 3-250 | .30480061 | .48 | .4896 |
| .014 | 7-500 | .35560071 | .56 | .5712 |
| .016 | 2-125 ($\frac{1}{8}+$) | .40640081 | .64 | .6528 |
| .018 | 9-500 | .45720091 | .72 | .7344 |
| .020 | 1-50 | .50800102 | .80 | .8160 |
| .022 | 11-500 | .55880112 | .88 | .8976 |
| .025 | 1-40 | .63500127 | 1.00 | 1.0200 |
| .028 | 7-250 | .71120142 | 1.12 | 1.1424 |
| .032 | 4-125 ($\frac{1}{4}+$) | .81280163 | 1.28 | 1.3056 |
| .036 | 9-250 | .91440183 | 1.44 | 1.4688 |
| .040 | 1-25 | 1.01600203 | 1.60 | 1.6320 |
| .045 | 9-200 | 1.14300229 | 1.80 | 1.8360 |
| .050 | 1-20 | 1.27000254 | 2.00 | 2.0400 |
| .055 | 11-200 | 1.39700280 | 2.20 | 2.2440 |
| .060 | 3-50 ($\frac{3}{16}-$) | 1.52400305 | 2.40 | 2.4480 |
| .065 | 13-200 | 1.65100330 | 2.60 | 2.6520 |
| .070 | 7-100 | 1.77800356 | 2.80 | 2.8560 |
| .075 | 3-40 | 1.90500381 | 3.00 | 3.0600 |
| .080 | 2-25 | 2.03200406 | 3.20 | 3.2640 |
| .085 | 17-200 | 2.15900432 | 3.40 | 3.4680 |
| .090 | 9-100 | 2.28600457 | 3.60 | 3.6720 |
| .095 | 19-200 | 2.41300483 | 3.80 | 3.8760 |
| .100 | 1-10 | 2.54000508 | 4.00 | 4.0800 |
| .110 | 11-100 | 2.79400559 | 4.40 | 4.4880 |
| .125 | 1-8 | 3.17500630 | 5.00 | 5.1000 |
| .135 | 27-200 | 3.42900686 | 5.40 | 5.5080 |
| .150 | 3-20 | 3.81000762 | 6.00 | 6.1200 |
| .165 | 33-200 | 4.19100838 | 6.60 | 6.7320 |
| .180 | 9-50 | 4.57200914 | 7.20 | 7.3440 |
| .200 | 1-5 | 5.08001016 | 8.00 | 8.1600 |
| .220 | 11-50 | 5.58801118 | 8.80 | 8.9760 |
| .240 | 6-25 | 6.09601219 | 9.60 | 9.7920 |
| .250 | 1-4 | 6.35001270 | 10.00 | 10.2000 |

WIRE AND SHEET METAL GAUGES.

In Decimals of an Inch.

| Number of Gauge. | Birmingham or Stubbs Iron Wire Gauge (B. W. G.) | American or Brown & Sharpe Wire Gauge. | United States Standard Gauge for Sheet and Plate Iron and Steel. | Washburn & Moen Manufacturing Co. and John A. Roebbing's Sons Co. Wire Gauge. | Trenton Iron Co. Wire Gauge. | American Screw Co. Screw Wire Gauge. | British Imperial or English Legal Standard Wire Gauge. | New Birmingham Standard Sheet and Hoop Gauge (B. G.) |
|------------------------|---|--|---|--|---------------------------------|---|--|--|
| 7/0 | | | .5 | | | | .500 | .6666 |
| 6/0 | | | .46875 | .4600 | | | .464 | .625 |
| 5/0 | | | .4375 | .4300 | .450 | | .432 | .5883 |
| 4/0 | .454 | .460000 | .40625 | .3938 | .400 | | .400 | .5416 |
| 3/0 | .425 | .409642 | .375 | .3625 | .360 | .0315 | .372 | .500 |
| 00 | .380 | .364796 | .34375 | .3310 | .330 | .0447 | .348 | .4452 |
| 0 | .340 | .324861 | .3125 | .3065 | .305 | .0578 | .324 | .3964 |
| 1 | .300 | .289297 | .28125 | .2830 | .285 | .0710 | .300 | .3532 |
| 2 | .284 | .257627 | .265625 | .2625 | .265 | .0842 | .276 | .3147 |
| 3 | .259 | .229423 | .25 | .2437 | .245 | .0973 | .252 | .2804 |
| 4 | .238 | .204307 | .234375 | .2263 | .225 | .1105 | .232 | .250 |
| 5 | .220 | .181940 | .21875 | .2070 | .205 | .1236 | .212 | .2225 |
| 6 | .203 | .162023 | .203125 | .1920 | .190 | .1368 | .192 | .1981 |
| 7 | .180 | .144285 | .1875 | .1770 | .175 | .1500 | .176 | .1764 |
| 8 | .165 | .128490 | .171875 | .1620 | .160 | .1631 | .160 | .1570 |
| 9 | .148 | .114423 | .15625 | .1483 | .145 | .1763 | .144 | .1398 |
| 10 | .134 | .101897 | .140625 | .1350 | .130 | .1894 | .128 | .1250 |
| 11 | .120 | .090742 | .125 | .1205 | .1175 | .2026 | .116 | .1113 |
| 12 | .109 | .080808 | .109375 | .1055 | .105 | .2158 | .104 | .0991 |
| 13 | .095 | .071962 | .09375 | .0915 | .0925 | .2289 | .092 | .0882 |
| 14 | .083 | .064084 | .078125 | .0800 | .0806 | .2421 | .080 | .0785 |
| 15 | .072 | .057068 | .0703125 | .0720 | .070 | .2552 | .072 | .0699 |
| 16 | .065 | .050821 | .0625 | .0625 | .061 | .2684 | .064 | .0625 |
| 17 | .058 | .045257 | .05625 | .0540 | .0525 | .2816 | .056 | .0556 |
| 18 | .049 | .040303 | .05 | .0475 | .045 | .2947 | .048 | .0495 |
| 19 | .042 | .035890 | .04375 | .0410 | .040 | .3079 | .040 | .0440 |
| 20 | .035 | .031961 | .0375 | .0348 | .035 | .3210 | .036 | .0392 |
| 21 | .032 | .028462 | .034375 | .03175 | .031 | .3342 | .032 | .0349 |
| 22 | .028 | .025346 | .03125 | .0286 | .028 | .3474 | .028 | .03125 |
| 23 | .025 | .022572 | .028125 | .0258 | .025 | .3605 | .024 | .02782 |
| 24 | .022 | .020101 | .025 | .0230 | .0225 | .3737 | .022 | .02476 |
| 25 | .020 | .017900 | .021875 | .0204 | .020 | .3868 | .020 | .02204 |
| 26 | .018 | .015941 | .01875 | .0181 | .018 | .4000 | .018 | .01961 |
| 27 | .016 | .014195 | .0171875 | .0173 | .017 | .4132 | .0164 | .01745 |
| 28 | .014 | .012641 | .015625 | .0162 | .016 | .4263 | .0148 | .015625 |
| 29 | .013 | .011257 | .0140625 | .0150 | .015 | .4395 | .0136 | .0139 |
| 30 | .012 | .010025 | .0125 | .0140 | .014 | .4526 | .0124 | .0123 |
| 31 | .010 | .008928 | .0109375 | .0132 | .013 | .4658 | .0116 | .0110 |
| 32 | .009 | .007950 | .01015625 | .0128 | .012 | .4790 | .0108 | .0098 |
| 33 | .008 | .007080 | .009375 | .0118 | .011 | .4921 | .0100 | .0087 |
| 34 | .007 | .006305 | .00859375 | .0104 | .010 | .5053 | .0092 | .0077 |
| 35 | .005 | .005615 | .0078125 | .0095 | .0095 | .5184 | .0084 | .0069 |
| 36 | .004 | .005000 | .00703125 | .0090 | .009 | .5316 | .0076 | .0061 |
| 37 | | .004453 | .006640625 | .0085 | .0085 | .5448 | .0068 | .0054 |
| 38 | | .003965 | .00625 | .0080 | .008 | .5579 | .0060 | .0048 |
| 39 | | .003531 | | .0075 | .0075 | .5711 | .0052 | .0043 |
| 40 | | .003144 | | .0070 | .007 | .5842 | .0048 | .00386 |

WEIGHTS OF SHEETS AND PLATES OF STEEL, WROUGHT IRON, COPPER AND BRASS.

American or Browne & Sharpe Gauge.

| Number of Gauge. | Thickness in Inches. | Weight per Square Foot. | | | |
|------------------------|----------------------------|-------------------------|---------|---------|---------|
| | | Steel. | Iron. | Copper. | Brass. |
| 0000 | .460000 | 18.7680 | 18.4000 | 20.8380 | 19.6880 |
| 000 | .409642 | 16.7134 | 16.3857 | 18.5568 | 17.5327 |
| 00 | .364796 | 14.8837 | 14.5918 | 16.5253 | 15.6133 |
| 0 | .324861 | 13.2543 | 12.9944 | 14.7162 | 13.9041 |
| 1 | .289297 | 11.8033 | 11.5719 | 13.1052 | 12.3819 |
| 2 | .257627 | 10.5112 | 10.3051 | 11.6705 | 11.0264 |
| 3 | .229423 | 9.3605 | 9.1769 | 10.3929 | 9.8193 |
| 4 | .204307 | 8.3357 | 8.1723 | 9.2551 | 8.7443 |
| 5 | .181940 | 7.4232 | 7.2776 | 8.2419 | 7.7870 |
| 6 | .162023 | 6.6105 | 6.4809 | 7.3396 | 6.9346 |
| 7 | .144285 | 5.8868 | 5.7714 | 6.5361 | 6.1754 |
| 8 | .128490 | 5.2424 | 5.1396 | 5.8206 | 5.4994 |
| 9 | .114423 | 4.6685 | 4.5769 | 5.1834 | 4.8973 |
| 10 | .101897 | 4.1574 | 4.0759 | 4.6159 | 4.3612 |
| 11 | .090742 | 3.7023 | 3.6297 | 4.1106 | 3.8838 |
| 12 | .080808 | 3.2970 | 3.2323 | 3.6606 | 3.4586 |
| 13 | .071962 | 2.9360 | 2.8785 | 3.2599 | 3.0800 |
| 14 | .064084 | 2.6146 | 2.5634 | 2.9030 | 2.7428 |
| 15 | .057068 | 2.3284 | 2.2827 | 2.5852 | 2.4425 |
| 16 | .050821 | 2.0735 | 2.0328 | 2.3022 | 2.1751 |
| 17 | .045257 | 1.8465 | 1.8103 | 2.0501 | 1.9370 |
| 18 | .040303 | 1.6444 | 1.6121 | 1.8257 | 1.7250 |
| 19 | .035890 | 1.4643 | 1.4356 | 1.6258 | 1.5361 |
| 20 | .031961 | 1.3040 | 1.2784 | 1.4478 | 1.3679 |
| 21 | .028462 | 1.1612 | 1.1385 | 1.2893 | 1.2182 |
| 22 | .025346 | 1.0341 | 1.0138 | 1.1482 | 1.0848 |
| 23 | .022572 | .92094 | .90288 | 1.0225 | .96608 |
| 24 | .020101 | .82012 | .80404 | .91058 | .86032 |
| 25 | .017900 | .73032 | .71600 | .81087 | .76612 |
| 26 | .015941 | .65039 | .63764 | .72213 | .68227 |
| 27 | .014195 | .57916 | .56780 | .64303 | .60755 |
| 28 | .012641 | .51575 | .50564 | .57264 | .54103 |
| 29 | .011257 | .45929 | .45028 | .50994 | .48180 |
| 30 | .010025 | .40902 | .40100 | .45413 | .42907 |
| 31 | .008928 | .36426 | .35712 | .40444 | .38212 |
| 32 | .007950 | .32436 | .31800 | .36014 | .34026 |
| 33 | .007080 | .28886 | .28320 | .32072 | .30302 |
| 34 | .006305 | .25724 | .25220 | .28562 | .26985 |
| 35 | .005615 | .22909 | .22460 | .25436 | .24032 |
| 36 | .005000 | .20400 | .20000 | .22650 | .21400 |
| 37 | .004453 | .18168 | .17812 | .20172 | .19059 |
| 38 | .003965 | .16177 | .15860 | .17961 | .16970 |
| 39 | .003531 | .14406 | .14124 | .15995 | .15113 |
| 40 | .003144 | .12828 | .12576 | .14242 | .13456 |

For weights of steel plates $\frac{1}{16}$ " and over in thickness, see "Table of Weights of Flat Rolled Bars," pages 475 to 483 inclusive.

WEIGHTS OF SHEETS AND PLATES OF STEEL, WROUGHT IRON, COPPER AND BRASS.

Birmingham Wire Gauge (B. W. G.)

| Number of Gauge. | Thickness in Inches. | Weight per Square Foot. | | | |
|------------------------|----------------------------|-------------------------|-------|---------|---------|
| | | Steel. | Iron. | Copper. | Brass. |
| 0000 | .454 | 18.5232 | 18.16 | 20.5662 | 19.4312 |
| 000 | .425 | 17.3400 | 17.00 | 19.2525 | 18.1900 |
| 00 | .380 | 15.5040 | 15.20 | 17.2140 | 16.2640 |
| 0 | .340 | 13.8720 | 13.60 | 15.4020 | 14.5520 |
| 1 | .300 | 12.2400 | 12.00 | 13.5900 | 12.8400 |
| 2 | .284 | 11.5872 | 11.36 | 12.8652 | 12.1552 |
| 3 | .259 | 10.5672 | 10.36 | 11.7327 | 11.0852 |
| 4 | .238 | 9.7104 | 9.52 | 10.7814 | 10.1864 |
| 5 | .220 | 8.9760 | 8.80 | 9.966 | 9.4160 |
| 6 | .203 | 8.2824 | 8.12 | 9.1959 | 8.6884 |
| 7 | .180 | 7.3440 | 7.20 | 8.1540 | 7.7040 |
| 8 | .165 | 6.7320 | 6.60 | 7.4745 | 7.0620 |
| 9 | .148 | 6.0384 | 5.92 | 6.7044 | 6.3344 |
| 10 | .134 | 5.4672 | 5.36 | 6.0702 | 5.7352 |
| 11 | .120 | 4.8960 | 4.80 | 5.4360 | 5.1360 |
| 12 | .109 | 4.4472 | 4.36 | 4.9377 | 4.6652 |
| 13 | .095 | 3.8760 | 3.80 | 4.3035 | 4.0660 |
| 14 | .083 | 3.3864 | 3.32 | 3.7599 | 3.5524 |
| 15 | .072 | 2.9376 | 2.88 | 3.2616 | 3.0816 |
| 16 | .065 | 2.6520 | 2.60 | 2.9445 | 2.7820 |
| 17 | .058 | 2.3664 | 2.32 | 2.6274 | 2.4824 |
| 18 | .049 | 1.9992 | 1.96 | 2.2197 | 2.0972 |
| 19 | .042 | 1.7136 | 1.68 | 1.9026 | 1.7976 |
| 20 | .035 | 1.4280 | 1.40 | 1.5855 | 1.4980 |
| 21 | .032 | 1.3056 | 1.28 | 1.4496 | 1.3696 |
| 22 | .028 | 1.1424 | 1.12 | 1.2684 | 1.1984 |
| 23 | .025 | 1.0200 | 1.00 | 1.1325 | 1.0700 |
| 24 | .022 | .8976 | .88 | .9966 | .9416 |
| 25 | .020 | .8160 | .80 | .9060 | .8560 |
| 26 | .018 | .7344 | .72 | .8154 | .7704 |
| 27 | .016 | .6528 | .64 | .7248 | .6848 |
| 28 | .014 | .5712 | .56 | .6342 | .5992 |
| 29 | .013 | .5304 | .52 | .5889 | .5564 |
| 30 | .012 | .4896 | .48 | .5436 | .5136 |
| 31 | .010 | .4080 | .40 | .4530 | .4280 |
| 32 | .009 | .3672 | .36 | .4077 | .3852 |
| 33 | .008 | .3264 | .32 | .3624 | .3424 |
| 34 | .007 | .2856 | .28 | .3171 | .2996 |
| 35 | .005 | .2040 | .20 | .2265 | .2140 |
| 36 | .004 | .1632 | .16 | .1812 | .1712 |

Specific Gravities

Weight of a Cubic Foot ..

" " " Inch ..

7.85

489.6

.2833

7.70

480.0

.2778

8.72

543.6

.3146

8.24

513.6

.2972

COMBINED TABLE OF SIZES IN THE PRINCIPAL WIRE GAUGES.

Values printed in bold-faced type are exact; values not exact are rounded off to four significant figures, except diameters of the American (B. & S.) Wire Gauge and of the Metric Wire Gauge in the column headed "Diameter, inches," are given to 0.001 inch for the larger sizes and to 0.0001 inch for the smaller. This represents the usual degree of accuracy in the measurement of wires.

| Diameter | | | Wire Gauge Numbers | | | | | Cross Section | | | |
|--------------|-------------|--------------|-----------------------|--------------------|-------------------------|---------------------|------------|---------------|-------------|------------------|------------|
| Mils | Mm. | Ins. | American (B. & S.) | Washburn & Moen | Birmingham (Stubbs') | British Standard | Metric | Sq. Ins. | Sq. Mils | Circular Mils | Sq. Mm. |
| 500 | 12.70 | .500 | | | | 7-0 | | .1963 | 196 300 | 250 000 | 126.7 |
| 490 | 12.45 | .490 | | 7-0 | | | | .1886 | 188 600 | 240 100 | 121.7 |
| 464 | 11.79 | .464 | | | | 6-0 | | .1691 | 169 100 | 215 300 | 109.1 |
| 461.5 | 11.70 | .4615 | | 6-0 | | | | .1673 | 167 300 | 213 000 | 107.9 |
| 460 | 11.68 | .460 | 4-0 | | 4-0 | | | .1662 | 166 200 | 211 600 | 107.2 |
| 454 | 11.53 | .454 | | | | | | .1619 | 161 900 | 206 100 | 104.4 |
| 432 | 10.97 | .432 | | | | 5-0 | | .1466 | 146 600 | 186 600 | 94.56 |
| 430.5 | 10.93 | .4305 | | 5-0 | | | | .1456 | 145 600 | 185 300 | 93.91 |
| 425 | 10.80 | .425 | | | 3-0 | | | .1419 | 141 900 | 180 600 | 91.52 |
| 409.6 | 10.40 | .410 | 3-0 | | | | | .1318 | 131 800 | 167 800 | 85.03 |
| 400 | 10.16 | .400 | | | | 4-0 | | .1257 | 125 700 | 160 000 | 81.07 |
| 393.8 | 10.00 | .3938 | | 4-0 | | | | .1218 | 121 800 | 155 100 | 78.58 |
| 393.7 | 10.0 | .3937 | | | | | 100 | .1217 | 121 700 | 155 000 | 78.54 |
| 380 | 9.652 | .380 | | | 2-0 | | | .1134 | 113 400 | 144 400 | 73.17 |
| 372 | 9.449 | .372 | | | | 3-0 | | .1087 | 108 700 | 138 400 | 70.12 |
| 364.8 | 9.266 | .365 | 2-0 | | | | | .1045 | 104 500 | 133 100 | 67.43 |
| 362.5 | 9.208 | .3625 | | 3-0 | | | | .1032 | 103 200 | 131 400 | 66.58 |
| 354.3 | 9.0 | .354 | | | | | 90 | .098 61 | 98 610 | 125 500 | 63.62 |
| 348 | 8.839 | .348 | | | | 2-0 | | .095 11 | 95 110 | 121 100 | 61.36 |
| 340 | 8.636 | .340 | | | 0 | | | .090 79 | 90 790 | 115 600 | 58.58 |
| 331 | 8.407 | .331 | | 2-0 | | | | .086 05 | 86 050 | 109 600 | 55.52 |
| 324.9 | 8.251 | .325 | 0 | | | | | .082 89 | 82 890 | 105 500 | 53.48 |
| 324 | 8.230 | .324 | | | | 0 | | .082 45 | 82 450 | 105 000 | 53.19 |
| 315 | 8.0 | .315 | | | | | 80 | .077 91 | 77 910 | 99 200 | 50.27 |
| 306.5 | 7.785 | .3065 | | 0 | | | | .073 78 | 73 780 | 93 940 | 47.60 |
| 300 | 7.620 | .300 | | | 1 | 1 | | .070 69 | 70 690 | 90 000 | 45.60 |
| 289.3 | 7.348 | .289 | 1 | | | | | .065 73 | 65 730 | 83 690 | 42.41 |

COMBINED TABLE OF SIZES IN THE PRINCIPAL WIRE GAUGES—(Continued).

| Diameter | | | Wire Gauge Numbers | | | | | Cross Section | | | |
|--------------|------------|--------------|-----------------------|--------------------|-----------------------|---------------------|-----------|---------------|-------------|------------------|------------|
| Mils | Mm. | Ins. | American (B. & S.) | Washburn & Moen | Birmingham (Stubs) | British Standard | Metric | Sq. Ins. | Sq. Mils | Circular Mils | Sq. Mm. |
| 264 | 7.214 | .284 | | | 2 | | | .063 35 | 63 350 | 80 660 | 40.87 |
| 283 | 7.188 | .283 | | 1 | | | | .062 90 | 62 900 | 80 090 | 40.58 |
| 276 | 7.010 | .276 | | | | 2 | | .059 83 | 59 830 | 76 180 | 38.60 |
| 275.6 | 7.0 | .276 | | | | | 70 | .059 65 | 59 650 | 75 950 | 38.48 |
| 262.5 | 6.668 | .2625 | | 2 | | | | .054 12 | 54 120 | 68 910 | 34.92 |
| 259 | 6.579 | .259 | | | 3 | | | .052 69 | 52 690 | 67 080 | 33.99 |
| 257.6 | 6.544 | .258 | 2 | | | | | .052 13 | 52 130 | 66 370 | 33.63 |
| 252 | 6.401 | .252 | | | | 3 | | .049 88 | 49 880 | 63 500 | 32.18 |
| 243.7 | 6.190 | .2437 | | 3 | | | | .046 64 | 46 640 | 59 390 | 30.09 |
| 238 | 6.045 | .238 | | | 4 | | | .044 49 | 44 490 | 56 640 | 28.70 |
| 236.2 | 6.0 | .236 | | | | | 60 | .043 83 | 43 830 | 55 800 | 28.27 |
| 232 | 5.893 | .232 | | | | 4 | | .042 27 | 42 270 | 53 820 | 27.27 |
| 229.4 | 5.827 | .229 | 3 | | | | | .041 34 | 41 340 | 52 630 | 26.67 |
| 225.3 | 5.723 | .2253 | | 4 | | | | .039 87 | 39 870 | 50 760 | 25.72 |
| 220 | 5.588 | .220 | | | 5 | | | .038 01 | 38 010 | 48 400 | 24.52 |
| 212 | 5.385 | .212 | | | | 5 | | .035 30 | 35 300 | 44 940 | 22.77 |
| 207 | 5.258 | .207 | | 5 | | | | .033 65 | 33 650 | 42 850 | 21.71 |
| 204.3 | 5.189 | .204 | 4 | | | | | .032 78 | 32 780 | 41 740 | 21.15 |
| 203 | 5.156 | .203 | | | 6 | | | .032 37 | 32 370 | 41 210 | 20.88 |
| 196.8 | 5.0 | .197 | | | | | 50 | .030 43 | 30 430 | 38 750 | 19.63 |
| 192 | 4.877 | .192 | | 6 | | 6 | | .028 95 | 28 950 | 36 860 | 18.68 |
| 181.9 | 4.621 | .182 | 5 | | | | | .026 00 | 26 000 | 33 100 | 16.77 |
| 180 | 4.572 | .180 | | | 7 | | | .025 45 | 25 450 | 32 400 | 16.42 |
| 177.2 | 4.5 | .177 | | | | | 45 | .024 65 | 24 650 | 31 390 | 15.90 |
| 177 | 4.496 | .177 | | 7 | | | | .024 61 | 24 610 | 31 330 | 15.87 |
| 176 | 4.470 | .176 | | | | 7 | | .024 33 | 24 330 | 30 980 | 15.70 |
| 165 | 4.191 | .165 | | | 8 | | | .021 38 | 21 380 | 27 220 | 13.80 |
| 162 | 4.115 | .162 | 6 | 8 | | | | .020 62 | 20 620 | 26 250 | 13.30 |
| 160 | 4.064 | .160 | | | | 8 | | .020 11 | 20 110 | 25 600 | 12.97 |
| 157.5 | 4.0 | .157 | | | | | 40 | .019 48 | 19 480 | 24 810 | 12.57 |
| 148.3 | 3.767 | .1483 | | 9 | | | | .017 27 | 17 270 | 21 990 | 11.14 |
| 148 | 3.759 | .148 | | | 9 | | | .017 20 | 17 200 | 21 900 | 11.10 |
| 144.3 | 3.665 | .144 | 7 | | | | | .016 35 | 16 350 | 20 820 | 10.55 |
| 144 | 3.658 | .144 | | | | 9 | | .016 29 | 16 290 | 20 740 | 10.51 |
| 137.8 | 3.5 | .138 | | | | | 35 | .014 91 | 14 910 | 18 990 | 9.621 |
| 135 | 3.429 | .135 | | 10 | | | | .014 31 | 14 310 | 18 220 | 9.235 |
| 134 | 3.404 | .134 | | | 10 | | | .014 10 | 14 100 | 17 960 | 9.098 |
| 128.5 | 3.264 | .128 | 8 | | | | | .012 97 | 12 970 | 16 510 | 8.366 |
| 128 | 3.251 | .128 | | | | 10 | | .012 87 | 12 870 | 16 380 | 8.302 |

COMBINED TABLE OF SIZES IN THE PRINCIPAL WIRE GAUGES—(Continued).

| Diameter | | | Wire Gauge Numbers | | | | | Cross Section | | | |
|--------------|------------|--------------|-----------------------|--------------------|------------------------|---------------------|-----------|---------------|-------------|------------------|------------|
| Mils | Mm. | Ins. | American (B. & S.) | Washburn & Moen | Birmingham (Stubbs) | British Standard | Metric | Sq. Ins. | Sq. Mils | Circular Mils | Sq. Mm. |
| 120.5 | 3.061 | .1205 | | 11 | | | | .011 40 | 11 400 | 14 520 | 7.358 |
| 120 | 3.048 | .120 | | | 11 | | | .011 31 | 11 310 | 14 400 | 7.297 |
| 118.1 | 3.0 | .118 | | | | | 30 | .010 96 | 10 960 | 13 950 | 7.069 |
| 116 | 2.946 | .116 | | | | 11 | | .010 57 | 10 570 | 13 460 | 6.818 |
| 114.4 | 2.906 | .114 | 9 | | | | | .010 28 | 10 280 | 13 090 | 6.634 |
| 109 | 2.769 | .109 | | | 12 | | | .009 331 | 9331 | 11 880 | 6.020 |
| 105.5 | 2.680 | .1055 | | 12 | | | | .008 742 | 8742 | 11 130 | 5.640 |
| 104 | 2.642 | .104 | | | | 12 | | .008 495 | 8495 | 10 820 | 5.481 |
| 101.9 | 2.588 | .102 | 10 | | | | | .008 155 | 8155 | 10 380 | 5.261 |
| 98.42 | 2.5 | .098 | | | | | 25 | .007 609 | 7609 | 9687 | 4.909 |
| 95 | 2.413 | .095 | | | 13 | | | .007 088 | 7088 | 9025 | 4.573 |
| 92 | 2.337 | .092 | | | | 13 | | .006 648 | 6648 | 8464 | 4.289 |
| 91.5 | 2.324 | .0915 | | 13 | | | | .006 576 | 6576 | 8372 | 4.242 |
| 90.74 | 2.305 | .091 | 11 | | | | | .006 467 | 6467 | 8234 | 4.172 |
| 83 | 2.108 | .083 | | | 14 | | | .005 411 | 5411 | 6889 | 3.491 |
| 80.81 | 2.053 | .081 | 12 | | | | | .005 129 | 5129 | 6530 | 3.309 |
| 80 | 2.032 | .080 | | 14 | | 14 | | .005 027 | 5027 | 6450 | 3.243 |
| 78.74 | 2.0 | .079 | | | | | 20 | .004 869 | 4869 | 6200 | 3.142 |
| 72 | 1.829 | .072 | | 15 | 15 | 15 | | .004 072 | 4072 | 5184 | 2.627 |
| 71.96 | 1.828 | .072 | 13 | | | | | .004 067 | 4067 | 5178 | 2.624 |
| 70.87 | 1.8 | .071 | | | | | 18 | .003 944 | 3944 | 5022 | 2.545 |
| 65 | 1.651 | .065 | | | 16 | | | .003 318 | 3318 | 4225 | 2.141 |
| 64.08 | 1.628 | .064 | 14 | | | | | .003 225 | 3225 | 4107 | 2.081 |
| 64 | 1.626 | .064 | | | | 16 | | .003 217 | 3217 | 4096 | 2.075 |
| 62.99 | 1.6 | .063 | | | | | 16 | .003 116 | 3116 | 3968 | 2.011 |
| 62.5 | 1.588 | .0625 | | 16 | | | | .003 068 | 3068 | 3906 | 1.979 |
| 58 | 1.473 | .058 | | | 17 | | | .002 642 | 2642 | 3364 | 1.705 |
| 57.07 | 1.450 | .057 | 15 | | | | | .002 558 | 2558 | 3257 | 1.650 |
| 56 | 1.422 | .056 | | | | 17 | | .002 463 | 2463 | 3136 | 1.589 |
| 55.12 | 1.4 | .055 | | | | | 14 | .002 386 | 2386 | 3038 | 1.539 |
| 54 | 1.372 | .054 | | 17 | | | | .002 290 | 2290 | 2916 | 1.478 |
| 50.82 | 1.291 | .051 | 16 | | | | | .002 028 | 2028 | 2583 | 1.309 |
| 49 | 1.245 | .049 | | | 18 | | | .001 886 | 1886 | 2401 | 1.217 |
| 48 | 1.219 | .048 | | | | 18 | | .001 810 | 1810 | 2304 | 1.167 |
| 47.5 | 1.207 | .0475 | | 18 | | | | .001 772 | 1772 | 2256 | 1.143 |
| 47.24 | 1.2 | .047 | | | | | 12 | .001 753 | 1753 | 2232 | 1.131 |
| 45.26 | 1.150 | .045 | 17 | | | | | .001 609 | 1609 | 2048 | 1.038 |
| 42 | 1.067 | .042 | | | 19 | | | .001 385 | 1385 | 1764 | 0.938 |
| 41 | 1.041 | .041 | | 19 | | | | .001 320 | 1320 | 1681 | 0.8518 |

COMBINED TABLE OF SIZES IN THE PRINCIPAL WIRE GAUGES—(Continued).

| Diameter | | | Wire Gauge Numbers | | | | | Cross Section | | | |
|----------|-------|-------|-----------------------|--------------------|------------------------|---------------------|--------|---------------|-------------|------------------|------------|
| Mils | Mm. | Ins. | American (B. & S.) | Washburn & Moen | Birmingham (Stubs') | British Standard | Metric | Sq. Ins. | Sq. Mils | Circular Mils | Sq. Mm. |
| 40.3 | 1.024 | .040 | 18 | | | | | .001 276 | 1276 | 1624 | .8231 |
| 40 | 1.016 | .040 | | | | 19 | | .001 257 | 1257 | 1600 | .8107 |
| 39.37 | 1.0 | .039 | | | | | 10 | .001 217 | 1217 | 1550 | .7854 |
| 36 | .9144 | .036 | | | | 20 | | .001 018 | 1018 | 1296 | .6567 |
| 35.89 | .9116 | .036 | 19 | | | | | .001 012 | 1012 | 1288 | .6527 |
| 35.43 | .90 | .035 | | | | | 9 | .0009861 | 986.1 | 1255 | .6362 |
| 35 | .8890 | .035 | | | 20 | | | .0009621 | 962.1 | 1225 | .6207 |
| 34.8 | .8839 | .0343 | | 20 | | | | .0009511 | 951.1 | 1211 | .6136 |
| 32 | .8128 | .032 | | | 21 | 21 | | .0008042 | 804.2 | 1024 | .5189 |
| 31.96 | .8118 | .032 | 20 | | | | | .0008023 | 802.3 | 1022 | .5176 |
| 31.7 | .8052 | .0317 | | 21 | | | | .0007892 | 789.2 | 1005 | .5092 |
| 31.5 | .80 | .031 | | | | | 8 | .0007791 | 779.1 | 992 | .5027 |
| 28.6 | .7264 | .0286 | | 22 | | | | .0006424 | 642.4 | 818 | .4145 |
| 28.46 | .7229 | .0285 | 21 | | | | | .0006363 | 636.3 | 810.1 | .4105 |
| 28 | .7112 | .028 | | | 22 | 22 | | .0006158 | 615.8 | 784 | .3973 |
| 27.56 | .70 | .0276 | | | | | 7 | .0005965 | 596.5 | 759.5 | .3848 |
| 25.8 | .6553 | .0258 | | 23 | | | | .0005228 | 522.8 | 665.6 | .3373 |
| 25.35 | .6438 | .0253 | 22 | | | | | .0005046 | 504.6 | 642.4 | .3255 |
| 25 | .6350 | .025 | | | 23 | | | .0004909 | 490.9 | 625 | .3167 |
| 24 | .6096 | .024 | | | | 23 | | .0004524 | 452.4 | 576 | .2919 |
| 23.62 | .60 | .0236 | | | | | 6 | .0004383 | 438.3 | 558 | .2827 |
| 23 | .5842 | .023 | | 24 | | | | .0004155 | 415.5 | 529 | .2675 |
| 22.57 | .5733 | .0226 | 23 | | | | | .0004001 | 400.1 | 509.5 | .2582 |
| 22 | .5588 | .022 | | | 24 | 24 | | .0003801 | 380.1 | 484 | .2452 |
| 20.4 | .5182 | .0204 | | 25 | | | | .0003269 | 326.9 | 416.2 | .2109 |
| 20.1 | .5106 | .0201 | 24 | | | | | .0003173 | 317.3 | 404 | .2047 |
| 20 | .5080 | .020 | | | 25 | 25 | | .0003142 | 314.2 | 400 | .2027 |
| 19.68 | .50 | .0197 | | | | | 5 | .0003043 | 304.3 | 387.5 | .1963 |
| 18.1 | .4597 | .0181 | | 26 | | | | .0002573 | 257.3 | 327.6 | .1660 |
| 18 | .4572 | .018 | | | 26 | 26 | | .0002545 | 254.5 | 324 | .1642 |
| 17.9 | .4547 | .0179 | 25 | | | | | .0002517 | 251.7 | 320.4 | .1624 |
| 17.72 | .45 | .0177 | | | | | 4.5 | .0002465 | 246.5 | 313.9 | .1590 |
| 17.3 | .4394 | .0173 | | 27 | | | | .0002351 | 235.1 | 299.3 | .1517 |
| 16.4 | .4166 | .0164 | | | | 27 | | .0002112 | 211.2 | 269 | .1363 |
| 16.2 | .4115 | .0162 | | 28 | | | | .0002061 | 206.1 | 262.4 | .1330 |
| 16 | .4064 | .016 | | | 27 | | | .0002011 | 201.1 | 256 | .1297 |
| 15.94 | .4049 | .0159 | 26 | | | | | .0001996 | 199.6 | 254.1 | .1288 |
| 15.75 | .40 | .0157 | | | | | 4 | .0001948 | 194.8 | 248 | .1257 |
| 15 | .3810 | .015 | | 29 | | | | .0001767 | 176.7 | 225 | .1140 |

COMBINED TABLE OF SIZES IN THE PRINCIPAL WIRE GAUGES—(Continued).

| Diameter | | | Wire Gauge Numbers | | | | | Cross Section | | | |
|----------|-------|-------|-----------------------|--------------------|------------------------|---------------------|--------|---------------|-------------|------------------|------------|
| Mils | Mm. | Ins. | American (B. & S.) | Washburn & Moen | Birmingham (Stubs') | British Standard | Metric | Sq. Ins. | Sq. Mils | Circular Mils | Sq. Mm. |
| 14.8 | .3759 | .0148 | | | | 28 | | .031720 | 172.0 | 219 | .1110 |
| 14.2 | .3606 | .0142 | 27 | | | | | .031583 | 158.3 | 201.5 | .1021 |
| 14 | .3556 | .0140 | | 30 | 28 | | | .031539 | 153.9 | 196 | .099 32 |
| 13.78 | .35 | .0138 | | | | | 3-5 | .031491 | 149.1 | 189.9 | .096 21 |
| 13.5 | .3454 | .0136 | | | | 29 | | .031453 | 145.3 | 185 | .093 72 |
| 13.2 | .3353 | .0132 | | 31 | | | | .031368 | 136.8 | 174.2 | .088 29 |
| 13 | .3302 | .0130 | | | 29 | | | .031327 | 132.7 | 169 | .085 63 |
| 12.8 | .3251 | .0128 | | 32 | | | | .031287 | 128.7 | 163.8 | .083 02 |
| 12.64 | .3211 | .0126 | 28 | | | | | .031255 | 125.5 | 159.8 | .080 98 |
| 12.4 | .3150 | .0124 | | | | 30 | | .031208 | 120.8 | 153.8 | .077 91 |
| 12 | .3048 | .0120 | | | 30 | | | .031131 | 113.1 | 144 | .072 97 |
| 11.81 | .30 | .0118 | | | | | 3 | .031096 | 109.6 | 139.5 | .070 69 |
| 11.8 | .2997 | .0118 | | 33 | | | | .031094 | 109.4 | 139.2 | .070 55 |
| 11.6 | .2946 | .0116 | | | | 31 | | .031057 | 105.7 | 134.6 | .068 18 |
| 11.26 | .2859 | .0113 | 29 | | | | | .030954 | 99.54 | 126.7 | .064 22 |
| 10.8 | .2743 | .0108 | | | | 32 | | .0309161 | 91.61 | 116.6 | .059 10 |
| 10.4 | .2642 | .0104 | | 34 | | | | .0308495 | 84.95 | 108.2 | .054 81 |
| 10.03 | .2546 | .0100 | 30 | | | | | .0307894 | 78.94 | 100.5 | .050 93 |
| 10 | .2540 | .0100 | | | 31 | 33 | | .0307854 | 78.54 | 100 | .050 67 |
| 9.842 | .25 | .0098 | | | | | 2-5 | .0307609 | 76.09 | 96.87 | .049 09 |
| 9.5 | .2413 | .0095 | | 35 | | | | .0307088 | 70.88 | 90.25 | .045 73 |
| 9.2 | .2337 | .0092 | | | | 34 | | .0306648 | 66.48 | 84.64 | .042 89 |
| 9 | .2286 | .0090 | | 36 | 32 | | | .0306362 | 63.62 | 81 | .041 04 |
| 8.928 | .2268 | .0089 | 31 | | | | | .0306260 | 62.60 | 79.7 | .040 39 |
| 8.5 | .2159 | .0085 | | 37 | | | | .0305675 | 56.75 | 72.25 | .036 61 |
| 8.4 | .2134 | .0084 | | | | 35 | | .0305542 | 55.42 | 70.56 | .035 75 |
| 8 | .2032 | .0080 | | 38 | 33 | | | .0305027 | 50.27 | 64 | .032 43 |
| 7.95 | .2019 | .0080 | 32 | | | | | .0304964 | 49.64 | 63.21 | .032 03 |
| 7.874 | .20 | .0079 | | | | | 2 | .0304869 | 48.69 | 62.00 | .031 42 |
| 7.6 | .1930 | .0076 | | | | 36 | | .0304536 | 45.36 | 57.76 | .029 27 |
| 7.5 | .1905 | .0075 | | 39 | | | | .0304418 | 44.18 | 56.25 | .028 50 |
| 7.087 | .18 | .0071 | | | | | 1-8 | .0303944 | 39.44 | 50.22 | .025 45 |
| 7.08 | .1798 | .0071 | 33 | | | | | .0303937 | 39.37 | 50.13 | .025 40 |
| 7 | .1778 | .0070 | | 40 | 34 | | | .0303848 | 38.48 | 49 | .024 83 |
| 6.8 | .1727 | .0068 | | | | 37 | | .0303632 | 36.32 | 46.24 | .023 43 |
| 6.6 | .1676 | .0066 | | 41 | | | | .0303421 | 34.21 | 43.56 | .022 07 |
| 6.305 | .1601 | .0063 | 34 | | | | | .0303122 | 31.22 | 39.75 | .020 14 |
| 6.299 | .16 | .0063 | | | | | 1-6 | .0303116 | 31.16 | 39.68 | .020 11 |
| 6.2 | .1575 | .0062 | | 42 | | | | .0303019 | 30.19 | 38.44 | .019 48 |

COMBINED TABLE OF SIZES IN THE PRINCIPAL WIRE GAUGES—(Continued).

| Diameter | | | Wire Gauge Numbers | | | | | Cross Section | | | |
|--------------|--------|-------|-----------------------|--------------------|------------------------|---------------------|------------|---------------|-------------|------------------|------------|
| Mils | Mm. | Ins. | American (B. & S.) | Washburn & Moen | Birmingham (Stubs') | British Standard | Metric | Sq. Ins. | Sq. Mils | Circular Mils | Sq. Mm. |
| 6 | .1524 | .0060 | | 43 | | 38 | | .042827 | 28.27 | 36 | .018 24 |
| 5.906 | .15 | .0059 | | | | | 1-5 | .042739 | 27.39 | 34.87 | .017 67 |
| 5.8 | .1473 | .0058 | | 44 | | | | .042642 | 26.42 | 33.64 | .017 05 |
| 5.615 | .1426 | .0056 | 35 | | | | | .042476 | 24.76 | 31.52 | .015 97 |
| 5.512 | .14 | .0055 | | | | | 1-4 | .042386 | 23.86 | 30.38 | .015 39 |
| 5.5 | .1397 | .0055 | | 45 | | | | .042376 | 23.76 | 30.25 | .015 33 |
| 5.2 | .1321 | .0052 | | 46 | | 39 | | .042124 | 21.24 | 27.04 | .013 70 |
| 5 | .1270 | .0050 | 36 | 47 | 35 | | | .041963 | 19.63 | 25 | .012 67 |
| 4.8 | .1219 | .0048 | | 48 | | 40 | | .041810 | 18.10 | 23.04 | .011 67 |
| 4.724 | .12 | .0047 | | | | | 1-2 | .041753 | 17.53 | 22.32 | .011 31 |
| 4.6 | .1168 | .0046 | | 49 | | | | .041662 | 16.62 | 21.16 | .010 72 |
| 4.453 | .1131 | .0045 | 37 | | | | | .041557 | 15.57 | 19.83 | .010 05 |
| 4.4 | .1118 | .0044 | | 50 | | 41 | | .041521 | 15.21 | 19.36 | .009 810 |
| 4 | .1016 | .0040 | | | 36 | 42 | | .041257 | 12.57 | 16 | .008 107 |
| 3.965 | .1007 | .0040 | 38 | | | | | .041235 | 12.35 | 15.72 | .007 967 |
| 3.937 | .10 | .0039 | | | | | 1 | .041217 | 12.17 | 15.50 | .007 854 |
| 3.6 | .09144 | .0036 | | | | 43 | | .041018 | 10.18 | 12.96 | .006 567 |
| 3.531 | .08969 | .0035 | 39 | | | | | .0409793 | 9.793 | 12.47 | .006 318 |
| 3.2 | .08128 | .0032 | | | | 44 | | .0408042 | 8.042 | 10.24 | .005 189 |
| 3.145 | .07987 | .0031 | 40 | | | | | .0407766 | 7.766 | 9.888 | .005 010 |
| 2.800 | .07113 | .0028 | 41 | | | | | .0406159 | 6.159 | 7.842 | .003 973 |
| 2.8 | .07112 | .0028 | | | | 45 | | .0406158 | 6.158 | 7.84 | .003 973 |
| 2.494 | .06334 | .0025 | 42 | | | | | .0404884 | 4.884 | 6.219 | .003 151 |
| 2.4 | .06096 | .0024 | | | | 46 | | .0404524 | 4.524 | 5.76 | .002 919 |
| 2.221 | .05641 | .0022 | 43 | | | | | .0403873 | 3.873 | 4.932 | .002 499 |
| 2 | .05080 | .0020 | | | | 47 | | .0403142 | 3.142 | 4 | .002 027 |
| 1.978 | .05023 | .0020 | 44 | | | | | .0403072 | 3.072 | 3.911 | .001 982 |
| 1.969 | .05 | .0020 | | | | | 0-5 | .0403044 | 3.044 | 3.875 | .001 963 |
| 1.761 | .04473 | .0018 | 45 | | | | | .0402436 | 2.436 | 3.102 | .001 572 |
| 1.6 | .04064 | .0016 | | | | 48 | | .0402011 | 2.011 | 2.560 | .001 297 |
| 1.568 | .03984 | .0016 | 46 | | | | | .0401932 | 1.932 | 2.460 | .001 246 |
| 1.397 | .03547 | .0014 | 47 | | | | | .0401532 | 1.532 | 1.951 | .001 0884 |
| 1.243 | .03159 | .0012 | 48 | | | | | .0401215 | 1.215 | 1.547 | .001 0838 |
| 1.2 | .03048 | .0012 | | | | 49 | | .0401131 | 1.131 | 1.44 | .001 07297 |
| 1.107 | .02813 | .0011 | 49 | | | | | .0400635 | .9635 | 1.227 | .001 06216 |
| 1 | .02540 | .0010 | | | | 50 | | .04007854 | .7854 | 1 | .001 05067 |
| .9863 | .02505 | .0010 | 50 | | | | | .04007641 | .7641 | .9728 | .001 04929 |

DECIMAL EQUIVALENTS OF NON-BINARY FRACTIONS

(Denominators 7 to 19)

| Nu- mer- ator | DENOMINATOR | | | | | | | | | |
|---------------------|-------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| | 7 | 9 | 11 | 12 | 13 | 14 | 15 | 17 | 18 | 19 |
| 1 | .1429 | .1111 | .0909 | .0833 | .0769 | .0714 | .0667 | .0588 | .0556 | .0526 |
| 2 | .2857 | .2222 | .1818 | .1667 | .1538 | .1429 | .1333 | .1176 | .1111 | .1053 |
| 3 | .4286 | .3333 | .2727 | .2500 | .2308 | .2143 | .2000 | .1765 | .1667 | .1579 |
| 4 | .5714 | .4444 | .3636 | .3333 | .3077 | .2857 | .2667 | .2353 | .2222 | .2105 |
| 5 | .7143 | .5556 | .4545 | .4167 | .3846 | .3571 | .3333 | .2941 | .2778 | .2632 |
| 6 | .8571 | .6667 | .5455 | .5000 | .4615 | .4286 | .4000 | .3529 | .3333 | .3158 |
| 7 | | .7778 | .6364 | .5833 | .5385 | .5000 | .4667 | .4118 | .3889 | .3684 |
| 8 | | .8889 | .7273 | .6667 | .6154 | .5714 | .5333 | .4706 | .4444 | .4211 |
| 9 | | | .8182 | .7500 | .6923 | .6429 | .6000 | .5294 | .5000 | .4737 |
| 10 | | | .9091 | .8333 | .7692 | .7143 | .6667 | .5882 | .5556 | .5263 |
| 11 | | | | .9167 | .8462 | .7857 | .7333 | .6471 | .6111 | .5789 |
| 12 | | | | | .9231 | .8571 | .8000 | .7059 | .6667 | .6316 |
| 13 | | | | | | .9286 | .8667 | .7647 | .7222 | .6842 |
| 14 | | | | | | | .9333 | .8235 | .7778 | .7368 |
| 15 | | | | | | | | .8824 | .8333 | .7895 |
| 16 | | | | | | | | .9412 | .8889 | .8421 |
| 17 | | | | | | | | | .9444 | .8947 |
| 18 | | | | | | | | | | .9474 |

SQUARE ROOTS AND CUBE ROOTS OF FRACTIONS

| Frac- tion | Square Root | Cube Root | Frac- tion | Square Root | Cube Root | Frac- tion | Square Root | Cube Root |
|---------------|----------------|--------------|---------------|----------------|--------------|-----------------|----------------|--------------|
| $\frac{1}{2}$ | .70711 | .79370 | $\frac{6}{7}$ | .92582 | .94991 | $\frac{1}{12}$ | .28868 | .43679 |
| $\frac{1}{3}$ | .57735 | .69336 | $\frac{1}{8}$ | .35355 | .50000 | $\frac{5}{12}$ | .64550 | .74690 |
| $\frac{2}{3}$ | .81650 | .87358 | $\frac{3}{8}$ | .61237 | .72112 | $\frac{7}{12}$ | .76876 | .83555 |
| $\frac{1}{4}$ | .50000 | .62996 | $\frac{5}{8}$ | .79057 | .85499 | $\frac{11}{12}$ | .95743 | .97141 |
| $\frac{3}{4}$ | .86603 | .90856 | $\frac{7}{8}$ | .93541 | .95647 | $\frac{1}{16}$ | .25000 | .39685 |
| $\frac{1}{6}$ | .40825 | .55032 | $\frac{1}{9}$ | .33333 | .48075 | $\frac{3}{16}$ | .43301 | .57236 |
| $\frac{5}{6}$ | .91287 | .94104 | $\frac{2}{9}$ | .47140 | .60571 | $\frac{5}{16}$ | .55902 | .67860 |
| $\frac{1}{7}$ | .37796 | .52275 | $\frac{4}{9}$ | .66667 | .76314 | $\frac{7}{16}$ | .66144 | .75915 |
| $\frac{2}{7}$ | .53452 | .65863 | $\frac{5}{9}$ | .74536 | .82207 | $\frac{9}{16}$ | .75000 | .82548 |
| $\frac{3}{7}$ | .65465 | .75395 | $\frac{7}{9}$ | .88192 | .91963 | $\frac{11}{16}$ | .82916 | .88259 |
| $\frac{4}{7}$ | .75593 | .82983 | $\frac{8}{9}$ | .94281 | .96150 | $\frac{13}{16}$ | .90138 | .93313 |
| $\frac{5}{7}$ | .84515 | .89390 | | | | $\frac{15}{16}$ | .96825 | .97872 |

*(Denominators 21 to 31.)

[illegible]

**DECIMALS OF A FOOT FOR EACH $\frac{1}{32}$ OF
AN INCH.**

| Inch. | 0" | 1" | 2" | 3" | 4" | 5" |
|-----------------|----------|--------------|--------------|--------------|--------------|--------------|
| 0 | 0 | .0833 | .1667 | .2500 | .3333 | .4167 |
| $\frac{1}{64}$ | .0013 | .0846 | .1680 | .2513 | .3346 | .4180 |
| $\frac{3}{32}$ | .0026 | .0859 | .1693 | .2526 | .3359 | .4193 |
| $\frac{3}{64}$ | .0039 | .0872 | .1706 | .2539 | .3372 | .4206 |
| $\frac{1}{16}$ | .0052 | .0885 | .1719 | .2552 | .3385 | .4219 |
| $\frac{5}{64}$ | .0065 | .0898 | .1732 | .2565 | .3398 | .4232 |
| $\frac{3}{32}$ | .0078 | .0911 | .1745 | .2578 | .3411 | .4245 |
| $\frac{7}{64}$ | .0091 | .0924 | .1758 | .2591 | .3424 | .4258 |
| $\frac{1}{8}$ | .0104 | .0937 | .1771 | .2604 | .3437 | .4271 |
| $\frac{9}{64}$ | .0117 | .0951 | .1784 | .2617 | .3451 | .4284 |
| $\frac{5}{32}$ | .0130 | .0964 | .1797 | .2630 | .3464 | .4297 |
| $\frac{11}{64}$ | .0143 | .0977 | .1810 | .2643 | .3477 | .4310 |
| $\frac{3}{16}$ | .0156 | .0990 | .1823 | .2656 | .3490 | .4323 |
| $\frac{13}{64}$ | .0169 | .1003 | .1836 | .2669 | .3503 | .4336 |
| $\frac{7}{32}$ | .0182 | .1016 | .1849 | .2682 | .3516 | .4349 |
| $\frac{15}{64}$ | .0195 | .1029 | .1862 | .2695 | .3529 | .4362 |
| $\frac{1}{4}$ | .0208 | .1042 | .1875 | .2708 | .3542 | .4375 |
| $\frac{17}{64}$ | .0221 | .1055 | .1888 | .2721 | .3555 | .4388 |
| $\frac{9}{32}$ | .0234 | .1068 | .1901 | .2734 | .3568 | .4401 |
| $\frac{19}{64}$ | .0247 | .1081 | .1914 | .2747 | .3581 | .4414 |
| $\frac{5}{16}$ | .0260 | .1094 | .1927 | .2760 | .3594 | .4427 |
| $\frac{21}{64}$ | .0273 | .1107 | .1940 | .2773 | .3607 | .4440 |
| $\frac{11}{32}$ | .0286 | .1120 | .1953 | .2786 | .3620 | .4453 |
| $\frac{23}{64}$ | .0299 | .1133 | .1966 | .2799 | .3633 | .4466 |
| $\frac{3}{8}$ | .0312 | .1146 | .1979 | .2812 | .3646 | .4479 |
| $\frac{25}{64}$ | .0326 | .1159 | .1992 | .2826 | .3659 | .4492 |
| $\frac{13}{32}$ | .0339 | .1172 | .2005 | .2839 | .3672 | .4505 |
| $\frac{27}{64}$ | .0352 | .1185 | .2018 | .2852 | .3685 | .4518 |
| $\frac{7}{16}$ | .0365 | .1198 | .2031 | .2865 | .3698 | .4531 |
| $\frac{29}{64}$ | .0378 | .1211 | .2044 | .2878 | .3711 | .4544 |
| $\frac{15}{32}$ | .0391 | .1224 | .2057 | .2891 | .3724 | .4557 |
| $\frac{31}{64}$ | .0404 | .1237 | .2070 | .2904 | .3737 | .4570 |
| $\frac{1}{2}$ | .0417 | .1250 | .2083 | .2917 | .3750 | .4583 |

**DECIMALS OF A FOOT FOR EACH $\frac{1}{64}$ OF
AN INCH.**

| Inch. | 6" | 7" | 8" | 9" | 10" | 11" |
|-----------------|-------|-------|-------|-------|-------|-------|
| 0 | .5000 | .5833 | .6667 | .7500 | .8333 | .9167 |
| $\frac{1}{64}$ | .5013 | .5846 | .6680 | .7513 | .8346 | .9180 |
| $\frac{2}{64}$ | .5026 | .5859 | .6693 | .7526 | .8359 | .9193 |
| $\frac{3}{64}$ | .5039 | .5872 | .6706 | .7539 | .8372 | .9206 |
| $\frac{4}{64}$ | .5052 | .5885 | .6719 | .7552 | .8385 | .9219 |
| $\frac{5}{64}$ | .5065 | .5898 | .6732 | .7565 | .8398 | .9232 |
| $\frac{6}{64}$ | .5078 | .5911 | .6745 | .7578 | .8411 | .9245 |
| $\frac{7}{64}$ | .5091 | .5924 | .6758 | .7591 | .8424 | .9258 |
| $\frac{8}{64}$ | .5104 | .5937 | .6771 | .7604 | .8437 | .9271 |
| $\frac{9}{64}$ | .5117 | .5951 | .6784 | .7617 | .8451 | .9284 |
| $\frac{10}{64}$ | .5130 | .5964 | .6797 | .7630 | .8464 | .9297 |
| $\frac{11}{64}$ | .5143 | .5977 | .6810 | .7643 | .8477 | .9310 |
| $\frac{12}{64}$ | .5156 | .5990 | .6823 | .7656 | .8490 | .9323 |
| $\frac{13}{64}$ | .5169 | .6003 | .6836 | .7669 | .8503 | .9336 |
| $\frac{14}{64}$ | .5182 | .6016 | .6849 | .7682 | .8516 | .9349 |
| $\frac{15}{64}$ | .5195 | .6029 | .6862 | .7695 | .8529 | .9362 |
| $\frac{16}{64}$ | .5208 | .6042 | .6875 | .7708 | .8542 | .9375 |
| $\frac{17}{64}$ | .5221 | .6055 | .6888 | .7721 | .8555 | .9388 |
| $\frac{18}{64}$ | .5234 | .6068 | .6901 | .7734 | .8568 | .9401 |
| $\frac{19}{64}$ | .5247 | .6081 | .6914 | .7747 | .8581 | .9414 |
| $\frac{20}{64}$ | .5260 | .6094 | .6927 | .7760 | .8594 | .9427 |
| $\frac{21}{64}$ | .5273 | .6107 | .6940 | .7773 | .8607 | .9440 |
| $\frac{22}{64}$ | .5286 | .6120 | .6953 | .7786 | .8620 | .9453 |
| $\frac{23}{64}$ | .5299 | .6133 | .6966 | .7799 | .8633 | .9466 |
| $\frac{24}{64}$ | .5312 | .6146 | .6979 | .7812 | .8646 | .9479 |
| $\frac{25}{64}$ | .5326 | .6159 | .6992 | .7826 | .8659 | .9492 |
| $\frac{26}{64}$ | .5339 | .6172 | .7005 | .7839 | .8672 | .9505 |
| $\frac{27}{64}$ | .5352 | .6185 | .7018 | .7852 | .8685 | .9518 |
| $\frac{28}{64}$ | .5365 | .6198 | .7031 | .7865 | .8698 | .9531 |
| $\frac{29}{64}$ | .5378 | .6211 | .7044 | .7878 | .8711 | .9544 |
| $\frac{30}{64}$ | .5391 | .6224 | .7057 | .7891 | .8724 | .9557 |
| $\frac{31}{64}$ | .5404 | .6237 | .7070 | .7904 | .8737 | .9570 |
| $\frac{32}{64}$ | .5417 | .6250 | .7083 | .7917 | .8750 | .9583 |

**DECIMALS OF A FOOT FOR EACH $\frac{1}{64}$ OF
AN INCH.**

| Inch. | 0" | 1" | 2" | 3" | 4" | 5" |
|-----------------|-------|-------|-------|-------|-------|-------|
| $\frac{33}{64}$ | .0430 | .1263 | .2096 | .2930 | .3763 | .4596 |
| $\frac{34}{64}$ | .0443 | .1276 | .2109 | .2943 | .3776 | .4609 |
| $\frac{35}{64}$ | .0456 | .1289 | .2122 | .2956 | .3789 | .4622 |
| $\frac{36}{64}$ | .0469 | .1302 | .2135 | .2969 | .3802 | .4635 |
| $\frac{37}{64}$ | .0482 | .1315 | .2148 | .2982 | .3815 | .4648 |
| $\frac{38}{64}$ | .0495 | .1328 | .2161 | .2995 | .3828 | .4661 |
| $\frac{39}{64}$ | .0508 | .1341 | .2174 | .3008 | .3841 | .4674 |
| $\frac{40}{64}$ | .0521 | .1354 | .2188 | .3021 | .3854 | .4688 |
| $\frac{41}{64}$ | .0534 | .1367 | .2201 | .3034 | .3867 | .4701 |
| $\frac{42}{64}$ | .0547 | .1380 | .2214 | .3047 | .3880 | .4714 |
| $\frac{43}{64}$ | .0560 | .1393 | .2227 | .3060 | .3893 | .4727 |
| $\frac{44}{64}$ | .0573 | .1406 | .2240 | .3073 | .3906 | .4740 |
| $\frac{45}{64}$ | .0586 | .1419 | .2253 | .3086 | .3919 | .4753 |
| $\frac{46}{64}$ | .0599 | .1432 | .2266 | .3099 | .3932 | .4766 |
| $\frac{47}{64}$ | .0612 | .1445 | .2279 | .3112 | .3945 | .4779 |
| $\frac{48}{64}$ | .0625 | .1458 | .2292 | .3125 | .3958 | .4792 |
| $\frac{49}{64}$ | .0638 | .1471 | .2305 | .3138 | .3971 | .4805 |
| $\frac{50}{64}$ | .0651 | .1484 | .2318 | .3151 | .3984 | .4818 |
| $\frac{51}{64}$ | .0664 | .1497 | .2331 | .3164 | .3997 | .4831 |
| $\frac{52}{64}$ | .0677 | .1510 | .2344 | .3177 | .4010 | .4844 |
| $\frac{53}{64}$ | .0690 | .1523 | .2357 | .3190 | .4023 | .4857 |
| $\frac{54}{64}$ | .0703 | .1536 | .2370 | .3203 | .4036 | .4870 |
| $\frac{55}{64}$ | .0716 | .1549 | .2383 | .3216 | .4049 | .4883 |
| $\frac{56}{64}$ | .0729 | .1562 | .2396 | .3229 | .4062 | .4896 |
| $\frac{57}{64}$ | .0742 | .1576 | .2409 | .3242 | .4076 | .4909 |
| $\frac{58}{64}$ | .0755 | .1589 | .2422 | .3255 | .4089 | .4922 |
| $\frac{59}{64}$ | .0768 | .1602 | .2435 | .3268 | .4102 | .4935 |
| $\frac{60}{64}$ | .0781 | .1615 | .2448 | .3281 | .4115 | .4948 |
| $\frac{61}{64}$ | .0794 | .1628 | .2461 | .3294 | .4128 | .4961 |
| $\frac{62}{64}$ | .0807 | .1641 | .2474 | .3307 | .4141 | .4974 |
| $\frac{63}{64}$ | .0820 | .1654 | .2487 | .3320 | .4154 | .4987 |
| 1 | | | | | | |

DECIMALS OF A FOOT FOR EACH $\frac{1}{16}$ OF AN INCH.

| Inch. | 6" | 7" | 8" | 9" | 10" | 11" |
|------------------|-------|-------|-------|-------|-------|--------|
| $\frac{32}{64}$ | .5430 | .6263 | .7096 | .7930 | .8763 | .9596 |
| $\frac{17}{32}$ | .5443 | .6276 | .7109 | .7943 | .8776 | .9609 |
| $\frac{33}{64}$ | .5456 | .6289 | .7122 | .7956 | .8789 | .9622 |
| $\frac{64}{128}$ | .5469 | .6302 | .7135 | .7969 | .8802 | .9635 |
| $\frac{27}{64}$ | .5482 | .6315 | .7148 | .7982 | .8815 | .9648 |
| $\frac{19}{32}$ | .5495 | .6328 | .7161 | .7995 | .8828 | .9661 |
| $\frac{39}{64}$ | .5508 | .6341 | .7174 | .8008 | .8841 | .9674 |
| $\frac{64}{128}$ | .5521 | .6354 | .7188 | .8021 | .8854 | .9688 |
| $\frac{41}{64}$ | .5534 | .6367 | .7201 | .8034 | .8867 | .9701 |
| $\frac{21}{32}$ | .5547 | .6380 | .7214 | .8047 | .8880 | .9714 |
| $\frac{43}{64}$ | .5560 | .6393 | .7227 | .8060 | .8893 | .9727 |
| $\frac{11}{16}$ | .5573 | .6406 | .7240 | .8073 | .8906 | .9740 |
| $\frac{45}{64}$ | .5586 | .6419 | .7253 | .8086 | .8919 | .9753 |
| $\frac{23}{32}$ | .5599 | .6432 | .7266 | .8099 | .8932 | .9766 |
| $\frac{47}{64}$ | .5612 | .6445 | .7279 | .8112 | .8945 | .9779 |
| $\frac{64}{128}$ | .5625 | .6458 | .7292 | .8125 | .8958 | .9792 |
| $\frac{49}{64}$ | .5638 | .6471 | .7305 | .8138 | .8971 | .9805 |
| $\frac{25}{32}$ | .5651 | .6484 | .7318 | .8151 | .8984 | .9818 |
| $\frac{51}{64}$ | .5664 | .6497 | .7331 | .8164 | .8997 | .9831 |
| $\frac{11}{16}$ | .5677 | .6510 | .7344 | .8177 | .9010 | .9844 |
| $\frac{53}{64}$ | .5690 | .6523 | .7357 | .8190 | .9023 | .9857 |
| $\frac{27}{32}$ | .5703 | .6536 | .7370 | .8203 | .9036 | .9870 |
| $\frac{55}{64}$ | .5716 | .6549 | .7383 | .8216 | .9049 | .9883 |
| $\frac{64}{128}$ | .5729 | .6562 | .7396 | .8229 | .9062 | .9896 |
| $\frac{57}{64}$ | .5742 | .6576 | .7409 | .8242 | .9076 | .9909 |
| $\frac{29}{32}$ | .5755 | .6589 | .7422 | .8255 | .9089 | .9922 |
| $\frac{59}{64}$ | .5768 | .6602 | .7435 | .8268 | .9102 | .9935 |
| $\frac{11}{16}$ | .5781 | .6615 | .7448 | .8281 | .9115 | .9948 |
| $\frac{61}{64}$ | .5794 | .6628 | .7461 | .8294 | .9128 | .9961 |
| $\frac{31}{32}$ | .5807 | .6641 | .7474 | .8307 | .9141 | .9974 |
| $\frac{63}{64}$ | .5820 | .6654 | .7487 | .8320 | .9154 | .9987 |
| 1 | | | | | | 1.0000 |






**DECIMALS OF AN INCH FOR EACH $\frac{1}{64}$ TH.
WITH MILLIMETRE EQUIVALENTS.**

| Frac- tion | $\frac{1}{64}$ ths | Decimal | Millime- tres | Frac- tion | $\frac{1}{64}$ ths | Decimal | Millime- tres |
|-----------------|--------------------|---------|------------------|-----------------|--------------------|---------|------------------|
| .. | 1 | .015625 | 0.397 | ... | 33 | .515625 | 13.097 |
| $\frac{1}{32}$ | 2 | .03125 | 0.794 | $\frac{17}{32}$ | 34 | .53125 | 13.494 |
| .. | 3 | .046875 | 1.191 | ... | 35 | .546875 | 13.891 |
| $\frac{1}{16}$ | 4 | .0625 | 1.588 | $\frac{9}{16}$ | 36 | .5625 | 14.288 |
| .. | 5 | .078125 | 1.984 | ... | 37 | .578125 | 14.684 |
| $\frac{3}{32}$ | 6 | .09375 | 2.381 | $\frac{19}{32}$ | 38 | .59375 | 15.081 |
| .. | 7 | .109375 | 2.778 | ... | 39 | .609375 | 15.478 |
| $\frac{1}{8}$ | 8 | .125 | 3.175 | $\frac{5}{8}$ | 40 | .625 | 15.875 |
| .. | 9 | .140625 | 3.572 | ... | 41 | .640625 | 16.272 |
| $\frac{5}{32}$ | 10 | .15625 | 3.969 | $\frac{21}{32}$ | 42 | .65625 | 16.669 |
| .. | 11 | .171875 | 4.366 | ... | 43 | .671875 | 17.066 |
| $\frac{3}{16}$ | 12 | .1875 | 4.763 | $\frac{11}{16}$ | 44 | .6875 | 17.463 |
| .. | 13 | .203125 | 5.159 | ... | 45 | .703125 | 17.859 |
| $\frac{7}{32}$ | 14 | .21875 | 5.556 | $\frac{23}{32}$ | 46 | .71875 | 18.256 |
| .. | 15 | .234375 | 5.953 | ... | 47 | .734375 | 18.653 |
| $\frac{1}{4}$ | 16 | .25 | 6.350 | $\frac{3}{4}$ | 48 | .75 | 19.050 |
| .. | 17 | .265625 | 6.747 | ... | 49 | .765625 | 19.447 |
| $\frac{9}{32}$ | 18 | .28125 | 7.144 | $\frac{25}{32}$ | 50 | .78125 | 19.844 |
| .. | 19 | .296875 | 7.541 | ... | 51 | .796875 | 20.241 |
| $\frac{5}{16}$ | 20 | .3125 | 7.938 | $\frac{13}{16}$ | 52 | .8125 | 20.638 |
| .. | 21 | .328125 | 8.334 | ... | 53 | .828125 | 21.034 |
| $\frac{11}{32}$ | 22 | .34375 | 8.731 | $\frac{27}{32}$ | 54 | .84375 | 21.431 |
| .. | 23 | .359375 | 9.128 | ... | 55 | .859375 | 21.828 |
| $\frac{3}{8}$ | 24 | .375 | 9.525 | $\frac{7}{8}$ | 56 | .875 | 22.225 |
| .. | 25 | .390625 | 9.922 | ... | 57 | .890625 | 22.622 |
| $\frac{13}{32}$ | 26 | .40625 | 10.319 | $\frac{29}{32}$ | 58 | .90625 | 23.019 |
| .. | 27 | .421875 | 10.716 | ... | 59 | .921875 | 23.416 |
| $\frac{7}{16}$ | 28 | .4375 | 11.113 | $\frac{15}{16}$ | 60 | .9375 | 23.813 |
| .. | 29 | .453125 | 11.509 | ... | 61 | .953125 | 24.209 |
| $\frac{15}{32}$ | 30 | .46875 | 11.906 | $\frac{31}{32}$ | 62 | .96875 | 24.606 |
| .. | 31 | .484375 | 12.303 | ... | 63 | .984375 | 25.003 |
| $\frac{1}{2}$ | 32 | .5 | 12.700 | 1 | 64 | 1. | 25.400 |

WEIGHTS AND AREAS OF SQUARE AND ROUND BARS AND CIRCUMFERENCES OF ROUND BARS.






One cubic foot of steel weighs 489.6 lbs.

The following tables of weights of rounds, squares, flats, etc., are theoretical only. The various sizes made by us are listed elsewhere herein under appropriate headings, and the weights of rolled steel are subject to variation in accordance with mill practice for the different classes of products.

| Thickness or Diameter in Inches. | Weight of  Bar One Foot Long. | Weight of  Bar One Foot Long. | Area of  Bar in Sq. Inches. | Area of  Bar in Sq. Inches. | Circumference of  Bar in Inches. |
|--|--|--|--|--|---|
| $\frac{1}{16}$ | .013 | .010 | .0039 | .0031 | .1964 |
| $\frac{5}{64}$ | .021 | .016 | .0061 | .0048 | .2454 |
| $\frac{3}{32}$ | .030 | .023 | .0088 | .0069 | .2945 |
| $\frac{7}{64}$ | .041 | .032 | .0120 | .0094 | .3436 |
| $\frac{1}{8}$ | .053 | .042 | .0156 | .0123 | .3927 |
| $\frac{9}{64}$ | .067 | .053 | .0198 | .0155 | .4418 |
| $\frac{5}{32}$ | .083 | .065 | .0244 | .0192 | .4909 |
| $\frac{11}{64}$ | .100 | .079 | .0295 | .0232 | .5400 |
| $\frac{3}{16}$ | .120 | .094 | .0352 | .0276 | .5891 |
| $\frac{13}{64}$ | .140 | .110 | .0413 | .0324 | .6381 |
| $\frac{7}{32}$ | .163 | .128 | .0479 | .0376 | .6872 |
| $\frac{15}{64}$ | .187 | .147 | .0549 | .0431 | .7363 |
| $\frac{1}{4}$ | .212 | .167 | .0625 | .0491 | .7854 |
| $\frac{17}{64}$ | .240 | .188 | .0706 | .0554 | .8345 |
| $\frac{9}{32}$ | .269 | .211 | .0791 | .0621 | .8836 |
| $\frac{19}{64}$ | .300 | .235 | .0881 | .0692 | .9327 |
| $\frac{5}{16}$ | .332 | .261 | .0977 | .0767 | .9818 |
| $\frac{21}{64}$ | .366 | .288 | .1077 | .0846 | 1.0308 |
| $\frac{11}{32}$ | .402 | .316 | .1182 | .0928 | 1.0799 |
| $\frac{23}{64}$ | .439 | .345 | .1292 | .1014 | 1.1290 |
| $\frac{3}{8}$ | .478 | .376 | .1406 | .1104 | 1.1781 |
| $\frac{25}{64}$ | .519 | .407 | .1526 | .1198 | 1.2272 |
| $\frac{13}{32}$ | .561 | .441 | .1650 | .1296 | 1.2763 |
| $\frac{27}{64}$ | .605 | .475 | .1780 | .1398 | 1.3254 |
| $\frac{7}{16}$ | .651 | .511 | .1914 | .1503 | 1.3745 |
| $\frac{29}{64}$ | .698 | .548 | .2053 | .1613 | 1.4235 |
| $\frac{15}{32}$ | .747 | .587 | .2197 | .1726 | 1.4726 |
| $\frac{31}{64}$ | .798 | .627 | .2346 | .1843 | 1.5217 |
| $\frac{1}{2}$ | .850 | .668 | .2500 | .1963 | 1.5708 |
| $\frac{33}{64}$ | .904 | .710 | .2659 | .2088 | 1.6199 |
| $\frac{17}{32}$ | .960 | .754 | .2822 | .2217 | 1.6690 |
| $\frac{35}{64}$ | 1.017 | .799 | .2991 | .2349 | 1.7181 |






SQUARE AND ROUND BARS.

(CONTINUED.)

| Thickness or Diameter in Inches. | Weight of  Bar One Foot Long. | Weight of  Bar One Foot Long. | Area of  Bar in Sq. Inches. | Area of  Bar in Sq. Inches. | Circumference of  Bar in Inches. |
|--|--|--|--|--|---|
| $\frac{9}{16}$ | 1.076 | .845 | .3164 | .2485 | 1.7672 |
| $\frac{1}{2}$ | 1.136 | .893 | .3342 | .2625 | 1.8162 |
| $\frac{5}{8}$ | 1.199 | .941 | .3525 | .2769 | 1.8653 |
| $\frac{3}{4}$ | 1.263 | .992 | .3713 | .2916 | 1.9144 |
| $\frac{7}{8}$ | 1.328 | 1.043 | .3906 | .3068 | 1.9635 |
| $\frac{1}{2}$ | 1.395 | 1.096 | .4104 | .3223 | 2.0126 |
| $\frac{1}{2}$ | 1.464 | 1.150 | .4307 | .3382 | 2.0617 |
| $\frac{1}{2}$ | 1.535 | 1.205 | .4514 | .3545 | 2.1108 |
| $\frac{1}{2}$ | 1.607 | 1.262 | .4727 | .3712 | 2.1599 |
| $\frac{1}{2}$ | 1.681 | 1.320 | .4944 | .3883 | 2.2089 |
| $\frac{1}{2}$ | 1.756 | 1.380 | .5166 | .4057 | 2.2580 |
| $\frac{1}{2}$ | 1.834 | 1.440 | .5393 | .4236 | 2.3071 |
| $\frac{3}{4}$ | 1.913 | 1.502 | .5625 | .4418 | 2.3562 |
| $\frac{1}{2}$ | 2.245 | 1.763 | .6602 | .5185 | 2.5526 |
| $\frac{1}{2}$ | 2.603 | 2.044 | .7656 | .6013 | 2.7489 |
| $\frac{1}{2}$ | 2.988 | 2.347 | .8789 | .6903 | 2.9453 |
| 1 | 3.400 | 2.670 | 1.0000 | .7854 | 3.1416 |
| $\frac{1}{2}$ | 3.838 | 3.015 | 1.1289 | .8866 | 3.3380 |
| $\frac{1}{2}$ | 4.303 | 3.380 | 1.2656 | .9940 | 3.5343 |
| $\frac{1}{2}$ | 4.795 | 3.766 | 1.4102 | 1.1075 | 3.7306 |
| $\frac{1}{2}$ | 5.313 | 4.172 | 1.5625 | 1.2272 | 3.9270 |
| $\frac{1}{2}$ | 5.857 | 4.600 | 1.7227 | 1.3530 | 4.1234 |
| $\frac{1}{2}$ | 6.428 | 5.049 | 1.8906 | 1.4849 | 4.3197 |
| $\frac{1}{2}$ | 7.026 | 5.518 | 2.0664 | 1.6230 | 4.5161 |
| $\frac{1}{2}$ | 7.650 | 6.008 | 2.2500 | 1.7671 | 4.7124 |
| $\frac{1}{2}$ | 8.301 | 6.519 | 2.4414 | 1.9175 | 4.9088 |
| $\frac{1}{2}$ | 8.978 | 7.051 | 2.6406 | 2.0739 | 5.1051 |
| $\frac{1}{2}$ | 9.682 | 7.604 | 2.8477 | 2.2365 | 5.3015 |
| $\frac{3}{4}$ | 10.41 | 8.178 | 3.0625 | 2.4053 | 5.4978 |
| $\frac{1}{2}$ | 11.17 | 8.773 | 3.2852 | 2.5802 | 5.6942 |
| $\frac{1}{2}$ | 11.95 | 9.388 | 3.5156 | 2.7612 | 5.8905 |
| $\frac{1}{2}$ | 12.76 | 10.02 | 3.7539 | 2.9483 | 6.0869 |






SQUARE AND ROUND BARS.

(CONTINUED.)

| Thickness or Diameter in Inches. | Weight of  Bar One Foot Long. | Weight of  Bar One Foot Long. | Area of  Bar in Sq. Inches. | Area of  Bar in Sq. Inches. | Circumference of  Bar in Inches. |
|--|--|--|--|--|---|
| 2 | 13.60 | 10.68 | 4.0000 | 3.1416 | 6.2832 |
| $1\frac{1}{16}$ | 14.46 | 11.36 | 4.2539 | 3.3410 | 6.4796 |
| $1\frac{1}{8}$ | 15.35 | 12.06 | 4.5156 | 3.5466 | 6.6759 |
| $1\frac{3}{16}$ | 16.27 | 12.78 | 4.7852 | 3.7583 | 6.8723 |
| $1\frac{1}{2}$ | 17.21 | 13.52 | 5.0625 | 3.9761 | 7.0686 |
| $1\frac{5}{16}$ | 18.18 | 14.28 | 5.3477 | 4.2000 | 7.2650 |
| $1\frac{3}{8}$ | 19.18 | 15.06 | 5.6406 | 4.4301 | 7.4613 |
| $1\frac{7}{16}$ | 20.20 | 15.87 | 5.9414 | 4.6664 | 7.6577 |
| $1\frac{1}{2}$ | 21.25 | 16.69 | 6.2500 | 4.9087 | 7.8540 |
| $1\frac{9}{16}$ | 22.33 | 17.53 | 6.5664 | 5.1573 | 8.0504 |
| $1\frac{5}{8}$ | 23.43 | 18.40 | 6.8906 | 5.4119 | 8.2467 |
| $1\frac{11}{16}$ | 24.56 | 19.29 | 7.2227 | 5.6727 | 8.4431 |
| $1\frac{3}{4}$ | 25.71 | 20.19 | 7.5625 | 5.9396 | 8.6394 |
| $1\frac{13}{16}$ | 26.90 | 21.12 | 7.9102 | 6.2126 | 8.8358 |
| $1\frac{7}{8}$ | 28.10 | 22.07 | 8.2656 | 6.4918 | 9.0321 |
| $1\frac{15}{16}$ | 29.34 | 23.04 | 8.6289 | 6.7771 | 9.2285 |
| 3 | 30.60 | 24.03 | 9.0000 | 7.0686 | 9.4248 |
| $1\frac{1}{16}$ | 31.89 | 25.05 | 9.3789 | 7.3662 | 9.6212 |
| $1\frac{1}{8}$ | 33.20 | 26.08 | 9.7656 | 7.6699 | 9.8175 |
| $1\frac{3}{16}$ | 34.55 | 27.13 | 10.160 | 7.9798 | 10.014 |
| $1\frac{1}{2}$ | 35.92 | 28.21 | 10.563 | 8.2958 | 10.210 |
| $1\frac{5}{16}$ | 37.31 | 29.30 | 10.973 | 8.6179 | 10.407 |
| $1\frac{3}{8}$ | 38.73 | 30.42 | 11.391 | 8.9462 | 10.603 |
| $1\frac{7}{16}$ | 40.18 | 31.55 | 11.816 | 9.2806 | 10.799 |
| $1\frac{1}{2}$ | 41.65 | 32.71 | 12.250 | 9.6211 | 10.996 |
| $1\frac{9}{16}$ | 43.15 | 33.89 | 12.691 | 9.9678 | 11.192 |
| $1\frac{5}{8}$ | 44.68 | 35.09 | 13.141 | 10.321 | 11.388 |
| $1\frac{11}{16}$ | 46.23 | 36.31 | 13.598 | 10.680 | 11.585 |
| $1\frac{3}{4}$ | 47.82 | 37.55 | 14.063 | 11.045 | 11.781 |
| $1\frac{13}{16}$ | 49.42 | 38.81 | 14.535 | 11.416 | 11.977 |
| $1\frac{7}{8}$ | 51.05 | 40.10 | 15.016 | 11.793 | 12.174 |
| $1\frac{15}{16}$ | 52.71 | 41.40 | 15.504 | 12.177 | 12.370 |






SQUARE AND ROUND BARS.

(CONTINUED.)

| Thickness or Diameter in Inches. | Weight of  Bar One Foot Long. | Weight of  Bar One Foot Long. | Area of  Bar in Sq. Inches. | Area of  Bar in Sq. Inches. | Circumference of  Bar in Inches. |
|--|--|--|--|--|---|
| 4 | 54.40 | 42.73 | 16.000 | 12.566 | 12.566 |
| $4\frac{1}{16}$ | 56.11 | 44.07 | 16.504 | 12.962 | 12.763 |
| $4\frac{1}{8}$ | 57.85 | 45.44 | 17.016 | 13.364 | 12.959 |
| $4\frac{3}{16}$ | 59.62 | 46.83 | 17.535 | 13.772 | 13.155 |
| $4\frac{1}{2}$ | 61.41 | 48.24 | 18.063 | 14.186 | 13.352 |
| $4\frac{5}{16}$ | 63.23 | 49.66 | 18.598 | 14.607 | 13.548 |
| $4\frac{3}{8}$ | 65.08 | 51.11 | 19.141 | 15.033 | 13.745 |
| $4\frac{7}{16}$ | 66.95 | 52.58 | 19.691 | 15.466 | 13.941 |
| $4\frac{1}{2}$ | 68.85 | 54.07 | 20.250 | 15.904 | 14.137 |
| $4\frac{9}{16}$ | 70.78 | 55.59 | 20.816 | 16.349 | 14.334 |
| $4\frac{5}{8}$ | 72.73 | 57.12 | 21.391 | 16.800 | 14.530 |
| $4\frac{11}{16}$ | 74.71 | 58.67 | 21.973 | 17.257 | 14.726 |
| $4\frac{3}{4}$ | 76.71 | 60.25 | 22.563 | 17.721 | 14.923 |
| $4\frac{13}{16}$ | 78.74 | 61.85 | 23.160 | 18.190 | 15.119 |
| $4\frac{7}{8}$ | 80.80 | 63.46 | 23.766 | 18.665 | 15.315 |
| $4\frac{15}{16}$ | 82.89 | 65.10 | 24.379 | 19.147 | 15.512 |
| 5 | 85.00 | 66.76 | 25.000 | 19.635 | 15.708 |
| $5\frac{1}{16}$ | 87.14 | 68.44 | 25.629 | 20.129 | 15.904 |
| $5\frac{1}{8}$ | 89.30 | 70.14 | 26.266 | 20.629 | 16.101 |
| $5\frac{3}{16}$ | 91.49 | 71.86 | 26.910 | 21.135 | 16.297 |
| $5\frac{1}{2}$ | 93.71 | 73.60 | 27.563 | 21.648 | 16.493 |
| $5\frac{5}{16}$ | 95.96 | 75.37 | 28.223 | 22.166 | 16.690 |
| $5\frac{3}{8}$ | 98.23 | 77.15 | 28.891 | 22.691 | 16.886 |
| $5\frac{7}{16}$ | 100.5 | 78.95 | 29.566 | 23.221 | 17.082 |
| $5\frac{1}{2}$ | 102.9 | 80.78 | 30.250 | 23.758 | 17.279 |
| $5\frac{9}{16}$ | 105.2 | 82.62 | 30.941 | 24.301 | 17.475 |
| $5\frac{5}{8}$ | 107.6 | 84.49 | 31.641 | 24.851 | 17.672 |
| $5\frac{11}{16}$ | 110.0 | 86.38 | 32.348 | 25.406 | 17.868 |
| $5\frac{3}{4}$ | 112.4 | 88.29 | 33.063 | 25.967 | 18.064 |
| $5\frac{13}{16}$ | 114.9 | 90.22 | 33.785 | 26.535 | 18.261 |
| $5\frac{7}{8}$ | 117.4 | 92.17 | 34.516 | 27.109 | 18.457 |
| $5\frac{15}{16}$ | 119.9 | 94.14 | 35.254 | 27.688 | 18.653 |






SQUARE AND ROUND BARS.

(CONTINUED.)

| Thickness or Diameter in Inches. | Weight of  Bar One Foot Long. | Weight of  Bar One Foot Long. | Area of  Bar in Sq. Inches. | Area of  Bar in Sq. Inches. | Circumference of  Bar in Inches. |
|--|--|--|--|--|---|
| 6 | 122.4 | 96.13 | 36.000 | 28.274 | 18.850 |
| $\frac{1}{16}$ | 125.0 | 98.15 | 36.754 | 28.867 | 19.046 |
| $\frac{1}{8}$ | 127.6 | 100.2 | 37.516 | 29.465 | 19.242 |
| $\frac{3}{16}$ | 130.2 | 102.2 | 38.285 | 30.069 | 19.439 |
| $\frac{1}{4}$ | 132.8 | 104.3 | 39.063 | 30.680 | 19.635 |
| $\frac{5}{16}$ | 135.5 | 106.4 | 39.848 | 31.296 | 19.831 |
| $\frac{3}{8}$ | 138.2 | 108.5 | 40.641 | 31.919 | 20.028 |
| $\frac{7}{16}$ | 140.9 | 110.7 | 41.441 | 32.548 | 20.224 |
| $\frac{1}{2}$ | 143.7 | 112.8 | 42.250 | 33.183 | 20.420 |
| $\frac{9}{16}$ | 146.5 | 115.0 | 43.066 | 33.824 | 20.617 |
| $\frac{5}{8}$ | 149.2 | 117.2 | 43.891 | 34.472 | 20.813 |
| $\frac{11}{16}$ | 152.1 | 119.4 | 44.723 | 35.125 | 21.009 |
| $\frac{3}{4}$ | 154.9 | 121.7 | 45.563 | 35.785 | 21.206 |
| $\frac{13}{16}$ | 157.8 | 123.9 | 46.410 | 36.451 | 21.402 |
| $\frac{7}{8}$ | 160.7 | 126.2 | 47.266 | 37.122 | 21.599 |
| $\frac{15}{16}$ | 163.6 | 128.5 | 48.129 | 37.800 | 21.795 |
| 7 | 166.6 | 130.8 | 49.000 | 38.485 | 21.991 |
| $\frac{1}{16}$ | 169.6 | 133.2 | 49.879 | 39.175 | 22.188 |
| $\frac{1}{8}$ | 172.6 | 135.6 | 50.766 | 39.871 | 22.384 |
| $\frac{3}{8}$ | 175.6 | 138.0 | 51.660 | 40.574 | 22.580 |
| $\frac{1}{4}$ | 178.7 | 140.4 | 52.563 | 41.283 | 22.777 |
| $\frac{5}{16}$ | 181.8 | 142.8 | 53.473 | 41.997 | 22.973 |
| $\frac{3}{8}$ | 184.9 | 145.2 | 54.391 | 42.718 | 23.169 |
| $\frac{7}{16}$ | 188.1 | 147.7 | 55.316 | 43.446 | 23.366 |
| $\frac{1}{2}$ | 191.3 | 150.2 | 56.250 | 44.179 | 23.562 |
| $\frac{9}{16}$ | 194.5 | 152.7 | 57.191 | 44.918 | 23.758 |
| $\frac{5}{8}$ | 197.7 | 155.3 | 58.141 | 45.664 | 23.955 |
| $\frac{11}{16}$ | 200.9 | 157.8 | 59.098 | 46.415 | 24.151 |
| $\frac{3}{4}$ | 204.2 | 160.4 | 60.063 | 47.173 | 24.347 |
| $\frac{13}{16}$ | 207.5 | 163.0 | 61.035 | 47.937 | 24.544 |
| $\frac{7}{8}$ | 210.9 | 165.6 | 62.016 | 48.707 | 24.740 |
| $\frac{15}{16}$ | 214.2 | 168.2 | 63.004 | 49.483 | 24.936 |






SQUARE AND ROUND BARS.

(CONTINUED.)

| Thickness or Diameter in Inches. | Weight of  Bar One Foot Long. | Weight of  Bar One Foot Long. | Area of  Bar in Sq. Inches. | Area of  Bar in Sq. Inches. | Circumference of  Bar in Inches. |
|--|--|--|--|--|---|
| 8 | 217.6 | 170.9 | 64.000 | 50.266 | 25.133 |
| $\frac{1}{16}$ | 221.0 | 173.6 | 65.004 | 51.054 | 25.329 |
| $\frac{1}{8}$ | 224.5 | 176.3 | 66.016 | 51.849 | 25.526 |
| $\frac{3}{16}$ | 227.9 | 179.0 | 67.035 | 52.649 | 25.722 |
| $\frac{1}{4}$ | 231.4 | 181.8 | 68.063 | 53.456 | 25.918 |
| $\frac{5}{16}$ | 234.9 | 184.5 | 69.098 | 54.269 | 26.115 |
| $\frac{3}{8}$ | 238.5 | 187.3 | 70.141 | 55.088 | 26.311 |
| $\frac{7}{16}$ | 242.1 | 190.1 | 71.191 | 55.914 | 26.507 |
| $\frac{1}{2}$ | 245.7 | 192.9 | 72.250 | 56.745 | 26.704 |
| $\frac{9}{16}$ | 249.3 | 195.8 | 73.316 | 57.583 | 26.900 |
| $\frac{5}{8}$ | 252.9 | 198.6 | 74.391 | 58.426 | 27.096 |
| $\frac{11}{16}$ | 256.6 | 201.5 | 75.473 | 59.276 | 27.293 |
| $\frac{3}{4}$ | 260.3 | 204.4 | 76.563 | 60.132 | 27.489 |
| $\frac{13}{16}$ | 264.0 | 207.4 | 77.660 | 60.994 | 27.685 |
| $\frac{7}{8}$ | 267.8 | 210.3 | 78.766 | 61.863 | 27.882 |
| $\frac{15}{16}$ | 271.6 | 213.3 | 79.879 | 62.737 | 28.078 |
| 9 | 275.4 | 216.3 | 81.000 | 63.617 | 28.274 |
| $\frac{1}{16}$ | 279.2 | 219.3 | 82.129 | 64.504 | 28.471 |
| $\frac{1}{8}$ | 283.1 | 222.3 | 83.266 | 65.397 | 28.667 |
| $\frac{3}{16}$ | 287.0 | 225.4 | 84.410 | 66.296 | 28.863 |
| $\frac{1}{4}$ | 290.9 | 228.5 | 85.563 | 67.201 | 29.060 |
| $\frac{5}{16}$ | 294.9 | 231.6 | 86.723 | 68.112 | 29.256 |
| $\frac{3}{8}$ | 298.8 | 234.7 | 87.891 | 69.029 | 29.453 |
| $\frac{7}{16}$ | 302.8 | 237.8 | 89.066 | 69.953 | 29.649 |
| $\frac{1}{2}$ | 306.9 | 241.0 | 90.250 | 70.882 | 29.845 |
| $\frac{9}{16}$ | 310.9 | 244.2 | 91.441 | 71.818 | 30.042 |
| $\frac{5}{8}$ | 315.0 | 247.4 | 92.641 | 72.760 | 30.238 |
| $\frac{11}{16}$ | 319.1 | 250.6 | 93.848 | 73.708 | 30.434 |
| $\frac{3}{4}$ | 323.2 | 253.8 | 95.063 | 74.662 | 30.631 |
| $\frac{13}{16}$ | 327.4 | 257.1 | 96.285 | 75.622 | 30.827 |
| $\frac{7}{8}$ | 331.6 | 260.4 | 97.516 | 76.589 | 31.023 |
| $\frac{15}{16}$ | 335.8 | 263.7 | 98.754 | 77.561 | 31.220 |

SQUARE AND ROUND BARS.

(CONCLUDED.)

| Thickness or Diameter in Inches. | Weight of  Bar One Foot Long. | Weight of  Bar One Foot Long. | Area of  Bar in Sq. Inches. | Area of  Bar in Sq. Inches. | Circumference of  Bar in Inches. |
|--|--|--|--|--|---|
| 10 | 340.0 | 267.0 | 100.00 | 78.540 | 31.416 |
| $\frac{1}{16}$ | 344.3 | 270.4 | 101.25 | 79.525 | 31.612 |
| $\frac{1}{8}$ | 348.6 | 273.8 | 102.52 | 80.516 | 31.809 |
| $\frac{3}{16}$ | 352.9 | 277.1 | 103.79 | 81.513 | 32.005 |
| $\frac{1}{4}$ | 357.2 | 280.6 | 105.06 | 82.516 | 32.201 |
| $\frac{5}{16}$ | 361.6 | 284.0 | 106.35 | 83.525 | 32.398 |
| $\frac{3}{8}$ | 366.0 | 287.4 | 107.64 | 84.541 | 32.594 |
| $\frac{7}{16}$ | 370.4 | 290.9 | 108.94 | 85.563 | 32.790 |
| $\frac{1}{2}$ | 374.9 | 294.4 | 110.25 | 86.590 | 32.987 |
| $\frac{9}{16}$ | 379.3 | 297.9 | 111.57 | 87.624 | 33.183 |
| $\frac{5}{8}$ | 383.8 | 301.5 | 112.89 | 88.664 | 33.380 |
| $\frac{11}{16}$ | 388.4 | 305.0 | 114.22 | 89.710 | 33.576 |
| $\frac{3}{4}$ | 392.9 | 308.6 | 115.56 | 90.763 | 33.772 |
| $\frac{13}{16}$ | 397.5 | 312.2 | 116.91 | 91.821 | 33.969 |
| $\frac{7}{8}$ | 402.1 | 315.8 | 118.27 | 92.886 | 34.165 |
| $\frac{15}{16}$ | 406.7 | 319.5 | 119.63 | 93.957 | 34.361 |
| 11 | 411.4 | 323.1 | 121.00 | 95.033 | 34.558 |
| $\frac{1}{16}$ | 416.1 | 326.8 | 122.38 | 96.116 | 34.754 |
| $\frac{1}{8}$ | 420.8 | 330.5 | 123.77 | 97.206 | 34.950 |
| $\frac{3}{16}$ | 425.5 | 334.3 | 125.16 | 98.301 | 35.147 |
| $\frac{1}{4}$ | 430.3 | 338.0 | 126.56 | 99.402 | 35.343 |
| $\frac{5}{16}$ | 435.1 | 341.7 | 127.97 | 100.51 | 35.539 |
| $\frac{3}{8}$ | 439.9 | 345.5 | 129.39 | 101.62 | 35.736 |
| $\frac{7}{16}$ | 444.8 | 349.3 | 130.82 | 102.74 | 35.932 |
| $\frac{1}{2}$ | 449.7 | 353.2 | 132.25 | 103.87 | 36.128 |
| $\frac{9}{16}$ | 454.6 | 357.0 | 133.69 | 105.00 | 36.325 |
| $\frac{5}{8}$ | 459.5 | 360.9 | 135.14 | 106.14 | 36.521 |
| $\frac{11}{16}$ | 464.4 | 364.8 | 136.60 | 107.28 | 36.717 |
| $\frac{3}{4}$ | 469.4 | 368.7 | 138.06 | 108.43 | 36.914 |
| $\frac{13}{16}$ | 474.4 | 372.6 | 139.54 | 109.59 | 37.110 |
| $\frac{7}{8}$ | 479.5 | 376.6 | 141.02 | 110.75 | 37.307 |
| $\frac{15}{16}$ | 484.5 | 380.5 | 142.50 | 111.92 | 37.503 |

WEIGHTS OF SQUARE AND ROUND BARS PER RUNNING INCH.

One cubic inch of steel weighs 0.2833 lb.

| Thickness or Diameter in Inches. | Weight of □ Bar One Inch Long. | Weight of ○ Bar One Inch Long. | Thickness or Diameter in Inches. | Weight of □ Bar One Inch Long. | Weight of ○ Bar One Inch Long. |
|--|--------------------------------------|--------------------------------------|--|--------------------------------------|--------------------------------------|
| $\frac{1}{16}$ | | | 2 | 1.13 | .89 |
| $\frac{1}{8}$ | | | $\frac{1}{16}$ | 1.21 | .95 |
| $\frac{3}{16}$ | .01 | | $\frac{1}{8}$ | 1.28 | 1.01 |
| | | | $\frac{3}{16}$ | 1.36 | 1.07 |
| $\frac{1}{4}$ | .02 | .01 | $\frac{1}{4}$ | 1.43 | 1.13 |
| $\frac{5}{16}$ | .03 | .02 | $\frac{1}{2}$ | 1.52 | 1.19 |
| $\frac{3}{8}$ | .04 | .03 | $\frac{3}{16}$ | 1.60 | 1.26 |
| $\frac{7}{16}$ | .05 | .04 | $\frac{7}{16}$ | 1.68 | 1.32 |
| $\frac{1}{2}$ | .07 | .06 | $\frac{1}{2}$ | 1.77 | 1.39 |
| $\frac{9}{16}$ | .09 | .07 | $\frac{9}{16}$ | 1.86 | 1.46 |
| $\frac{5}{8}$ | .11 | .09 | $\frac{5}{8}$ | 1.95 | 1.54 |
| $\frac{11}{16}$ | .13 | .11 | $\frac{11}{16}$ | 2.05 | 1.61 |
| $\frac{3}{4}$ | .16 | .13 | $\frac{3}{4}$ | 2.14 | 1.69 |
| $\frac{13}{16}$ | .19 | .15 | $\frac{13}{16}$ | 2.24 | 1.76 |
| $\frac{7}{8}$ | .22 | .17 | $\frac{7}{8}$ | 2.34 | 1.84 |
| $\frac{15}{16}$ | .25 | .20 | $\frac{15}{16}$ | 2.44 | 1.92 |
| 1 | .28 | .22 | 3 | 2.55 | 2.01 |
| $\frac{1}{16}$ | .32 | .25 | $\frac{1}{16}$ | 2.66 | 2.09 |
| $\frac{1}{8}$ | .36 | .28 | $\frac{1}{8}$ | 2.77 | 2.18 |
| $\frac{3}{16}$ | .40 | .31 | $\frac{3}{16}$ | 2.88 | 2.26 |
| $\frac{1}{4}$ | .44 | .35 | $\frac{1}{4}$ | 2.99 | 2.35 |
| $\frac{5}{16}$ | .49 | .38 | $\frac{5}{16}$ | 3.11 | 2.44 |
| $\frac{3}{8}$ | .54 | .42 | $\frac{3}{8}$ | 3.23 | 2.53 |
| $\frac{7}{16}$ | .58 | .46 | $\frac{7}{16}$ | 3.35 | 2.63 |
| $\frac{1}{2}$ | .64 | .50 | $\frac{1}{2}$ | 3.47 | 2.73 |
| $\frac{9}{16}$ | .69 | .54 | $\frac{9}{16}$ | 3.60 | 2.82 |
| $\frac{5}{8}$ | .75 | .59 | $\frac{5}{8}$ | 3.72 | 2.92 |
| $\frac{11}{16}$ | .81 | .63 | $\frac{11}{16}$ | 3.85 | 3.03 |
| $\frac{3}{4}$ | .87 | .68 | $\frac{3}{4}$ | 3.98 | 3.13 |
| $\frac{13}{16}$ | .94 | .73 | $\frac{13}{16}$ | 4.12 | 3.23 |
| $\frac{7}{8}$ | 1.00 | .78 | $\frac{7}{8}$ | 4.25 | 3.34 |
| $\frac{15}{16}$ | 1.06 | .84 | $\frac{15}{16}$ | 4.39 | 3.45 |

SQUARE AND ROUND BARS.

(CONTINUED.)

| Thickness or Diameter in Inches. | Weight of □ Bar One Inch Long. | Weight of ○ Bar One Inch Long. | Thickness or Diameter in Inches. | Weight of □ Bar One Inch Long. | Weight of ○ Bar One Inch Long. |
|--|--------------------------------------|--------------------------------------|--|--------------------------------------|--------------------------------------|
| 4 | 4.53 | 3.57 | 6 | 10.20 | 8.01 |
| $\frac{1}{16}$ | 4.68 | 3.67 | $\frac{1}{16}$ | 10.41 | 8.18 |
| $\frac{1}{8}$ | 4.82 | 3.79 | $\frac{3}{16}$ | 10.63 | 8.35 |
| $\frac{3}{16}$ | 4.97 | 3.90 | $\frac{1}{2}$ | 10.85 | 8.52 |
| $\frac{1}{4}$ | 5.12 | 4.02 | $\frac{5}{16}$ | 11.07 | 8.69 |
| $\frac{5}{16}$ | 5.27 | 4.14 | $\frac{3}{8}$ | 11.29 | 8.87 |
| $\frac{3}{8}$ | 5.42 | 4.26 | $\frac{7}{16}$ | 11.51 | 9.04 |
| $\frac{7}{16}$ | 5.58 | 4.38 | $\frac{1}{2}$ | 11.74 | 9.22 |
| $\frac{1}{2}$ | 5.74 | 4.51 | $\frac{9}{16}$ | 11.97 | 9.40 |
| $\frac{9}{16}$ | 5.90 | 4.63 | $\frac{5}{8}$ | 12.20 | 9.58 |
| $\frac{5}{8}$ | 6.06 | 4.76 | $\frac{3}{4}$ | 12.43 | 9.77 |
| $\frac{11}{16}$ | 6.23 | 4.89 | $\frac{13}{16}$ | 12.67 | 9.95 |
| $\frac{3}{4}$ | 6.39 | 5.02 | $\frac{7}{8}$ | 12.91 | 10.14 |
| $\frac{13}{16}$ | 6.56 | 5.15 | $\frac{15}{16}$ | 13.15 | 10.33 |
| $\frac{7}{8}$ | 6.73 | 5.29 | $\frac{1}{2}$ | 13.39 | 10.52 |
| $\frac{15}{16}$ | 6.91 | 5.42 | $\frac{1}{2}$ | 13.64 | 10.71 |
| 5 | 7.08 | 5.56 | 7 | 13.88 | 10.90 |
| $\frac{1}{16}$ | 7.26 | 5.70 | $\frac{1}{16}$ | 14.13 | 11.10 |
| $\frac{1}{8}$ | 7.44 | 5.84 | $\frac{1}{8}$ | 14.38 | 11.30 |
| $\frac{3}{16}$ | 7.62 | 5.99 | $\frac{3}{16}$ | 14.64 | 11.50 |
| $\frac{1}{4}$ | 7.81 | 6.13 | $\frac{1}{4}$ | 14.89 | 11.70 |
| $\frac{5}{16}$ | 8.00 | 6.28 | $\frac{5}{16}$ | 15.15 | 11.90 |
| $\frac{3}{8}$ | 8.19 | 6.43 | $\frac{3}{8}$ | 15.41 | 12.10 |
| $\frac{7}{16}$ | 8.38 | 6.58 | $\frac{7}{16}$ | 15.67 | 12.31 |
| $\frac{1}{2}$ | 8.57 | 6.73 | $\frac{1}{2}$ | 15.94 | 12.52 |
| $\frac{9}{16}$ | 8.77 | 6.88 | $\frac{9}{16}$ | 16.20 | 12.73 |
| $\frac{5}{8}$ | 8.96 | 7.04 | $\frac{5}{8}$ | 16.47 | 12.94 |
| $\frac{11}{16}$ | 9.16 | 7.20 | $\frac{11}{16}$ | 16.74 | 13.15 |
| $\frac{3}{4}$ | 9.37 | 7.36 | $\frac{3}{4}$ | 17.02 | 13.36 |
| $\frac{13}{16}$ | 9.57 | 7.52 | $\frac{13}{16}$ | 17.29 | 13.58 |
| $\frac{7}{8}$ | 9.78 | 7.68 | $\frac{7}{8}$ | 17.57 | 13.80 |
| $\frac{15}{16}$ | 9.99 | 7.84 | $\frac{15}{16}$ | 17.85 | 14.02 |

SQUARE AND ROUND BARS.

(CONTINUED.)

| Thickness or Diameter in Inches. | Weight of □ Bar One Inch Long. | Weight of ○ Bar One Inch Long. | Thickness or Diameter in Inches. | Weight of □ Bar One Inch Long. | Weight of ○ Bar One Inch Long. |
|--|--------------------------------------|--------------------------------------|--|--------------------------------------|--------------------------------------|
| 8 | 18.11 | 14.24 | 10 | 28.33 | 22.25 |
| $\frac{1}{16}$ | 18.42 | 14.46 | $\frac{1}{16}$ | 28.69 | 22.53 |
| $\frac{1}{8}$ | 18.70 | 14.69 | $\frac{1}{8}$ | 29.04 | 22.81 |
| $\frac{3}{16}$ | 18.99 | 14.92 | $\frac{3}{16}$ | 29.41 | 23.09 |
| $\frac{1}{4}$ | 19.28 | 15.14 | $\frac{1}{4}$ | 29.77 | 23.38 |
| $\frac{5}{16}$ | 19.58 | 15.38 | $\frac{5}{16}$ | 30.13 | 23.66 |
| $\frac{3}{8}$ | 19.87 | 15.61 | $\frac{3}{8}$ | 30.50 | 23.95 |
| $\frac{7}{16}$ | 20.17 | 15.84 | $\frac{7}{16}$ | 30.87 | 24.24 |
| $\frac{1}{2}$ | 20.47 | 16.08 | $\frac{1}{2}$ | 31.24 | 24.53 |
| $\frac{9}{16}$ | 20.77 | 16.31 | $\frac{9}{16}$ | 31.61 | 24.82 |
| $\frac{5}{8}$ | 21.08 | 16.55 | $\frac{5}{8}$ | 31.98 | 25.12 |
| $\frac{11}{16}$ | 21.38 | 16.79 | $\frac{11}{16}$ | 32.36 | 25.42 |
| $\frac{3}{4}$ | 21.69 | 17.04 | $\frac{3}{4}$ | 32.74 | 25.71 |
| $\frac{13}{16}$ | 22.00 | 17.28 | $\frac{13}{16}$ | 33.12 | 26.01 |
| $\frac{7}{8}$ | 22.31 | 17.53 | $\frac{7}{8}$ | 33.51 | 26.32 |
| $\frac{15}{16}$ | 22.63 | 17.77 | $\frac{15}{16}$ | 33.89 | 26.62 |
| 9 | 22.95 | 18.02 | 11 | 34.28 | 26.92 |
| $\frac{1}{16}$ | 23.27 | 18.27 | $\frac{1}{16}$ | 34.67 | 27.23 |
| $\frac{1}{8}$ | 23.59 | 18.53 | $\frac{1}{8}$ | 35.06 | 27.54 |
| $\frac{3}{16}$ | 23.91 | 18.78 | $\frac{3}{16}$ | 35.46 | 27.85 |
| $\frac{1}{4}$ | 24.24 | 19.04 | $\frac{1}{4}$ | 35.86 | 28.16 |
| $\frac{5}{16}$ | 24.57 | 19.30 | $\frac{5}{16}$ | 36.26 | 28.48 |
| $\frac{3}{8}$ | 24.90 | 19.56 | $\frac{3}{8}$ | 36.66 | 28.79 |
| $\frac{7}{16}$ | 25.23 | 19.82 | $\frac{7}{16}$ | 37.06 | 29.11 |
| $\frac{1}{2}$ | 25.57 | 20.08 | $\frac{1}{2}$ | 37.47 | 29.43 |
| $\frac{9}{16}$ | 25.91 | 20.35 | $\frac{9}{16}$ | 37.88 | 29.75 |
| $\frac{5}{8}$ | 26.25 | 20.61 | $\frac{5}{8}$ | 38.29 | 30.07 |
| $\frac{11}{16}$ | 26.59 | 20.88 | $\frac{11}{16}$ | 38.70 | 30.39 |
| $\frac{3}{4}$ | 26.93 | 21.15 | $\frac{3}{4}$ | 39.12 | 30.72 |
| $\frac{13}{16}$ | 27.28 | 21.42 | $\frac{13}{16}$ | 39.53 | 31.04 |
| $\frac{7}{8}$ | 27.63 | 21.70 | $\frac{7}{8}$ | 39.95 | 31.38 |
| $\frac{15}{16}$ | 27.98 | 21.97 | $\frac{15}{16}$ | 40.37 | 31.71 |

SQUARE AND ROUND BARS.

(CONTINUED.)

| Thickness or Diameter in Inches. | Weight of □ Bar One Inch Long. | Weight of ○ Bar One Inch Long. | Thickness or Diameter in Inches. | Weight of □ Bar One Inch Long. | Weight of ○ Bar One Inch Long. |
|--|--------------------------------------|--------------------------------------|--|--------------------------------------|--------------------------------------|
| 12 | 40.80 | 32.04 | 16 | 72.53 | 56.96 |
| $\frac{1}{8}$ | 41.65 | 32.71 | $\frac{1}{8}$ | 73.67 | 57.86 |
| $\frac{1}{4}$ | 42.52 | 33.39 | $\frac{1}{4}$ | 74.81 | 58.76 |
| $\frac{3}{8}$ | 43.39 | 34.08 | $\frac{3}{8}$ | 75.97 | 59.66 |
| $\frac{1}{2}$ | 44.27 | 34.77 | $\frac{1}{2}$ | 77.13 | 60.58 |
| $\frac{5}{8}$ | 45.16 | 35.47 | $\frac{5}{8}$ | 78.31 | 61.50 |
| $\frac{3}{4}$ | 46.06 | 36.17 | $\frac{3}{4}$ | 79.49 | 62.43 |
| $\frac{7}{8}$ | 46.96 | 36.88 | $\frac{7}{8}$ | 80.68 | 63.36 |
| 13 | 47.88 | 37.60 | 17 | 81.88 | 64.30 |
| $\frac{1}{8}$ | 48.81 | 38.33 | $\frac{1}{8}$ | 83.09 | 65.25 |
| $\frac{1}{4}$ | 49.74 | 39.06 | $\frac{1}{4}$ | 84.30 | 66.21 |
| $\frac{3}{8}$ | 50.68 | 39.80 | $\frac{3}{8}$ | 85.53 | 67.17 |
| $\frac{1}{2}$ | 51.63 | 40.55 | $\frac{1}{2}$ | 86.77 | 68.14 |
| $\frac{5}{8}$ | 52.59 | 41.31 | $\frac{5}{8}$ | 88.01 | 69.12 |
| $\frac{3}{4}$ | 53.56 | 42.07 | $\frac{3}{4}$ | 89.26 | 70.10 |
| $\frac{7}{8}$ | 54.54 | 42.84 | $\frac{7}{8}$ | 90.52 | 71.09 |
| 14 | 55.53 | 43.62 | 18 | 91.79 | 72.09 |
| $\frac{1}{8}$ | 56.53 | 44.39 | $\frac{1}{8}$ | 93.07 | 73.10 |
| $\frac{1}{4}$ | 57.53 | 45.18 | $\frac{1}{4}$ | 94.36 | 74.11 |
| $\frac{3}{8}$ | 58.54 | 45.98 | $\frac{3}{8}$ | 95.66 | 75.13 |
| $\frac{1}{2}$ | 59.57 | 46.78 | $\frac{1}{2}$ | 96.96 | 76.15 |
| $\frac{5}{8}$ | 60.60 | 47.59 | $\frac{5}{8}$ | 98.28 | 77.19 |
| $\frac{3}{4}$ | 61.64 | 48.41 | $\frac{3}{4}$ | 99.60 | 78.22 |
| $\frac{7}{8}$ | 62.69 | 49.23 | $\frac{7}{8}$ | 100.94 | 79.27 |
| 15 | 63.75 | 50.06 | 19 | 102.28 | 80.32 |
| $\frac{1}{8}$ | 64.81 | 50.90 | $\frac{1}{8}$ | 103.63 | 81.39 |
| $\frac{1}{4}$ | 65.89 | 51.75 | $\frac{1}{4}$ | 104.99 | 82.45 |
| $\frac{3}{8}$ | 66.97 | 52.60 | $\frac{3}{8}$ | 106.35 | 83.53 |
| $\frac{1}{2}$ | 68.07 | 53.46 | $\frac{1}{2}$ | 107.73 | 84.61 |
| $\frac{5}{8}$ | 69.17 | 54.32 | $\frac{5}{8}$ | 109.12 | 85.70 |
| $\frac{3}{4}$ | 70.28 | 55.20 | $\frac{3}{4}$ | 110.51 | 86.79 |
| $\frac{7}{8}$ | 71.40 | 56.08 | $\frac{7}{8}$ | 111.91 | 87.89 |

SQUARE AND ROUND BARS.

(CONTINUED.)

| Thickness or Diameter in Inches. | Weight of □ Bar One Inch Long. | Weight of ○ Bar One Inch Long. | Thickness or Diameter in Inches. | Weight of □ Bar One Inch Long. | Weight of ○ Bar One Inch Long. |
|--|--------------------------------------|--------------------------------------|--|--------------------------------------|--------------------------------------|
| 20 | 113.33 | 89.00 | 24 | 163.19 | 128.16 |
| $\frac{1}{8}$ | 114.75 | 90.12 | $\frac{1}{8}$ | 164.89 | 129.50 |
| $\frac{1}{4}$ | 116.18 | 91.24 | $\frac{1}{4}$ | 166.61 | 130.85 |
| $\frac{3}{8}$ | 117.62 | 92.37 | $\frac{3}{8}$ | 168.33 | 132.20 |
| $\frac{1}{2}$ | 119.06 | 93.51 | $\frac{1}{2}$ | 170.06 | 133.57 |
| $\frac{5}{8}$ | 120.52 | 94.65 | $\frac{5}{8}$ | 171.80 | 134.93 |
| $\frac{3}{4}$ | 121.98 | 95.80 | $\frac{3}{4}$ | 173.55 | 136.30 |
| $\frac{7}{8}$ | 123.46 | 96.96 | $\frac{7}{8}$ | 175.31 | 137.68 |
| 21 | 124.94 | 98.13 | 25 | 177.07 | 139.07 |
| $\frac{1}{8}$ | 126.43 | 99.30 | $\frac{1}{8}$ | 178.85 | 140.46 |
| $\frac{1}{4}$ | 127.93 | 100.48 | $\frac{1}{4}$ | 180.63 | 141.86 |
| $\frac{3}{8}$ | 129.44 | 101.66 | $\frac{3}{8}$ | 182.42 | 143.27 |
| $\frac{1}{2}$ | 130.96 | 102.85 | $\frac{1}{2}$ | 184.23 | 144.68 |
| $\frac{5}{8}$ | 132.49 | 104.05 | $\frac{5}{8}$ | 186.04 | 146.11 |
| $\frac{3}{4}$ | 134.03 | 105.26 | $\frac{3}{4}$ | 187.86 | 147.54 |
| $\frac{7}{8}$ | 135.57 | 106.47 | $\frac{7}{8}$ | 189.68 | 148.97 |
| 22 | 137.12 | 107.69 | 26 | 191.52 | 150.41 |
| $\frac{1}{8}$ | 138.69 | 108.92 | $\frac{1}{8}$ | 193.37 | 151.86 |
| $\frac{1}{4}$ | 140.26 | 110.15 | $\frac{1}{4}$ | 195.22 | 153.32 |
| $\frac{3}{8}$ | 141.84 | 111.40 | $\frac{3}{8}$ | 197.09 | 154.78 |
| $\frac{1}{2}$ | 143.43 | 112.64 | $\frac{1}{2}$ | 198.96 | 156.25 |
| $\frac{5}{8}$ | 145.03 | 113.90 | $\frac{5}{8}$ | 200.84 | 157.73 |
| $\frac{3}{4}$ | 146.63 | 115.16 | $\frac{3}{4}$ | 202.73 | 159.22 |
| $\frac{7}{8}$ | 148.25 | 116.43 | $\frac{7}{8}$ | 204.63 | 160.71 |
| 23 | 149.88 | 117.71 | 27 | 206.54 | 162.21 |
| $\frac{1}{8}$ | 151.51 | 118.99 | $\frac{1}{8}$ | 208.45 | 163.71 |
| $\frac{1}{4}$ | 153.15 | 120.28 | $\frac{1}{4}$ | 210.38 | 165.22 |
| $\frac{3}{8}$ | 154.81 | 121.58 | $\frac{3}{8}$ | 212.31 | 166.74 |
| $\frac{1}{2}$ | 156.46 | 122.88 | $\frac{1}{2}$ | 214.26 | 168.27 |
| $\frac{5}{8}$ | 158.13 | 124.19 | $\frac{5}{8}$ | 216.21 | 169.80 |
| $\frac{3}{4}$ | 159.81 | 125.51 | $\frac{3}{4}$ | 218.17 | 171.34 |
| $\frac{7}{8}$ | 161.49 | 126.83 | $\frac{7}{8}$ | 220.14 | 172.89 |

SQUARE AND ROUND BARS.

(CONTINUED.)

| Thickness or Diameter in Inches. | Weight of □ Bar One Inch Long. | Weight of ○ Bar One Inch Long. | Thickness or Diameter in Inches. | Weight of □ Bar One Inch Long. | Weight of ○ Bar One Inch Long. |
|--|--------------------------------------|--------------------------------------|--|--------------------------------------|--------------------------------------|
| 28 | 222.12 | 174.44 | 32 | 290.11 | 227.85 |
| $\frac{1}{8}$ | 224.11 | 176.01 | $\frac{1}{8}$ | 292.39 | 229.63 |
| $\frac{1}{4}$ | 226.10 | 177.57 | $\frac{1}{4}$ | 294.67 | 231.42 |
| $\frac{3}{8}$ | 228.11 | 179.15 | $\frac{3}{8}$ | 296.95 | 233.22 |
| $\frac{1}{2}$ | 230.12 | 180.73 | $\frac{1}{2}$ | 299.25 | 235.02 |
| $\frac{5}{8}$ | 232.15 | 182.32 | $\frac{5}{8}$ | 301.56 | 236.83 |
| $\frac{3}{4}$ | 234.18 | 183.91 | $\frac{3}{4}$ | 303.87 | 238.65 |
| $\frac{7}{8}$ | 236.22 | 185.52 | $\frac{7}{8}$ | 306.20 | 240.48 |
| 29 | 238.27 | 187.13 | 33 | 308.53 | 242.31 |
| $\frac{1}{8}$ | 240.33 | 188.74 | $\frac{1}{8}$ | 310.87 | 244.15 |
| $\frac{1}{4}$ | 242.39 | 190.37 | $\frac{1}{4}$ | 313.22 | 245.99 |
| $\frac{3}{8}$ | 244.47 | 192.00 | $\frac{3}{8}$ | 315.58 | 247.85 |
| $\frac{1}{2}$ | 246.56 | 193.64 | $\frac{1}{2}$ | 317.95 | 249.71 |
| $\frac{5}{8}$ | 248.65 | 195.28 | $\frac{5}{8}$ | 320.33 | 251.57 |
| $\frac{3}{4}$ | 250.75 | 196.93 | $\frac{3}{4}$ | 322.71 | 253.45 |
| $\frac{7}{8}$ | 252.86 | 198.59 | $\frac{7}{8}$ | 325.11 | 255.33 |
| 30 | 254.98 | 200.25 | 34 | 327.51 | 257.22 |
| $\frac{1}{8}$ | 257.11 | 201.93 | $\frac{1}{8}$ | 329.93 | 259.11 |
| $\frac{1}{4}$ | 259.25 | 203.61 | $\frac{1}{4}$ | 332.35 | 261.01 |
| $\frac{3}{8}$ | 261.40 | 205.29 | $\frac{3}{8}$ | 334.78 | 262.92 |
| $\frac{1}{2}$ | 263.55 | 206.99 | $\frac{1}{2}$ | 337.22 | 264.84 |
| $\frac{5}{8}$ | 265.72 | 208.69 | $\frac{5}{8}$ | 339.66 | 266.76 |
| $\frac{3}{4}$ | 267.89 | 210.39 | $\frac{3}{4}$ | 342.12 | 268.69 |
| $\frac{7}{8}$ | 270.07 | 212.11 | $\frac{7}{8}$ | 344.59 | 270.63 |
| 31 | 272.27 | 213.83 | 35 | 347.06 | 272.57 |
| $\frac{1}{8}$ | 274.47 | 215.56 | $\frac{1}{8}$ | 349.54 | 274.52 |
| $\frac{1}{4}$ | 276.68 | 217.29 | $\frac{1}{4}$ | 352.04 | 276.48 |
| $\frac{3}{8}$ | 278.89 | 219.03 | $\frac{3}{8}$ | 354.54 | 278.44 |
| $\frac{1}{2}$ | 281.12 | 220.78 | $\frac{1}{2}$ | 357.05 | 280.41 |
| $\frac{5}{8}$ | 283.36 | 222.54 | $\frac{5}{8}$ | 359.57 | 282.39 |
| $\frac{3}{4}$ | 285.60 | 224.30 | $\frac{3}{4}$ | 362.09 | 284.38 |
| $\frac{7}{8}$ | 287.85 | 226.07 | $\frac{7}{8}$ | 364.63 | 286.37 |

WEIGHTS OF CIRCULAR STEEL PLATES.

POUNDS.

Diameters 35 to 134 ins.; Thicknesses $\frac{3}{16}$ to 1 inch.

| Diameter in Inches | Thickness, Inches | | | | | | |
|-----------------------|-------------------|---------------|----------------|---------------|----------------|---------------|----------------|
| | $\frac{3}{16}$ | $\frac{1}{4}$ | $\frac{5}{16}$ | $\frac{3}{8}$ | $\frac{7}{16}$ | $\frac{1}{2}$ | $\frac{9}{16}$ |
| 35 | 51.1 | 68.1 | 85.2 | 102.2 | 119.3 | 136.3 | 153.3 |
| 36 | 54.1 | 72.1 | 90.1 | 108.1 | 126.2 | 144.2 | 162.2 |
| 37 | 57.1 | 76.2 | 95.2 | 114.2 | 133.3 | 152.3 | 171.4 |
| 38 | 60.2 | 80.3 | 100.4 | 120.5 | 140.6 | 160.7 | 180.7 |
| 39 | 63.5 | 84.6 | 105.8 | 126.9 | 148.1 | 169.2 | 190.4 |
| 40 | 66.8 | 89.0 | 111.3 | 133.5 | 155.8 | 178.0 | 200.3 |
| 41 | 70.1 | 93.5 | 116.9 | 140.3 | 163.7 | 187.0 | 210.4 |
| 42 | 73.6 | 98.1 | 122.7 | 147.2 | 171.7 | 196.3 | 220.8 |
| 43 | 77.1 | 102.9 | 128.6 | 154.3 | 180.0 | 205.7 | 231.4 |
| 44 | 80.8 | 107.7 | 134.6 | 161.6 | 188.5 | 215.4 | 242.3 |
| 45 | 84.5 | 112.6 | 140.8 | 169.0 | 197.1 | 225.3 | 253.5 |
| 46 | 88.3 | 117.7 | 147.1 | 176.6 | 206.0 | 235.4 | 264.9 |
| 47 | 92.2 | 122.9 | 153.6 | 184.3 | 215.1 | 245.8 | 276.5 |
| 48 | 96.1 | 128.2 | 160.2 | 192.3 | 224.3 | 256.4 | 288.4 |
| 49 | 100.2 | 133.6 | 167.0 | 200.4 | 233.8 | 267.1 | 300.5 |
| 50 | 104.3 | 139.1 | 173.9 | 208.6 | 243.4 | 278.2 | 312.9 |
| 51 | 108.5 | 144.7 | 180.9 | 217.0 | 253.2 | 289.4 | 325.6 |
| 52 | 112.8 | 150.4 | 188.0 | 225.6 | 263.3 | 300.9 | 338.5 |
| 53 | 117.2 | 156.3 | 195.3 | 234.4 | 273.5 | 312.5 | 351.6 |
| 54 | 121.7 | 162.2 | 202.8 | 243.3 | 283.9 | 324.4 | 365.0 |
| 55 | 126.2 | 168.3 | 210.4 | 252.4 | 294.5 | 336.6 | 378.6 |
| 56 | 130.8 | 174.5 | 218.1 | 261.7 | 305.3 | 348.9 | 392.5 |
| 57 | 135.6 | 180.7 | 225.9 | 271.1 | 316.3 | 361.5 | 406.7 |
| 58 | 140.4 | 187.1 | 233.9 | 280.7 | 327.5 | 374.3 | 421.1 |
| 59 | 145.2 | 193.7 | 242.1 | 290.5 | 338.9 | 387.3 | 435.7 |
| 60 | 150.2 | 200.3 | 250.3 | 300.4 | 350.5 | 400.6 | 450.6 |
| 61 | 155.3 | 207.0 | 258.8 | 310.5 | 362.3 | 414.0 | 465.8 |
| 62 | 160.4 | 213.9 | 267.3 | 320.8 | 374.2 | 427.7 | 481.2 |
| 63 | 165.6 | 220.8 | 276.0 | 331.2 | 386.4 | 441.6 | 496.8 |
| 64 | 170.9 | 227.9 | 284.8 | 341.8 | 398.8 | 455.7 | 512.7 |
| 65 | 176.3 | 235.0 | 293.8 | 352.6 | 411.3 | 470.1 | 528.9 |
| 66 | 181.8 | 242.3 | 302.9 | 363.5 | 424.1 | 484.7 | 545.3 |
| 67 | 187.3 | 249.7 | 312.2 | 374.6 | 437.0 | 499.5 | 561.9 |
| 68 | 192.9 | 257.2 | 321.6 | 385.9 | 450.2 | 514.5 | 578.8 |
| 69 | 198.6 | 264.9 | 331.1 | 397.3 | 463.5 | 529.7 | 595.9 |
| 70 | 204.4 | 272.6 | 340.7 | 408.9 | 477.0 | 545.2 | 613.3 |
| 71 | 210.3 | 280.4 | 350.6 | 420.7 | 490.8 | 560.9 | 631.0 |
| 72 | 216.3 | 288.4 | 360.5 | 432.6 | 504.7 | 576.8 | 648.9 |
| 73 | 222.3 | 296.5 | 370.6 | 444.7 | 518.8 | 592.9 | 667.0 |
| 74 | 228.5 | 304.6 | 380.8 | 457.0 | 533.1 | 609.3 | 685.4 |
| 75 | 234.7 | 312.9 | 391.2 | 469.4 | 547.6 | 625.9 | 704.1 |
| 76 | 241.0 | 321.3 | 401.7 | 482.0 | 562.3 | 642.7 | 723.0 |
| 77 | 247.4 | 329.8 | 412.3 | 494.8 | 577.2 | 659.7 | 742.1 |
| 78 | 253.9 | 338.5 | 423.1 | 507.7 | 592.3 | 676.9 | 761.6 |
| 79 | 260.4 | 347.2 | 434.0 | 520.8 | 607.6 | 694.4 | 781.2 |
| 80 | 267.0 | 356.0 | 445.1 | 534.1 | 623.1 | 712.1 | 801.1 |
| 81 | 273.8 | 365.0 | 456.3 | 547.5 | 638.8 | 730.0 | 821.3 |
| 82 | 280.6 | 374.1 | 467.6 | 561.1 | 654.6 | 748.1 | 841.7 |
| 83 | 287.4 | 383.3 | 479.1 | 574.9 | 670.7 | 766.5 | 862.3 |
| 84 | 294.4 | 392.5 | 490.7 | 588.8 | 686.9 | 785.1 | 883.2 |

WEIGHTS OF CIRCULAR STEEL PLATES.

POUNDS.

Diameters 35 to 134 ins.; Thicknesses $\frac{3}{16}$ to 1 inch.

| Thickness, Inches | | | | | | | Diameter in Inches |
|-------------------|-----------------|---------------|-----------------|---------------|-----------------|-------|-----------------------|
| $\frac{5}{8}$ | $\frac{11}{16}$ | $\frac{3}{4}$ | $\frac{13}{16}$ | $\frac{7}{8}$ | $\frac{15}{16}$ | 1 | |
| 170.4 | 187.4 | 204.4 | 221.5 | 238.6 | 255.6 | 272.6 | 35 |
| 180.2 | 198.3 | 216.3 | 234.3 | 252.4 | 270.3 | 288.3 | 36 |
| 190.4 | 209.4 | 228.3 | 247.5 | 266.6 | 285.6 | 304.6 | 37 |
| 200.8 | 220.9 | 241.0 | 261.0 | 281.2 | 301.2 | 321.3 | 38 |
| 211.5 | 232.7 | 253.9 | 275.0 | 296.2 | 317.3 | 338.4 | 39 |
| 222.5 | 244.8 | 267.0 | 289.3 | 311.6 | 333.8 | 356.0 | 40 |
| 233.8 | 257.2 | 280.6 | 303.9 | 327.5 | 350.7 | 374.1 | 41 |
| 245.3 | 269.9 | 294.4 | 318.9 | 343.4 | 368.0 | 392.5 | 42 |
| 257.2 | 282.9 | 308.6 | 334.3 | 360.0 | 385.8 | 411.5 | 43 |
| 269.3 | 296.2 | 323.1 | 350.1 | 377.0 | 403.9 | 430.9 | 44 |
| 281.6 | 309.8 | 338.0 | 366.1 | 394.3 | 422.4 | 450.6 | 45 |
| 294.3 | 323.7 | 353.2 | 382.6 | 412.1 | 441.4 | 470.9 | 46 |
| 307.2 | 338.0 | 368.7 | 399.4 | 430.2 | 460.8 | 491.5 | 47 |
| 320.4 | 352.5 | 384.5 | 416.5 | 448.6 | 480.6 | 512.7 | 48 |
| 333.9 | 367.3 | 400.7 | 434.1 | 467.6 | 500.9 | 534.3 | 49 |
| 347.7 | 382.5 | 417.2 | 452.0 | 486.8 | 521.6 | 556.3 | 50 |
| 361.7 | 397.9 | 434.1 | 470.2 | 506.4 | 542.6 | 578.7 | 51 |
| 376.1 | 413.7 | 451.3 | 488.9 | 526.6 | 564.1 | 601.7 | 52 |
| 390.7 | 429.7 | 468.8 | 507.9 | 547.0 | 586.0 | 625.1 | 53 |
| 405.6 | 446.1 | 486.7 | 527.3 | 567.8 | 608.4 | 648.9 | 54 |
| 420.7 | 462.8 | 504.9 | 546.9 | 589.0 | 631.1 | 673.2 | 55 |
| 436.2 | 479.8 | 523.4 | 567.0 | 610.7 | 654.3 | 697.9 | 56 |
| 451.9 | 497.1 | 542.2 | 587.4 | 632.6 | 677.8 | 723.0 | 57 |
| 467.9 | 514.7 | 561.4 | 608.2 | 655.0 | 701.8 | 748.6 | 58 |
| 484.1 | 532.6 | 581.0 | 629.4 | 677.8 | 726.2 | 774.7 | 59 |
| 500.7 | 550.8 | 600.8 | 650.9 | 701.0 | 751.0 | 801.1 | 60 |
| 517.5 | 569.3 | 621.0 | 672.8 | 724.5 | 776.3 | 828.1 | 61 |
| 534.6 | 588.1 | 641.6 | 695.1 | 758.5 | 800.9 | 855.4 | 62 |
| 552.0 | 607.2 | 662.4 | 717.6 | 772.8 | 828.0 | 883.2 | 63 |
| 569.7 | 626.6 | 683.6 | 740.6 | 797.6 | 854.5 | 911.4 | 64 |
| 587.6 | 646.4 | 705.1 | 763.9 | 822.6 | 881.4 | 940.2 | 65 |
| 605.8 | 666.4 | 727.0 | 787.6 | 848.1 | 908.7 | 969.3 | 66 |
| 624.3 | 686.8 | 749.2 | 811.6 | 874.0 | 936.5 | 999.0 | 67 |
| 643.1 | 707.4 | 771.7 | 836.0 | 900.3 | 964.7 | 1029 | 68 |
| 662.2 | 728.4 | 794.6 | 860.8 | 927.1 | 993.3 | 1060 | 69 |
| 681.5 | 749.6 | 817.8 | 885.9 | 954.1 | 1023 | 1091 | 70 |
| 701.1 | 771.2 | 841.3 | 919.4 | 985.5 | 1052 | 1122 | 71 |
| 721.0 | 793.1 | 865.2 | 937.8 | 1010 | 1082 | 1154 | 72 |
| 741.2 | 815.3 | 889.4 | 963.5 | 1038 | 1112 | 1186 | 73 |
| 761.6 | 837.8 | 913.9 | 990.0 | 1066 | 1143 | 1219 | 74 |
| 782.3 | 860.6 | 938.8 | 1017 | 1096 | 1174 | 1252 | 75 |
| 803.3 | 883.7 | 964.0 | 1045 | 1125 | 1205 | 1286 | 76 |
| 824.6 | 907.1 | 989.5 | 1072 | 1155 | 1237 | 1320 | 77 |
| 846.2 | 930.8 | 1015 | 1100 | 1185 | 1270 | 1354 | 78 |
| 868.0 | 954.8 | 1042 | 1129 | 1216 | 1302 | 1389 | 79 |
| 890.1 | 979.1 | 1068 | 1158 | 1247 | 1336 | 1425 | 80 |
| 912.5 | 1004 | 1095 | 1187 | 1278 | 1369 | 1460 | 81 |
| 935.2 | 1029 | 1122 | 1216 | 1310 | 1403 | 1497 | 82 |
| 958.1 | 1054 | 1150 | 1246 | 1342 | 1438 | 1533 | 83 |
| 981.4 | 1080 | 1178 | 1276 | 1374 | 1472 | 1571 | 84 |

WEIGHTS OF CIRCULAR STEEL PLATES.

POUNDS.

Diameters 35 to 134 ins.; Thicknesses $\frac{3}{16}$ to 1 inch.

| Diameter in Inches | Thickness, Inches | | | | | | |
|-----------------------|-------------------|---------------|----------------|---------------|----------------|---------------|----------------|
| | $\frac{3}{16}$ | $\frac{1}{4}$ | $\frac{5}{16}$ | $\frac{3}{8}$ | $\frac{7}{16}$ | $\frac{1}{2}$ | $\frac{9}{16}$ |
| 85 | 301.5 | 401.9 | 502.4 | 602.9 | 703.4 | 803.9 | 904.4 |
| 86 | 308.6 | 411.5 | 514.3 | 617.2 | 720.0 | 822.9 | 925.8 |
| 87 | 315.8 | 421.1 | 526.4 | 631.6 | 736.9 | 842.2 | 947.4 |
| 88 | 323.1 | 430.8 | 538.5 | 646.2 | 753.9 | 861.6 | 969.3 |
| 89 | 330.5 | 440.7 | 550.8 | 661.0 | 771.2 | 881.3 | 991.5 |
| 90 | 338.0 | 450.6 | 563.3 | 675.9 | 788.6 | 901.2 | 1014 |
| 91 | 345.5 | 460.7 | 575.9 | 691.0 | 806.2 | 921.4 | 1037 |
| 92 | 353.2 | 470.9 | 588.6 | 706.3 | 824.0 | 941.7 | 1060 |
| 93 | 360.9 | 481.2 | 601.5 | 721.7 | 842.0 | 962.3 | 1083 |
| 94 | 368.7 | 491.6 | 614.5 | 737.4 | 860.2 | 983.1 | 1106 |
| 95 | 376.6 | 502.1 | 627.6 | 753.1 | 878.6 | 1004 | 1130 |
| 96 | 384.5 | 512.7 | 640.9 | 769.1 | 897.2 | 1025 | 1154 |
| 97 | 392.6 | 523.4 | 654.3 | 785.2 | 916.0 | 1047 | 1178 |
| 98 | 400.7 | 534.3 | 667.9 | 801.4 | 935.0 | 1069 | 1202 |
| 99 | 408.9 | 545.3 | 681.6 | 817.9 | 954.2 | 1091 | 1227 |
| 100 | 417.2 | 556.3 | 695.4 | 834.5 | 973.6 | 1113 | 1252 |
| 101 | 425.6 | 567.5 | 709.4 | 851.3 | 993.1 | 1135 | 1277 |
| 102 | 434.1 | 578.8 | 723.5 | 868.2 | 1013 | 1158 | 1302 |
| 103 | 442.7 | 590.2 | 737.8 | 885.3 | 1033 | 1180 | 1328 |
| 104 | 451.3 | 601.7 | 752.1 | 902.6 | 1053 | 1203 | 1354 |
| 105 | 460.0 | 613.3 | 766.7 | 920.0 | 1073 | 1227 | 1380 |
| 106 | 468.8 | 625.1 | 781.4 | 937.6 | 1094 | 1250 | 1406 |
| 107 | 477.7 | 636.9 | 796.2 | 955.4 | 1115 | 1274 | 1433 |
| 108 | 486.7 | 648.9 | 811.1 | 973.3 | 1136 | 1298 | 1460 |
| 109 | 495.7 | 661.0 | 826.2 | 991.5 | 1157 | 1322 | 1487 |
| 110 | 504.9 | 673.2 | 841.4 | 1010 | 1178 | 1346 | 1515 |
| 111 | 514.1 | 685.4 | 856.8 | 1028 | 1200 | 1371 | 1542 |
| 112 | 523.4 | 697.9 | 872.3 | 1047 | 1221 | 1396 | 1570 |
| 113 | 532.8 | 710.4 | 888.0 | 1066 | 1243 | 1421 | 1598 |
| 114 | 542.2 | 723.0 | 903.7 | 1085 | 1265 | 1446 | 1627 |
| 115 | 551.8 | 735.7 | 919.7 | 1104 | 1288 | 1472 | 1655 |
| 116 | 561.4 | 748.6 | 935.7 | 1123 | 1310 | 1497 | 1684 |
| 117 | 571.2 | 761.6 | 951.9 | 1142 | 1333 | 1523 | 1714 |
| 118 | 581.0 | 774.6 | 968.3 | 1162 | 1356 | 1549 | 1743 |
| 119 | 590.9 | 787.8 | 984.8 | 1182 | 1379 | 1576 | 1773 |
| 120 | 600.8 | 801.1 | 1001 | 1202 | 1402 | 1602 | 1803 |
| 121 | 610.9 | 814.5 | 1018 | 1222 | 1425 | 1629 | 1833 |
| 122 | 621.0 | 828.0 | 1035 | 1242 | 1449 | 1656 | 1863 |
| 123 | 631.2 | 841.7 | 1052 | 1263 | 1473 | 1683 | 1894 |
| 124 | 641.6 | 855.4 | 1069 | 1283 | 1497 | 1711 | 1925 |
| 125 | 651.9 | 869.3 | 1087 | 1304 | 1521 | 1739 | 1956 |
| 126 | 662.4 | 883.2 | 1104 | 1325 | 1546 | 1766 | 1987 |
| 127 | 673.0 | 897.3 | 1122 | 1346 | 1570 | 1795 | 2019 |
| 128 | 683.6 | 911.5 | 1139 | 1367 | 1595 | 1823 | 2051 |
| 129 | 694.3 | 925.8 | 1157 | 1389 | 1620 | 1852 | 2083 |
| 130 | 705.1 | 940.2 | 1175 | 1410 | 1645 | 1880 | 2115 |
| 131 | 716.0 | 954.7 | 1193 | 1432 | 1671 | 1909 | 2148 |
| 132 | 727.0 | 969.3 | 1212 | 1454 | 1696 | 1939 | 2181 |
| 133 | 738.1 | 984.1 | 1230 | 1476 | 1722 | 1968 | 2214 |
| 134 | 749.2 | 998.9 | 1249 | 1498 | 1748 | 1998 | 2248 |

WEIGHTS OF CIRCULAR STEEL PLATES.

POUNDS.

Diameters 35 to 134 ins.; Thicknesses $\frac{3}{16}$ to 1 inch.

| Thickness, Inches | | | | | | | Diameter in Inches |
|-------------------|-----------------|---------------|-----------------|---------------|-----------------|------|-----------------------|
| $\frac{5}{8}$ | $\frac{11}{16}$ | $\frac{3}{4}$ | $\frac{13}{16}$ | $\frac{7}{8}$ | $\frac{15}{16}$ | 1 | |
| 1005 | 1105 | 1206 | 1307 | 1407 | 1509 | 1608 | 85 |
| 1029 | 1132 | 1234 | 1338 | 1441 | 1543 | 1646 | 86 |
| 1053 | 1158 | 1263 | 1369 | 1474 | 1580 | 1685 | 87 |
| 1077 | 1185 | 1293 | 1400 | 1508 | 1616 | 1724 | 88 |
| 1102 | 1212 | 1322 | 1433 | 1543 | 1653 | 1763 | 89 |
| 1127 | 1239 | 1352 | 1465 | 1577 | 1690 | 1803 | 90 |
| 1152 | 1267 | 1382 | 1498 | 1613 | 1728 | 1843 | 91 |
| 1177 | 1295 | 1413 | 1531 | 1648 | 1766 | 1884 | 92 |
| 1203 | 1323 | 1444 | 1564 | 1684 | 1804 | 1925 | 93 |
| 1229 | 1352 | 1475 | 1598 | 1721 | 1843 | 1967 | 94 |
| 1255 | 1381 | 1506 | 1632 | 1757 | 1883 | 2008 | 95 |
| 1282 | 1410 | 1538 | 1666 | 1795 | 1923 | 2051 | 96 |
| 1309 | 1440 | 1570 | 1701 | 1832 | 1963 | 2094 | 97 |
| 1336 | 1469 | 1603 | 1737 | 1870 | 2004 | 2137 | 98 |
| 1363 | 1499 | 1636 | 1772 | 1908 | 2045 | 2181 | 99 |
| 1391 | 1530 | 1669 | 1808 | 1947 | 2086 | 2225 | 100 |
| 1419 | 1561 | 1703 | 1844 | 1986 | 2128 | 2270 | 101 |
| 1447 | 1592 | 1736 | 1881 | 2026 | 2171 | 2315 | 102 |
| 1476 | 1623 | 1771 | 1918 | 2066 | 2213 | 2361 | 103 |
| 1504 | 1655 | 1805 | 1956 | 2106 | 2256 | 2407 | 104 |
| 1533 | 1687 | 1840 | 1993 | 2147 | 2300 | 2453 | 105 |
| 1563 | 1719 | 1875 | 2032 | 2188 | 2344 | 2500 | 106 |
| 1592 | 1752 | 1911 | 2070 | 2229 | 2389 | 2548 | 107 |
| 1622 | 1785 | 1947 | 2109 | 2271 | 2433 | 2596 | 108 |
| 1652 | 1818 | 1983 | 2148 | 2313 | 2479 | 2644 | 109 |
| 1683 | 1851 | 2020 | 2188 | 2356 | 2524 | 2693 | 110 |
| 1714 | 1885 | 2056 | 2228 | 2399 | 2570 | 2742 | 111 |
| 1745 | 1919 | 2094 | 2268 | 2443 | 2617 | 2791 | 112 |
| 1776 | 1954 | 2131 | 2309 | 2486 | 2664 | 2842 | 113 |
| 1808 | 1988 | 2169 | 2350 | 2531 | 2711 | 2892 | 114 |
| 1839 | 2023 | 2207 | 2391 | 2575 | 2759 | 2943 | 115 |
| 1872 | 2059 | 2246 | 2433 | 2620 | 2807 | 2994 | 116 |
| 1904 | 2094 | 2285 | 2475 | 2665 | 2856 | 3046 | 117 |
| 1937 | 2130 | 2324 | 2518 | 2711 | 2905 | 3099 | 118 |
| 1970 | 2167 | 2363 | 2560 | 2757 | 2954 | 3151 | 119 |
| 2003 | 2203 | 2403 | 2604 | 2804 | 3004 | 3204 | 120 |
| 2036 | 2240 | 2444 | 2647 | 2851 | 3054 | 3258 | 121 |
| 2070 | 2277 | 2484 | 2691 | 2898 | 3105 | 3312 | 122 |
| 2104 | 2315 | 2525 | 2735 | 2946 | 3156 | 3367 | 123 |
| 2139 | 2352 | 2566 | 2780 | 2994 | 3208 | 3422 | 124 |
| 2173 | 2391 | 2608 | 2825 | 3042 | 3260 | 3477 | 125 |
| 2208 | 2429 | 2650 | 2871 | 3091 | 3312 | 3533 | 126 |
| 2243 | 2468 | 2692 | 2916 | 3141 | 3365 | 3589 | 127 |
| 2279 | 2507 | 2734 | 2962 | 3190 | 3418 | 3646 | 128 |
| 2314 | 2546 | 2777 | 3009 | 3240 | 3472 | 3703 | 129 |
| 2351 | 2586 | 2821 | 3056 | 3291 | 3526 | 3761 | 130 |
| 2387 | 2625 | 2864 | 3103 | 3342 | 3580 | 3819 | 131 |
| 2423 | 2666 | 2908 | 3150 | 3393 | 3635 | 3877 | 132 |
| 2460 | 2706 | 2952 | 3198 | 3444 | 3690 | 3936 | 133 |
| 2497 | 2747 | 2997 | 3247 | 3496 | 3746 | 3996 | 134 |

AREAS OF FLAT ROLLED STEEL BARS.

For Thicknesses from $\frac{1}{16}$ in. to 2 in. and Widths from 1 in. to $12\frac{1}{2}$ in.

| Thickness in Inches. | 1" | 1 $\frac{1}{4}$ " | 1 $\frac{1}{2}$ " | 1 $\frac{3}{4}$ " | 2" | 2 $\frac{1}{4}$ " | 2 $\frac{1}{2}$ " | 2 $\frac{3}{4}$ " | 12" |
|-------------------------|------|-------------------|-------------------|-------------------|------|-------------------|-------------------|-------------------|-------|
| $\frac{1}{16}$ | .063 | .078 | .094 | .109 | .125 | .141 | .156 | .172 | .750 |
| $\frac{1}{8}$ | .125 | .156 | .188 | .219 | .250 | .281 | .313 | .344 | 1.50 |
| $\frac{3}{16}$ | .188 | .234 | .281 | .328 | .375 | .422 | .469 | .516 | 2.25 |
| $\frac{1}{4}$ | .250 | .313 | .375 | .438 | .500 | .563 | .625 | .688 | 3.00 |
| $\frac{5}{16}$ | .313 | .391 | .469 | .547 | .625 | .703 | .781 | .859 | 3.75 |
| $\frac{3}{8}$ | .375 | .469 | .563 | .656 | .750 | .844 | .938 | 1.03 | 4.50 |
| $\frac{7}{16}$ | .438 | .547 | .656 | .766 | .875 | .984 | 1.09 | 1.20 | 5.25 |
| $\frac{1}{2}$ | .500 | .625 | .750 | .875 | 1.00 | 1.13 | 1.25 | 1.38 | 6.00 |
| $\frac{9}{16}$ | .563 | .703 | .844 | .984 | 1.13 | 1.27 | 1.41 | 1.55 | 6.75 |
| $\frac{5}{8}$ | .625 | .781 | .938 | 1.09 | 1.25 | 1.41 | 1.56 | 1.72 | 7.50 |
| $\frac{11}{16}$ | .688 | .859 | 1.03 | 1.20 | 1.38 | 1.55 | 1.72 | 1.89 | 8.25 |
| $\frac{3}{4}$ | .750 | .938 | 1.13 | 1.31 | 1.50 | 1.69 | 1.88 | 2.06 | 9.00 |
| $\frac{13}{16}$ | .813 | 1.02 | 1.22 | 1.42 | 1.63 | 1.83 | 2.03 | 2.23 | 9.75 |
| $\frac{7}{8}$ | .875 | 1.09 | 1.31 | 1.53 | 1.75 | 1.97 | 2.19 | 2.41 | 10.50 |
| $\frac{15}{16}$ | .938 | 1.17 | 1.41 | 1.64 | 1.88 | 2.11 | 2.34 | 2.58 | 11.25 |
| 1 | 1.00 | 1.25 | 1.50 | 1.75 | 2.00 | 2.25 | 2.50 | 2.75 | 12.00 |
| $1\frac{1}{16}$ | 1.06 | 1.33 | 1.59 | 1.86 | 2.13 | 2.39 | 2.66 | 2.92 | 12.75 |
| $1\frac{1}{8}$ | 1.13 | 1.41 | 1.69 | 1.97 | 2.25 | 2.53 | 2.81 | 3.09 | 13.50 |
| $1\frac{1}{4}$ | 1.19 | 1.48 | 1.78 | 2.08 | 2.38 | 2.67 | 2.97 | 3.27 | 14.25 |
| $1\frac{1}{2}$ | 1.25 | 1.56 | 1.88 | 2.19 | 2.50 | 2.81 | 3.13 | 3.44 | 15.00 |
| $1\frac{5}{16}$ | 1.31 | 1.64 | 1.97 | 2.30 | 2.63 | 2.95 | 3.28 | 3.61 | 15.75 |
| $1\frac{3}{8}$ | 1.38 | 1.72 | 2.06 | 2.41 | 2.75 | 3.09 | 3.44 | 3.78 | 16.50 |
| $1\frac{7}{16}$ | 1.44 | 1.80 | 2.16 | 2.52 | 2.88 | 3.23 | 3.59 | 3.95 | 17.25 |
| $1\frac{1}{2}$ | 1.50 | 1.88 | 2.25 | 2.63 | 3.00 | 3.38 | 3.75 | 4.13 | 18.00 |
| $1\frac{9}{16}$ | 1.56 | 1.95 | 2.34 | 2.73 | 3.13 | 3.52 | 3.91 | 4.30 | 18.75 |
| $1\frac{5}{8}$ | 1.63 | 2.03 | 2.44 | 2.84 | 3.25 | 3.66 | 4.06 | 4.47 | 19.50 |
| $1\frac{11}{16}$ | 1.69 | 2.11 | 2.53 | 2.95 | 3.38 | 3.80 | 4.22 | 4.64 | 20.25 |
| $1\frac{3}{4}$ | 1.75 | 2.19 | 2.63 | 3.06 | 3.50 | 3.94 | 4.38 | 4.81 | 21.00 |
| $1\frac{13}{16}$ | 1.81 | 2.27 | 2.72 | 3.17 | 3.63 | 4.08 | 4.53 | 4.98 | 21.75 |
| $1\frac{7}{8}$ | 1.88 | 2.34 | 2.81 | 3.28 | 3.75 | 4.22 | 4.69 | 5.16 | 22.50 |
| $1\frac{15}{16}$ | 1.94 | 2.42 | 2.91 | 3.39 | 3.88 | 4.36 | 4.84 | 5.33 | 23.25 |
| 2 | 2.00 | 2.50 | 3.00 | 3.50 | 4.00 | 4.50 | 5.00 | 5.50 | 24.00 |

AREAS OF FLAT ROLLED STEEL BARS.

(CONTINUED.)

| Thickness in Inches. | 3" | 3 $\frac{1}{4}$ " | 3 $\frac{1}{2}$ " | 3 $\frac{3}{4}$ " | 4" | 4 $\frac{1}{4}$ " | 4 $\frac{1}{2}$ " | 4 $\frac{3}{4}$ " | 12" |
|-------------------------|------|-------------------|-------------------|-------------------|------|-------------------|-------------------|-------------------|-------|
| $\frac{1}{16}$ | .188 | .203 | .219 | .234 | .250 | .266 | .281 | .297 | .750 |
| $\frac{1}{8}$ | .375 | .406 | .438 | .469 | .500 | .531 | .563 | .594 | 1.50 |
| $\frac{3}{16}$ | .563 | .609 | .656 | .703 | .750 | .797 | .844 | .891 | 2.25 |
| $\frac{1}{4}$ | .750 | .813 | .875 | .938 | 1.00 | 1.06 | 1.13 | 1.19 | 3.00 |
| $\frac{5}{16}$ | .938 | 1.02 | 1.09 | 1.17 | 1.25 | 1.33 | 1.41 | 1.48 | 3.75 |
| $\frac{3}{8}$ | 1.13 | 1.22 | 1.31 | 1.41 | 1.50 | 1.59 | 1.69 | 1.78 | 4.50 |
| $\frac{7}{16}$ | 1.31 | 1.42 | 1.53 | 1.64 | 1.75 | 1.86 | 1.97 | 2.08 | 5.25 |
| $\frac{1}{2}$ | 1.50 | 1.63 | 1.75 | 1.88 | 2.00 | 2.13 | 2.25 | 2.38 | 6.00 |
| $\frac{9}{16}$ | 1.69 | 1.83 | 1.97 | 2.11 | 2.25 | 2.39 | 2.53 | 2.67 | 6.75 |
| $\frac{5}{8}$ | 1.88 | 2.03 | 2.19 | 2.34 | 2.50 | 2.66 | 2.81 | 2.97 | 7.50 |
| $\frac{11}{16}$ | 2.06 | 2.23 | 2.41 | 2.58 | 2.75 | 2.92 | 3.09 | 3.27 | 8.25 |
| $\frac{3}{4}$ | 2.25 | 2.44 | 2.63 | 2.81 | 3.00 | 3.19 | 3.38 | 3.56 | 9.00 |
| $\frac{13}{16}$ | 2.44 | 2.64 | 2.84 | 3.05 | 3.25 | 3.45 | 3.66 | 3.86 | 9.75 |
| $\frac{7}{8}$ | 2.63 | 2.84 | 3.06 | 3.28 | 3.50 | 3.72 | 3.94 | 4.16 | 10.50 |
| $\frac{15}{16}$ | 2.81 | 3.05 | 3.28 | 3.52 | 3.75 | 3.98 | 4.22 | 4.45 | 11.25 |
| 1 | 3.00 | 3.25 | 3.50 | 3.75 | 4.00 | 4.25 | 4.50 | 4.75 | 12.00 |
| $1\frac{1}{16}$ | 3.19 | 3.45 | 3.72 | 3.98 | 4.25 | 4.52 | 4.78 | 5.05 | 12.75 |
| $1\frac{1}{8}$ | 3.38 | 3.66 | 3.94 | 4.22 | 4.50 | 4.78 | 5.06 | 5.34 | 13.50 |
| $1\frac{3}{16}$ | 3.56 | 3.86 | 4.16 | 4.45 | 4.75 | 5.05 | 5.34 | 5.64 | 14.25 |
| $1\frac{1}{4}$ | 3.75 | 4.06 | 4.38 | 4.69 | 5.00 | 5.31 | 5.63 | 5.94 | 15.00 |
| $1\frac{5}{16}$ | 3.94 | 4.27 | 4.59 | 4.92 | 5.25 | 5.58 | 5.91 | 6.23 | 15.75 |
| $1\frac{3}{8}$ | 4.13 | 4.47 | 4.81 | 5.16 | 5.50 | 5.84 | 6.19 | 6.53 | 16.50 |
| $1\frac{7}{16}$ | 4.31 | 4.67 | 5.03 | 5.39 | 5.75 | 6.11 | 6.47 | 6.83 | 17.25 |
| $1\frac{1}{2}$ | 4.50 | 4.88 | 5.25 | 5.63 | 6.00 | 6.38 | 6.75 | 7.13 | 18.00 |
| $1\frac{9}{16}$ | 4.69 | 5.08 | 5.47 | 5.86 | 6.25 | 6.64 | 7.03 | 7.42 | 18.75 |
| $1\frac{5}{8}$ | 4.88 | 5.28 | 5.69 | 6.09 | 6.50 | 6.91 | 7.31 | 7.72 | 19.50 |
| $1\frac{11}{16}$ | 5.06 | 5.48 | 5.91 | 6.33 | 6.75 | 7.17 | 7.59 | 8.02 | 20.25 |
| $1\frac{3}{4}$ | 5.25 | 5.69 | 6.13 | 6.56 | 7.00 | 7.44 | 7.88 | 8.31 | 21.00 |
| $1\frac{13}{16}$ | 5.44 | 5.89 | 6.34 | 6.80 | 7.25 | 7.70 | 8.16 | 8.61 | 21.75 |
| $1\frac{7}{8}$ | 5.63 | 6.09 | 6.56 | 7.03 | 7.50 | 7.97 | 8.44 | 8.91 | 22.50 |
| $1\frac{15}{16}$ | 5.81 | 6.30 | 6.78 | 7.27 | 7.75 | 8.23 | 8.72 | 9.20 | 23.25 |
| 2 | 6.00 | 6.50 | 7.00 | 7.50 | 8.00 | 8.50 | 9.00 | 9.50 | 24.00 |

AREAS OF FLAT ROLLED STEEL BARS.

(CONTINUED.)

| Thickness in Inches. | 5" | 5¼" | 5½" | 5¾" | 6" | 6¼" | 6½" | 6¾" | 12" |
|-------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| $\frac{1}{16}$ | .313 | .328 | .344 | .359 | .375 | .391 | .406 | .422 | .750 |
| $\frac{1}{8}$ | .625 | .656 | .688 | .719 | .750 | .781 | .813 | .844 | 1.50 |
| $\frac{3}{16}$ | .938 | .984 | 1.03 | 1.08 | 1.13 | 1.17 | 1.22 | 1.27 | 2.25 |
| $\frac{1}{4}$ | 1.25 | 1.31 | 1.38 | 1.44 | 1.50 | 1.56 | 1.63 | 1.69 | 3.00 |
| $\frac{5}{16}$ | 1.56 | 1.64 | 1.72 | 1.80 | 1.88 | 1.95 | 2.03 | 2.11 | 3.75 |
| $\frac{3}{8}$ | 1.88 | 1.97 | 2.06 | 2.16 | 2.25 | 2.34 | 2.44 | 2.53 | 4.50 |
| $\frac{7}{16}$ | 2.19 | 2.30 | 2.41 | 2.52 | 2.63 | 2.73 | 2.84 | 2.95 | 5.25 |
| $\frac{1}{2}$ | 2.50 | 2.63 | 2.75 | 2.88 | 3.00 | 3.13 | 3.25 | 3.38 | 6.00 |
| $\frac{9}{16}$ | 2.81 | 2.95 | 3.09 | 3.23 | 3.38 | 3.52 | 3.66 | 3.80 | 6.75 |
| $\frac{5}{8}$ | 3.13 | 3.28 | 3.44 | 3.59 | 3.75 | 3.91 | 4.06 | 4.22 | 7.50 |
| $\frac{11}{16}$ | 3.44 | 3.61 | 3.78 | 3.95 | 4.13 | 4.30 | 4.47 | 4.64 | 8.25 |
| $\frac{3}{4}$ | 3.75 | 3.94 | 4.13 | 4.31 | 4.50 | 4.69 | 4.88 | 5.06 | 9.00 |
| $\frac{13}{16}$ | 4.06 | 4.27 | 4.47 | 4.67 | 4.88 | 5.08 | 5.28 | 5.48 | 9.75 |
| $\frac{7}{8}$ | 4.38 | 4.59 | 4.81 | 5.03 | 5.25 | 5.47 | 5.69 | 5.91 | 10.50 |
| $\frac{15}{16}$ | 4.69 | 4.92 | 5.16 | 5.39 | 5.63 | 5.86 | 6.09 | 6.33 | 11.25 |
| 1 | 5.00 | 5.25 | 5.50 | 5.75 | 6.00 | 6.25 | 6.50 | 6.75 | 12.00 |
| $1\frac{1}{16}$ | 5.31 | 5.58 | 5.84 | 6.11 | 6.38 | 6.64 | 6.91 | 7.17 | 12.75 |
| $1\frac{1}{8}$ | 5.63 | 5.91 | 6.19 | 6.47 | 6.75 | 7.03 | 7.31 | 7.59 | 13.50 |
| $1\frac{3}{16}$ | 5.94 | 6.23 | 6.53 | 6.83 | 7.13 | 7.42 | 7.72 | 8.02 | 14.25 |
| $1\frac{1}{4}$ | 6.25 | 6.56 | 6.88 | 7.19 | 7.50 | 7.81 | 8.13 | 8.44 | 15.00 |
| $1\frac{5}{16}$ | 6.56 | 6.89 | 7.22 | 7.55 | 7.88 | 8.20 | 8.53 | 8.86 | 15.75 |
| $1\frac{3}{8}$ | 6.88 | 7.22 | 7.56 | 7.91 | 8.25 | 8.59 | 8.94 | 9.28 | 16.50 |
| $1\frac{7}{16}$ | 7.19 | 7.55 | 7.91 | 8.27 | 8.63 | 8.98 | 9.34 | 9.70 | 17.25 |
| $1\frac{1}{2}$ | 7.50 | 7.88 | 8.25 | 8.63 | 9.00 | 9.38 | 9.75 | 10.13 | 18.00 |
| $1\frac{9}{16}$ | 7.81 | 8.20 | 8.59 | 8.98 | 9.38 | 9.77 | 10.16 | 10.55 | 18.75 |
| $1\frac{5}{8}$ | 8.13 | 8.53 | 8.94 | 9.34 | 9.75 | 10.16 | 10.56 | 10.97 | 19.50 |
| $1\frac{11}{16}$ | 8.44 | 8.86 | 9.28 | 9.70 | 10.13 | 10.55 | 10.97 | 11.39 | 20.25 |
| $1\frac{3}{4}$ | 8.75 | 9.19 | 9.63 | 10.06 | 10.50 | 10.94 | 11.38 | 11.81 | 21.00 |
| $1\frac{13}{16}$ | 9.06 | 9.52 | 9.97 | 10.42 | 10.88 | 11.33 | 11.78 | 12.23 | 21.75 |
| $1\frac{7}{8}$ | 9.38 | 9.84 | 10.31 | 10.78 | 11.25 | 11.72 | 12.19 | 12.66 | 22.50 |
| $1\frac{15}{16}$ | 9.69 | 10.17 | 10.66 | 11.14 | 11.63 | 12.11 | 12.59 | 13.08 | 23.25 |
| 2 | 10.00 | 10.50 | 11.00 | 11.50 | 12.00 | 12.50 | 13.00 | 13.50 | 24.00 |

AREAS OF FLAT ROLLED STEEL BARS.

(CONTINUED.)

| Thickness in Inches. | 7" | 7 $\frac{1}{4}$ " | 7 $\frac{1}{2}$ " | 7 $\frac{3}{4}$ " | 8" | 8 $\frac{1}{4}$ " | 8 $\frac{1}{2}$ " | 8 $\frac{3}{4}$ " | 12" |
|-------------------------|-------|-------------------|-------------------|-------------------|-------|-------------------|-------------------|-------------------|-------|
| $\frac{1}{16}$ | .438 | .453 | .469 | .484 | .500 | .516 | .531 | .547 | .750 |
| $\frac{1}{8}$ | .875 | .906 | .938 | .969 | 1.00 | 1.03 | 1.06 | 1.09 | 1.50 |
| $\frac{3}{16}$ | 1.31 | 1.36 | 1.41 | 1.45 | 1.50 | 1.55 | 1.59 | 1.64 | 2.25 |
| $\frac{1}{4}$ | 1.75 | 1.81 | 1.88 | 1.94 | 2.00 | 2.06 | 2.13 | 2.19 | 3.00 |
| $\frac{5}{16}$ | 2.19 | 2.27 | 2.34 | 2.42 | 2.50 | 2.58 | 2.66 | 2.73 | 3.75 |
| $\frac{3}{8}$ | 2.63 | 2.72 | 2.81 | 2.91 | 3.00 | 3.09 | 3.19 | 3.28 | 4.50 |
| $\frac{7}{16}$ | 3.06 | 3.17 | 3.28 | 3.39 | 3.50 | 3.61 | 3.72 | 3.83 | 5.25 |
| $\frac{1}{2}$ | 3.50 | 3.63 | 3.75 | 3.88 | 4.00 | 4.13 | 4.25 | 4.38 | 6.00 |
| $\frac{9}{16}$ | 3.94 | 4.08 | 4.22 | 4.36 | 4.50 | 4.64 | 4.78 | 4.92 | 6.75 |
| $\frac{5}{8}$ | 4.38 | 4.53 | 4.69 | 4.84 | 5.00 | 5.16 | 5.31 | 5.47 | 7.50 |
| $\frac{11}{16}$ | 4.81 | 4.98 | 5.16 | 5.33 | 5.50 | 5.67 | 5.84 | 6.02 | 8.25 |
| $\frac{3}{4}$ | 5.25 | 5.44 | 5.63 | 5.81 | 6.00 | 6.19 | 6.38 | 6.56 | 9.00 |
| $\frac{13}{16}$ | 5.69 | 5.89 | 6.09 | 6.30 | 6.50 | 6.70 | 6.91 | 7.11 | 9.75 |
| $\frac{7}{8}$ | 6.13 | 6.34 | 6.56 | 6.78 | 7.00 | 7.22 | 7.44 | 7.66 | 10.50 |
| $\frac{15}{16}$ | 6.56 | 6.80 | 7.03 | 7.27 | 7.50 | 7.73 | 7.97 | 8.20 | 11.25 |
| 1 | 7.00 | 7.25 | 7.50 | 7.75 | 8.00 | 8.25 | 8.50 | 8.75 | 12.00 |
| $1\frac{1}{16}$ | 7.44 | 7.70 | 7.97 | 8.23 | 8.50 | 8.77 | 9.03 | 9.30 | 12.75 |
| $1\frac{1}{8}$ | 7.88 | 8.16 | 8.44 | 8.72 | 9.00 | 9.28 | 9.56 | 9.84 | 13.50 |
| $1\frac{3}{16}$ | 8.31 | 8.61 | 8.91 | 9.20 | 9.50 | 9.80 | 10.09 | 10.39 | 14.25 |
| $1\frac{1}{4}$ | 8.75 | 9.06 | 9.38 | 9.69 | 10.00 | 10.31 | 10.63 | 10.94 | 15.00 |
| $1\frac{5}{16}$ | 9.19 | 9.52 | 9.84 | 10.17 | 10.50 | 10.83 | 11.16 | 11.48 | 15.75 |
| $1\frac{3}{8}$ | 9.63 | 9.97 | 10.31 | 10.66 | 11.00 | 11.34 | 11.69 | 12.03 | 16.50 |
| $1\frac{7}{16}$ | 10.06 | 10.42 | 10.78 | 11.14 | 11.50 | 11.86 | 12.22 | 12.58 | 17.25 |
| $1\frac{1}{2}$ | 10.50 | 10.88 | 11.25 | 11.63 | 12.00 | 12.38 | 12.75 | 13.13 | 18.00 |
| $1\frac{9}{16}$ | 10.94 | 11.33 | 11.72 | 12.11 | 12.50 | 12.89 | 13.28 | 13.67 | 18.75 |
| $1\frac{5}{8}$ | 11.38 | 11.78 | 12.19 | 12.59 | 13.00 | 13.41 | 13.81 | 14.22 | 19.50 |
| $1\frac{11}{16}$ | 11.81 | 12.23 | 12.66 | 13.08 | 13.50 | 13.92 | 14.34 | 14.77 | 20.25 |
| $1\frac{3}{4}$ | 12.25 | 12.69 | 13.13 | 13.56 | 14.00 | 14.44 | 14.88 | 15.31 | 21.00 |
| $1\frac{13}{16}$ | 12.69 | 13.14 | 13.59 | 14.05 | 14.50 | 14.95 | 15.41 | 15.86 | 21.75 |
| $1\frac{7}{8}$ | 13.13 | 13.59 | 14.06 | 14.53 | 15.00 | 15.47 | 15.94 | 16.41 | 22.50 |
| $1\frac{15}{16}$ | 13.56 | 14.05 | 14.53 | 15.02 | 15.50 | 15.98 | 16.47 | 16.95 | 23.25 |
| 2 | 14.00 | 14.50 | 15.00 | 15.50 | 16.00 | 16.50 | 17.00 | 17.50 | 24.00 |

AREAS OF FLAT ROLLED STEEL BARS.

(CONTINUED.)

| Thickness in Inches. | 9" | 9 $\frac{1}{4}$ " | 9 $\frac{1}{2}$ " | 9 $\frac{3}{4}$ " | 10" | 10 $\frac{1}{4}$ " | 10 $\frac{1}{2}$ " | 10 $\frac{3}{4}$ " | 12" |
|-------------------------|-------|-------------------|-------------------|-------------------|-------|--------------------|--------------------|--------------------|-------|
| $\frac{1}{16}$ | .563 | .578 | .594 | .609 | .625 | .641 | .656 | .672 | .750 |
| $\frac{1}{8}$ | 1.13 | 1.16 | 1.19 | 1.22 | 1.25 | 1.28 | 1.31 | 1.34 | 1.50 |
| $\frac{3}{16}$ | 1.69 | 1.73 | 1.78 | 1.83 | 1.88 | 1.92 | 1.97 | 2.02 | 2.25 |
| $\frac{1}{4}$ | 2.25 | 2.31 | 2.38 | 2.44 | 2.50 | 2.56 | 2.63 | 2.69 | 3.00 |
| $\frac{5}{16}$ | 2.81 | 2.89 | 2.97 | 3.05 | 3.13 | 3.20 | 3.28 | 3.36 | 3.75 |
| $\frac{3}{8}$ | 3.38 | 3.47 | 3.56 | 3.66 | 3.75 | 3.84 | 3.94 | 4.03 | 4.50 |
| $\frac{7}{16}$ | 3.94 | 4.05 | 4.16 | 4.27 | 4.38 | 4.48 | 4.59 | 4.70 | 5.25 |
| $\frac{1}{2}$ | 4.50 | 4.63 | 4.75 | 4.88 | 5.00 | 5.13 | 5.25 | 5.38 | 6.00 |
| $\frac{9}{16}$ | 5.06 | 5.20 | 5.34 | 5.48 | 5.63 | 5.77 | 5.91 | 6.05 | 6.75 |
| $\frac{5}{8}$ | 5.63 | 5.78 | 5.94 | 6.09 | 6.25 | 6.41 | 6.56 | 6.72 | 7.50 |
| $\frac{11}{16}$ | 6.19 | 6.36 | 6.53 | 6.70 | 6.88 | 7.05 | 7.22 | 7.39 | 8.25 |
| $\frac{3}{4}$ | 6.75 | 6.94 | 7.13 | 7.31 | 7.50 | 7.69 | 7.88 | 8.06 | 9.00 |
| $1\frac{1}{16}$ | 7.31 | 7.52 | 7.72 | 7.92 | 8.13 | 8.33 | 8.53 | 8.73 | 9.75 |
| $1\frac{1}{8}$ | 7.88 | 8.09 | 8.31 | 8.53 | 8.75 | 8.97 | 9.19 | 9.41 | 10.50 |
| $1\frac{3}{16}$ | 8.44 | 8.67 | 8.91 | 9.14 | 9.38 | 9.61 | 9.84 | 10.08 | 11.25 |
| 1 | 9.00 | 9.25 | 9.50 | 9.75 | 10.00 | 10.25 | 10.50 | 10.75 | 12.00 |
| $1\frac{1}{16}$ | 9.56 | 9.83 | 10.09 | 10.36 | 10.63 | 10.89 | 11.16 | 11.42 | 12.75 |
| $1\frac{1}{8}$ | 10.13 | 10.41 | 10.69 | 10.97 | 11.25 | 11.53 | 11.81 | 12.09 | 13.50 |
| $1\frac{3}{16}$ | 10.69 | 10.98 | 11.28 | 11.58 | 11.88 | 12.17 | 12.47 | 12.77 | 14.25 |
| $1\frac{1}{4}$ | 11.25 | 11.56 | 11.88 | 12.19 | 12.50 | 12.81 | 13.13 | 13.44 | 15.00 |
| $1\frac{5}{16}$ | 11.81 | 12.14 | 12.47 | 12.80 | 13.13 | 13.45 | 13.78 | 14.11 | 15.75 |
| $1\frac{3}{8}$ | 12.38 | 12.72 | 13.06 | 13.41 | 13.75 | 14.09 | 14.44 | 14.78 | 16.50 |
| $1\frac{7}{16}$ | 12.94 | 13.30 | 13.66 | 14.02 | 14.38 | 14.73 | 15.09 | 15.45 | 17.25 |
| $1\frac{1}{2}$ | 13.50 | 13.88 | 14.25 | 14.63 | 15.00 | 15.38 | 15.75 | 16.13 | 18.00 |
| $1\frac{9}{16}$ | 14.06 | 14.45 | 14.84 | 15.23 | 15.63 | 16.02 | 16.41 | 16.80 | 18.75 |
| $1\frac{5}{8}$ | 14.63 | 15.03 | 15.44 | 15.84 | 16.25 | 16.66 | 17.06 | 17.47 | 19.50 |
| $1\frac{11}{16}$ | 15.19 | 15.61 | 16.03 | 16.45 | 16.88 | 17.30 | 17.72 | 18.14 | 20.25 |
| $1\frac{3}{4}$ | 15.75 | 16.19 | 16.63 | 17.06 | 17.50 | 17.94 | 18.38 | 18.81 | 21.00 |
| $1\frac{13}{16}$ | 16.31 | 16.77 | 17.22 | 17.67 | 18.13 | 18.58 | 19.03 | 19.48 | 21.75 |
| $1\frac{7}{8}$ | 16.88 | 17.34 | 17.81 | 18.28 | 18.75 | 19.22 | 19.69 | 20.16 | 22.50 |
| $1\frac{15}{16}$ | 17.44 | 17.92 | 18.41 | 18.89 | 19.38 | 19.86 | 20.34 | 20.83 | 23.25 |
| 2 | 18.00 | 18.50 | 19.00 | 19.50 | 20.00 | 20.50 | 21.00 | 21.50 | 24.00 |

AREAS OF FLAT ROLLED STEEL BARS.

(CONCLUDED.)

| Thickness in Inches. | 11" | 11 $\frac{1}{4}$ " | 11 $\frac{1}{2}$ " | 11 $\frac{3}{4}$ " | 12" | 12 $\frac{1}{4}$ " | 12 $\frac{1}{2}$ " | 12 $\frac{3}{4}$ " |
|-------------------------|-------|--------------------|--------------------|--------------------|-------|--------------------|--------------------|--------------------|
| $\frac{1}{16}$ | .688 | .703 | .719 | .734 | .750 | .766 | .781 | .797 |
| $\frac{1}{8}$ | 1.38 | 1.41 | 1.44 | 1.47 | 1.50 | 1.53 | 1.56 | 1.59 |
| $\frac{3}{16}$ | 2.06 | 2.11 | 2.16 | 2.20 | 2.25 | 2.30 | 2.34 | 2.39 |
| $\frac{1}{4}$ | 2.75 | 2.81 | 2.88 | 2.94 | 3.00 | 3.06 | 3.13 | 3.19 |
| $\frac{5}{16}$ | 3.44 | 3.52 | 3.59 | 3.67 | 3.75 | 3.83 | 3.91 | 3.98 |
| $\frac{3}{8}$ | 4.13 | 4.22 | 4.31 | 4.41 | 4.50 | 4.59 | 4.69 | 4.78 |
| $\frac{7}{16}$ | 4.81 | 4.92 | 5.03 | 5.14 | 5.25 | 5.36 | 5.47 | 5.58 |
| $\frac{1}{2}$ | 5.50 | 5.63 | 5.75 | 5.88 | 6.00 | 6.13 | 6.25 | 6.38 |
| $\frac{9}{16}$ | 6.19 | 6.33 | 6.47 | 6.61 | 6.75 | 6.89 | 7.03 | 7.17 |
| $\frac{5}{8}$ | 6.88 | 7.03 | 7.19 | 7.34 | 7.50 | 7.66 | 7.81 | 7.97 |
| $\frac{11}{16}$ | 7.56 | 7.73 | 7.91 | 8.08 | 8.25 | 8.42 | 8.59 | 8.77 |
| $\frac{3}{4}$ | 8.25 | 8.44 | 8.63 | 8.81 | 9.00 | 9.19 | 9.38 | 9.56 |
| $\frac{13}{16}$ | 8.94 | 9.14 | 9.34 | 9.55 | 9.75 | 9.95 | 10.16 | 10.36 |
| $\frac{7}{8}$ | 9.63 | 9.84 | 10.06 | 10.28 | 10.50 | 10.72 | 10.94 | 11.16 |
| $\frac{15}{16}$ | 10.31 | 10.55 | 10.78 | 11.02 | 11.25 | 11.48 | 11.72 | 11.95 |
| 1 | 11.00 | 11.25 | 11.50 | 11.75 | 12.00 | 12.25 | 12.50 | 12.75 |
| $1\frac{1}{16}$ | 11.69 | 11.95 | 12.22 | 12.48 | 12.75 | 13.02 | 13.28 | 13.55 |
| $1\frac{1}{8}$ | 12.38 | 12.66 | 12.94 | 13.22 | 13.50 | 13.78 | 14.06 | 14.34 |
| $1\frac{3}{16}$ | 13.06 | 13.36 | 13.66 | 13.95 | 14.25 | 14.55 | 14.84 | 15.14 |
| $1\frac{1}{4}$ | 13.75 | 14.06 | 14.38 | 14.69 | 15.00 | 15.31 | 15.63 | 15.94 |
| $1\frac{5}{16}$ | 14.44 | 14.77 | 15.09 | 15.42 | 15.75 | 16.08 | 16.41 | 16.73 |
| $1\frac{3}{8}$ | 15.13 | 15.47 | 15.81 | 16.16 | 16.50 | 16.84 | 17.19 | 17.53 |
| $1\frac{7}{16}$ | 15.81 | 16.17 | 16.53 | 16.89 | 17.25 | 17.61 | 17.97 | 18.33 |
| $1\frac{1}{2}$ | 16.50 | 16.88 | 17.25 | 17.63 | 18.00 | 18.38 | 18.75 | 19.13 |
| $1\frac{9}{16}$ | 17.19 | 17.58 | 17.97 | 18.36 | 18.75 | 19.14 | 19.53 | 19.92 |
| $1\frac{5}{8}$ | 17.88 | 18.28 | 18.69 | 19.09 | 19.50 | 19.91 | 20.31 | 20.72 |
| $1\frac{11}{16}$ | 18.56 | 18.98 | 19.41 | 19.83 | 20.25 | 20.67 | 21.09 | 21.52 |
| $1\frac{3}{4}$ | 19.25 | 19.69 | 20.13 | 20.56 | 21.00 | 21.44 | 21.88 | 22.31 |
| $1\frac{13}{16}$ | 19.94 | 20.39 | 20.84 | 21.30 | 21.75 | 22.20 | 22.66 | 23.11 |
| $1\frac{7}{8}$ | 20.63 | 21.09 | 21.56 | 22.03 | 22.50 | 22.97 | 23.44 | 23.91 |
| $1\frac{15}{16}$ | 21.31 | 21.80 | 22.28 | 22.77 | 23.25 | 23.73 | 24.22 | 24.70 |
| 2 | 22.00 | 22.50 | 23.00 | 23.50 | 24.00 | 24.50 | 25.00 | 25.50 |

The areas for 12" width are repeated on each page to facilitate making the additions necessary to obtain the areas of plates of any width greater than 12". Thus, to find the area of $15\frac{1}{4}" \times \frac{1}{8}"$, add the areas to be found in the same line for $3\frac{1}{4}" \times \frac{1}{8}"$ and $12" \times \frac{1}{8}" = 2.84 + 10.50 = 13.34$ square inches. Area of plate $4' 6\frac{1}{2}" \times \frac{5}{8}" = 4 \times 7.50 + 4.06 = 34.06$ square inches.

WEIGHTS OF FLAT ROLLED STRIPS, HOOP OR BAND STEEL.

Pounds per Lineal Foot.

Thicknesses by Birmingham Wire Gauge.

One cubic foot of steel weighs 489.6 pounds.

For widths from $\frac{1}{4}$ inch to $\frac{3}{4}$ inch and thicknesses from No. 19 to No. 11 B.W.G.

| Width in Inches. | No. 19. .042 In. | No. 18. .049 In. | No. 17. .058 In. | No. 16. .065 In. | No. 15. .072 In. | No. 14. .083 In. | No. 13. .095 In. | No. 12. .109 In. | No. 11. .120 In. |
|---------------------|---------------------|---------------------|---------------------|---------------------|---------------------|---------------------|---------------------|---------------------|---------------------|
| $\frac{1}{4}$ | .036 | .042 | .049 | .055 | .061 | .071 | .081 | .093 | .102 |
| $\frac{1}{2}$ | .038 | .044 | .052 | .059 | .065 | .075 | .086 | .098 | .108 |
| $\frac{3}{4}$ | .040 | .047 | .055 | .062 | .069 | .079 | .091 | .104 | .115 |
| $\frac{1}{2}$ | .042 | .049 | .059 | .066 | .073 | .084 | .096 | .110 | .121 |
| $\frac{1}{2}$ | .045 | .052 | .062 | .069 | .077 | .088 | .101 | .116 | .128 |
| $\frac{1}{2}$ | .047 | .055 | .065 | .073 | .080 | .093 | .106 | .122 | .134 |
| $\frac{1}{2}$ | .049 | .057 | .068 | .076 | .084 | .097 | .111 | .127 | .140 |
| $\frac{1}{2}$ | .051 | .060 | .071 | .079 | .088 | .101 | .116 | .133 | .147 |
| $\frac{1}{2}$ | .054 | .062 | .074 | .083 | .092 | .106 | .121 | .139 | .153 |
| $\frac{1}{2}$ | .056 | .065 | .077 | .086 | .096 | .110 | .126 | .145 | .159 |
| $\frac{1}{2}$ | .058 | .068 | .080 | .090 | .099 | .115 | .131 | .151 | .166 |
| $\frac{1}{2}$ | .060 | .070 | .083 | .093 | .103 | .119 | .136 | .156 | .172 |
| $\frac{1}{2}$ | .062 | .073 | .086 | .097 | .107 | .123 | .141 | .162 | .179 |
| $\frac{1}{2}$ | .065 | .075 | .089 | .100 | .111 | .128 | .146 | .168 | .185 |
| $\frac{1}{2}$ | .067 | .078 | .092 | .104 | .115 | .132 | .151 | .174 | .191 |
| $\frac{1}{2}$ | .069 | .081 | .096 | .107 | .119 | .137 | .156 | .180 | .198 |
| $\frac{1}{2}$ | .071 | .083 | .099 | .111 | .122 | .141 | .162 | .185 | .204 |
| $\frac{1}{2}$ | .074 | .086 | .102 | .114 | .126 | .146 | .167 | .191 | .210 |
| $\frac{1}{2}$ | .076 | .089 | .105 | .117 | .130 | .150 | .172 | .197 | .217 |
| $\frac{1}{2}$ | .078 | .091 | .108 | .121 | .134 | .154 | .177 | .203 | .223 |
| $\frac{1}{2}$ | .080 | .094 | .111 | .124 | .138 | .159 | .182 | .208 | .230 |
| $\frac{1}{2}$ | .083 | .096 | .114 | .128 | .142 | .163 | .187 | .214 | .236 |
| $\frac{1}{2}$ | .085 | .099 | .117 | .131 | .145 | .168 | .192 | .220 | .242 |
| $\frac{1}{2}$ | .087 | .102 | .120 | .135 | .149 | .172 | .197 | .226 | .249 |
| $\frac{1}{2}$ | .089 | .104 | .123 | .138 | .153 | .176 | .202 | .232 | .255 |
| $\frac{1}{2}$ | .091 | .107 | .126 | .142 | .157 | .181 | .207 | .237 | .261 |
| $\frac{1}{2}$ | .094 | .109 | .129 | .145 | .161 | .185 | .212 | .243 | .268 |
| $\frac{1}{2}$ | .096 | .112 | .132 | .148 | .164 | .190 | .217 | .249 | .274 |
| $\frac{1}{2}$ | .098 | .115 | .136 | .152 | .168 | .194 | .222 | .255 | .281 |
| $\frac{1}{2}$ | .100 | .117 | .139 | .155 | .172 | .198 | .227 | .261 | .287 |
| $\frac{1}{2}$ | .103 | .120 | .142 | .159 | .176 | .203 | .232 | .266 | .293 |
| $\frac{1}{2}$ | .105 | .122 | .145 | .162 | .180 | .207 | .237 | .272 | .300 |
| $\frac{1}{2}$ | .107 | .125 | .148 | .166 | .184 | .212 | .242 | .278 | .306 |

WEIGHTS OF FLAT ROLLED STEEL BARS.

Pounds per Lineal Foot.

One cubic foot of steel weighs 489.6 pounds.

For thicknesses from $\frac{1}{16}$ inch to $\frac{1}{2}$ inch and widths from $\frac{1}{4}$ inch to 1 inch.

| Thickness in Inches. | $\frac{1}{4}$ " | $\frac{1}{2}$ " | $\frac{3}{4}$ " | $\frac{1}{2}$ " | $\frac{5}{16}$ " | $\frac{3}{4}$ " | $\frac{1}{2}$ " | $\frac{3}{4}$ " | $\frac{1}{2}$ " |
|-------------------------|-----------------|-----------------|-----------------|-----------------|------------------|-----------------|-----------------|-----------------|-----------------|
| $\frac{1}{16}$ | .053 | .056 | .060 | .063 | .066 | .070 | .073 | .076 | .080 |
| $\frac{1}{8}$ | .066 | .071 | .075 | .079 | .083 | .087 | .091 | .095 | .100 |
| $\frac{3}{16}$ | .080 | .085 | .090 | .095 | .100 | .105 | .110 | .115 | .120 |
| $\frac{1}{4}$ | .093 | .099 | .105 | .110 | .116 | .122 | .128 | .134 | .139 |
| $\frac{5}{16}$ | .106 | .113 | .120 | .126 | .133 | .139 | .146 | .153 | .159 |
| $\frac{3}{8}$ | .120 | .127 | .134 | .142 | .149 | .157 | .164 | .172 | .179 |
| $\frac{7}{16}$ | .133 | .141 | .149 | .158 | .166 | .174 | .183 | .191 | .199 |
| $\frac{1}{2}$ | .146 | .155 | .164 | .173 | .183 | .192 | .201 | .210 | .219 |
| $\frac{5}{8}$ | .159 | .169 | .179 | .189 | .199 | .209 | .219 | .229 | .239 |
| $\frac{3}{4}$ | .173 | .183 | .194 | .205 | .216 | .227 | .237 | .248 | .259 |
| $\frac{7}{8}$ | .186 | .198 | .209 | .221 | .232 | .244 | .256 | .267 | .279 |
| $\frac{15}{16}$ | .199 | .212 | .224 | .237 | .249 | .261 | .274 | .286 | .299 |
| $\frac{1}{4}$ | .213 | .226 | .239 | .252 | .266 | .279 | .292 | .305 | .319 |
| $\frac{1}{2}$ | .226 | .240 | .254 | .268 | .282 | .296 | .310 | .325 | .339 |
| $\frac{3}{4}$ | .239 | .254 | .269 | .284 | .299 | .314 | .329 | .344 | .359 |
| $\frac{15}{16}$ | .252 | .268 | .284 | .300 | .315 | .331 | .347 | .363 | .379 |
| $\frac{5}{8}$ | .266 | .282 | .299 | .315 | .332 | .349 | .365 | .382 | .398 |
| $\frac{3}{4}$ | .279 | .296 | .314 | .331 | .349 | .366 | .383 | .401 | .418 |
| $\frac{7}{8}$ | .292 | .310 | .329 | .347 | .365 | .383 | .402 | .420 | .438 |
| $\frac{15}{16}$ | .305 | .325 | .344 | .363 | .382 | .401 | .420 | .439 | .458 |
| $\frac{1}{2}$ | .319 | .339 | .359 | .379 | .398 | .418 | .438 | .458 | .478 |
| $\frac{3}{4}$ | .332 | .353 | .374 | .394 | .415 | .436 | .457 | .477 | .498 |
| $\frac{7}{8}$ | .345 | .367 | .388 | .410 | .432 | .453 | .475 | .496 | .518 |
| $\frac{15}{16}$ | .359 | .381 | .403 | .426 | .448 | .471 | .493 | .515 | .538 |
| $\frac{1}{2}$ | .372 | .395 | .418 | .442 | .465 | .488 | .511 | .535 | .558 |
| $\frac{3}{4}$ | .385 | .409 | .433 | .457 | .481 | .506 | .530 | .554 | .578 |
| $\frac{7}{8}$ | .398 | .423 | .448 | .473 | .498 | .523 | .548 | .573 | .598 |
| $\frac{15}{16}$ | .412 | .437 | .463 | .489 | .515 | .540 | .566 | .592 | .618 |
| $\frac{1}{2}$ | .425 | .452 | .478 | .505 | .531 | .558 | .584 | .611 | .638 |
| $\frac{3}{4}$ | .438 | .466 | .493 | .520 | .548 | .575 | .603 | .630 | .657 |
| $\frac{7}{8}$ | .452 | .480 | .508 | .536 | .564 | .593 | .621 | .649 | .677 |
| $\frac{15}{16}$ | .465 | .494 | .523 | .552 | .581 | .610 | .639 | .668 | .697 |
| $\frac{1}{2}$ | .478 | .508 | .538 | .567 | .598 | .628 | .657 | .687 | .717 |

WEIGHTS OF FLAT ROLLED STEEL BARS.

Pounds per Lineal Foot.

(CONTINUED.)

| Thickness in Inches. | $\frac{25}{64}$ " | $\frac{13}{32}$ " | $\frac{27}{64}$ " | $\frac{7}{16}$ " | $\frac{29}{64}$ " | $\frac{15}{32}$ " | $\frac{31}{64}$ " | $\frac{1}{2}$ " | 12" |
|-------------------------|-------------------|-------------------|-------------------|------------------|-------------------|-------------------|-------------------|-----------------|-------|
| $\frac{1}{16}$ | .083 | .086 | .090 | .093 | .096 | .100 | .103 | .106 | 2.55 |
| $\frac{5}{64}$ | .104 | .108 | .112 | .116 | .120 | .125 | .129 | .133 | 3.19 |
| $\frac{3}{32}$ | .125 | .129 | .134 | .139 | .144 | .149 | .154 | .159 | 3.83 |
| $\frac{7}{64}$ | .145 | .151 | .157 | .163 | .169 | .174 | .180 | .186 | 4.46 |
| $\frac{1}{8}$ | .166 | .173 | .179 | .186 | .193 | .199 | .206 | .212 | 5.10 |
| $\frac{9}{64}$ | .187 | .194 | .202 | .209 | .217 | .224 | .232 | .239 | 5.74 |
| $\frac{5}{32}$ | .208 | .216 | .224 | .232 | .241 | .249 | .257 | .266 | 6.38 |
| $\frac{11}{64}$ | .228 | .237 | .247 | .256 | .265 | .274 | .283 | .292 | 7.01 |
| $\frac{3}{16}$ | .249 | .259 | .269 | .279 | .289 | .299 | .309 | .319 | 7.65 |
| $\frac{13}{64}$ | .270 | .281 | .291 | .302 | .313 | .324 | .335 | .345 | 8.29 |
| $\frac{7}{32}$ | .291 | .302 | .314 | .325 | .337 | .349 | .360 | .372 | 8.93 |
| $\frac{15}{64}$ | .311 | .324 | .336 | .349 | .361 | .374 | .386 | .398 | 9.56 |
| $\frac{1}{4}$ | .332 | .345 | .359 | .372 | .385 | .398 | .412 | .425 | 10.20 |
| $\frac{17}{64}$ | .353 | .367 | .381 | .395 | .409 | .423 | .437 | .452 | 10.84 |
| $\frac{9}{32}$ | .374 | .388 | .403 | .418 | .433 | .448 | .463 | .478 | 11.48 |
| $\frac{19}{64}$ | .394 | .410 | .426 | .442 | .457 | .473 | .489 | .505 | 12.11 |
| $\frac{5}{16}$ | .415 | .432 | .448 | .465 | .481 | .498 | .515 | .531 | 12.75 |
| $\frac{21}{64}$ | .436 | .453 | .471 | .488 | .506 | .523 | .540 | .558 | 13.39 |
| $\frac{11}{32}$ | .457 | .475 | .493 | .511 | .530 | .548 | .566 | .584 | 14.03 |
| $\frac{23}{64}$ | .477 | .496 | .515 | .535 | .554 | .573 | .592 | .611 | 14.66 |
| $\frac{3}{8}$ | .498 | .518 | .538 | .558 | .578 | .598 | .618 | .638 | 15.30 |
| $\frac{25}{64}$ | .519 | .540 | .560 | .581 | .602 | .623 | .643 | .664 | 15.94 |
| $\frac{13}{32}$ | .540 | .561 | .583 | .604 | .626 | .647 | .669 | .691 | 16.58 |
| $\frac{27}{64}$ | .560 | .583 | .605 | .628 | .650 | .672 | .695 | .717 | 17.21 |
| $\frac{7}{16}$ | .581 | .604 | .628 | .651 | .674 | .697 | .721 | .744 | 17.85 |
| $\frac{29}{64}$ | .602 | .626 | .650 | .674 | .698 | .722 | .746 | .770 | 18.49 |
| $\frac{15}{32}$ | .623 | .647 | .672 | .697 | .722 | .747 | .772 | .797 | 19.13 |
| $\frac{31}{64}$ | .643 | .669 | .695 | .721 | .746 | .772 | .798 | .823 | 19.76 |
| $\frac{1}{2}$ | .664 | .691 | .717 | .744 | .770 | .797 | .823 | .850 | 20.40 |
| $\frac{33}{64}$ | .685 | .712 | .740 | .767 | .794 | .822 | .849 | .877 | 21.04 |
| $\frac{17}{32}$ | .706 | .734 | .762 | .790 | .818 | .847 | .875 | .903 | 21.68 |
| $\frac{35}{64}$ | .726 | .755 | .784 | .813 | .843 | .872 | .901 | .930 | 22.31 |
| $\frac{37}{64}$ | .747 | .777 | .807 | .837 | .867 | .896 | .926 | .956 | 22.95 |

WEIGHTS OF FLAT ROLLED STEEL BARS.

Pounds per Lineal Foot.

(CONTINUED.)

| Thickness in Inches. | $\frac{3}{8}$ " | $\frac{1}{2}$ " | $\frac{5}{8}$ " | $\frac{3}{4}$ " | $\frac{7}{8}$ " | $1\frac{1}{8}$ " | $1\frac{1}{4}$ " | $1\frac{1}{2}$ " | $1\frac{3}{4}$ " |
|-------------------------|-----------------|-----------------|-----------------|-----------------|-----------------|------------------|------------------|------------------|------------------|
| $\frac{1}{16}$ | .110 | .113 | .116 | .120 | .123 | .126 | .129 | .133 | 2.55 |
| $\frac{5}{64}$ | .137 | .141 | .145 | .149 | .154 | .158 | .162 | .166 | 3.19 |
| $\frac{3}{32}$ | .164 | .169 | .174 | .179 | .184 | .189 | .194 | .199 | 3.83 |
| $\frac{7}{64}$ | .192 | .198 | .203 | .209 | .215 | .221 | .227 | .232 | 4.46 |
| $\frac{1}{8}$ | .219 | .226 | .232 | .239 | .246 | .252 | .259 | .266 | 5.10 |
| $\frac{9}{64}$ | .247 | .254 | .261 | .269 | .276 | .284 | .291 | .299 | 5.74 |
| $\frac{5}{32}$ | .274 | .282 | .291 | .299 | .307 | .315 | .324 | .332 | 6.38 |
| $\frac{11}{64}$ | .301 | .310 | .320 | .329 | .338 | .347 | .356 | .365 | 7.01 |
| $\frac{3}{16}$ | .329 | .339 | .349 | .359 | .369 | .379 | .388 | .398 | 7.65 |
| $\frac{13}{64}$ | .356 | .367 | .378 | .388 | .399 | .410 | .421 | .432 | 8.29 |
| $\frac{7}{32}$ | .383 | .395 | .407 | .418 | .430 | .442 | .453 | .465 | 8.93 |
| $\frac{15}{64}$ | .411 | .423 | .436 | .448 | .461 | .473 | .486 | .498 | 9.56 |
| $\frac{1}{4}$ | .438 | .452 | .465 | .478 | .491 | .505 | .518 | .531 | 10.20 |
| $\frac{17}{64}$ | .466 | .480 | .494 | .508 | .522 | .536 | .550 | .564 | 10.84 |
| $\frac{9}{32}$ | .493 | .508 | .523 | .538 | .553 | .568 | .583 | .598 | 11.48 |
| $\frac{19}{64}$ | .520 | .536 | .552 | .568 | .584 | .599 | .615 | .631 | 12.11 |
| $\frac{5}{16}$ | .548 | .564 | .581 | .598 | .614 | .631 | .647 | .664 | 12.75 |
| $\frac{21}{64}$ | .575 | .593 | .610 | .628 | .645 | .662 | .680 | .697 | 13.39 |
| $\frac{11}{32}$ | .603 | .621 | .639 | .657 | .676 | .694 | .712 | .730 | 14.03 |
| $\frac{23}{64}$ | .630 | .649 | .668 | .687 | .706 | .725 | .745 | .764 | 14.66 |
| $\frac{3}{8}$ | .657 | .677 | .697 | .717 | .737 | .757 | .777 | .797 | 15.30 |
| $\frac{25}{64}$ | .685 | .706 | .726 | .747 | .768 | .789 | .809 | .830 | 15.94 |
| $\frac{13}{32}$ | .712 | .734 | .755 | .777 | .799 | .820 | .842 | .863 | 16.58 |
| $\frac{27}{64}$ | .740 | .762 | .784 | .807 | .829 | .852 | .874 | .896 | 17.21 |
| $\frac{7}{16}$ | .767 | .790 | .813 | .837 | .860 | .883 | .906 | .930 | 17.85 |
| $\frac{29}{64}$ | .794 | .818 | .843 | .867 | .891 | .915 | .939 | .963 | 18.49 |
| $\frac{15}{32}$ | .822 | .847 | .872 | .896 | .921 | .946 | .971 | .996 | 19.13 |
| $\frac{31}{64}$ | .849 | .875 | .901 | .926 | .952 | .978 | 1.00 | 1.03 | 19.76 |
| $\frac{1}{2}$ | .877 | .903 | .930 | .956 | .983 | 1.01 | 1.04 | 1.06 | 20.40 |
| $\frac{33}{64}$ | .904 | .931 | .959 | .986 | 1.01 | 1.04 | 1.07 | 1.10 | 21.04 |
| $\frac{17}{32}$ | .931 | .960 | .988 | 1.02 | 1.04 | 1.07 | 1.10 | 1.13 | 21.68 |
| $\frac{35}{64}$ | .959 | .988 | 1.02 | 1.05 | 1.07 | 1.10 | 1.13 | 1.16 | 22.31 |
| $\frac{3}{4}$ | .986 | 1.02 | 1.05 | 1.08 | 1.11 | 1.14 | 1.17 | 1.20 | 22.95 |

WEIGHTS OF FLAT ROLLED STEEL BARS.

Pounds per Lineal Foot.

(CONTINUED.)

| Thickness in Inches. | $\frac{1}{4}$ " | $\frac{3}{8}$ " | $\frac{1}{2}$ " | $\frac{5}{8}$ " | $\frac{3}{4}$ " | $\frac{7}{8}$ " | 1 " | $1\frac{1}{4}$ " |
|-------------------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-------|------------------|
| $\frac{1}{16}$ | .136 | .139 | .143 | .146 | .149 | .153 | .156 | .159 |
| $\frac{5}{64}$ | .170 | .174 | .178 | .183 | .187 | .191 | .195 | .199 |
| $\frac{3}{32}$ | .204 | .209 | .214 | .219 | .224 | .229 | .234 | .239 |
| $\frac{7}{64}$ | .238 | .244 | .250 | .256 | .261 | .267 | .273 | .279 |
| $\frac{1}{8}$ | .272 | .279 | .286 | .292 | .299 | .305 | .312 | .319 |
| $\frac{9}{64}$ | .306 | .314 | .321 | .329 | .336 | .344 | .351 | .359 |
| $\frac{5}{32}$ | .340 | .349 | .357 | .365 | .374 | .382 | .390 | .398 |
| $\frac{11}{64}$ | .374 | .383 | .393 | .402 | .411 | .420 | .429 | .438 |
| $\frac{3}{8}$ | .408 | .418 | .428 | .438 | .448 | .458 | .468 | .478 |
| $\frac{13}{64}$ | .442 | .453 | .464 | .475 | .486 | .496 | .507 | .518 |
| $\frac{7}{32}$ | .476 | .488 | .500 | .511 | .523 | .535 | .546 | .558 |
| $\frac{15}{64}$ | .510 | .523 | .535 | .548 | .560 | .573 | .585 | .598 |
| $\frac{1}{2}$ | .545 | .558 | .571 | .584 | .598 | .611 | .624 | .638 |
| $\frac{17}{64}$ | .579 | .593 | .607 | .621 | .635 | .649 | .663 | .677 |
| $\frac{9}{32}$ | .613 | .628 | .642 | .657 | .672 | .687 | .702 | .717 |
| $\frac{19}{64}$ | .647 | .662 | .678 | .694 | .710 | .725 | .741 | .757 |
| $\frac{5}{8}$ | .681 | .697 | .714 | .730 | .747 | .764 | .780 | .797 |
| $\frac{21}{64}$ | .715 | .732 | .750 | .767 | .784 | .802 | .819 | .827 |
| $\frac{11}{32}$ | .749 | .767 | .785 | .804 | .822 | .840 | .858 | .877 |
| $\frac{23}{64}$ | .783 | .802 | .821 | .840 | .859 | .878 | .897 | .916 |
| $\frac{3}{4}$ | .817 | .837 | .857 | .877 | .896 | .916 | .936 | .956 |
| $\frac{25}{64}$ | .851 | .872 | .892 | .913 | .934 | .955 | .975 | .996 |
| $\frac{13}{32}$ | .885 | .906 | .928 | .950 | .971 | .993 | 1.01 | 1.04 |
| $\frac{27}{64}$ | .919 | .941 | .964 | .986 | 1.01 | 1.03 | 1.05 | 1.08 |
| $\frac{7}{8}$ | .953 | .976 | .999 | 1.02 | 1.05 | 1.07 | 1.09 | 1.12 |
| $\frac{29}{64}$ | .987 | 1.01 | 1.04 | 1.06 | 1.08 | 1.11 | 1.13 | 1.16 |
| $\frac{15}{32}$ | 1.02 | 1.05 | 1.07 | 1.10 | 1.12 | 1.15 | 1.17 | 1.20 |
| $\frac{31}{64}$ | 1.06 | 1.08 | 1.11 | 1.13 | 1.16 | 1.18 | 1.21 | 1.24 |
| $1\frac{1}{8}$ | 1.09 | 1.12 | 1.14 | 1.17 | 1.20 | 1.22 | 1.25 | 1.28 |
| $\frac{33}{64}$ | 1.12 | 1.15 | 1.18 | 1.21 | 1.23 | 1.26 | 1.29 | 1.31 |
| $\frac{17}{32}$ | 1.16 | 1.19 | 1.21 | 1.24 | 1.27 | 1.30 | 1.33 | 1.35 |
| $\frac{35}{64}$ | 1.19 | 1.22 | 1.25 | 1.28 | 1.31 | 1.34 | 1.37 | 1.39 |
| $1\frac{1}{4}$ | 1.23 | 1.26 | 1.28 | 1.31 | 1.34 | 1.37 | 1.40 | 1.43 |

WEIGHTS OF FLAT ROLLED STEEL BARS.

Pounds per Lineal Foot.

(CONTINUED.)

| Thickness in Inches. | $\frac{49}{64}$ " | $\frac{25}{32}$ " | $\frac{51}{64}$ " | $\frac{13}{16}$ " | $\frac{53}{64}$ " | $\frac{27}{32}$ " | $\frac{55}{64}$ " | $\frac{7}{8}$ " | 12" |
|-------------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-----------------|-------|
| $\frac{1}{16}$ | .163 | .166 | .169 | .173 | .176 | .179 | .183 | .186 | 2.55 |
| $\frac{5}{64}$ | .203 | .208 | .212 | .216 | .220 | .224 | .228 | .232 | 3.19 |
| $\frac{3}{32}$ | .244 | .249 | .254 | .259 | .264 | .269 | .274 | .279 | 3.83 |
| $\frac{7}{64}$ | .285 | .291 | .296 | .302 | .308 | .314 | .320 | .325 | 4.46 |
| $\frac{1}{8}$ | .325 | .332 | .339 | .345 | .352 | .359 | .365 | .372 | 5.10 |
| $\frac{9}{64}$ | .366 | .374 | .381 | .388 | .396 | .403 | .411 | .418 | 5.74 |
| $\frac{5}{32}$ | .407 | .415 | .423 | .432 | .440 | .448 | .457 | .465 | 6.38 |
| $\frac{11}{64}$ | .447 | .457 | .466 | .475 | .484 | .493 | .502 | .511 | 7.01 |
| $\frac{3}{16}$ | .488 | .498 | .508 | .518 | .528 | .538 | .548 | .558 | 7.65 |
| $\frac{13}{64}$ | .529 | .540 | .550 | .561 | .572 | .583 | .594 | .604 | 8.29 |
| $\frac{7}{32}$ | .569 | .581 | .593 | .604 | .616 | .628 | .639 | .651 | 8.93 |
| $\frac{15}{64}$ | .610 | .623 | .635 | .647 | .660 | .672 | .685 | .697 | 9.56 |
| $\frac{1}{4}$ | .651 | .664 | .677 | .691 | .704 | .717 | .730 | .744 | 10.20 |
| $\frac{17}{64}$ | .691 | .706 | .720 | .734 | .748 | .762 | .776 | .790 | 10.84 |
| $\frac{9}{32}$ | .732 | .747 | .762 | .777 | .792 | .807 | .822 | .837 | 11.48 |
| $\frac{19}{64}$ | .773 | .789 | .804 | .820 | .836 | .852 | .867 | .883 | 12.11 |
| $\frac{5}{16}$ | .813 | .830 | .847 | .863 | .880 | .897 | .913 | .930 | 12.75 |
| $\frac{21}{64}$ | .854 | .872 | .889 | .906 | .924 | .941 | .959 | .976 | 13.39 |
| $\frac{11}{32}$ | .895 | .913 | .931 | .950 | .968 | .986 | 1.00 | 1.02 | 14.03 |
| $\frac{23}{64}$ | .936 | .955 | .974 | .993 | 1.01 | 1.03 | 1.05 | 1.07 | 14.66 |
| $\frac{3}{8}$ | .976 | .996 | 1.02 | 1.04 | 1.06 | 1.08 | 1.10 | 1.12 | 15.30 |
| $\frac{25}{64}$ | 1.02 | 1.04 | 1.06 | 1.08 | 1.10 | 1.12 | 1.14 | 1.16 | 15.94 |
| $\frac{13}{32}$ | 1.06 | 1.08 | 1.10 | 1.12 | 1.14 | 1.17 | 1.19 | 1.21 | 16.58 |
| $\frac{27}{64}$ | 1.10 | 1.12 | 1.14 | 1.17 | 1.19 | 1.21 | 1.23 | 1.26 | 17.21 |
| $\frac{7}{16}$ | 1.14 | 1.16 | 1.19 | 1.21 | 1.23 | 1.26 | 1.28 | 1.30 | 17.85 |
| $\frac{29}{64}$ | 1.18 | 1.20 | 1.23 | 1.25 | 1.28 | 1.30 | 1.32 | 1.35 | 18.49 |
| $\frac{15}{32}$ | 1.22 | 1.25 | 1.27 | 1.30 | 1.32 | 1.35 | 1.37 | 1.40 | 19.13 |
| $\frac{31}{64}$ | 1.26 | 1.29 | 1.31 | 1.34 | 1.36 | 1.39 | 1.42 | 1.44 | 19.76 |
| $\frac{1}{2}$ | 1.30 | 1.33 | 1.35 | 1.38 | 1.41 | 1.43 | 1.46 | 1.49 | 20.40 |
| $\frac{33}{64}$ | 1.34 | 1.37 | 1.40 | 1.42 | 1.45 | 1.48 | 1.51 | 1.53 | 21.04 |
| $\frac{17}{32}$ | 1.38 | 1.41 | 1.44 | 1.47 | 1.50 | 1.52 | 1.55 | 1.58 | 21.68 |
| $\frac{35}{64}$ | 1.42 | 1.45 | 1.48 | 1.51 | 1.54 | 1.57 | 1.60 | 1.63 | 22.31 |
| $\frac{9}{16}$ | 1.46 | 1.49 | 1.52 | 1.55 | 1.58 | 1.61 | 1.64 | 1.67 | 22.95 |

WEIGHTS OF FLAT ROLLED STEEL BARS.

Pounds per Lineal Foot.

(CONTINUED.)

| Thickness in Inches. | $\frac{5}{16}$ " | $\frac{3}{8}$ " | $\frac{7}{16}$ " | $\frac{1}{2}$ " | $\frac{9}{16}$ " | $\frac{5}{8}$ " | $\frac{3}{4}$ " | 1" | 12" |
|-------------------------|------------------|-----------------|------------------|-----------------|------------------|-----------------|-----------------|------|-------|
| $\frac{1}{16}$ | .189 | .193 | .196 | .199 | .203 | .206 | .209 | .213 | 2.55 |
| $\frac{5}{64}$ | .237 | .241 | .245 | .249 | .253 | .257 | .262 | .266 | 3.19 |
| $\frac{3}{32}$ | .284 | .289 | .294 | .299 | .304 | .309 | .314 | .319 | 3.83 |
| $\frac{7}{64}$ | .331 | .337 | .343 | .349 | .354 | .360 | .366 | .372 | 4.46 |
| $\frac{1}{8}$ | .379 | .385 | .392 | .398 | .405 | .412 | .418 | .425 | 5.10 |
| $\frac{9}{64}$ | .426 | .433 | .441 | .448 | .456 | .463 | .471 | .478 | 5.74 |
| $\frac{5}{32}$ | .473 | .481 | .490 | .498 | .506 | .515 | .523 | .531 | 6.38 |
| $\frac{11}{64}$ | .520 | .529 | .538 | .548 | .557 | .566 | .575 | .584 | 7.01 |
| $\frac{3}{16}$ | .568 | .578 | .588 | .598 | .608 | .618 | .628 | .638 | 7.65 |
| $\frac{13}{64}$ | .615 | .626 | .637 | .648 | .658 | .669 | .680 | .691 | 8.29 |
| $\frac{7}{32}$ | .662 | .674 | .686 | .697 | .709 | .721 | .732 | .744 | 8.93 |
| $\frac{15}{64}$ | .710 | .722 | .735 | .747 | .760 | .772 | .784 | .797 | 9.56 |
| $\frac{1}{4}$ | .757 | .770 | .784 | .797 | .810 | .823 | .837 | .850 | 10.20 |
| $\frac{17}{64}$ | .804 | .818 | .833 | .847 | .861 | .875 | .889 | .903 | 10.84 |
| $\frac{9}{32}$ | .852 | .867 | .882 | .896 | .911 | .926 | .941 | .956 | 11.48 |
| $\frac{19}{64}$ | .899 | .915 | .931 | .946 | .962 | .978 | .994 | 1.01 | 12.11 |
| $\frac{5}{16}$ | .946 | .963 | .980 | .996 | 1.01 | 1.03 | 1.05 | 1.06 | 12.75 |
| $\frac{21}{64}$ | .994 | 1.01 | 1.03 | 1.05 | 1.06 | 1.08 | 1.10 | 1.12 | 13.39 |
| $\frac{11}{32}$ | 1.04 | 1.06 | 1.08 | 1.10 | 1.11 | 1.13 | 1.15 | 1.17 | 14.03 |
| $\frac{23}{64}$ | 1.09 | 1.11 | 1.13 | 1.15 | 1.17 | 1.18 | 1.20 | 1.22 | 14.66 |
| $\frac{3}{8}$ | 1.14 | 1.16 | 1.18 | 1.20 | 1.22 | 1.24 | 1.26 | 1.28 | 15.30 |
| $\frac{25}{64}$ | 1.18 | 1.20 | 1.22 | 1.25 | 1.27 | 1.29 | 1.31 | 1.33 | 15.94 |
| $\frac{13}{32}$ | 1.23 | 1.25 | 1.27 | 1.30 | 1.32 | 1.34 | 1.36 | 1.38 | 16.58 |
| $\frac{27}{64}$ | 1.28 | 1.30 | 1.32 | 1.35 | 1.37 | 1.39 | 1.41 | 1.43 | 17.21 |
| $\frac{7}{16}$ | 1.33 | 1.35 | 1.37 | 1.40 | 1.42 | 1.44 | 1.46 | 1.49 | 17.85 |
| $\frac{29}{64}$ | 1.37 | 1.40 | 1.42 | 1.44 | 1.47 | 1.49 | 1.52 | 1.54 | 18.49 |
| $\frac{15}{32}$ | 1.42 | 1.44 | 1.47 | 1.49 | 1.52 | 1.54 | 1.57 | 1.59 | 19.13 |
| $\frac{31}{64}$ | 1.47 | 1.49 | 1.52 | 1.54 | 1.57 | 1.60 | 1.62 | 1.65 | 19.76 |
| $\frac{1}{2}$ | 1.51 | 1.54 | 1.57 | 1.59 | 1.62 | 1.65 | 1.67 | 1.70 | 20.40 |
| $\frac{33}{64}$ | 1.56 | 1.59 | 1.62 | 1.64 | 1.67 | 1.70 | 1.73 | 1.75 | 21.04 |
| $\frac{17}{32}$ | 1.61 | 1.64 | 1.67 | 1.69 | 1.72 | 1.75 | 1.78 | 1.81 | 21.68 |
| $\frac{35}{64}$ | 1.66 | 1.69 | 1.71 | 1.74 | 1.77 | 1.80 | 1.83 | 1.86 | 22.31 |
| $\frac{9}{16}$ | 1.70 | 1.73 | 1.76 | 1.79 | 1.82 | 1.85 | 1.88 | 1.91 | 22.95 |

WEIGHTS OF FLAT ROLLED STEEL BARS.

Pounds per Lineal Foot.

One cubic foot of steel weighs 489.6 pounds.

For Thicknesses from $\frac{1}{16}$ in. to 2 ins. and Widths from 1 in. to $12\frac{3}{4}$ ins.

| Thickness in Inches. | 1" | 1 $\frac{1}{4}$ " | 1 $\frac{1}{2}$ " | 1 $\frac{3}{4}$ " | 2" | 2 $\frac{1}{4}$ " | 2 $\frac{1}{2}$ " | 2 $\frac{3}{4}$ " | 12" |
|-------------------------|------|-------------------|-------------------|-------------------|-------|-------------------|-------------------|-------------------|-------|
| $\frac{1}{16}$ | .213 | .266 | .319 | .372 | .425 | .478 | .531 | .584 | 2.55 |
| $\frac{1}{8}$ | .425 | .531 | .638 | .744 | .850 | .956 | 1.06 | 1.17 | 5.10 |
| $\frac{3}{16}$ | .638 | .797 | .956 | 1.12 | 1.28 | 1.43 | 1.59 | 1.75 | 7.65 |
| $\frac{1}{4}$ | .850 | 1.06 | 1.28 | 1.49 | 1.70 | 1.91 | 2.13 | 2.34 | 10.20 |
| $\frac{5}{16}$ | 1.06 | 1.33 | 1.59 | 1.86 | 2.13 | 2.39 | 2.66 | 2.92 | 12.75 |
| $\frac{3}{8}$ | 1.28 | 1.59 | 1.91 | 2.23 | 2.55 | 2.87 | 3.19 | 3.51 | 15.30 |
| $\frac{7}{16}$ | 1.49 | 1.86 | 2.23 | 2.60 | 2.98 | 3.35 | 3.72 | 4.09 | 17.85 |
| $\frac{1}{2}$ | 1.70 | 2.13 | 2.55 | 2.98 | 3.40 | 3.83 | 4.25 | 4.68 | 20.40 |
| $\frac{9}{16}$ | 1.91 | 2.39 | 2.87 | 3.35 | 3.83 | 4.30 | 4.78 | 5.26 | 22.95 |
| $\frac{5}{8}$ | 2.13 | 2.66 | 3.19 | 3.72 | 4.25 | 4.78 | 5.31 | 5.84 | 25.50 |
| $\frac{11}{16}$ | 2.34 | 2.92 | 3.51 | 4.09 | 4.68 | 5.26 | 5.84 | 6.43 | 28.05 |
| $\frac{3}{4}$ | 2.55 | 3.19 | 3.83 | 4.46 | 5.10 | 5.74 | 6.38 | 7.01 | 30.60 |
| $\frac{13}{16}$ | 2.76 | 3.45 | 4.14 | 4.83 | 5.53 | 6.22 | 6.91 | 7.60 | 33.15 |
| $\frac{7}{8}$ | 2.98 | 3.72 | 4.46 | 5.21 | 5.95 | 6.69 | 7.44 | 8.18 | 35.70 |
| $\frac{15}{16}$ | 3.19 | 3.98 | 4.78 | 5.58 | 6.38 | 7.17 | 7.97 | 8.77 | 38.25 |
| 1 | 3.40 | 4.25 | 5.10 | 5.95 | 6.80 | 7.65 | 8.50 | 9.35 | 40.80 |
| 1 $\frac{1}{16}$ | 3.61 | 4.52 | 5.42 | 6.32 | 7.23 | 8.13 | 9.03 | 9.93 | 43.35 |
| 1 $\frac{1}{8}$ | 3.83 | 4.78 | 5.74 | 6.69 | 7.65 | 8.61 | 9.56 | 10.52 | 45.90 |
| 1 $\frac{1}{16}$ | 4.04 | 5.05 | 6.06 | 7.07 | 8.08 | 9.08 | 10.09 | 11.10 | 48.45 |
| 1 $\frac{1}{4}$ | 4.25 | 5.31 | 6.38 | 7.44 | 8.50 | 9.56 | 10.63 | 11.69 | 51.00 |
| 1 $\frac{5}{16}$ | 4.46 | 5.58 | 6.69 | 7.81 | 8.93 | 10.04 | 11.16 | 12.27 | 53.55 |
| 1 $\frac{3}{8}$ | 4.68 | 5.84 | 7.01 | 8.18 | 9.35 | 10.52 | 11.69 | 12.86 | 56.10 |
| 1 $\frac{7}{16}$ | 4.89 | 6.11 | 7.33 | 8.55 | 9.78 | 11.00 | 12.22 | 13.44 | 58.65 |
| 1 $\frac{1}{2}$ | 5.10 | 6.38 | 7.65 | 8.93 | 10.20 | 11.48 | 12.75 | 14.03 | 61.20 |
| 1 $\frac{9}{16}$ | 5.31 | 6.64 | 7.97 | 9.30 | 10.63 | 11.95 | 13.28 | 14.61 | 63.75 |
| 1 $\frac{5}{8}$ | 5.53 | 6.91 | 8.29 | 9.67 | 11.05 | 12.43 | 13.81 | 15.19 | 66.30 |
| 1 $\frac{11}{16}$ | 5.74 | 7.17 | 8.61 | 10.04 | 11.48 | 12.91 | 14.34 | 15.78 | 68.85 |
| 1 $\frac{3}{4}$ | 5.95 | 7.44 | 8.93 | 10.41 | 11.90 | 13.39 | 14.88 | 16.36 | 71.40 |
| 1 $\frac{13}{16}$ | 6.16 | 7.70 | 9.24 | 10.78 | 12.33 | 13.87 | 15.41 | 16.95 | 73.95 |
| 1 $\frac{7}{8}$ | 6.38 | 7.97 | 9.56 | 11.16 | 12.75 | 14.34 | 15.94 | 17.53 | 76.50 |
| 1 $\frac{15}{16}$ | 6.59 | 8.23 | 9.88 | 11.53 | 13.18 | 14.82 | 16.47 | 18.12 | 79.05 |
| 2 | 6.80 | 8.50 | 10.20 | 11.90 | 13.60 | 15.30 | 17.00 | 18.70 | 81.60 |

WEIGHTS OF FLAT ROLLED STEEL BARS.

Pounds per Lineal Foot.

(CONTINUED.)

| Thickness in Inches. | 3" | 3½" | 3½" | 3¾" | 4" | 4½" | 4½" | 4¾" | 12" |
|-------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| $\frac{1}{16}$ | .638 | .691 | .744 | .797 | .850 | .903 | .956 | 1.01 | 2.55 |
| $\frac{1}{8}$ | 1.28 | 1.38 | 1.49 | 1.59 | 1.70 | 1.81 | 1.91 | 2.20 | 5.10 |
| $\frac{1}{4}$ | 1.91 | 2.07 | 2.23 | 2.39 | 2.55 | 2.71 | 2.87 | 3.03 | 7.65 |
| $\frac{3}{8}$ | 2.55 | 2.76 | 2.98 | 3.19 | 3.40 | 3.61 | 3.83 | 4.04 | 10.20 |
| $\frac{5}{16}$ | 3.19 | 3.45 | 3.72 | 3.98 | 4.25 | 4.52 | 4.78 | 5.05 | 12.75 |
| $\frac{3}{8}$ | 3.83 | 4.14 | 4.46 | 4.78 | 5.10 | 5.42 | 5.74 | 6.06 | 15.30 |
| $\frac{7}{16}$ | 4.46 | 4.83 | 5.21 | 5.58 | 5.95 | 6.32 | 6.69 | 7.07 | 17.85 |
| $\frac{1}{2}$ | 5.10 | 5.53 | 5.95 | 6.38 | 6.80 | 7.22 | 7.65 | 8.08 | 20.40 |
| $\frac{9}{16}$ | 5.74 | 6.22 | 6.69 | 7.17 | 7.65 | 8.13 | 8.61 | 9.08 | 22.95 |
| $\frac{5}{8}$ | 6.38 | 6.91 | 7.44 | 7.97 | 8.50 | 9.03 | 9.56 | 10.09 | 25.50 |
| $\frac{11}{16}$ | 7.01 | 7.60 | 8.18 | 8.77 | 9.35 | 9.93 | 10.52 | 11.10 | 28.05 |
| $\frac{3}{4}$ | 7.65 | 8.29 | 8.93 | 9.56 | 10.20 | 10.84 | 11.48 | 12.11 | 30.60 |
| $\frac{13}{16}$ | 8.29 | 8.98 | 9.67 | 10.36 | 11.05 | 11.74 | 12.43 | 13.12 | 33.15 |
| $\frac{7}{8}$ | 8.93 | 9.67 | 10.41 | 11.16 | 11.90 | 12.64 | 13.39 | 14.13 | 35.70 |
| $\frac{15}{16}$ | 9.56 | 10.36 | 11.16 | 11.95 | 12.75 | 13.55 | 14.34 | 15.14 | 38.25 |
| 1 | 10.20 | 11.05 | 11.90 | 12.75 | 13.60 | 14.45 | 15.30 | 16.15 | 40.80 |
| $1\frac{1}{16}$ | 10.84 | 11.74 | 12.64 | 13.55 | 14.45 | 15.35 | 16.26 | 17.16 | 43.35 |
| $1\frac{1}{8}$ | 11.48 | 12.43 | 13.39 | 14.34 | 15.30 | 16.26 | 17.21 | 18.17 | 45.90 |
| $1\frac{3}{16}$ | 12.11 | 13.12 | 14.13 | 15.14 | 16.15 | 17.16 | 18.17 | 19.18 | 48.45 |
| $1\frac{1}{4}$ | 12.75 | 13.81 | 14.88 | 15.94 | 17.00 | 18.06 | 19.13 | 20.19 | 51.00 |
| $1\frac{5}{16}$ | 13.39 | 14.50 | 15.62 | 16.73 | 17.85 | 18.97 | 20.08 | 21.20 | 53.55 |
| $1\frac{3}{8}$ | 14.03 | 15.19 | 16.36 | 17.53 | 18.70 | 19.87 | 21.04 | 22.21 | 56.10 |
| $1\frac{7}{16}$ | 14.66 | 15.88 | 17.11 | 18.33 | 19.55 | 20.77 | 21.99 | 23.22 | 58.65 |
| $1\frac{1}{2}$ | 15.30 | 16.58 | 17.85 | 19.13 | 20.40 | 21.68 | 22.95 | 24.23 | 61.20 |
| $1\frac{9}{16}$ | 15.92 | 17.27 | 18.59 | 19.92 | 21.25 | 22.58 | 23.91 | 25.23 | 63.75 |
| $1\frac{5}{8}$ | 16.58 | 17.96 | 19.34 | 20.72 | 22.10 | 23.48 | 24.86 | 26.24 | 66.30 |
| $1\frac{11}{16}$ | 17.21 | 18.65 | 20.08 | 21.52 | 22.95 | 24.38 | 25.82 | 27.25 | 68.85 |
| $1\frac{3}{4}$ | 17.85 | 19.34 | 20.83 | 22.31 | 23.80 | 25.29 | 26.78 | 28.26 | 71.40 |
| $1\frac{13}{16}$ | 18.49 | 20.03 | 21.57 | 23.11 | 24.65 | 26.19 | 27.73 | 29.27 | 73.95 |
| $1\frac{7}{8}$ | 19.13 | 20.72 | 22.31 | 23.91 | 25.50 | 27.09 | 28.69 | 30.28 | 76.50 |
| $1\frac{15}{16}$ | 19.76 | 21.41 | 23.06 | 24.70 | 26.35 | 28.00 | 29.64 | 31.29 | 79.05 |
| 2 | 20.40 | 22.10 | 23.80 | 25.50 | 27.20 | 28.90 | 30.60 | 32.30 | 81.60 |

WEIGHTS OF FLAT ROLLED STEEL BARS.

Pounds per Lineal Foot.

(CONTINUED.)

| Thickness in Inches. | 5" | 5½" | 5½" | 5¾" | 6" | 6½" | 6½" | 6¾" | 12" |
|-------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| $\frac{1}{16}$ | 1.06 | 1.12 | 1.17 | 1.22 | 1.28 | 1.33 | 1.38 | 1.43 | 2.55 |
| $\frac{3}{16}$ | 2.13 | 2.23 | 2.34 | 2.44 | 2.55 | 2.66 | 2.76 | 2.87 | 5.10 |
| $\frac{1}{8}$ | 3.19 | 3.35 | 3.51 | 3.67 | 3.83 | 3.98 | 4.14 | 4.30 | 7.65 |
| $\frac{5}{16}$ | 4.25 | 4.46 | 4.68 | 4.89 | 5.10 | 5.31 | 5.53 | 5.74 | 10.20 |
| $\frac{3}{8}$ | 5.31 | 5.58 | 5.84 | 6.11 | 6.38 | 6.64 | 6.91 | 7.17 | 12.75 |
| $\frac{7}{16}$ | 6.38 | 6.69 | 7.01 | 7.33 | 7.65 | 7.97 | 8.29 | 8.61 | 15.30 |
| $\frac{1}{2}$ | 7.44 | 7.81 | 8.18 | 8.55 | 8.93 | 9.30 | 9.67 | 10.04 | 17.85 |
| | 8.50 | 8.93 | 9.35 | 9.78 | 10.20 | 10.63 | 11.05 | 11.48 | 20.40 |
| $\frac{9}{16}$ | 9.56 | 10.04 | 10.52 | 11.00 | 11.48 | 11.95 | 12.43 | 12.91 | 22.95 |
| $\frac{5}{8}$ | 10.63 | 11.16 | 11.69 | 12.22 | 12.75 | 13.28 | 13.81 | 14.34 | 25.50 |
| $\frac{11}{16}$ | 11.69 | 12.27 | 12.86 | 13.44 | 14.03 | 14.61 | 15.19 | 15.78 | 28.05 |
| $\frac{3}{4}$ | 12.75 | 13.39 | 14.03 | 14.67 | 15.30 | 15.94 | 16.58 | 17.21 | 30.60 |
| $1\frac{1}{16}$ | 13.81 | 14.50 | 15.19 | 15.88 | 16.58 | 17.27 | 17.96 | 18.65 | 33.15 |
| $1\frac{1}{8}$ | 14.88 | 15.62 | 16.36 | 17.11 | 17.85 | 18.59 | 19.34 | 20.08 | 35.70 |
| $1\frac{3}{16}$ | 15.94 | 16.73 | 17.53 | 18.33 | 19.13 | 19.92 | 20.72 | 21.52 | 38.25 |
| 1 | 17.00 | 17.85 | 18.70 | 19.55 | 20.40 | 21.25 | 22.10 | 22.95 | 40.80 |
| $1\frac{1}{16}$ | 18.06 | 18.97 | 19.87 | 20.77 | 21.68 | 22.58 | 23.48 | 24.38 | 43.35 |
| $1\frac{1}{8}$ | 19.13 | 20.08 | 21.04 | 21.99 | 22.95 | 23.91 | 24.86 | 25.82 | 45.90 |
| $1\frac{3}{16}$ | 20.19 | 21.20 | 22.21 | 23.22 | 24.23 | 25.23 | 26.24 | 27.25 | 48.45 |
| $1\frac{1}{4}$ | 21.25 | 22.31 | 23.38 | 24.44 | 25.50 | 26.56 | 27.63 | 28.69 | 51.00 |
| $1\frac{5}{16}$ | 22.31 | 23.43 | 24.54 | 25.66 | 26.78 | 27.89 | 29.01 | 30.12 | 53.55 |
| $1\frac{3}{8}$ | 23.38 | 24.54 | 25.71 | 26.88 | 28.05 | 29.22 | 30.39 | 31.56 | 56.10 |
| $1\frac{7}{16}$ | 24.44 | 25.66 | 26.88 | 28.10 | 29.33 | 30.55 | 31.77 | 32.99 | 58.65 |
| $1\frac{1}{2}$ | 25.50 | 26.78 | 28.05 | 29.33 | 30.60 | 31.88 | 33.15 | 34.43 | 61.20 |
| $1\frac{9}{16}$ | 26.56 | 27.89 | 29.22 | 30.55 | 31.88 | 33.20 | 34.53 | 35.86 | 63.75 |
| $1\frac{5}{8}$ | 27.63 | 29.01 | 30.39 | 31.77 | 33.15 | 34.53 | 35.91 | 37.29 | 66.30 |
| $1\frac{11}{16}$ | 28.69 | 30.12 | 31.56 | 32.99 | 34.43 | 35.86 | 37.29 | 38.73 | 68.85 |
| $1\frac{3}{4}$ | 29.75 | 31.24 | 32.73 | 34.21 | 35.70 | 37.19 | 38.68 | 40.16 | 71.40 |
| $1\frac{13}{16}$ | 30.81 | 32.35 | 33.89 | 35.43 | 36.98 | 38.52 | 40.06 | 41.60 | 73.95 |
| $1\frac{7}{8}$ | 31.88 | 33.47 | 35.06 | 36.66 | 38.25 | 39.84 | 41.44 | 43.03 | 76.50 |
| $1\frac{15}{16}$ | 32.94 | 34.58 | 36.23 | 37.88 | 39.53 | 41.17 | 42.82 | 44.47 | 79.05 |
| 2 | 34.00 | 35.70 | 37.40 | 39.10 | 40.80 | 42.50 | 44.20 | 45.90 | 81.60 |

WEIGHTS OF FLAT ROLLED STEEL BARS.

Pounds per Lineal Foot.

(CONTINUED.)

| Thickness in Inches. | 7" | 7 $\frac{1}{4}$ " | 7 $\frac{1}{2}$ " | 7 $\frac{3}{4}$ " | 8" | 8 $\frac{1}{4}$ " | 8 $\frac{1}{2}$ " | 8 $\frac{3}{4}$ " | 12" |
|-------------------------|-------|-------------------|-------------------|-------------------|-------|-------------------|-------------------|-------------------|-------|
| $\frac{1}{16}$ | 1.49 | 1.54 | 1.59 | 1.65 | 1.70 | 1.75 | 1.81 | 1.86 | 2.55 |
| $\frac{1}{8}$ | 2.98 | 3.08 | 3.19 | 3.29 | 3.40 | 3.51 | 3.61 | 3.72 | 5.10 |
| $\frac{3}{16}$ | 4.46 | 4.62 | 4.78 | 4.94 | 5.10 | 5.26 | 5.42 | 5.58 | 7.65 |
| $\frac{1}{4}$ | 5.95 | 6.16 | 6.38 | 6.59 | 6.80 | 7.01 | 7.23 | 7.44 | 10.20 |
| $\frac{5}{16}$ | 7.44 | 7.70 | 7.97 | 8.23 | 8.50 | 8.77 | 9.03 | 9.30 | 12.75 |
| $\frac{3}{8}$ | 8.93 | 9.24 | 9.56 | 9.88 | 10.20 | 10.52 | 10.84 | 11.16 | 15.30 |
| $\frac{7}{16}$ | 10.41 | 10.78 | 11.16 | 11.53 | 11.90 | 12.27 | 12.64 | 13.02 | 17.85 |
| $\frac{1}{2}$ | 11.90 | 12.33 | 12.75 | 13.18 | 13.60 | 14.03 | 14.45 | 14.88 | 20.40 |
| $\frac{9}{16}$ | 13.39 | 13.87 | 14.34 | 14.82 | 15.30 | 15.78 | 16.26 | 16.73 | 22.95 |
| $\frac{5}{8}$ | 14.88 | 15.41 | 15.94 | 16.47 | 17.00 | 17.53 | 18.06 | 18.59 | 25.50 |
| $\frac{11}{16}$ | 16.36 | 16.95 | 17.53 | 18.12 | 18.70 | 19.28 | 19.87 | 20.45 | 28.05 |
| $\frac{3}{4}$ | 17.85 | 18.49 | 19.13 | 19.76 | 20.40 | 21.04 | 21.68 | 22.31 | 30.60 |
| $\frac{13}{16}$ | 19.34 | 20.03 | 20.72 | 21.41 | 22.10 | 22.79 | 23.48 | 24.17 | 33.15 |
| $\frac{7}{8}$ | 20.83 | 21.57 | 22.31 | 23.06 | 23.80 | 24.54 | 25.29 | 26.03 | 35.70 |
| $\frac{15}{16}$ | 22.31 | 23.11 | 23.91 | 24.70 | 25.50 | 26.30 | 27.09 | 27.89 | 38.25 |
| 1 | 23.80 | 24.65 | 25.50 | 26.35 | 27.20 | 28.05 | 28.90 | 29.75 | 40.80 |
| $1\frac{1}{16}$ | 25.29 | 26.19 | 27.09 | 28.00 | 28.90 | 29.80 | 30.71 | 31.61 | 43.35 |
| $1\frac{1}{8}$ | 26.78 | 27.73 | 28.69 | 29.64 | 30.60 | 31.56 | 32.51 | 33.47 | 45.90 |
| $1\frac{1}{4}$ | 28.26 | 29.27 | 30.28 | 31.29 | 32.30 | 33.31 | 34.32 | 35.33 | 48.45 |
| $1\frac{1}{2}$ | 29.75 | 30.81 | 31.88 | 32.94 | 34.00 | 35.06 | 36.13 | 37.19 | 51.00 |
| $1\frac{5}{16}$ | 31.24 | 32.35 | 33.47 | 34.58 | 35.70 | 36.82 | 37.93 | 39.05 | 53.55 |
| $1\frac{3}{8}$ | 32.73 | 33.89 | 35.05 | 36.23 | 37.40 | 38.57 | 39.74 | 40.91 | 56.10 |
| $1\frac{7}{16}$ | 34.21 | 35.43 | 36.66 | 37.88 | 39.10 | 40.32 | 41.54 | 42.77 | 58.65 |
| $1\frac{1}{2}$ | 35.70 | 36.98 | 38.25 | 39.53 | 40.80 | 42.08 | 43.35 | 44.63 | 61.20 |
| $1\frac{9}{16}$ | 37.19 | 38.52 | 39.84 | 41.17 | 42.50 | 43.83 | 45.16 | 46.48 | 63.75 |
| $1\frac{5}{8}$ | 38.68 | 40.06 | 41.44 | 42.82 | 44.20 | 45.58 | 46.96 | 48.34 | 66.30 |
| $1\frac{11}{16}$ | 40.16 | 41.60 | 43.03 | 44.47 | 45.90 | 47.33 | 48.77 | 50.20 | 68.85 |
| $1\frac{3}{4}$ | 41.65 | 43.14 | 44.63 | 46.11 | 47.60 | 49.09 | 50.58 | 52.06 | 71.40 |
| $1\frac{13}{16}$ | 43.14 | 44.68 | 46.22 | 47.76 | 49.30 | 50.84 | 52.38 | 53.92 | 73.95 |
| $1\frac{7}{8}$ | 44.63 | 46.22 | 47.81 | 49.41 | 51.00 | 52.59 | 54.19 | 55.78 | 76.50 |
| $1\frac{15}{16}$ | 46.11 | 47.76 | 49.41 | 51.05 | 52.70 | 54.35 | 55.99 | 57.64 | 79.05 |
| 2 | 47.60 | 49.30 | 51.00 | 52.70 | 54.40 | 56.10 | 57.80 | 59.50 | 81.60 |

WEIGHTS OF FLAT ROLLED STEEL BARS.

Pounds per Lineal Foot.

(CONTINUED.)

| Thickness in Inches. | 9" | 9 $\frac{1}{4}$ " | 9 $\frac{1}{2}$ " | 9 $\frac{3}{4}$ " | 10" | 10 $\frac{1}{4}$ " | 10 $\frac{1}{2}$ " | 10 $\frac{3}{4}$ " | 12" |
|-------------------------|-------|-------------------|-------------------|-------------------|-------|--------------------|--------------------|--------------------|-------|
| $\frac{1}{16}$ | 1.91 | 1.97 | 2.02 | 2.07 | 2.13 | 2.18 | 2.23 | 2.28 | 2.55 |
| $\frac{1}{8}$ | 3.83 | 3.93 | 4.04 | 4.15 | 4.25 | 4.36 | 4.46 | 4.57 | 5.10 |
| $\frac{3}{16}$ | 5.74 | 5.90 | 6.06 | 6.22 | 6.38 | 6.53 | 6.69 | 6.85 | 7.65 |
| $\frac{1}{4}$ | 7.65 | 7.86 | 8.08 | 8.29 | 8.50 | 8.71 | 8.93 | 9.14 | 10.20 |
| $\frac{5}{16}$ | 9.56 | 9.83 | 10.09 | 10.36 | 10.63 | 10.89 | 11.16 | 11.42 | 12.75 |
| $\frac{3}{8}$ | 11.48 | 11.79 | 12.11 | 12.43 | 12.75 | 13.07 | 13.39 | 13.71 | 15.30 |
| $\frac{7}{16}$ | 13.39 | 13.76 | 14.13 | 14.50 | 14.88 | 15.25 | 15.62 | 15.99 | 17.85 |
| $\frac{1}{2}$ | 15.30 | 15.73 | 16.15 | 16.58 | 17.00 | 17.43 | 17.85 | 18.28 | 20.40 |
| $\frac{9}{16}$ | 17.21 | 17.69 | 18.17 | 18.65 | 19.13 | 19.60 | 20.08 | 20.56 | 22.95 |
| $\frac{5}{8}$ | 19.13 | 19.66 | 20.19 | 20.72 | 21.25 | 21.78 | 22.31 | 22.84 | 25.50 |
| $\frac{11}{16}$ | 21.04 | 21.62 | 22.21 | 22.79 | 23.38 | 23.96 | 24.54 | 25.13 | 28.05 |
| $\frac{3}{4}$ | 22.95 | 23.59 | 24.23 | 24.86 | 25.50 | 26.14 | 26.78 | 27.41 | 30.60 |
| $\frac{13}{16}$ | 24.86 | 25.55 | 26.24 | 26.93 | 27.63 | 28.32 | 29.01 | 29.70 | 33.15 |
| $\frac{7}{8}$ | 26.78 | 27.52 | 28.26 | 29.01 | 29.75 | 30.49 | 31.24 | 31.98 | 35.70 |
| $\frac{15}{16}$ | 28.69 | 29.48 | 30.28 | 31.08 | 31.88 | 32.67 | 33.47 | 34.27 | 38.25 |
| 1 | 30.60 | 31.45 | 32.30 | 33.15 | 34.00 | 34.85 | 35.70 | 36.55 | 40.80 |
| $1\frac{1}{16}$ | 32.51 | 33.42 | 34.32 | 35.22 | 36.13 | 37.03 | 37.93 | 38.83 | 43.35 |
| $1\frac{1}{8}$ | 34.43 | 35.38 | 36.34 | 37.29 | 38.25 | 39.21 | 40.16 | 41.12 | 45.90 |
| $1\frac{3}{16}$ | 36.34 | 37.35 | 38.36 | 39.37 | 40.38 | 41.38 | 42.39 | 43.40 | 48.45 |
| $1\frac{1}{4}$ | 38.25 | 39.31 | 40.38 | 41.44 | 42.50 | 43.56 | 44.63 | 45.69 | 51.00 |
| $1\frac{5}{16}$ | 40.16 | 41.28 | 42.39 | 43.51 | 44.63 | 45.74 | 46.86 | 47.97 | 53.55 |
| $1\frac{3}{8}$ | 42.08 | 43.24 | 44.41 | 45.58 | 46.75 | 47.92 | 49.09 | 50.26 | 56.10 |
| $1\frac{7}{16}$ | 43.99 | 45.21 | 46.43 | 47.65 | 48.88 | 50.10 | 51.32 | 52.54 | 58.65 |
| $1\frac{1}{2}$ | 45.90 | 47.18 | 48.45 | 49.73 | 51.00 | 52.28 | 53.55 | 54.83 | 61.20 |
| $1\frac{9}{16}$ | 47.81 | 49.14 | 50.47 | 51.80 | 53.13 | 54.45 | 55.78 | 57.11 | 63.75 |
| $1\frac{5}{8}$ | 49.73 | 51.11 | 52.49 | 53.87 | 55.25 | 56.63 | 58.01 | 59.39 | 66.30 |
| $1\frac{11}{16}$ | 51.64 | 53.07 | 54.51 | 55.94 | 57.38 | 58.81 | 60.24 | 61.68 | 68.85 |
| $1\frac{3}{4}$ | 53.55 | 55.04 | 56.53 | 58.01 | 59.50 | 60.99 | 62.48 | 63.96 | 71.40 |
| $1\frac{13}{16}$ | 55.46 | 57.00 | 58.54 | 60.08 | 61.63 | 63.17 | 64.71 | 66.25 | 73.95 |
| $1\frac{7}{8}$ | 57.38 | 58.97 | 60.56 | 62.16 | 63.75 | 65.34 | 66.94 | 68.53 | 76.50 |
| $1\frac{15}{16}$ | 59.29 | 60.93 | 62.58 | 64.23 | 65.88 | 67.52 | 69.17 | 70.82 | 79.05 |
| 2 | 61.20 | 62.90 | 64.60 | 66.30 | 68.00 | 69.70 | 71.40 | 73.10 | 81.60 |

WEIGHTS OF FLAT ROLLED STEEL BARS.

Pounds per Lineal Foot.

(CONCLUDED.)

| Thick- ness in Inches. | 11" | 11 $\frac{1}{4}$ " | 11 $\frac{1}{2}$ " | 11 $\frac{3}{4}$ " | 12" | 12 $\frac{1}{4}$ " | 12 $\frac{1}{2}$ " | 12 $\frac{3}{4}$ " |
|------------------------------|-------|--------------------|--------------------|--------------------|-------|--------------------|--------------------|--------------------|
| $\frac{1}{16}$ | 2.34 | 2.39 | 2.44 | 2.50 | 2.55 | 2.60 | 2.66 | 2.71 |
| $\frac{3}{16}$ | 4.68 | 4.78 | 4.89 | 4.99 | 5.10 | 5.21 | 5.31 | 5.42 |
| $\frac{1}{8}$ | 7.01 | 7.17 | 7.33 | 7.49 | 7.65 | 7.81 | 7.97 | 8.13 |
| $\frac{1}{4}$ | 9.35 | 9.56 | 9.78 | 9.99 | 10.20 | 10.41 | 10.63 | 10.84 |
| $\frac{5}{16}$ | 11.69 | 11.95 | 12.22 | 12.48 | 12.75 | 13.02 | 13.28 | 13.55 |
| $\frac{3}{8}$ | 14.03 | 14.34 | 14.66 | 14.98 | 15.30 | 15.62 | 15.94 | 16.26 |
| $\frac{7}{16}$ | 16.36 | 16.73 | 17.11 | 17.48 | 17.85 | 18.22 | 18.59 | 18.97 |
| $\frac{1}{2}$ | 18.70 | 19.13 | 19.55 | 19.98 | 20.40 | 20.83 | 21.25 | 21.68 |
| $\frac{9}{16}$ | 21.04 | 21.52 | 21.99 | 22.47 | 22.95 | 23.43 | 23.91 | 24.38 |
| $\frac{5}{8}$ | 23.38 | 23.91 | 24.44 | 24.97 | 25.50 | 26.03 | 26.56 | 27.09 |
| $\frac{11}{16}$ | 25.71 | 26.30 | 26.88 | 27.47 | 28.05 | 28.63 | 29.22 | 29.80 |
| $\frac{3}{4}$ | 28.05 | 28.69 | 29.33 | 29.96 | 30.60 | 31.24 | 31.88 | 32.51 |
| $1\frac{1}{16}$ | 30.39 | 31.08 | 31.77 | 32.46 | 33.15 | 33.84 | 34.53 | 35.22 |
| $\frac{7}{8}$ | 32.73 | 33.47 | 34.21 | 34.96 | 35.70 | 36.44 | 37.19 | 37.93 |
| $1\frac{1}{8}$ | 35.06 | 35.86 | 36.66 | 37.45 | 38.25 | 39.05 | 39.84 | 40.64 |
| 1 | 37.40 | 38.25 | 39.10 | 39.95 | 40.80 | 41.65 | 42.50 | 43.35 |
| $1\frac{1}{16}$ | 39.74 | 40.64 | 41.54 | 42.45 | 43.35 | 44.25 | 45.16 | 46.06 |
| $1\frac{1}{8}$ | 42.08 | 43.03 | 43.99 | 44.94 | 45.90 | 46.86 | 47.81 | 48.77 |
| $1\frac{3}{16}$ | 44.41 | 45.42 | 46.43 | 47.44 | 48.45 | 49.46 | 50.47 | 51.48 |
| $1\frac{1}{4}$ | 46.75 | 47.81 | 48.88 | 49.94 | 51.00 | 52.06 | 53.13 | 54.19 |
| $1\frac{5}{16}$ | 49.09 | 50.20 | 51.32 | 52.43 | 53.55 | 54.67 | 55.78 | 56.90 |
| $1\frac{3}{8}$ | 51.43 | 52.59 | 53.76 | 54.93 | 56.10 | 57.27 | 58.44 | 59.61 |
| $1\frac{7}{16}$ | 53.76 | 54.98 | 56.21 | 57.43 | 58.65 | 59.87 | 61.09 | 62.32 |
| $1\frac{1}{2}$ | 56.10 | 57.38 | 58.65 | 59.93 | 61.20 | 62.48 | 63.75 | 65.03 |
| $1\frac{9}{16}$ | 58.44 | 59.77 | 61.09 | 62.42 | 63.75 | 65.08 | 66.41 | 67.73 |
| $1\frac{5}{8}$ | 60.78 | 62.16 | 63.54 | 64.92 | 66.30 | 67.68 | 69.06 | 70.44 |
| $1\frac{11}{16}$ | 63.11 | 64.55 | 65.98 | 67.42 | 68.85 | 70.28 | 71.72 | 73.15 |
| $1\frac{3}{4}$ | 65.45 | 66.94 | 68.43 | 69.91 | 71.40 | 72.89 | 74.38 | 75.86 |
| $1\frac{13}{16}$ | 67.79 | 69.33 | 70.87 | 72.41 | 73.95 | 75.49 | 77.03 | 78.57 |
| $1\frac{7}{8}$ | 70.13 | 71.72 | 73.31 | 74.91 | 76.50 | 78.09 | 79.69 | 81.28 |
| $1\frac{15}{16}$ | 72.46 | 74.11 | 75.76 | 77.40 | 79.05 | 80.70 | 82.34 | 83.99 |
| 2 | 74.80 | 76.50 | 78.20 | 79.90 | 81.60 | 83.30 | 85.00 | 86.70 |

The weights for 12" width are repeated on each page to facilitate making the additions necessary to obtain the weights of plates of any width greater than 12". Thus, to find the weight of $15\frac{1}{2}" \times \frac{7}{8}"$, add the weights to be found in the same line for $3\frac{1}{2}" \times \frac{7}{8}"$ and $12" \times \frac{7}{8}" = 10.41 + 35.70 = 46.11$ pounds. Weight of plate $4' 6\frac{1}{2}" \times \frac{9}{8}" = 4 \times 25.50 + 13.31 = 115.31$.

AREAS AND CIRCUMFERENCES OF CIRCLES.For Diameters from $\frac{1}{10}$ to 100, advancing by Tenths.

| Diameter. | Area. | Circumference. | Diameter. | Area. | Circumference. |
|-----------|---------|----------------|-----------|---------|----------------|
| 0.0 | | | 4.0 | 12.5664 | 12.5664 |
| .1 | .007854 | .31416 | .1 | 13.2025 | 12.8805 |
| .2 | .031416 | .62832 | .2 | 13.8544 | 13.1947 |
| .3 | .070686 | .94248 | .3 | 14.5220 | 13.5088 |
| .4 | .12566 | 1.2566 | .4 | 15.2053 | 13.8230 |
| .5 | .19635 | 1.5708 | .5 | 15.9043 | 14.1372 |
| .6 | .28274 | 1.8850 | .6 | 16.6190 | 14.4513 |
| .7 | .38485 | 2.1991 | .7 | 17.3494 | 14.7655 |
| .8 | .50265 | 2.5133 | .8 | 18.0956 | 15.0796 |
| .9 | .63617 | 2.8274 | .9 | 18.8574 | 15.3938 |
| 1.0 | .7854 | 3.1416 | 5.0 | 19.6350 | 15.7080 |
| .1 | .9503 | 3.4558 | .1 | 20.4282 | 16.0221 |
| .2 | 1.1310 | 3.7699 | .2 | 21.2372 | 16.3363 |
| .3 | 1.3273 | 4.0841 | .3 | 22.0618 | 16.6504 |
| .4 | 1.5394 | 4.3982 | .4 | 22.9022 | 16.9646 |
| .5 | 1.7671 | 4.7124 | .5 | 23.7583 | 17.2788 |
| .6 | 2.0106 | 5.0265 | .6 | 24.6301 | 17.5929 |
| .7 | 2.2698 | 5.3407 | .7 | 25.5176 | 17.9071 |
| .8 | 2.5447 | 5.6549 | .8 | 26.4208 | 18.2212 |
| .9 | 2.8353 | 5.9690 | .9 | 27.3397 | 18.5354 |
| 2.0 | 3.1416 | 6.2832 | 6.0 | 28.2743 | 18.8496 |
| .1 | 3.4636 | 6.5973 | .1 | 29.2247 | 19.1637 |
| .2 | 3.8013 | 6.9115 | .2 | 30.1907 | 19.4779 |
| .3 | 4.1548 | 7.2257 | .3 | 31.1725 | 19.7920 |
| .4 | 4.5239 | 7.5398 | .4 | 32.1699 | 20.1062 |
| .5 | 4.9087 | 7.8540 | .5 | 33.1831 | 20.4204 |
| .6 | 5.3093 | 8.1681 | .6 | 34.2119 | 20.7345 |
| .7 | 5.7256 | 8.4823 | .7 | 35.2565 | 21.0487 |
| .8 | 6.1575 | 8.7965 | .8 | 36.3168 | 21.3628 |
| .9 | 6.6052 | 9.1106 | .9 | 37.3928 | 21.6770 |
| 3.0 | 7.0686 | 9.4248 | 7.0 | 38.4845 | 21.9911 |
| .1 | 7.5477 | 9.7389 | .1 | 39.5919 | 22.3053 |
| .2 | 8.0425 | 10.0531 | .2 | 40.7150 | 22.6195 |
| .3 | 8.5530 | 10.3673 | .3 | 41.8539 | 22.9336 |
| .4 | 9.0792 | 10.6814 | .4 | 43.0084 | 23.2478 |
| .5 | 9.6211 | 10.9956 | .5 | 44.1786 | 23.5619 |
| .6 | 10.1788 | 11.3097 | .6 | 45.3646 | 23.8761 |
| .7 | 10.7521 | 11.6239 | .7 | 46.5663 | 24.1903 |
| .8 | 11.3411 | 11.9381 | .8 | 47.7836 | 24.5044 |
| .9 | 11.9459 | 12.2522 | .9 | 49.0167 | 24.8186 |

AREAS AND CIRCUMFERENCES OF CIRCLES.

(CONTINUED.)

| Diameter. | Area. | Circumference. | Diameter. | Area. | Circumference. |
|-----------|----------|----------------|-----------|----------|----------------|
| 8.0 | 50.2655 | 25.1327 | 12.0 | 113.0973 | 37.6991 |
| .1 | 51.5300 | 25.4469 | .1 | 114.9901 | 38.0133 |
| .2 | 52.8102 | 25.7611 | .2 | 116.8987 | 38.3274 |
| .3 | 54.1061 | 26.0752 | .3 | 118.8229 | 38.6416 |
| .4 | 55.4177 | 26.3894 | .4 | 120.7628 | 38.9557 |
| .5 | 56.7450 | 26.7035 | .5 | 122.7185 | 39.2699 |
| .6 | 58.0880 | 27.0177 | .6 | 124.6898 | 39.5841 |
| .7 | 59.4468 | 27.3319 | .7 | 126.6769 | 39.8982 |
| .8 | 60.8212 | 27.6460 | .8 | 128.6796 | 40.2124 |
| .9 | 62.2114 | 27.9602 | .9 | 130.6981 | 40.5265 |
| 9.0 | 63.6173 | 28.2743 | 13.0 | 132.7323 | 40.8407 |
| .1 | 65.0388 | 28.5885 | .1 | 134.7822 | 41.1549 |
| .2 | 66.4761 | 28.9027 | .2 | 136.8478 | 41.4690 |
| .3 | 67.9291 | 29.2168 | .3 | 138.9291 | 41.7832 |
| .4 | 69.3978 | 29.5310 | .4 | 141.0261 | 42.0973 |
| .5 | 70.8822 | 29.8451 | .5 | 143.1388 | 42.4115 |
| .6 | 72.3823 | 30.1593 | .6 | 145.2672 | 42.7257 |
| .7 | 73.8981 | 30.4734 | .7 | 147.4114 | 43.0398 |
| .8 | 75.4296 | 30.7876 | .8 | 149.5712 | 43.3540 |
| .9 | 76.9769 | 31.1018 | .9 | 151.7468 | 43.6681 |
| 10.0 | 78.5398 | 31.4159 | 14.0 | 153.9380 | 43.9823 |
| .1 | 80.1185 | 31.7301 | .1 | 156.1450 | 44.2965 |
| .2 | 81.7128 | 32.0442 | .2 | 158.3677 | 44.6106 |
| .3 | 83.3229 | 32.3584 | .3 | 160.6061 | 44.9248 |
| .4 | 84.9487 | 32.6726 | .4 | 162.8602 | 45.2389 |
| .5 | 86.5901 | 32.9867 | .5 | 165.1300 | 45.5531 |
| .6 | 88.2473 | 33.3009 | .6 | 167.4155 | 45.8673 |
| .7 | 89.9202 | 33.6150 | .7 | 169.7167 | 46.1814 |
| .8 | 91.6088 | 33.9292 | .8 | 172.0336 | 46.4956 |
| .9 | 93.3132 | 34.2434 | .9 | 174.3662 | 46.8097 |
| 11.0 | 95.0332 | 34.5575 | 15.0 | 176.7146 | 47.1239 |
| .1 | 96.7689 | 34.8717 | .1 | 179.0786 | 47.4380 |
| .2 | 98.5203 | 35.1858 | .2 | 181.4584 | 47.7522 |
| .3 | 100.2875 | 35.5000 | .3 | 183.8539 | 48.0664 |
| .4 | 102.0703 | 35.8142 | .4 | 186.2650 | 48.3805 |
| .5 | 103.8689 | 36.1283 | .5 | 188.6919 | 48.6947 |
| .6 | 105.6832 | 36.4425 | .6 | 191.1345 | 49.0088 |
| .7 | 107.5132 | 36.7566 | .7 | 193.5928 | 49.3230 |
| .8 | 109.3588 | 37.0708 | .8 | 196.0668 | 49.6372 |
| .9 | 111.2202 | 37.3850 | .9 | 198.5565 | 49.9513 |

AREAS AND CIRCUMFERENCES OF CIRCLES.

(CONTINUED.)

| Diameter. | Area. | Circumference. | Diameter. | Area. | Circumference. |
|-----------|----------|----------------|-----------|----------|----------------|
| 16.0 | 201.0619 | 50.2655 | 20.0 | 314.1593 | 62.8319 |
| .1 | 203.5831 | 50.5796 | .1 | 317.3087 | 63.1460 |
| .2 | 206.1199 | 50.8938 | .2 | 320.4739 | 63.4602 |
| .3 | 208.6724 | 51.2080 | .3 | 323.6547 | 63.7743 |
| .4 | 211.2407 | 51.5221 | .4 | 326.8513 | 64.0885 |
| .5 | 213.8246 | 51.8363 | .5 | 330.0636 | 64.4026 |
| .6 | 216.4243 | 52.1504 | .6 | 333.2916 | 64.7168 |
| .7 | 219.0397 | 52.4646 | .7 | 336.5353 | 65.0310 |
| .8 | 221.6708 | 52.7788 | .8 | 339.7947 | 65.3451 |
| .9 | 224.3176 | 53.0929 | .9 | 343.0698 | 65.6593 |
| 17.0 | 226.9801 | 53.4071 | 21.0 | 346.3606 | 65.9734 |
| .1 | 229.6583 | 53.7212 | .1 | 349.6671 | 66.2876 |
| .2 | 232.3522 | 54.0354 | .2 | 352.9893 | 66.6018 |
| .3 | 235.0618 | 54.3496 | .3 | 356.3273 | 66.9159 |
| .4 | 237.7871 | 54.6637 | .4 | 359.6809 | 67.2301 |
| .5 | 240.5282 | 54.9779 | .5 | 363.0503 | 67.5442 |
| .6 | 243.2849 | 55.2920 | .6 | 366.4354 | 67.8584 |
| .7 | 246.0574 | 55.6062 | .7 | 369.8361 | 68.1726 |
| .8 | 248.8456 | 55.9203 | .8 | 373.2526 | 68.4867 |
| .9 | 251.6494 | 56.2345 | .9 | 376.6848 | 68.8009 |
| 18.0 | 254.4690 | 56.5487 | 22.0 | 380.1327 | 69.1150 |
| .1 | 257.3043 | 56.8628 | .1 | 383.5963 | 69.4292 |
| .2 | 260.1553 | 57.1770 | .2 | 387.0756 | 69.7434 |
| .3 | 263.0220 | 57.4911 | .3 | 390.5707 | 70.0575 |
| .4 | 265.9044 | 57.8053 | .4 | 394.0814 | 70.3717 |
| .5 | 268.8025 | 58.1195 | .5 | 397.6078 | 70.6858 |
| .6 | 271.7163 | 58.4336 | .6 | 401.1500 | 71.0000 |
| .7 | 274.6459 | 58.7478 | .7 | 404.7078 | 71.3142 |
| .8 | 277.5911 | 59.0619 | .8 | 408.2814 | 71.6283 |
| .9 | 280.5521 | 59.3761 | .9 | 411.8706 | 71.9425 |
| 19.0 | 283.5287 | 59.6903 | 23.0 | 415.4756 | 72.2566 |
| .1 | 286.5211 | 60.0044 | .1 | 419.0963 | 72.5708 |
| .2 | 289.5292 | 60.3186 | .2 | 422.7327 | 72.8849 |
| .3 | 292.5530 | 60.6327 | .3 | 426.3848 | 73.1991 |
| .4 | 295.5925 | 60.9469 | .4 | 430.0526 | 73.5133 |
| .5 | 298.6477 | 61.2611 | .5 | 433.7361 | 73.8274 |
| .6 | 301.7186 | 61.5752 | .6 | 437.4354 | 74.1416 |
| .7 | 304.8052 | 61.8894 | .7 | 441.1503 | 74.4557 |
| .8 | 307.9075 | 62.2035 | .8 | 444.8809 | 74.7699 |
| .9 | 311.0255 | 62.5177 | .9 | 448.6273 | 75.0841 |

AREAS AND CIRCUMFERENCES OF CIRCLES.

(CONTINUED.)

| Diameter. | Area. | Circumference. | Diameter. | Area. | Circumference. |
|-----------|----------|----------------|-----------|----------|----------------|
| 24.0 | 452.3893 | 75.3982 | 28.0 | 615.7522 | 87.9646 |
| .1 | 456.1671 | 75.7124 | .1 | 620.1582 | 88.2788 |
| .2 | 459.9606 | 76.0265 | .2 | 624.5800 | 88.5929 |
| .3 | 463.7698 | 76.3407 | .3 | 629.0175 | 88.9071 |
| .4 | 467.5946 | 76.6549 | .4 | 633.4707 | 89.2212 |
| .5 | 471.4352 | 76.9690 | .5 | 637.9397 | 89.5354 |
| .6 | 475.2916 | 77.2832 | .6 | 642.4243 | 89.8495 |
| .7 | 479.1636 | 77.5973 | .7 | 646.9246 | 90.1637 |
| .8 | 483.0513 | 77.9115 | .8 | 651.4406 | 90.4779 |
| .9 | 486.9547 | 78.2257 | .9 | 655.9724 | 90.7920 |
| 25.0 | 490.8739 | 78.5398 | 29.0 | 660.5199 | 91.1062 |
| .1 | 494.8087 | 78.8540 | .1 | 665.0830 | 91.4203 |
| .2 | 498.7592 | 79.1681 | .2 | 669.6619 | 91.7345 |
| .3 | 502.7255 | 79.4823 | .3 | 674.2565 | 92.0487 |
| .4 | 506.7075 | 79.7965 | .4 | 678.8668 | 92.3628 |
| .5 | 510.7052 | 80.1106 | .5 | 683.4927 | 92.6770 |
| .6 | 514.7185 | 80.4248 | .6 | 688.1345 | 92.9911 |
| .7 | 518.7476 | 80.7389 | .7 | 692.7919 | 93.3053 |
| .8 | 522.7924 | 81.0531 | .8 | 697.4650 | 93.6195 |
| .9 | 526.8529 | 81.3672 | .9 | 702.1538 | 93.9336 |
| 26.0 | 530.9292 | 81.6814 | 30.0 | 706.8583 | 94.2478 |
| .1 | 535.0211 | 81.9956 | .1 | 711.5786 | 94.5619 |
| .2 | 539.1287 | 82.3097 | .2 | 716.3145 | 94.8761 |
| .3 | 543.2521 | 82.6239 | .3 | 721.0662 | 95.1903 |
| .4 | 547.3911 | 82.9380 | .4 | 725.8336 | 95.5044 |
| .5 | 551.5459 | 83.2522 | .5 | 730.6167 | 95.8186 |
| .6 | 555.7163 | 83.5664 | .6 | 735.4154 | 96.1327 |
| .7 | 559.9025 | 83.8805 | .7 | 740.2299 | 96.4469 |
| .8 | 564.1044 | 84.1947 | .8 | 745.0601 | 96.7611 |
| .9 | 568.3220 | 84.5088 | .9 | 749.9060 | 97.0752 |
| 27.0 | 572.5553 | 84.8230 | 31.0 | 754.7676 | 97.3894 |
| .1 | 576.8043 | 85.1372 | .1 | 759.6450 | 97.7035 |
| .2 | 581.0690 | 85.4513 | .2 | 764.5380 | 98.0177 |
| .3 | 585.3494 | 85.7655 | .3 | 769.4467 | 98.3319 |
| .4 | 589.6455 | 86.0796 | .4 | 774.3712 | 98.6460 |
| .5 | 593.9574 | 86.3938 | .5 | 779.3113 | 98.9602 |
| .6 | 598.2849 | 86.7080 | .6 | 784.2672 | 99.2743 |
| .7 | 602.6282 | 87.0221 | .7 | 789.2388 | 99.5885 |
| .8 | 606.9871 | 87.3363 | .8 | 794.2260 | 99.9026 |
| .9 | 611.3618 | 87.6504 | .9 | 799.2290 | 100.2168 |

AREAS AND CIRCUMFERENCES OF CIRCLES.

(CONTINUED.)

| Diameter. | Area. | Circumference. | Diameter. | Area. | Circumference. |
|-----------|-----------|----------------|-----------|-----------|----------------|
| 32.0 | 804.2477 | 100.5310 | 36.0 | 1017.8760 | 113.0973 |
| .1 | 809.2821 | 100.8451 | .1 | 1023.5387 | 113.4115 |
| .2 | 814.3322 | 101.1593 | .2 | 1029.2172 | 113.7257 |
| .3 | 819.3980 | 101.4734 | .3 | 1034.9113 | 114.0398 |
| .4 | 824.4796 | 101.7876 | .4 | 1040.6211 | 114.3540 |
| .5 | 829.5768 | 102.1018 | .5 | 1046.3467 | 114.6681 |
| .6 | 834.6897 | 102.4159 | .6 | 1052.0880 | 114.9823 |
| .7 | 839.8184 | 102.7301 | .7 | 1057.8449 | 115.2965 |
| .8 | 844.9628 | 103.0442 | .8 | 1063.6176 | 115.6106 |
| .9 | 850.1229 | 103.3584 | .9 | 1069.4060 | 115.9248 |
| 33.0 | 855.2986 | 103.6726 | 37.0 | 1075.2101 | 116.2389 |
| .1 | 860.4902 | 103.9867 | .1 | 1081.0299 | 116.5531 |
| .2 | 865.6973 | 104.3009 | .2 | 1086.8654 | 116.8672 |
| .3 | 870.9202 | 104.6150 | .3 | 1092.7166 | 117.1814 |
| .4 | 876.1588 | 104.9292 | .4 | 1098.5835 | 117.4956 |
| .5 | 881.4131 | 105.2434 | .5 | 1104.4662 | 117.8097 |
| .6 | 886.6831 | 105.5575 | .6 | 1110.3645 | 118.1239 |
| .7 | 891.9688 | 105.8717 | .7 | 1116.2786 | 118.4380 |
| .8 | 897.2703 | 106.1858 | .8 | 1122.2083 | 118.7522 |
| .9 | 902.5874 | 106.5000 | .9 | 1128.1538 | 119.0664 |
| 34.0 | 907.9203 | 106.8142 | 38.0 | 1134.1149 | 119.3805 |
| .1 | 913.2688 | 107.1283 | .1 | 1140.0918 | 119.6947 |
| .2 | 918.6331 | 107.4425 | .2 | 1146.0844 | 120.0088 |
| .3 | 924.0131 | 107.7566 | .3 | 1152.0927 | 120.3230 |
| .4 | 929.4088 | 108.0708 | .4 | 1158.1167 | 120.6372 |
| .5 | 934.8202 | 108.3849 | .5 | 1164.1564 | 120.9513 |
| .6 | 940.2473 | 108.6991 | .6 | 1170.2118 | 121.2655 |
| .7 | 945.6901 | 109.0133 | .7 | 1176.2830 | 121.5796 |
| .8 | 951.1486 | 109.3274 | .8 | 1182.3698 | 121.8938 |
| .9 | 956.6228 | 109.6416 | .9 | 1188.4723 | 122.2080 |
| 35.0 | 962.1127 | 109.9557 | 39.0 | 1194.5906 | 122.5221 |
| .1 | 967.6184 | 110.2699 | .1 | 1200.7246 | 122.8363 |
| .2 | 973.1397 | 110.5841 | .2 | 1206.8742 | 123.1504 |
| .3 | 978.6768 | 110.8982 | .3 | 1213.0396 | 123.4646 |
| .4 | 984.2296 | 111.2124 | .4 | 1219.2207 | 123.7788 |
| .5 | 989.7980 | 111.5265 | .5 | 1225.4175 | 124.0929 |
| .6 | 995.3822 | 111.8407 | .6 | 1231.6300 | 124.4071 |
| .7 | 1000.9821 | 112.1549 | .7 | 1237.8582 | 124.7212 |
| .8 | 1006.5977 | 112.4690 | .8 | 1244.1021 | 125.0354 |
| .9 | 1012.2290 | 112.7832 | .9 | 1250.3617 | 125.3495 |

AREAS AND CIRCUMFERENCES OF CIRCLES.

(CONTINUED.)

| Diameter. | Area. | Circumference. | Diameter. | Area. | Circumference. |
|-----------|-----------|----------------|-----------|-----------|----------------|
| 40.0 | 1256.6371 | 125.6637 | 44.0 | 1520.5308 | 138.2301 |
| .1 | 1262.9281 | 125.9779 | .1 | 1527.4502 | 138.5442 |
| .2 | 1269.2348 | 126.2920 | .2 | 1534.3853 | 138.8584 |
| .3 | 1275.5573 | 126.6062 | .3 | 1541.3360 | 139.1726 |
| .4 | 1281.8955 | 126.9203 | .4 | 1548.3025 | 139.4867 |
| .5 | 1288.2493 | 127.2345 | .5 | 1555.2847 | 139.8009 |
| .6 | 1294.6189 | 127.5487 | .6 | 1562.2826 | 140.1150 |
| .7 | 1301.0042 | 127.8628 | .7 | 1569.2962 | 140.4292 |
| .8 | 1307.4052 | 128.1770 | .8 | 1576.3255 | 140.7434 |
| .9 | 1313.8219 | 128.4911 | .9 | 1583.3705 | 141.0575 |
| 41.0 | 1320.2543 | 128.8053 | 45.0 | 1590.4313 | 141.3717 |
| .1 | 1326.7024 | 129.1195 | .1 | 1597.5077 | 141.6858 |
| .2 | 1333.1663 | 129.4336 | .2 | 1604.5999 | 142.0000 |
| .3 | 1339.6458 | 129.7478 | .3 | 1611.7077 | 142.3141 |
| .4 | 1346.1410 | 130.0619 | .4 | 1618.8313 | 142.6283 |
| .5 | 1352.6520 | 130.3761 | .5 | 1625.9705 | 142.9425 |
| .6 | 1359.1786 | 130.6903 | .6 | 1633.1255 | 143.2566 |
| .7 | 1365.7210 | 131.0044 | .7 | 1640.2962 | 143.5708 |
| .8 | 1372.2791 | 131.3186 | .8 | 1647.4826 | 143.8849 |
| .9 | 1378.8529 | 131.6327 | .9 | 1654.6847 | 144.1991 |
| 42.0 | 1385.4424 | 131.9469 | 46.0 | 1661.9025 | 144.5133 |
| .1 | 1392.0476 | 132.2611 | .1 | 1669.1360 | 144.8274 |
| .2 | 1398.6685 | 132.5752 | .2 | 1676.3852 | 145.1416 |
| .3 | 1405.3051 | 132.8894 | .3 | 1683.6502 | 145.4557 |
| .4 | 1411.9574 | 133.2035 | .4 | 1690.9308 | 145.7699 |
| .5 | 1418.6254 | 133.5177 | .5 | 1698.2272 | 146.0841 |
| .6 | 1425.3092 | 133.8318 | .6 | 1705.5392 | 146.3982 |
| .7 | 1432.0086 | 134.1460 | .7 | 1712.8670 | 146.7124 |
| .8 | 1438.7238 | 134.4602 | .8 | 1720.2105 | 147.0265 |
| .9 | 1445.4546 | 134.7743 | .9 | 1727.5696 | 147.3407 |
| 43.0 | 1452.2012 | 135.0885 | 47.0 | 1734.9445 | 147.6549 |
| .1 | 1458.9635 | 135.4026 | .1 | 1742.3351 | 147.9690 |
| .2 | 1465.7415 | 135.7168 | .2 | 1749.7414 | 148.2832 |
| .3 | 1472.5352 | 136.0310 | .3 | 1757.1634 | 148.5973 |
| .4 | 1479.3446 | 136.3451 | .4 | 1764.6012 | 148.9115 |
| .5 | 1486.1697 | 136.6593 | .5 | 1772.0546 | 149.2257 |
| .6 | 1493.0105 | 136.9734 | .6 | 1779.5237 | 149.5398 |
| .7 | 1499.8670 | 137.2876 | .7 | 1787.0086 | 149.8540 |
| .8 | 1506.7392 | 137.6018 | .8 | 1794.5091 | 150.1681 |
| .9 | 1513.6272 | 137.9159 | .9 | 1802.0254 | 150.4823 |

AREAS AND CIRCUMFERENCES OF CIRCLES.

(CONTINUED.)

| Diameter. | Area. | Circumference. | Diameter. | Area. | Circumference. |
|-----------|-----------|----------------|-----------|-----------|----------------|
| 48.0 | 1809.5574 | 150.7964 | 52.0 | 2123.7166 | 163.3628 |
| .1 | 1817.1050 | 151.1106 | .1 | 2131.8926 | 163.6770 |
| .2 | 1824.6684 | 151.4248 | .2 | 2140.0843 | 163.9911 |
| .3 | 1832.2475 | 151.7389 | .3 | 2148.2917 | 164.3053 |
| .4 | 1839.8423 | 152.0531 | .4 | 2156.5149 | 164.6195 |
| .5 | 1847.4528 | 152.3672 | .5 | 2164.7537 | 164.9336 |
| .6 | 1855.0790 | 152.6814 | .6 | 2173.0082 | 165.2478 |
| .7 | 1862.7210 | 152.9956 | .7 | 2181.2785 | 165.5619 |
| .8 | 1870.3786 | 153.3097 | .8 | 2189.5644 | 165.8761 |
| .9 | 1878.0519 | 153.6239 | .9 | 2197.8661 | 166.1903 |
| 49.0 | 1885.7410 | 153.9380 | 53.0 | 2206.1834 | 166.5044 |
| .1 | 1893.4457 | 154.2522 | .1 | 2214.5165 | 166.8186 |
| .2 | 1901.1662 | 154.5664 | .2 | 2222.8653 | 167.1327 |
| .3 | 1908.9024 | 154.8805 | .3 | 2231.2298 | 167.4469 |
| .4 | 1916.6543 | 155.1947 | .4 | 2239.6100 | 167.7610 |
| .5 | 1924.4218 | 155.5088 | .5 | 2248.0059 | 168.0752 |
| .6 | 1932.2051 | 155.8230 | .6 | 2256.4175 | 168.3894 |
| .7 | 1940.0041 | 156.1372 | .7 | 2264.8448 | 168.7035 |
| .8 | 1947.8189 | 156.4513 | .8 | 2273.2879 | 169.0177 |
| .9 | 1955.6493 | 156.7655 | .9 | 2281.7466 | 169.3318 |
| 50.0 | 1963.4954 | 157.0796 | 54.0 | 2290.2210 | 169.6460 |
| .1 | 1971.3572 | 157.3938 | .1 | 2298.7112 | 169.9602 |
| .2 | 1979.2348 | 157.7080 | .2 | 2307.2171 | 170.2743 |
| .3 | 1987.1280 | 158.0221 | .3 | 2315.7386 | 170.5885 |
| .4 | 1995.0370 | 158.3363 | .4 | 2324.2759 | 170.9026 |
| .5 | 2002.9617 | 158.6504 | .5 | 2332.8289 | 171.2168 |
| .6 | 2010.9020 | 158.9646 | .6 | 2341.3976 | 171.5310 |
| .7 | 2018.8581 | 159.2787 | .7 | 2349.9820 | 171.8451 |
| .8 | 2026.8299 | 159.5929 | .8 | 2358.5821 | 172.1593 |
| .9 | 2034.8174 | 159.9071 | .9 | 2367.1979 | 172.4734 |
| 51.0 | 2042.8206 | 160.2212 | 55.0 | 2375.8294 | 172.7876 |
| .1 | 2050.8395 | 160.5354 | .1 | 2384.4767 | 173.1018 |
| .2 | 2058.8742 | 160.8495 | .2 | 2393.1396 | 173.4159 |
| .3 | 2066.9245 | 161.1637 | .3 | 2401.8183 | 173.7301 |
| .4 | 2074.9905 | 161.4779 | .4 | 2410.5126 | 174.0442 |
| .5 | 2083.0723 | 161.7920 | .5 | 2419.2227 | 174.3584 |
| .6 | 2091.1697 | 162.1062 | .6 | 2427.9485 | 174.6726 |
| .7 | 2099.2829 | 162.4203 | .7 | 2436.6899 | 174.9867 |
| .8 | 2107.4118 | 162.7345 | .8 | 2445.4471 | 175.3009 |
| .9 | 2115.5563 | 163.0487 | .9 | 2454.2200 | 175.6150 |

AREAS AND CIRCUMFERENCES OF CIRCLES.

(CONTINUED.)

| Diameter. | Area. | Circumference. | Diameter. | Area. | Circumference. |
|-----------|-----------|----------------|-----------|-----------|----------------|
| 56.0 | 2463.0086 | 175.9292 | 60.0 | 2827.4334 | 188.4956 |
| .1 | 2471.8129 | 176.2433 | .1 | 2836.8660 | 188.8097 |
| .2 | 2480.6330 | 176.5575 | .2 | 2846.3143 | 189.1239 |
| .3 | 2489.4687 | 176.8717 | .3 | 2855.7784 | 189.4380 |
| .4 | 2498.3201 | 177.1858 | .4 | 2865.2582 | 189.7522 |
| .5 | 2507.1873 | 177.5000 | .5 | 2874.7536 | 190.0664 |
| .6 | 2516.0701 | 177.8141 | .6 | 2884.2648 | 190.3805 |
| .7 | 2524.9687 | 178.1283 | .7 | 2893.7917 | 190.6947 |
| .8 | 2533.8830 | 178.4425 | .8 | 2903.3343 | 191.0088 |
| .9 | 2542.8129 | 178.7566 | .9 | 2912.8925 | 191.3230 |
| 57.0 | 2551.7586 | 179.0708 | 61.0 | 2922.4666 | 191.6372 |
| .1 | 2560.7200 | 179.3849 | .1 | 2932.0563 | 191.9513 |
| .2 | 2569.6971 | 179.6991 | .2 | 2941.6617 | 192.2655 |
| .3 | 2578.6899 | 180.0133 | .3 | 2951.2828 | 192.5796 |
| .4 | 2587.6984 | 180.3274 | .4 | 2960.9196 | 192.8938 |
| .5 | 2596.7227 | 180.6416 | .5 | 2970.5722 | 193.2079 |
| .6 | 2605.7626 | 180.9557 | .6 | 2980.2404 | 193.5221 |
| .7 | 2614.8182 | 181.2699 | .7 | 2989.9244 | 193.8363 |
| .8 | 2623.8896 | 181.5841 | .8 | 2999.6241 | 194.1504 |
| .9 | 2632.9766 | 181.8982 | .9 | 3009.3394 | 194.4646 |
| 58.0 | 2642.0794 | 182.2124 | 62.0 | 3019.0705 | 194.7787 |
| .1 | 2651.1979 | 182.5265 | .1 | 3028.8173 | 195.0929 |
| .2 | 2660.3321 | 182.8407 | .2 | 3038.5798 | 195.4071 |
| .3 | 2669.4820 | 183.1549 | .3 | 3048.3580 | 195.7212 |
| .4 | 2678.6475 | 183.4690 | .4 | 3058.1519 | 196.0354 |
| .5 | 2687.8289 | 183.7832 | .5 | 3067.9616 | 196.3495 |
| .6 | 2697.0259 | 184.0973 | .6 | 3077.7869 | 196.6637 |
| .7 | 2706.2386 | 184.4115 | .7 | 3087.6279 | 196.9779 |
| .8 | 2715.4670 | 184.7256 | .8 | 3097.4847 | 197.2920 |
| .9 | 2724.7112 | 185.0398 | .9 | 3107.3571 | 197.6062 |
| 59.0 | 2733.9710 | 185.3540 | 63.0 | 3117.2453 | 197.9203 |
| .1 | 2743.2465 | 185.6681 | .1 | 3127.1492 | 198.2345 |
| .2 | 2752.5378 | 185.9823 | .2 | 3137.0687 | 198.5487 |
| .3 | 2761.8448 | 186.2964 | .3 | 3147.0040 | 198.8628 |
| .4 | 2771.1675 | 186.6106 | .4 | 3156.9550 | 199.1770 |
| .5 | 2780.5058 | 186.9248 | .5 | 3166.9217 | 199.4911 |
| .6 | 2789.8599 | 187.2389 | .6 | 3176.9041 | 199.8053 |
| .7 | 2799.2297 | 187.5531 | .7 | 3186.9023 | 200.1195 |
| .8 | 2808.6152 | 187.8672 | .8 | 3196.9161 | 200.4336 |
| .9 | 2818.0165 | 188.1814 | .9 | 3206.9456 | 200.7478 |

AREAS AND CIRCUMFERENCES OF CIRCLES.

(CONTINUED.)

| Diameter. | Area. | Circumference. | Diameter. | Area. | Circumference. |
|-----------|-----------|----------------|-----------|-----------|----------------|
| 64.0 | 3216.9909 | 201.0620 | 68.0 | 3631.6811 | 213.6283 |
| .1 | 3227.0518 | 201.3761 | .1 | 3642.3704 | 213.9425 |
| .2 | 3237.1285 | 201.6902 | .2 | 3653.0753 | 214.2566 |
| .3 | 3247.2208 | 202.0044 | .3 | 3663.7960 | 214.5708 |
| .4 | 3257.3289 | 202.3186 | .4 | 3674.5324 | 214.8849 |
| .5 | 3267.4527 | 202.6327 | .5 | 3685.2845 | 215.1991 |
| .6 | 3277.5922 | 202.9469 | .6 | 3696.0523 | 215.5133 |
| .7 | 3287.7474 | 203.2610 | .7 | 3706.8358 | 215.8274 |
| .8 | 3297.9183 | 203.5752 | .8 | 3717.6351 | 216.1416 |
| .9 | 3308.1049 | 203.8894 | .9 | 3728.4500 | 216.4556 |
| 65.0 | 3318.3072 | 204.2035 | 69.0 | 3739.2807 | 216.7699 |
| .1 | 3328.5253 | 204.5177 | .1 | 3750.1270 | 217.0841 |
| .2 | 3338.7590 | 204.8318 | .2 | 3760.9890 | 217.3982 |
| .3 | 3349.0084 | 205.1460 | .3 | 3771.8668 | 217.7124 |
| .4 | 3359.2736 | 205.4602 | .4 | 3782.7603 | 218.0265 |
| .5 | 3369.5545 | 205.7743 | .5 | 3793.6695 | 218.3407 |
| .6 | 3379.8510 | 206.0885 | .6 | 3804.5944 | 218.6548 |
| .7 | 3390.1633 | 206.4026 | .7 | 3815.5349 | 218.9690 |
| .8 | 3400.4913 | 206.7168 | .8 | 3826.4913 | 219.2832 |
| .9 | 3410.8350 | 207.0310 | .9 | 3837.4633 | 219.5973 |
| 66.0 | 3421.1944 | 207.3451 | 70.0 | 3848.4510 | 219.9115 |
| .1 | 3431.5695 | 207.6593 | .1 | 3859.4544 | 220.2256 |
| .2 | 3441.9603 | 207.9734 | .2 | 3870.4735 | 220.5398 |
| .3 | 3452.3668 | 208.2876 | .3 | 3881.5084 | 220.8540 |
| .4 | 3462.7891 | 208.6017 | .4 | 3892.5589 | 221.1681 |
| .5 | 3473.2270 | 208.9159 | .5 | 3903.6252 | 221.4823 |
| .6 | 3483.6807 | 209.2301 | .6 | 3914.7072 | 221.7964 |
| .7 | 3494.1500 | 209.5442 | .7 | 3925.8048 | 222.1106 |
| .8 | 3504.6351 | 209.8584 | .8 | 3936.9182 | 222.4248 |
| .9 | 3515.1359 | 210.1725 | .9 | 3948.0473 | 222.7389 |
| 67.0 | 3525.6523 | 210.4867 | 71.0 | 3959.1921 | 223.0531 |
| .1 | 3536.1845 | 210.8009 | .1 | 3970.3526 | 223.3672 |
| .2 | 3546.7324 | 211.1150 | .2 | 3981.5288 | 223.6814 |
| .3 | 3557.2960 | 211.4292 | .3 | 3992.7208 | 223.9956 |
| .4 | 3567.8753 | 211.7433 | .4 | 4003.9284 | 224.3097 |
| .5 | 3578.4704 | 212.0575 | .5 | 4015.1517 | 224.6239 |
| .6 | 3589.0811 | 212.3717 | .6 | 4026.3908 | 224.9380 |
| .7 | 3599.7075 | 212.6858 | .7 | 4037.6455 | 225.2522 |
| .8 | 3610.3497 | 213.0000 | .8 | 4048.9160 | 225.5664 |
| .9 | 3621.0075 | 213.3141 | .9 | 4060.2022 | 225.8805 |

AREAS AND CIRCUMFERENCES OF CIRCLES.

(CONTINUED.)

| Diameter. | Area. | Circumference. | Diameter. | Area. | Circumference. |
|-----------|-----------|----------------|-----------|-----------|----------------|
| 72.0 | 4071.5041 | 226.1947 | 76.0 | 4536.4598 | 238.7610 |
| .1 | 4082.8216 | 226.5088 | .1 | 4548.4057 | 239.0752 |
| .2 | 4094.1549 | 226.8230 | .2 | 4560.3673 | 239.3894 |
| .3 | 4105.5039 | 227.1371 | .3 | 4572.3446 | 239.7035 |
| .4 | 4116.8687 | 227.4513 | .4 | 4584.3376 | 240.0177 |
| .5 | 4128.2491 | 227.7655 | .5 | 4596.3464 | 240.3318 |
| .6 | 4139.6452 | 228.0796 | .6 | 4608.3708 | 240.6460 |
| .7 | 4151.0570 | 228.3938 | .7 | 4620.4110 | 240.9602 |
| .8 | 4162.4846 | 228.7079 | .8 | 4632.4668 | 241.2743 |
| .9 | 4173.9278 | 229.0221 | .9 | 4644.5384 | 241.5885 |
| 73.0 | 4185.3868 | 229.3363 | 77.0 | 4656.6257 | 241.9026 |
| .1 | 4196.8615 | 229.6504 | .1 | 4668.7287 | 242.2168 |
| .2 | 4208.3518 | 229.9646 | .2 | 4680.8474 | 242.5310 |
| .3 | 4219.8579 | 230.2787 | .3 | 4692.9818 | 242.8451 |
| .4 | 4231.3797 | 230.5929 | .4 | 4705.1319 | 243.1592 |
| .5 | 4242.9172 | 230.9071 | .5 | 4717.2977 | 243.4734 |
| .6 | 4254.4704 | 231.2212 | .6 | 4729.4792 | 243.7876 |
| .7 | 4266.0393 | 231.5354 | .7 | 4741.6765 | 244.1017 |
| .8 | 4277.6240 | 231.8495 | .8 | 4753.8894 | 244.4159 |
| .9 | 4289.2243 | 232.1637 | .9 | 4766.1180 | 244.7301 |
| 74.0 | 4300.8403 | 232.4779 | 78.0 | 4778.3624 | 245.0442 |
| .1 | 4312.4721 | 232.7920 | .1 | 4790.6225 | 245.3584 |
| .2 | 4324.1195 | 233.1062 | .2 | 4802.8982 | 245.6725 |
| .3 | 4335.7827 | 233.4203 | .3 | 4815.1897 | 245.9867 |
| .4 | 4347.4616 | 233.7345 | .4 | 4827.4969 | 246.3009 |
| .5 | 4359.1562 | 234.0487 | .5 | 4839.8198 | 246.6150 |
| .6 | 4370.8664 | 234.3628 | .6 | 4852.1584 | 246.9292 |
| .7 | 4382.5924 | 234.6770 | .7 | 4864.5127 | 247.2433 |
| .8 | 4394.3341 | 234.9911 | .8 | 4876.8828 | 247.5575 |
| .9 | 4406.0915 | 235.3053 | .9 | 4889.2685 | 247.8717 |
| 75.0 | 4417.8647 | 235.6194 | 79.0 | 4901.6699 | 248.1858 |
| .1 | 4429.6535 | 235.9336 | .1 | 4914.0871 | 248.5000 |
| .2 | 4441.4580 | 236.2478 | .2 | 4926.5199 | 248.8141 |
| .3 | 4453.2783 | 236.5619 | .3 | 4938.9685 | 249.1283 |
| .4 | 4465.1142 | 236.8761 | .4 | 4951.4328 | 249.4425 |
| .5 | 4476.9659 | 237.1902 | .5 | 4963.9127 | 249.7566 |
| .6 | 4488.8332 | 237.5044 | .6 | 4976.4084 | 250.0708 |
| .7 | 4500.7163 | 237.8186 | .7 | 4988.9198 | 250.3849 |
| .8 | 4512.6151 | 238.1327 | .8 | 5001.4469 | 250.6991 |
| .9 | 4524.5296 | 238.4469 | .9 | 5013.9897 | 251.0133 |

AREAS AND CIRCUMFERENCES OF CIRCLES.

(CONTINUED.)

| Diameter. | Area. | Circumference. | Diameter. | Area. | Circumference. |
|-----------|-----------|----------------|-----------|-----------|----------------|
| 80.0 | 5026.5482 | 251.3274 | 84.0 | 5541.7694 | 263.8938 |
| .1 | 5039.1224 | 251.6416 | .1 | 5554.9720 | 264.2079 |
| .2 | 5051.7124 | 251.9557 | .2 | 5568.1902 | 264.5221 |
| .3 | 5064.3180 | 252.2699 | .3 | 5581.4242 | 264.8363 |
| .4 | 5076.9394 | 252.5840 | .4 | 5594.6738 | 265.1504 |
| .5 | 5089.5764 | 252.8982 | .5 | 5607.9392 | 265.4646 |
| .6 | 5102.2292 | 253.2124 | .6 | 5621.2203 | 265.7787 |
| .7 | 5114.8977 | 253.5265 | .7 | 5634.5171 | 266.0929 |
| .8 | 5127.5818 | 253.8407 | .8 | 5647.8296 | 266.4071 |
| .9 | 5140.2817 | 254.1548 | .9 | 5661.1578 | 266.7212 |
| 81.0 | 5152.9973 | 254.4690 | 85.0 | 5674.5017 | 267.0354 |
| .1 | 5165.7286 | 254.7832 | .1 | 5687.8613 | 267.3495 |
| .2 | 5178.4756 | 255.0973 | .2 | 5701.2367 | 267.6637 |
| .3 | 5191.2384 | 255.4115 | .3 | 5714.6277 | 267.9779 |
| .4 | 5204.0168 | 255.7256 | .4 | 5728.0344 | 268.2920 |
| .5 | 5216.8109 | 256.0398 | .5 | 5741.4569 | 268.6062 |
| .6 | 5229.6208 | 256.3540 | .6 | 5754.8951 | 268.9203 |
| .7 | 5242.4463 | 256.6681 | .7 | 5768.3489 | 269.2345 |
| .8 | 5255.2876 | 256.9823 | .8 | 5781.8185 | 269.5486 |
| .9 | 5268.1446 | 257.2964 | .9 | 5795.3038 | 269.8628 |
| 82.0 | 5281.0172 | 257.6106 | 86.0 | 5808.8048 | 270.1770 |
| .1 | 5293.9056 | 257.9248 | .1 | 5822.3215 | 270.4911 |
| .2 | 5306.8097 | 258.2389 | .2 | 5835.8539 | 270.8053 |
| .3 | 5319.7295 | 258.5531 | .3 | 5849.4020 | 271.1194 |
| .4 | 5332.6650 | 258.8672 | .4 | 5862.9659 | 271.4336 |
| .5 | 5345.6162 | 259.1814 | .5 | 5876.5454 | 271.7478 |
| .6 | 5358.5832 | 259.4956 | .6 | 5890.1406 | 272.0619 |
| .7 | 5371.5658 | 259.8097 | .7 | 5903.7516 | 272.3761 |
| .8 | 5384.5641 | 260.1239 | .8 | 5917.3782 | 272.6902 |
| .9 | 5397.5782 | 260.4380 | .9 | 5931.0206 | 273.0044 |
| 83.0 | 5410.6079 | 260.7522 | 87.0 | 5944.6787 | 273.3186 |
| .1 | 5423.6534 | 261.0663 | .1 | 5958.3525 | 273.6327 |
| .2 | 5436.7146 | 261.3805 | .2 | 5972.0419 | 273.9469 |
| .3 | 5449.7914 | 261.6947 | .3 | 5985.7471 | 274.2610 |
| .4 | 5462.8840 | 262.0088 | .4 | 5999.4680 | 274.5752 |
| .5 | 5475.9923 | 262.3230 | .5 | 6013.2047 | 274.8894 |
| .6 | 5489.1163 | 262.6371 | .6 | 6026.9570 | 275.2035 |
| .7 | 5502.2560 | 262.9513 | .7 | 6040.7250 | 275.5177 |
| .8 | 5515.4115 | 263.2655 | .8 | 6054.5088 | 275.8318 |
| .9 | 5528.5826 | 263.5796 | .9 | 6068.3082 | 276.1460 |

AREAS AND CIRCUMFERENCES OF CIRCLES.

(CONTINUED.)

| Diameter. | Area. | Circumference. | Diameter. | Area. | Circumference. |
|-----------|-----------|----------------|-----------|-----------|----------------|
| 88.0 | 6082.1234 | 276.4602 | 92.0 | 6647.6100 | 289.0265 |
| .1 | 6095.9542 | 276.7743 | .1 | 6662.0692 | 289.3407 |
| .2 | 6109.8008 | 277.0885 | .2 | 6676.5441 | 289.6548 |
| .3 | 6123.6631 | 277.4026 | .3 | 6691.0347 | 289.9690 |
| .4 | 6137.5410 | 277.7168 | .4 | 6705.5410 | 290.2832 |
| .5 | 6151.4347 | 278.0309 | .5 | 6720.0630 | 290.5973 |
| .6 | 6165.3441 | 278.3451 | .6 | 6734.6007 | 290.9115 |
| .7 | 6179.2692 | 278.6593 | .7 | 6749.1542 | 291.2256 |
| .8 | 6193.2101 | 278.9734 | .8 | 6763.7233 | 291.5398 |
| .9 | 6207.1666 | 279.2876 | .9 | 6778.3081 | 291.8540 |
| 89.0 | 6221.1388 | 279.6017 | 93.0 | 6792.9087 | 292.1681 |
| .1 | 6235.1268 | 279.9159 | .1 | 6807.5249 | 292.4823 |
| .2 | 6249.1304 | 280.2301 | .2 | 6822.1569 | 292.7964 |
| .3 | 6263.1498 | 280.5442 | .3 | 6836.8046 | 293.1106 |
| .4 | 6277.1848 | 280.8584 | .4 | 6851.4680 | 293.4248 |
| .5 | 6291.2356 | 281.1725 | .5 | 6866.1471 | 293.7389 |
| .6 | 6305.3021 | 281.4867 | .6 | 6880.8419 | 294.0531 |
| .7 | 6319.3843 | 281.8009 | .7 | 6895.5524 | 294.3672 |
| .8 | 6333.4822 | 282.1150 | .8 | 6910.2786 | 294.6814 |
| .9 | 6347.5958 | 282.4292 | .9 | 6925.0205 | 294.9956 |
| 90.0 | 6361.7251 | 282.7433 | 94.0 | 6939.7781 | 295.3097 |
| .1 | 6375.8701 | 283.0575 | .1 | 6954.5515 | 295.6239 |
| .2 | 6390.0308 | 283.3717 | .2 | 6969.3405 | 295.9380 |
| .3 | 6404.2073 | 283.6858 | .3 | 6984.1453 | 296.2522 |
| .4 | 6418.3994 | 284.0000 | .4 | 6998.9657 | 296.5663 |
| .5 | 6432.6073 | 284.3141 | .5 | 7013.8019 | 296.8805 |
| .6 | 6446.8308 | 284.6283 | .6 | 7028.6538 | 297.1947 |
| .7 | 6461.0701 | 284.9425 | .7 | 7043.5214 | 297.5088 |
| .8 | 6475.3251 | 285.2566 | .8 | 7058.4047 | 297.8230 |
| .9 | 6489.5958 | 285.5708 | .9 | 7073.3037 | 298.1371 |
| 91.0 | 6503.8822 | 285.8849 | 95.0 | 7088.2184 | 298.4513 |
| .1 | 6518.1843 | 286.1991 | .1 | 7103.1488 | 298.7655 |
| .2 | 6532.5021 | 286.5132 | .2 | 7118.0949 | 299.0796 |
| .3 | 6546.8356 | 286.8274 | .3 | 7133.0568 | 299.3938 |
| .4 | 6561.1848 | 287.1416 | .4 | 7148.0343 | 299.7079 |
| .5 | 6575.5497 | 287.4557 | .5 | 7163.0276 | 300.0221 |
| .6 | 6589.9304 | 287.7699 | .6 | 7178.0365 | 300.3363 |
| .7 | 6604.3267 | 288.0840 | .7 | 7193.0612 | 300.6504 |
| .8 | 6618.7388 | 288.3982 | .8 | 7208.1016 | 300.9646 |
| .9 | 6633.1666 | 288.7124 | .9 | 7223.1577 | 301.2787 |

AREAS AND CIRCUMFERENCES OF CIRCLES.

(CONCLUDED.)

| Diameter. | Area. | Circumference. | Diameter. | Area. | Circumference. |
|-----------|-----------|----------------|-----------|-----------|----------------|
| 96.0 | 7238.2294 | 301.5929 | 98.0 | 7542.9639 | 307.8761 |
| .1 | 7253.3169 | 301.9071 | .1 | 7558.3656 | 308.1902 |
| .2 | 7268.4201 | 302.2212 | .2 | 7573.7830 | 308.5044 |
| .3 | 7283.5391 | 302.5354 | .3 | 7589.2161 | 308.8186 |
| .4 | 7298.6737 | 302.8495 | .4 | 7604.6648 | 309.1327 |
| .5 | 7313.8240 | 303.1637 | .5 | 7620.1293 | 309.4469 |
| .6 | 7328.9901 | 303.4779 | .6 | 7635.6095 | 309.7610 |
| .7 | 7344.1718 | 303.7920 | .7 | 7651.1054 | 310.0752 |
| .8 | 7359.3693 | 304.1062 | .8 | 7666.6170 | 310.3894 |
| .9 | 7374.5824 | 304.4203 | .9 | 7682.1443 | 310.7035 |
| 97.0 | 7389.8113 | 304.7345 | 99.0 | 7697.6874 | 311.0177 |
| .1 | 7405.0559 | 305.0486 | .1 | 7713.2461 | 311.3318 |
| .2 | 7420.3162 | 305.3628 | .2 | 7728.8205 | 311.6460 |
| .3 | 7435.5921 | 305.6770 | .3 | 7744.4107 | 311.9602 |
| .4 | 7450.8838 | 305.9911 | .4 | 7760.0166 | 312.2743 |
| .5 | 7466.1913 | 306.3053 | .5 | 7775.6381 | 312.5885 |
| .6 | 7481.5144 | 306.6194 | .6 | 7791.2754 | 312.9026 |
| .7 | 7496.8532 | 306.9336 | .7 | 7806.9284 | 313.2168 |
| .8 | 7512.2077 | 307.2478 | .8 | 7822.5971 | 313.5309 |
| .9 | 7527.5780 | 307.5619 | .9 | 7838.2815 | 313.8451 |
| | | | 100.0 | 7853.9816 | 314.1593 |

To find from the table areas or circumferences for larger diameters than those given.

CASE I.

For diameters greater than 100 and less than 1001:

Take from the table the area or circumference for a circle the diameter of which is one-tenth of the given diameter.

To obtain the required area or circumference, multiply the area so found by 100 and the circumference so found by 10.

For Example.—What is the area and circumference corresponding to a diameter of 459?

From the tables the area and circumference for diameter 45.9 are 1 654.6847 and 144.1991. Therefore 165 468.47 and 1 441.991 are the area and circumference required.

CASE II.

For diameters greater than 1000:

Divide the given diameter by any convenient factor which will give as a quotient a diameter found in the table, and take from the table the area or circumference for this diameter.

To obtain the required area or circumference multiply the area so found by the square of the factor and the circumference so found by the factor.

For Example.—What is the area and circumference corresponding to a diameter of 1 983?

$1\ 983 \div 3 = 661$. From the tables and Case I the area and circumference for diameter 661 are 343 156.95 and 2 076.593. Therefore $343\ 156.95 \times 9 = 3\ 088\ 412.55 =$ area required, and $2\ 076.593 \times 3 = 6\ 229.779 =$ circumference required.

AREAS AND CIRCUMFERENCES OF CIRCLES.

Diameters $\frac{1}{16}$ to 100.

| Diameter. | Area. | Circumference. | Diameter. | Area. | Circumference. |
|----------------|---------|----------------|----------------|---------|----------------|
| $\frac{1}{16}$ | .0031 | .1963 | 5 | 19.6350 | 15.7080 |
| $\frac{1}{8}$ | .0123 | .3927 | $\frac{1}{8}$ | 20.6290 | 16.1007 |
| $\frac{3}{16}$ | .0491 | .7854 | $\frac{3}{16}$ | 21.6476 | 16.4934 |
| $\frac{1}{4}$ | .1104 | 1.1781 | $\frac{1}{4}$ | 22.6907 | 16.8861 |
| $\frac{5}{16}$ | .1963 | 1.5708 | $\frac{5}{16}$ | 23.7583 | 17.2788 |
| $\frac{3}{8}$ | .3068 | 1.9635 | $\frac{3}{8}$ | 24.8505 | 17.6715 |
| $\frac{7}{16}$ | .4418 | 2.3562 | $\frac{7}{16}$ | 25.9673 | 18.0642 |
| $\frac{1}{2}$ | .6013 | 2.7489 | $\frac{1}{2}$ | 27.1086 | 18.4569 |
| 1 | .7854 | 3.1416 | 6 | 28.2744 | 18.8496 |
| $\frac{1}{8}$ | .9940 | 3.5343 | $\frac{1}{8}$ | 29.4648 | 19.2423 |
| $\frac{1}{4}$ | 1.2272 | 3.9270 | $\frac{1}{4}$ | 30.6797 | 19.6350 |
| $\frac{3}{8}$ | 1.4849 | 4.3197 | $\frac{3}{8}$ | 31.9191 | 20.0277 |
| $\frac{1}{2}$ | 1.7671 | 4.7124 | $\frac{1}{2}$ | 33.1831 | 20.4204 |
| $\frac{5}{8}$ | 2.0739 | 5.1051 | $\frac{5}{8}$ | 34.4717 | 20.8131 |
| $\frac{3}{4}$ | 2.4053 | 5.4978 | $\frac{3}{4}$ | 35.7848 | 21.2058 |
| $\frac{7}{8}$ | 2.7612 | 5.8905 | $\frac{7}{8}$ | 37.1224 | 21.5985 |
| 2 | 3.1416 | 6.2832 | 7 | 38.4846 | 21.9912 |
| $\frac{1}{8}$ | 3.5466 | 6.6759 | $\frac{1}{8}$ | 39.8713 | 22.3839 |
| $\frac{1}{4}$ | 3.9761 | 7.0686 | $\frac{1}{4}$ | 41.2826 | 22.7766 |
| $\frac{3}{8}$ | 4.4301 | 7.4613 | $\frac{3}{8}$ | 42.7184 | 23.1693 |
| $\frac{1}{2}$ | 4.9087 | 7.8540 | $\frac{1}{2}$ | 44.1787 | 23.5620 |
| $\frac{5}{8}$ | 5.4119 | 8.2467 | $\frac{5}{8}$ | 45.6636 | 23.9547 |
| $\frac{3}{4}$ | 5.9396 | 8.6394 | $\frac{3}{4}$ | 47.1731 | 24.3474 |
| $\frac{7}{8}$ | 6.4918 | 9.0321 | $\frac{7}{8}$ | 48.7071 | 24.7401 |
| 3 | 7.0686 | 9.4248 | 8 | 50.2656 | 25.1328 |
| $\frac{1}{8}$ | 7.6699 | 9.8175 | $\frac{1}{8}$ | 51.8487 | 25.5255 |
| $\frac{1}{4}$ | 8.2958 | 10.2102 | $\frac{1}{4}$ | 53.4563 | 25.9182 |
| $\frac{3}{8}$ | 8.9462 | 10.6029 | $\frac{3}{8}$ | 55.0884 | 26.3109 |
| $\frac{1}{2}$ | 9.6211 | 10.9956 | $\frac{1}{2}$ | 56.7451 | 26.7036 |
| $\frac{5}{8}$ | 10.3206 | 11.3883 | $\frac{5}{8}$ | 58.4264 | 27.0963 |
| $\frac{3}{4}$ | 11.0447 | 11.7810 | $\frac{3}{4}$ | 60.1322 | 27.4890 |
| $\frac{7}{8}$ | 11.7933 | 12.1737 | $\frac{7}{8}$ | 61.8625 | 27.8817 |
| 4 | 12.5664 | 12.5664 | 9 | 63.6174 | 28.2744 |
| $\frac{1}{8}$ | 13.3641 | 12.9591 | $\frac{1}{8}$ | 65.3968 | 28.6671 |
| $\frac{1}{4}$ | 14.1863 | 13.3518 | $\frac{1}{4}$ | 67.2008 | 29.0598 |
| $\frac{3}{8}$ | 15.0330 | 13.7445 | $\frac{3}{8}$ | 69.0293 | 29.4525 |
| $\frac{1}{2}$ | 15.9043 | 14.1372 | $\frac{1}{2}$ | 70.8823 | 29.8452 |
| $\frac{5}{8}$ | 16.8002 | 14.5299 | $\frac{5}{8}$ | 72.7599 | 30.2379 |
| $\frac{3}{4}$ | 17.7206 | 14.9226 | $\frac{3}{4}$ | 74.6621 | 30.6306 |
| $\frac{7}{8}$ | 18.6655 | 15.3153 | $\frac{7}{8}$ | 76.5889 | 31.0233 |

AREAS AND CIRCUMFERENCES OF CIRCLES.

Diameters $\frac{1}{8}$ to 100.

| Diameter. | Area. | Circumference. | Diameter. | Area. | Circumference. |
|---------------|---------|----------------|---------------|---------|----------------|
| 10 | 78.540 | 31.4160 | 15 | 176.715 | 47.1240 |
| $\frac{1}{8}$ | 80.516 | 31.8087 | $\frac{1}{8}$ | 179.673 | 47.5167 |
| $\frac{1}{4}$ | 82.516 | 32.2014 | $\frac{1}{4}$ | 182.655 | 47.9094 |
| $\frac{3}{8}$ | 84.541 | 32.5941 | $\frac{3}{8}$ | 185.661 | 48.3021 |
| $\frac{1}{2}$ | 86.590 | 32.9868 | $\frac{1}{2}$ | 188.692 | 48.6948 |
| $\frac{5}{8}$ | 88.664 | 33.3795 | $\frac{5}{8}$ | 191.748 | 49.0875 |
| $\frac{3}{4}$ | 90.763 | 33.7722 | $\frac{3}{4}$ | 194.828 | 49.4802 |
| $\frac{7}{8}$ | 92.886 | 34.1649 | $\frac{7}{8}$ | 197.933 | 49.8729 |
| 11 | 95.033 | 34.5576 | 16 | 201.062 | 50.2656 |
| $\frac{1}{8}$ | 97.205 | 34.9503 | $\frac{1}{8}$ | 204.216 | 50.6583 |
| $\frac{1}{4}$ | 99.402 | 35.3430 | $\frac{1}{4}$ | 207.395 | 51.0510 |
| $\frac{3}{8}$ | 101.623 | 35.7357 | $\frac{3}{8}$ | 210.598 | 51.4437 |
| $\frac{1}{2}$ | 103.869 | 36.1284 | $\frac{1}{2}$ | 213.825 | 51.8364 |
| $\frac{5}{8}$ | 106.139 | 36.5211 | $\frac{5}{8}$ | 217.077 | 52.2291 |
| $\frac{3}{4}$ | 108.434 | 36.9138 | $\frac{3}{4}$ | 220.354 | 52.6218 |
| $\frac{7}{8}$ | 110.754 | 37.3065 | $\frac{7}{8}$ | 223.655 | 53.0145 |
| 12 | 113.098 | 37.6992 | 17 | 226.981 | 53.4072 |
| $\frac{1}{8}$ | 115.466 | 38.0919 | $\frac{1}{8}$ | 230.331 | 53.7999 |
| $\frac{1}{4}$ | 117.859 | 38.4846 | $\frac{1}{4}$ | 233.706 | 54.1926 |
| $\frac{3}{8}$ | 120.277 | 38.8773 | $\frac{3}{8}$ | 237.105 | 54.5853 |
| $\frac{1}{2}$ | 122.719 | 39.2700 | $\frac{1}{2}$ | 240.529 | 54.9780 |
| $\frac{5}{8}$ | 125.185 | 39.6627 | $\frac{5}{8}$ | 243.977 | 55.3707 |
| $\frac{3}{4}$ | 127.677 | 40.0554 | $\frac{3}{4}$ | 247.450 | 55.7634 |
| $\frac{7}{8}$ | 130.192 | 40.4481 | $\frac{7}{8}$ | 250.948 | 56.1561 |
| 13 | 132.733 | 40.8408 | 18 | 254.470 | 56.5488 |
| $\frac{1}{8}$ | 135.297 | 41.2335 | $\frac{1}{8}$ | 258.016 | 56.9415 |
| $\frac{1}{4}$ | 137.887 | 41.6262 | $\frac{1}{4}$ | 261.587 | 57.3342 |
| $\frac{3}{8}$ | 140.501 | 42.0189 | $\frac{3}{8}$ | 265.183 | 57.7269 |
| $\frac{1}{2}$ | 143.139 | 42.4116 | $\frac{1}{2}$ | 268.803 | 58.1196 |
| $\frac{5}{8}$ | 145.802 | 42.8043 | $\frac{5}{8}$ | 272.448 | 58.5123 |
| $\frac{3}{4}$ | 148.490 | 43.1970 | $\frac{3}{4}$ | 276.117 | 58.9050 |
| $\frac{7}{8}$ | 151.202 | 43.5897 | $\frac{7}{8}$ | 279.811 | 59.2977 |
| 14 | 153.938 | 43.9824 | 19 | 283.529 | 59.6904 |
| $\frac{1}{8}$ | 156.700 | 44.3751 | $\frac{1}{8}$ | 287.272 | 60.0831 |
| $\frac{1}{4}$ | 159.485 | 44.7678 | $\frac{1}{4}$ | 291.040 | 60.4758 |
| $\frac{3}{8}$ | 162.296 | 45.1605 | $\frac{3}{8}$ | 294.832 | 60.8685 |
| $\frac{1}{2}$ | 165.130 | 45.5532 | $\frac{1}{2}$ | 298.648 | 61.2612 |
| $\frac{5}{8}$ | 167.990 | 45.9459 | $\frac{5}{8}$ | 302.489 | 61.6539 |
| $\frac{3}{4}$ | 170.874 | 46.3386 | $\frac{3}{4}$ | 306.355 | 62.0466 |
| $\frac{7}{8}$ | 173.782 | 46.7313 | $\frac{7}{8}$ | 310.245 | 62.4393 |

AREAS AND CIRCUMFERENCES OF CIRCLES.

Diameters $\frac{1}{8}$ to 100.

| Diameter. | Area. | Circumference. | Diameter. | Area. | Circumference. |
|---------------|---------|----------------|---------------|---------|----------------|
| 20 | 314.160 | 62.8320 | 25 | 490.875 | 78.5400 |
| $\frac{1}{8}$ | 318.099 | 63.2247 | $\frac{1}{8}$ | 495.796 | 78.9327 |
| $\frac{1}{4}$ | 322.063 | 63.6174 | $\frac{1}{4}$ | 500.742 | 79.3254 |
| $\frac{3}{8}$ | 326.051 | 64.0101 | $\frac{3}{8}$ | 505.712 | 79.7181 |
| $\frac{1}{2}$ | 330.064 | 64.4028 | $\frac{1}{2}$ | 510.706 | 80.1108 |
| $\frac{5}{8}$ | 334.102 | 64.7955 | $\frac{5}{8}$ | 515.726 | 80.5035 |
| $\frac{3}{4}$ | 338.164 | 65.1882 | $\frac{3}{4}$ | 520.769 | 80.8962 |
| $\frac{7}{8}$ | 342.250 | 65.5809 | $\frac{7}{8}$ | 525.838 | 81.2889 |
| 21 | 346.361 | 65.9736 | 26 | 530.930 | 81.6816 |
| $\frac{1}{8}$ | 350.497 | 66.3663 | $\frac{1}{8}$ | 536.048 | 82.0743 |
| $\frac{1}{4}$ | 354.657 | 66.7590 | $\frac{1}{4}$ | 541.190 | 82.4670 |
| $\frac{3}{8}$ | 358.842 | 67.1517 | $\frac{3}{8}$ | 546.356 | 82.8597 |
| $\frac{1}{2}$ | 363.051 | 67.5444 | $\frac{1}{2}$ | 551.547 | 83.2524 |
| $\frac{5}{8}$ | 367.285 | 67.9371 | $\frac{5}{8}$ | 556.763 | 83.6451 |
| $\frac{3}{4}$ | 371.543 | 68.3298 | $\frac{3}{4}$ | 562.003 | 84.0378 |
| $\frac{7}{8}$ | 375.826 | 68.7225 | $\frac{7}{8}$ | 567.267 | 84.4305 |
| 22 | 380.134 | 69.1152 | 27 | 572.557 | 84.8232 |
| $\frac{1}{8}$ | 384.466 | 69.5079 | $\frac{1}{8}$ | 577.870 | 85.2159 |
| $\frac{1}{4}$ | 388.822 | 69.9006 | $\frac{1}{4}$ | 583.209 | 85.6086 |
| $\frac{3}{8}$ | 393.203 | 70.2933 | $\frac{3}{8}$ | 588.571 | 86.0013 |
| $\frac{1}{2}$ | 397.609 | 70.6860 | $\frac{1}{2}$ | 593.959 | 86.3940 |
| $\frac{5}{8}$ | 402.038 | 71.0787 | $\frac{5}{8}$ | 599.371 | 86.7867 |
| $\frac{3}{4}$ | 406.494 | 71.4714 | $\frac{3}{4}$ | 604.807 | 87.1794 |
| $\frac{7}{8}$ | 410.973 | 71.8641 | $\frac{7}{8}$ | 610.268 | 87.5721 |
| 23 | 415.477 | 72.2568 | 28 | 615.754 | 87.9648 |
| $\frac{1}{8}$ | 420.004 | 72.6495 | $\frac{1}{8}$ | 621.264 | 88.3575 |
| $\frac{1}{4}$ | 424.558 | 73.0422 | $\frac{1}{4}$ | 626.798 | 88.7502 |
| $\frac{3}{8}$ | 429.135 | 73.4349 | $\frac{3}{8}$ | 632.357 | 89.1429 |
| $\frac{1}{2}$ | 433.737 | 73.8276 | $\frac{1}{2}$ | 637.941 | 89.5356 |
| $\frac{5}{8}$ | 438.364 | 74.2203 | $\frac{5}{8}$ | 643.549 | 89.9283 |
| $\frac{3}{4}$ | 443.015 | 74.6130 | $\frac{3}{4}$ | 649.182 | 90.3210 |
| $\frac{7}{8}$ | 447.690 | 75.0057 | $\frac{7}{8}$ | 654.840 | 90.7137 |
| 24 | 452.390 | 75.3984 | 29 | 660.521 | 91.1064 |
| $\frac{1}{8}$ | 457.115 | 75.7911 | $\frac{1}{8}$ | 666.228 | 91.4991 |
| $\frac{1}{4}$ | 461.864 | 76.1838 | $\frac{1}{4}$ | 671.959 | 91.8918 |
| $\frac{3}{8}$ | 466.638 | 76.5765 | $\frac{3}{8}$ | 677.714 | 92.2845 |
| $\frac{1}{2}$ | 471.436 | 76.9692 | $\frac{1}{2}$ | 683.494 | 92.6772 |
| $\frac{5}{8}$ | 476.259 | 77.3619 | $\frac{5}{8}$ | 689.299 | 93.0699 |
| $\frac{3}{4}$ | 481.107 | 77.7546 | $\frac{3}{4}$ | 695.128 | 93.4626 |
| $\frac{7}{8}$ | 485.979 | 78.1473 | $\frac{7}{8}$ | 700.982 | 93.8553 |

AREAS AND CIRCUMFERENCES OF CIRCLES.

Diameters $\frac{1}{16}$ to 100.

| Diameter. | Area. | Circumference. | Diameter. | Area. | Circumference. |
|----------------|---------|----------------|----------------|----------|----------------|
| 30 | 706.860 | 94.248 | 35 | 962.115 | 109.956 |
| $\frac{1}{16}$ | 712.763 | 94.641 | $\frac{1}{16}$ | 969.000 | 110.349 |
| $\frac{1}{8}$ | 718.690 | 95.033 | $\frac{1}{8}$ | 975.909 | 110.741 |
| $\frac{3}{16}$ | 724.642 | 95.426 | $\frac{3}{16}$ | 982.842 | 111.134 |
| $\frac{1}{4}$ | 730.618 | 95.819 | $\frac{1}{4}$ | 989.800 | 111.527 |
| $\frac{5}{16}$ | 736.619 | 96.212 | $\frac{5}{16}$ | 996.783 | 111.919 |
| $\frac{3}{8}$ | 742.645 | 96.604 | $\frac{3}{8}$ | 1003.790 | 112.312 |
| $\frac{7}{16}$ | 748.695 | 96.997 | $\frac{7}{16}$ | 1010.822 | 112.705 |
| 31 | 754.769 | 97.390 | 36 | 1017.878 | 113.098 |
| $\frac{1}{16}$ | 760.869 | 97.782 | $\frac{1}{16}$ | 1024.960 | 113.490 |
| $\frac{1}{8}$ | 766.992 | 98.175 | $\frac{1}{8}$ | 1032.065 | 113.883 |
| $\frac{3}{16}$ | 773.140 | 98.568 | $\frac{3}{16}$ | 1039.195 | 114.276 |
| $\frac{1}{4}$ | 779.313 | 98.960 | $\frac{1}{4}$ | 1046.349 | 114.668 |
| $\frac{5}{16}$ | 785.510 | 99.353 | $\frac{5}{16}$ | 1053.528 | 115.061 |
| $\frac{3}{8}$ | 791.732 | 99.746 | $\frac{3}{8}$ | 1060.732 | 115.454 |
| $\frac{7}{16}$ | 797.979 | 100.138 | $\frac{7}{16}$ | 1067.960 | 115.846 |
| 32 | 804.250 | 100.531 | 37 | 1075.213 | 116.239 |
| $\frac{1}{16}$ | 810.545 | 100.924 | $\frac{1}{16}$ | 1082.490 | 116.632 |
| $\frac{1}{8}$ | 816.865 | 101.317 | $\frac{1}{8}$ | 1089.792 | 117.025 |
| $\frac{3}{16}$ | 823.210 | 101.709 | $\frac{3}{16}$ | 1097.118 | 117.417 |
| $\frac{1}{4}$ | 829.579 | 102.102 | $\frac{1}{4}$ | 1104.469 | 117.810 |
| $\frac{5}{16}$ | 835.972 | 102.495 | $\frac{5}{16}$ | 1111.844 | 118.203 |
| $\frac{3}{8}$ | 842.391 | 102.887 | $\frac{3}{8}$ | 1119.244 | 118.595 |
| $\frac{7}{16}$ | 848.833 | 103.280 | $\frac{7}{16}$ | 1126.669 | 118.988 |
| 33 | 855.301 | 103.673 | 38 | 1134.118 | 119.381 |
| $\frac{1}{16}$ | 861.792 | 104.065 | $\frac{1}{16}$ | 1141.591 | 119.773 |
| $\frac{1}{8}$ | 868.309 | 104.458 | $\frac{1}{8}$ | 1149.089 | 120.166 |
| $\frac{3}{16}$ | 874.850 | 104.851 | $\frac{3}{16}$ | 1156.612 | 120.559 |
| $\frac{1}{4}$ | 881.415 | 105.244 | $\frac{1}{4}$ | 1164.159 | 120.952 |
| $\frac{5}{16}$ | 888.005 | 105.636 | $\frac{5}{16}$ | 1171.731 | 121.344 |
| $\frac{3}{8}$ | 894.620 | 106.029 | $\frac{3}{8}$ | 1179.327 | 121.737 |
| $\frac{7}{16}$ | 901.259 | 106.422 | $\frac{7}{16}$ | 1186.948 | 122.130 |
| 34 | 907.922 | 106.814 | 39 | 1194.593 | 122.522 |
| $\frac{1}{16}$ | 914.611 | 107.207 | $\frac{1}{16}$ | 1202.263 | 122.915 |
| $\frac{1}{8}$ | 921.323 | 107.600 | $\frac{1}{8}$ | 1209.958 | 123.308 |
| $\frac{3}{16}$ | 928.061 | 107.992 | $\frac{3}{16}$ | 1217.677 | 123.700 |
| $\frac{1}{4}$ | 934.822 | 108.385 | $\frac{1}{4}$ | 1225.420 | 124.093 |
| $\frac{5}{16}$ | 941.609 | 108.778 | $\frac{5}{16}$ | 1233.188 | 124.486 |
| $\frac{3}{8}$ | 948.420 | 109.171 | $\frac{3}{8}$ | 1240.981 | 124.879 |
| $\frac{7}{16}$ | 955.255 | 109.563 | $\frac{7}{16}$ | 1248.798 | 125.271 |

AREAS AND CIRCUMFERENCES OF CIRCLES.

Diameters $\frac{1}{16}$ to 100.

| Diameter. | Area. | Circumference. | Diameter. | Area. | Circumference. |
|---------------|---------|----------------|---------------|---------|----------------|
| 40 | 1256.64 | 125.664 | 45 | 1590.43 | 141.372 |
| $\frac{1}{8}$ | 1264.51 | 126.057 | $\frac{1}{8}$ | 1599.28 | 141.765 |
| $\frac{1}{4}$ | 1272.40 | 126.449 | $\frac{1}{4}$ | 1608.16 | 142.157 |
| $\frac{3}{8}$ | 1280.31 | 126.842 | $\frac{3}{8}$ | 1617.05 | 142.550 |
| $\frac{1}{2}$ | 1288.25 | 127.235 | $\frac{1}{2}$ | 1625.97 | 142.943 |
| $\frac{5}{8}$ | 1296.22 | 127.627 | $\frac{5}{8}$ | 1634.92 | 143.335 |
| $\frac{3}{4}$ | 1304.21 | 128.020 | $\frac{3}{4}$ | 1643.89 | 143.728 |
| $\frac{7}{8}$ | 1312.22 | 128.413 | $\frac{7}{8}$ | 1652.89 | 144.121 |
| 41 | 1320.26 | 128.806 | 46 | 1661.91 | 144.514 |
| $\frac{1}{8}$ | 1328.32 | 129.198 | $\frac{1}{8}$ | 1670.95 | 144.906 |
| $\frac{1}{4}$ | 1336.41 | 129.591 | $\frac{1}{4}$ | 1680.02 | 145.299 |
| $\frac{3}{8}$ | 1344.52 | 129.984 | $\frac{3}{8}$ | 1689.11 | 145.692 |
| $\frac{1}{2}$ | 1352.66 | 130.376 | $\frac{1}{2}$ | 1698.23 | 146.084 |
| $\frac{5}{8}$ | 1360.82 | 130.769 | $\frac{5}{8}$ | 1707.37 | 146.477 |
| $\frac{3}{4}$ | 1369.00 | 131.162 | $\frac{3}{4}$ | 1716.54 | 146.870 |
| $\frac{7}{8}$ | 1377.21 | 131.554 | $\frac{7}{8}$ | 1725.73 | 147.262 |
| 42 | 1385.45 | 131.947 | 47 | 1734.95 | 147.655 |
| $\frac{1}{8}$ | 1393.70 | 132.340 | $\frac{1}{8}$ | 1744.19 | 148.048 |
| $\frac{1}{4}$ | 1401.99 | 132.733 | $\frac{1}{4}$ | 1753.45 | 148.441 |
| $\frac{3}{8}$ | 1410.30 | 133.125 | $\frac{3}{8}$ | 1762.74 | 148.833 |
| $\frac{1}{2}$ | 1418.63 | 133.518 | $\frac{1}{2}$ | 1772.06 | 149.226 |
| $\frac{5}{8}$ | 1426.99 | 133.911 | $\frac{5}{8}$ | 1781.40 | 149.619 |
| $\frac{3}{4}$ | 1435.37 | 134.303 | $\frac{3}{4}$ | 1790.76 | 150.011 |
| $\frac{7}{8}$ | 1443.77 | 134.696 | $\frac{7}{8}$ | 1800.15 | 150.404 |
| 43 | 1452.20 | 135.089 | 48 | 1809.56 | 150.797 |
| $\frac{1}{8}$ | 1460.66 | 135.481 | $\frac{1}{8}$ | 1819.00 | 151.189 |
| $\frac{1}{4}$ | 1469.14 | 135.874 | $\frac{1}{4}$ | 1828.46 | 151.582 |
| $\frac{3}{8}$ | 1477.64 | 136.267 | $\frac{3}{8}$ | 1837.95 | 151.975 |
| $\frac{1}{2}$ | 1486.17 | 136.660 | $\frac{1}{2}$ | 1847.46 | 152.368 |
| $\frac{5}{8}$ | 1494.73 | 137.052 | $\frac{5}{8}$ | 1856.99 | 152.760 |
| $\frac{3}{4}$ | 1503.30 | 137.445 | $\frac{3}{4}$ | 1866.55 | 153.153 |
| $\frac{7}{8}$ | 1511.91 | 137.838 | $\frac{7}{8}$ | 1876.14 | 153.546 |
| 44 | 1520.53 | 138.230 | 49 | 1885.75 | 153.938 |
| $\frac{1}{8}$ | 1529.19 | 138.623 | $\frac{1}{8}$ | 1895.38 | 154.331 |
| $\frac{1}{4}$ | 1537.86 | 139.016 | $\frac{1}{4}$ | 1905.04 | 154.724 |
| $\frac{3}{8}$ | 1546.56 | 139.408 | $\frac{3}{8}$ | 1914.72 | 155.116 |
| $\frac{1}{2}$ | 1555.29 | 139.801 | $\frac{1}{2}$ | 1924.43 | 155.509 |
| $\frac{5}{8}$ | 1564.04 | 140.194 | $\frac{5}{8}$ | 1934.16 | 155.902 |
| $\frac{3}{4}$ | 1572.81 | 140.587 | $\frac{3}{4}$ | 1943.91 | 156.295 |
| $\frac{7}{8}$ | 1581.61 | 140.979 | $\frac{7}{8}$ | 1953.69 | 156.687 |

AREAS AND CIRCUMFERENCES OF CIRCLES.

Diameters $\frac{1}{16}$ to 100.

| Diameter. | Area. | Circumference. | Diameter. | Area. | Circumference. |
|---------------|---------|----------------|---------------|---------|----------------|
| 50 | 1963.50 | 157.080 | 55 | 2375.83 | 172.788 |
| $\frac{1}{8}$ | 1973.33 | 157.473 | $\frac{1}{8}$ | 2386.65 | 173.181 |
| $\frac{1}{4}$ | 1983.18 | 157.865 | $\frac{1}{4}$ | 2397.48 | 173.573 |
| $\frac{3}{8}$ | 1993.06 | 158.258 | $\frac{3}{8}$ | 2408.34 | 173.966 |
| $\frac{1}{2}$ | 2002.97 | 158.651 | $\frac{1}{2}$ | 2419.23 | 174.359 |
| $\frac{5}{8}$ | 2012.89 | 159.043 | $\frac{5}{8}$ | 2430.14 | 174.751 |
| $\frac{3}{4}$ | 2022.85 | 159.436 | $\frac{3}{4}$ | 2441.07 | 175.144 |
| $\frac{7}{8}$ | 2032.82 | 159.829 | $\frac{7}{8}$ | 2452.03 | 175.537 |
| 51 | 2042.83 | 160.222 | 56 | 2463.01 | 175.930 |
| $\frac{1}{8}$ | 2052.85 | 160.614 | $\frac{1}{8}$ | 2474.02 | 176.322 |
| $\frac{1}{4}$ | 2062.90 | 161.007 | $\frac{1}{4}$ | 2485.05 | 176.715 |
| $\frac{3}{8}$ | 2072.98 | 161.400 | $\frac{3}{8}$ | 2496.11 | 177.108 |
| $\frac{1}{2}$ | 2083.08 | 161.792 | $\frac{1}{2}$ | 2507.19 | 177.500 |
| $\frac{5}{8}$ | 2093.20 | 162.185 | $\frac{5}{8}$ | 2518.30 | 177.893 |
| $\frac{3}{4}$ | 2103.35 | 162.578 | $\frac{3}{4}$ | 2529.43 | 178.286 |
| $\frac{7}{8}$ | 2113.52 | 162.970 | $\frac{7}{8}$ | 2540.58 | 178.678 |
| 52 | 2123.72 | 163.363 | 57 | 2551.76 | 179.071 |
| $\frac{1}{8}$ | 2133.94 | 163.756 | $\frac{1}{8}$ | 2562.97 | 179.464 |
| $\frac{1}{4}$ | 2144.19 | 164.149 | $\frac{1}{4}$ | 2574.20 | 179.857 |
| $\frac{3}{8}$ | 2154.46 | 164.541 | $\frac{3}{8}$ | 2585.45 | 180.249 |
| $\frac{1}{2}$ | 2164.76 | 164.934 | $\frac{1}{2}$ | 2596.73 | 180.642 |
| $\frac{5}{8}$ | 2175.08 | 165.327 | $\frac{5}{8}$ | 2608.03 | 181.035 |
| $\frac{3}{4}$ | 2185.42 | 165.719 | $\frac{3}{4}$ | 2619.36 | 181.427 |
| $\frac{7}{8}$ | 2195.79 | 166.112 | $\frac{7}{8}$ | 2630.71 | 181.820 |
| 53 | 2206.19 | 166.505 | 58 | 2642.09 | 182.213 |
| $\frac{1}{8}$ | 2216.61 | 166.897 | $\frac{1}{8}$ | 2653.49 | 182.605 |
| $\frac{1}{4}$ | 2227.05 | 167.290 | $\frac{1}{4}$ | 2664.91 | 182.998 |
| $\frac{3}{8}$ | 2237.52 | 167.688 | $\frac{3}{8}$ | 2676.36 | 183.391 |
| $\frac{1}{2}$ | 2248.01 | 168.076 | $\frac{1}{2}$ | 2687.84 | 183.784 |
| $\frac{5}{8}$ | 2258.53 | 168.468 | $\frac{5}{8}$ | 2699.33 | 184.176 |
| $\frac{3}{4}$ | 2269.07 | 168.861 | $\frac{3}{4}$ | 2710.86 | 184.569 |
| $\frac{7}{8}$ | 2279.64 | 169.254 | $\frac{7}{8}$ | 2722.41 | 184.962 |
| 54 | 2290.23 | 169.646 | 59 | 2733.98 | 185.354 |
| $\frac{1}{8}$ | 2300.84 | 170.039 | $\frac{1}{8}$ | 2745.57 | 185.747 |
| $\frac{1}{4}$ | 2311.48 | 170.432 | $\frac{1}{4}$ | 2757.20 | 186.140 |
| $\frac{3}{8}$ | 2322.15 | 170.824 | $\frac{3}{8}$ | 2768.84 | 186.532 |
| $\frac{1}{2}$ | 2332.83 | 171.217 | $\frac{1}{2}$ | 2780.51 | 186.925 |
| $\frac{5}{8}$ | 2343.55 | 171.610 | $\frac{5}{8}$ | 2792.21 | 187.318 |
| $\frac{3}{4}$ | 2354.29 | 172.003 | $\frac{3}{4}$ | 2803.93 | 187.711 |
| $\frac{7}{8}$ | 2365.05 | 172.395 | $\frac{7}{8}$ | 2815.67 | 188.103 |

AREAS AND CIRCUMFERENCES OF CIRCLES.

Diameters $\frac{1}{16}$ to 100.

| Diameter. | Area. | Circumference. | Diameter. | Area. | Circumference. |
|----------------|---------|----------------|----------------|---------|----------------|
| 60 | 2827.44 | 188.496 | 65 | 3318.31 | 204.204 |
| $\frac{1}{16}$ | 2839.23 | 188.889 | $\frac{1}{16}$ | 3331.09 | 204.597 |
| $\frac{1}{8}$ | 2851.05 | 189.281 | $\frac{1}{8}$ | 3343.89 | 204.989 |
| $\frac{3}{16}$ | 2862.89 | 189.674 | $\frac{3}{16}$ | 3356.71 | 205.382 |
| $\frac{1}{4}$ | 2874.76 | 190.067 | $\frac{1}{4}$ | 3369.56 | 205.775 |
| $\frac{5}{16}$ | 2886.65 | 190.459 | $\frac{5}{16}$ | 3382.44 | 206.167 |
| $\frac{3}{8}$ | 2898.57 | 190.852 | $\frac{3}{8}$ | 3395.33 | 206.560 |
| $\frac{7}{16}$ | 2910.51 | 191.245 | $\frac{7}{16}$ | 3408.26 | 206.953 |
| 61 | 2922.47 | 191.638 | 66 | 3421.20 | 207.346 |
| $\frac{1}{16}$ | 2934.46 | 192.030 | $\frac{1}{16}$ | 3434.17 | 207.738 |
| $\frac{1}{8}$ | 2946.48 | 192.423 | $\frac{1}{8}$ | 3447.17 | 208.131 |
| $\frac{3}{16}$ | 2958.52 | 192.816 | $\frac{3}{16}$ | 3460.19 | 208.524 |
| $\frac{1}{4}$ | 2970.58 | 193.208 | $\frac{1}{4}$ | 3473.24 | 208.916 |
| $\frac{5}{16}$ | 2982.67 | 193.601 | $\frac{5}{16}$ | 3486.30 | 209.309 |
| $\frac{3}{8}$ | 2994.78 | 193.994 | $\frac{3}{8}$ | 3499.40 | 209.702 |
| $\frac{7}{16}$ | 3006.92 | 194.386 | $\frac{7}{16}$ | 3512.52 | 210.094 |
| 62 | 3019.08 | 194.779 | 67 | 3525.66 | 210.487 |
| $\frac{1}{16}$ | 3031.26 | 195.172 | $\frac{1}{16}$ | 3538.83 | 210.880 |
| $\frac{1}{8}$ | 3043.47 | 195.565 | $\frac{1}{8}$ | 3552.02 | 211.273 |
| $\frac{3}{16}$ | 3055.71 | 195.957 | $\frac{3}{16}$ | 3565.24 | 211.665 |
| $\frac{1}{4}$ | 3067.97 | 196.350 | $\frac{1}{4}$ | 3578.48 | 212.058 |
| $\frac{5}{16}$ | 3080.25 | 196.743 | $\frac{5}{16}$ | 3591.74 | 212.451 |
| $\frac{3}{8}$ | 3092.56 | 197.135 | $\frac{3}{8}$ | 3605.04 | 212.843 |
| $\frac{7}{16}$ | 3104.89 | 197.528 | $\frac{7}{16}$ | 3618.35 | 213.236 |
| 63 | 3117.25 | 197.921 | 68 | 3631.69 | 213.629 |
| $\frac{1}{16}$ | 3129.64 | 198.313 | $\frac{1}{16}$ | 3645.05 | 214.021 |
| $\frac{1}{8}$ | 3142.04 | 198.706 | $\frac{1}{8}$ | 3658.44 | 214.414 |
| $\frac{3}{16}$ | 3154.47 | 199.099 | $\frac{3}{16}$ | 3671.86 | 214.807 |
| $\frac{1}{4}$ | 3166.93 | 199.492 | $\frac{1}{4}$ | 3685.29 | 215.200 |
| $\frac{5}{16}$ | 3179.41 | 199.884 | $\frac{5}{16}$ | 3698.76 | 215.592 |
| $\frac{3}{8}$ | 3191.91 | 200.277 | $\frac{3}{8}$ | 3712.24 | 215.985 |
| $\frac{7}{16}$ | 3204.44 | 200.670 | $\frac{7}{16}$ | 3725.75 | 216.378 |
| 64 | 3217.00 | 201.062 | 69 | 3739.29 | 216.770 |
| $\frac{1}{16}$ | 3229.58 | 201.455 | $\frac{1}{16}$ | 3752.85 | 217.163 |
| $\frac{1}{8}$ | 3242.18 | 201.848 | $\frac{1}{8}$ | 3766.43 | 217.556 |
| $\frac{3}{16}$ | 3254.81 | 202.240 | $\frac{3}{16}$ | 3780.04 | 217.948 |
| $\frac{1}{4}$ | 3267.46 | 202.633 | $\frac{1}{4}$ | 3793.68 | 218.341 |
| $\frac{5}{16}$ | 3280.14 | 203.026 | $\frac{5}{16}$ | 3807.34 | 218.734 |
| $\frac{3}{8}$ | 3292.84 | 203.419 | $\frac{3}{8}$ | 3821.02 | 219.127 |
| $\frac{7}{16}$ | 3305.56 | 203.811 | $\frac{7}{16}$ | 3834.73 | 219.519 |

AREAS AND CIRCUMFERENCES OF CIRCLES.

Diameters $\frac{1}{8}$ to 100.

| Diameter. | Area. | Circumference. | Diameter. | Area. | Circumference. |
|---------------|---------|----------------|---------------|---------|----------------|
| 70 | 3848.46 | 219.912 | 75 | 4417.87 | 235.620 |
| $\frac{1}{8}$ | 3862.22 | 220.305 | $\frac{1}{8}$ | 4432.61 | 236.013 |
| $\frac{1}{4}$ | 3876.00 | 220.697 | $\frac{1}{4}$ | 4447.38 | 236.405 |
| $\frac{3}{8}$ | 3889.80 | 221.090 | $\frac{3}{8}$ | 4462.16 | 236.798 |
| $\frac{1}{2}$ | 3903.63 | 221.483 | $\frac{1}{2}$ | 4476.98 | 237.191 |
| $\frac{5}{8}$ | 3917.49 | 221.875 | $\frac{5}{8}$ | 4491.81 | 237.583 |
| $\frac{3}{4}$ | 3931.37 | 222.268 | $\frac{3}{4}$ | 4506.67 | 237.976 |
| $\frac{7}{8}$ | 3945.27 | 222.661 | $\frac{7}{8}$ | 4521.56 | 238.369 |
| 71 | 3959.20 | 223.054 | 76 | 4536.47 | 238.762 |
| $\frac{1}{8}$ | 3973.15 | 223.446 | $\frac{1}{8}$ | 4551.41 | 239.154 |
| $\frac{1}{4}$ | 3987.13 | 223.839 | $\frac{1}{4}$ | 4566.36 | 239.547 |
| $\frac{3}{8}$ | 4001.13 | 224.232 | $\frac{3}{8}$ | 4581.35 | 239.940 |
| $\frac{1}{2}$ | 4015.16 | 224.624 | $\frac{1}{2}$ | 4596.36 | 240.332 |
| $\frac{5}{8}$ | 4029.21 | 225.017 | $\frac{5}{8}$ | 4611.39 | 240.725 |
| $\frac{3}{4}$ | 4043.29 | 225.410 | $\frac{3}{4}$ | 4626.45 | 241.118 |
| $\frac{7}{8}$ | 4057.39 | 225.802 | $\frac{7}{8}$ | 4641.53 | 241.510 |
| 72 | 4071.51 | 226.195 | 77 | 4656.64 | 241.903 |
| $\frac{1}{8}$ | 4085.66 | 226.588 | $\frac{1}{8}$ | 4671.77 | 242.296 |
| $\frac{1}{4}$ | 4099.84 | 226.981 | $\frac{1}{4}$ | 4686.92 | 242.689 |
| $\frac{3}{8}$ | 4114.04 | 227.373 | $\frac{3}{8}$ | 4702.10 | 243.081 |
| $\frac{1}{2}$ | 4128.26 | 227.766 | $\frac{1}{2}$ | 4717.31 | 243.474 |
| $\frac{5}{8}$ | 4142.51 | 228.159 | $\frac{5}{8}$ | 4732.54 | 243.867 |
| $\frac{3}{4}$ | 4156.78 | 228.551 | $\frac{3}{4}$ | 4747.79 | 244.259 |
| $\frac{7}{8}$ | 4171.08 | 228.944 | $\frac{7}{8}$ | 4763.07 | 244.652 |
| 73 | 4185.40 | 229.337 | 78 | 4778.37 | 245.045 |
| $\frac{1}{8}$ | 4199.74 | 229.729 | $\frac{1}{8}$ | 4793.70 | 245.437 |
| $\frac{1}{4}$ | 4214.11 | 230.122 | $\frac{1}{4}$ | 4809.05 | 245.830 |
| $\frac{3}{8}$ | 4228.51 | 230.515 | $\frac{3}{8}$ | 4824.43 | 246.223 |
| $\frac{1}{2}$ | 4242.93 | 230.908 | $\frac{1}{2}$ | 4839.83 | 246.616 |
| $\frac{5}{8}$ | 4257.37 | 231.300 | $\frac{5}{8}$ | 4855.26 | 247.008 |
| $\frac{3}{4}$ | 4271.84 | 231.693 | $\frac{3}{4}$ | 4870.71 | 247.401 |
| $\frac{7}{8}$ | 4286.33 | 232.086 | $\frac{7}{8}$ | 4886.18 | 247.794 |
| 74 | 4300.85 | 232.478 | 79 | 4901.68 | 248.186 |
| $\frac{1}{8}$ | 4315.39 | 232.871 | $\frac{1}{8}$ | 4917.21 | 248.579 |
| $\frac{1}{4}$ | 4329.96 | 233.264 | $\frac{1}{4}$ | 4932.75 | 248.972 |
| $\frac{3}{8}$ | 4344.55 | 233.656 | $\frac{3}{8}$ | 4948.33 | 249.364 |
| $\frac{1}{2}$ | 4359.17 | 234.049 | $\frac{1}{2}$ | 4963.92 | 249.757 |
| $\frac{5}{8}$ | 4373.81 | 234.442 | $\frac{5}{8}$ | 4979.55 | 250.150 |
| $\frac{3}{4}$ | 4388.47 | 234.835 | $\frac{3}{4}$ | 4995.19 | 250.543 |
| $\frac{7}{8}$ | 4403.16 | 235.227 | $\frac{7}{8}$ | 5010.86 | 250.935 |

AREAS AND CIRCUMFERENCES OF CIRCLES.

Diameters $\frac{1}{16}$ to 100.

| Diameter. | Area. | Circumference. | Diameter. | Area. | Circumference. |
|---------------|---------|----------------|---------------|---------|----------------|
| 80 | 5026.56 | 251.328 | 85 | 5674.51 | 267.036 |
| $\frac{1}{8}$ | 5042.28 | 251.721 | $\frac{1}{8}$ | 5691.22 | 267.429 |
| $\frac{1}{4}$ | 5058.03 | 252.113 | $\frac{1}{4}$ | 5707.94 | 267.821 |
| $\frac{3}{8}$ | 5073.79 | 252.506 | $\frac{3}{8}$ | 5724.69 | 268.214 |
| $\frac{1}{2}$ | 5089.59 | 252.899 | $\frac{1}{2}$ | 5741.47 | 268.607 |
| $\frac{5}{8}$ | 5105.41 | 253.291 | $\frac{5}{8}$ | 5758.27 | 268.999 |
| $\frac{3}{4}$ | 5121.25 | 253.684 | $\frac{3}{4}$ | 5775.10 | 269.392 |
| $\frac{7}{8}$ | 5137.12 | 254.077 | $\frac{7}{8}$ | 5791.94 | 269.785 |
| 81 | 5153.01 | 254.470 | 86 | 5808.82 | 270.178 |
| $\frac{1}{8}$ | 5168.93 | 254.862 | $\frac{1}{8}$ | 5825.72 | 270.570 |
| $\frac{1}{4}$ | 5184.87 | 255.255 | $\frac{1}{4}$ | 5842.64 | 270.963 |
| $\frac{3}{8}$ | 5200.83 | 255.648 | $\frac{3}{8}$ | 5859.59 | 271.356 |
| $\frac{1}{2}$ | 5216.82 | 256.040 | $\frac{1}{2}$ | 5876.56 | 271.748 |
| $\frac{5}{8}$ | 5232.84 | 256.433 | $\frac{5}{8}$ | 5893.55 | 272.141 |
| $\frac{3}{4}$ | 5248.88 | 256.826 | $\frac{3}{4}$ | 5910.58 | 272.534 |
| $\frac{7}{8}$ | 5264.94 | 257.218 | $\frac{7}{8}$ | 5927.62 | 272.926 |
| 82 | 5281.03 | 257.611 | 87 | 5944.69 | 273.319 |
| $\frac{1}{8}$ | 5297.14 | 258.004 | $\frac{1}{8}$ | 5961.79 | 273.712 |
| $\frac{1}{4}$ | 5313.28 | 258.397 | $\frac{1}{4}$ | 5978.91 | 274.105 |
| $\frac{3}{8}$ | 5329.44 | 258.789 | $\frac{3}{8}$ | 5996.05 | 274.497 |
| $\frac{1}{2}$ | 5345.63 | 259.182 | $\frac{1}{2}$ | 6013.22 | 274.890 |
| $\frac{5}{8}$ | 5361.84 | 259.575 | $\frac{5}{8}$ | 6030.41 | 275.283 |
| $\frac{3}{4}$ | 5378.08 | 259.967 | $\frac{3}{4}$ | 6047.63 | 275.675 |
| $\frac{7}{8}$ | 5394.34 | 260.360 | $\frac{7}{8}$ | 6064.87 | 276.068 |
| 83 | 5410.62 | 260.753 | 88 | 6082.14 | 276.461 |
| $\frac{1}{8}$ | 5426.93 | 261.145 | $\frac{1}{8}$ | 6099.43 | 276.853 |
| $\frac{1}{4}$ | 5443.26 | 261.538 | $\frac{1}{4}$ | 6116.74 | 277.246 |
| $\frac{3}{8}$ | 5459.62 | 261.931 | $\frac{3}{8}$ | 6134.08 | 277.638 |
| $\frac{1}{2}$ | 5476.01 | 262.324 | $\frac{1}{2}$ | 6151.45 | 278.032 |
| $\frac{5}{8}$ | 5492.41 | 262.716 | $\frac{5}{8}$ | 6168.84 | 278.424 |
| $\frac{3}{4}$ | 5508.84 | 263.109 | $\frac{3}{4}$ | 6186.25 | 278.817 |
| $\frac{7}{8}$ | 5525.30 | 263.502 | $\frac{7}{8}$ | 6203.69 | 279.210 |
| 84 | 5541.78 | 263.894 | 89 | 6221.15 | 279.602 |
| $\frac{1}{8}$ | 5558.29 | 264.287 | $\frac{1}{8}$ | 6238.64 | 279.995 |
| $\frac{1}{4}$ | 5574.82 | 264.680 | $\frac{1}{4}$ | 6256.15 | 280.388 |
| $\frac{3}{8}$ | 5591.37 | 265.072 | $\frac{3}{8}$ | 6273.69 | 280.780 |
| $\frac{1}{2}$ | 5607.95 | 265.465 | $\frac{1}{2}$ | 6291.25 | 281.173 |
| $\frac{5}{8}$ | 5624.56 | 265.858 | $\frac{5}{8}$ | 6308.84 | 281.566 |
| $\frac{3}{4}$ | 5641.18 | 266.251 | $\frac{3}{4}$ | 6326.45 | 281.959 |
| $\frac{7}{8}$ | 5657.84 | 266.643 | $\frac{7}{8}$ | 6344.08 | 282.351 |

AREAS AND CIRCUMFERENCES OF CIRCLES.

Diameters $\frac{1}{16}$ to 100.

| Diameter. | Area. | Circumference. | Diameter. | Area. | Circumference. |
|---------------|---------|----------------|---------------|---------|----------------|
| 90 | 6361.74 | 282.744 | 95 | 7088.24 | 298.452 |
| $\frac{1}{8}$ | 6379.42 | 283.137 | $\frac{1}{8}$ | 7106.90 | 298.845 |
| $\frac{1}{4}$ | 6397.13 | 283.529 | $\frac{1}{4}$ | 7125.59 | 299.237 |
| $\frac{3}{8}$ | 6414.86 | 283.922 | $\frac{3}{8}$ | 7144.31 | 299.630 |
| $\frac{1}{2}$ | 6432.62 | 284.315 | $\frac{1}{2}$ | 7163.04 | 300.023 |
| $\frac{5}{8}$ | 6450.40 | 284.707 | $\frac{5}{8}$ | 7181.81 | 300.415 |
| $\frac{3}{4}$ | 6468.21 | 285.100 | $\frac{3}{4}$ | 7200.60 | 300.808 |
| $\frac{7}{8}$ | 6486.04 | 285.493 | $\frac{7}{8}$ | 7219.41 | 301.201 |
| 91 | 6503.90 | 285.886 | 96 | 7238.25 | 301.594 |
| $\frac{1}{8}$ | 6521.78 | 286.278 | $\frac{1}{8}$ | 7257.11 | 301.986 |
| $\frac{1}{4}$ | 6539.68 | 286.671 | $\frac{1}{4}$ | 7275.99 | 302.379 |
| $\frac{3}{8}$ | 6557.61 | 287.064 | $\frac{3}{8}$ | 7294.91 | 302.772 |
| $\frac{1}{2}$ | 6575.56 | 287.456 | $\frac{1}{2}$ | 7313.84 | 303.164 |
| $\frac{5}{8}$ | 6593.54 | 287.849 | $\frac{5}{8}$ | 7332.80 | 303.557 |
| $\frac{3}{4}$ | 6611.55 | 288.242 | $\frac{3}{4}$ | 7351.79 | 303.950 |
| $\frac{7}{8}$ | 6629.57 | 288.634 | $\frac{7}{8}$ | 7370.79 | 304.342 |
| 92 | 6647.63 | 289.027 | 97 | 7389.83 | 304.735 |
| $\frac{1}{8}$ | 6665.70 | 289.420 | $\frac{1}{8}$ | 7408.89 | 305.128 |
| $\frac{1}{4}$ | 6683.80 | 289.813 | $\frac{1}{4}$ | 7427.97 | 305.521 |
| $\frac{3}{8}$ | 6701.93 | 290.205 | $\frac{3}{8}$ | 7447.08 | 305.913 |
| $\frac{1}{2}$ | 6720.08 | 290.598 | $\frac{1}{2}$ | 7466.21 | 306.306 |
| $\frac{5}{8}$ | 6738.25 | 290.991 | $\frac{5}{8}$ | 7485.37 | 306.699 |
| $\frac{3}{4}$ | 6756.45 | 291.383 | $\frac{3}{4}$ | 7504.55 | 307.091 |
| $\frac{7}{8}$ | 6774.68 | 291.776 | $\frac{7}{8}$ | 7523.75 | 307.484 |
| 93 | 6792.92 | 292.169 | 98 | 7542.98 | 307.877 |
| $\frac{1}{8}$ | 6811.20 | 292.562 | $\frac{1}{8}$ | 7562.24 | 308.270 |
| $\frac{1}{4}$ | 6829.49 | 292.954 | $\frac{1}{4}$ | 7581.52 | 308.662 |
| $\frac{3}{8}$ | 6847.82 | 293.347 | $\frac{3}{8}$ | 7600.82 | 309.055 |
| $\frac{1}{2}$ | 6866.16 | 293.740 | $\frac{1}{2}$ | 7620.15 | 309.448 |
| $\frac{5}{8}$ | 6884.53 | 294.132 | $\frac{5}{8}$ | 7639.50 | 309.840 |
| $\frac{3}{4}$ | 6902.93 | 294.525 | $\frac{3}{4}$ | 7658.88 | 310.233 |
| $\frac{7}{8}$ | 6921.35 | 294.918 | $\frac{7}{8}$ | 7678.28 | 310.626 |
| 94 | 6939.79 | 295.310 | 99 | 7697.71 | 311.018 |
| $\frac{1}{8}$ | 6958.26 | 295.703 | $\frac{1}{8}$ | 7717.16 | 311.411 |
| $\frac{1}{4}$ | 6976.76 | 296.096 | $\frac{1}{4}$ | 7736.63 | 311.804 |
| $\frac{3}{8}$ | 6995.28 | 296.488 | $\frac{3}{8}$ | 7756.13 | 312.196 |
| $\frac{1}{2}$ | 7013.82 | 296.881 | $\frac{1}{2}$ | 7775.66 | 312.589 |
| $\frac{5}{8}$ | 7032.39 | 297.274 | $\frac{5}{8}$ | 7795.21 | 312.982 |
| $\frac{3}{4}$ | 7050.98 | 297.667 | $\frac{3}{4}$ | 7814.78 | 313.375 |
| $\frac{7}{8}$ | 7069.59 | 298.059 | $\frac{7}{8}$ | 7834.38 | 313.767 |
| | | | 100 | 7854.00 | 314.160 |

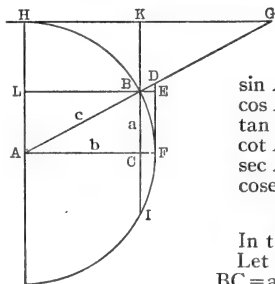
LOGARITHMS OF NUMBERS, FROM 0 TO 1000.

| No. | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
|-----|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 0 | 0 | 00000 | 30103 | 47712 | 60206 | 69897 | 77815 | 84510 | 90309 | 95424 |
| 10 | 00000 | 00432 | 00860 | 01284 | 01703 | 02119 | 02531 | 02938 | 03342 | 03743 |
| 11 | 04139 | 04532 | 04922 | 05308 | 05690 | 06070 | 06446 | 06819 | 07188 | 07555 |
| 12 | 07918 | 08279 | 08636 | 08991 | 09342 | 09691 | 10037 | 10380 | 10721 | 11059 |
| 13 | 11394 | 11727 | 12057 | 12385 | 12710 | 13033 | 13354 | 13672 | 13988 | 14301 |
| 14 | 14613 | 14922 | 15229 | 15534 | 15836 | 16137 | 16435 | 16732 | 17026 | 17319 |
| 15 | 17609 | 17898 | 18184 | 18469 | 18752 | 19033 | 19312 | 19590 | 19866 | 20140 |
| 16 | 20412 | 20683 | 20952 | 21219 | 21484 | 21748 | 22011 | 22272 | 22531 | 22789 |
| 17 | 23045 | 23300 | 23553 | 23805 | 24055 | 24304 | 24551 | 24797 | 25042 | 25285 |
| 18 | 25527 | 25768 | 26007 | 26245 | 26482 | 26717 | 26951 | 27184 | 27416 | 27646 |
| 19 | 27875 | 28103 | 28330 | 28556 | 28780 | 29003 | 29226 | 29447 | 29667 | 29885 |
| 20 | 30103 | 30320 | 30535 | 30750 | 30963 | 31175 | 31387 | 31597 | 31806 | 32015 |
| 21 | 32222 | 32428 | 32634 | 32838 | 33041 | 33244 | 33445 | 33646 | 33846 | 34044 |
| 22 | 34242 | 34439 | 34635 | 34830 | 35025 | 35218 | 35411 | 35603 | 35793 | 35984 |
| 23 | 36173 | 36361 | 36549 | 36736 | 36922 | 37107 | 37291 | 37475 | 37658 | 37840 |
| 24 | 38021 | 38202 | 38382 | 38561 | 38739 | 38917 | 39094 | 39270 | 39445 | 39620 |
| 25 | 39794 | 39967 | 40140 | 40312 | 40483 | 40654 | 40824 | 40993 | 41162 | 41330 |
| 26 | 41497 | 41664 | 41830 | 41996 | 42160 | 42325 | 42488 | 42651 | 42813 | 42975 |
| 27 | 43136 | 43297 | 43457 | 43616 | 43775 | 43933 | 44091 | 44248 | 44404 | 44560 |
| 28 | 44716 | 44871 | 45025 | 45179 | 45332 | 45484 | 45637 | 45788 | 45939 | 46090 |
| 29 | 46240 | 46389 | 46538 | 46687 | 46835 | 46982 | 47129 | 47276 | 47422 | 47567 |
| 30 | 47712 | 47857 | 48001 | 48144 | 48287 | 48430 | 48572 | 48714 | 48855 | 48996 |
| 31 | 49136 | 49276 | 49415 | 49554 | 49693 | 49831 | 49969 | 50106 | 50243 | 50379 |
| 32 | 50515 | 50651 | 50786 | 50920 | 51055 | 51188 | 51322 | 51455 | 51587 | 51720 |
| 33 | 51851 | 51983 | 52114 | 52244 | 52375 | 52504 | 52634 | 52763 | 52892 | 53020 |
| 34 | 53148 | 53275 | 53403 | 53529 | 53656 | 53782 | 53908 | 54033 | 54158 | 54283 |
| 35 | 54407 | 54531 | 54654 | 54777 | 54900 | 55023 | 55145 | 55267 | 55388 | 55509 |
| 36 | 55630 | 55751 | 55871 | 55991 | 56110 | 56229 | 56348 | 56467 | 56585 | 56703 |
| 37 | 56820 | 56937 | 57054 | 57171 | 57287 | 57403 | 57519 | 57634 | 57749 | 57864 |
| 38 | 57978 | 58093 | 58206 | 58320 | 58433 | 58546 | 58659 | 58771 | 58883 | 58995 |
| 39 | 59106 | 59218 | 59329 | 59439 | 59550 | 59660 | 59770 | 59879 | 59988 | 60097 |
| 40 | 60206 | 60314 | 60423 | 60531 | 60638 | 60746 | 60853 | 60959 | 61066 | 61172 |
| 41 | 61278 | 61384 | 61490 | 61595 | 61700 | 61805 | 61909 | 62014 | 62118 | 62221 |
| 42 | 62325 | 62428 | 62531 | 62634 | 62737 | 62839 | 62941 | 63043 | 63144 | 63246 |
| 43 | 63347 | 63448 | 63548 | 63649 | 63749 | 63849 | 63949 | 64048 | 64147 | 64246 |
| 44 | 64345 | 64444 | 64542 | 64640 | 64738 | 64836 | 64933 | 65031 | 65128 | 65225 |
| 45 | 65321 | 65418 | 65514 | 65610 | 65706 | 65801 | 65896 | 65992 | 66087 | 66181 |
| 46 | 66276 | 66370 | 66464 | 66558 | 66652 | 66745 | 66839 | 66932 | 67025 | 67117 |
| 47 | 67210 | 67302 | 67394 | 67486 | 67578 | 67669 | 67761 | 67852 | 67943 | 68034 |
| 48 | 68124 | 68215 | 68305 | 68395 | 68485 | 68574 | 68664 | 68753 | 68842 | 68931 |
| 49 | 69020 | 69108 | 69197 | 69285 | 69373 | 69461 | 69548 | 69636 | 69723 | 69810 |
| 50 | 69897 | 69984 | 70070 | 70157 | 70243 | 70329 | 70415 | 70501 | 70586 | 70672 |
| 51 | 70757 | 70842 | 70927 | 71012 | 71096 | 71181 | 71265 | 71349 | 71433 | 71517 |
| 52 | 71600 | 71684 | 71767 | 71850 | 71933 | 72016 | 72099 | 72181 | 72263 | 72346 |
| 53 | 72428 | 72509 | 72591 | 72673 | 72754 | 72835 | 72916 | 72997 | 73078 | 73159 |
| 54 | 73239 | 73320 | 73400 | 73480 | 73560 | 73640 | 73719 | 73799 | 73878 | 73957 |

LOGARITHMS OF NUMBERS, FROM 0 TO 1000

(CONTINUED.)

| No. | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
|-----|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 55 | 74036 | 74115 | 74194 | 74273 | 74351 | 74429 | 74507 | 74586 | 74663 | 74741 |
| 56 | 74819 | 74896 | 74974 | 75051 | 75128 | 75205 | 75282 | 75358 | 75435 | 75511 |
| 57 | 75587 | 75664 | 75740 | 75815 | 75891 | 75967 | 76042 | 76118 | 76193 | 76268 |
| 58 | 76343 | 76418 | 76492 | 76567 | 76641 | 76716 | 76790 | 76864 | 76938 | 77012 |
| 59 | 77085 | 77159 | 77232 | 77305 | 77379 | 77452 | 77525 | 77597 | 77670 | 77743 |
| 60 | 77815 | 77887 | 77960 | 78032 | 78104 | 78176 | 78247 | 78319 | 78390 | 78462 |
| 61 | 78533 | 78604 | 78675 | 78746 | 78817 | 78888 | 78958 | 79029 | 79099 | 79169 |
| 62 | 79239 | 79309 | 79379 | 79449 | 79518 | 79588 | 79657 | 79727 | 79796 | 79865 |
| 63 | 79934 | 80003 | 80072 | 80140 | 80209 | 80277 | 80346 | 80414 | 80482 | 80550 |
| 64 | 80618 | 80686 | 80754 | 80821 | 80889 | 80956 | 81023 | 81090 | 81158 | 81224 |
| 65 | 81291 | 81358 | 81425 | 81491 | 81558 | 81624 | 81690 | 81757 | 81823 | 81889 |
| 66 | 81954 | 82020 | 82086 | 82151 | 82217 | 82282 | 82347 | 82413 | 82478 | 82543 |
| 67 | 82607 | 82672 | 82737 | 82802 | 82866 | 82930 | 82995 | 83059 | 83123 | 83187 |
| 68 | 83251 | 83315 | 83378 | 83442 | 83506 | 83569 | 83632 | 83696 | 83759 | 83822 |
| 69 | 83885 | 83948 | 84011 | 84073 | 84136 | 84198 | 84261 | 84323 | 84386 | 84448 |
| 70 | 84510 | 84572 | 84634 | 84696 | 84757 | 84819 | 84880 | 84942 | 85003 | 85065 |
| 71 | 85126 | 85187 | 85248 | 85309 | 85370 | 85431 | 85491 | 85552 | 85612 | 85673 |
| 72 | 85733 | 85794 | 85854 | 85914 | 85974 | 86034 | 86094 | 86153 | 86213 | 86273 |
| 73 | 86332 | 86392 | 86451 | 86510 | 86570 | 86629 | 86688 | 86747 | 86806 | 86864 |
| 74 | 86923 | 86982 | 87040 | 87099 | 87157 | 87216 | 87274 | 87332 | 87390 | 87448 |
| 75 | 87506 | 87564 | 87622 | 87680 | 87737 | 87795 | 87852 | 87910 | 87967 | 88024 |
| 76 | 88081 | 88138 | 88196 | 88252 | 88309 | 88366 | 88423 | 88480 | 88536 | 88593 |
| 77 | 88649 | 88705 | 88762 | 88818 | 88874 | 88930 | 88986 | 89042 | 89098 | 89154 |
| 78 | 89209 | 89265 | 89321 | 89376 | 89432 | 89487 | 89542 | 89597 | 89653 | 89708 |
| 79 | 89763 | 89818 | 89873 | 89927 | 89982 | 90037 | 90091 | 90146 | 90200 | 90255 |
| 80 | 90309 | 90363 | 90417 | 90472 | 90526 | 90580 | 90634 | 90687 | 90741 | 90795 |
| 81 | 90849 | 90902 | 90956 | 91009 | 91062 | 91116 | 91169 | 91222 | 91275 | 91328 |
| 82 | 91381 | 91434 | 91487 | 91540 | 91593 | 91645 | 91698 | 91751 | 91803 | 91855 |
| 83 | 91908 | 91960 | 92012 | 92065 | 92117 | 92169 | 92221 | 92273 | 92324 | 92376 |
| 84 | 92428 | 92480 | 92531 | 92583 | 92634 | 92686 | 92737 | 92788 | 92840 | 92891 |
| 85 | 92942 | 92993 | 93044 | 93095 | 93146 | 93197 | 93247 | 93298 | 93349 | 93399 |
| 86 | 93450 | 93500 | 93551 | 93601 | 93651 | 93702 | 93752 | 93802 | 93852 | 93902 |
| 87 | 93952 | 94002 | 94052 | 94101 | 94151 | 94201 | 94250 | 94300 | 94349 | 94399 |
| 88 | 94448 | 94498 | 94547 | 94596 | 94645 | 94694 | 94743 | 94792 | 94841 | 94890 |
| 89 | 94939 | 94988 | 95036 | 95085 | 95134 | 95182 | 95231 | 95279 | 95328 | 95376 |
| 90 | 95424 | 95472 | 95521 | 95569 | 95617 | 95665 | 95713 | 95761 | 95809 | 95856 |
| 91 | 95904 | 95952 | 95999 | 96047 | 96095 | 96142 | 96190 | 96237 | 96284 | 96332 |
| 92 | 96379 | 96426 | 96473 | 96520 | 96567 | 96614 | 96661 | 96708 | 96755 | 96802 |
| 93 | 96848 | 96895 | 96942 | 96988 | 97035 | 97081 | 97128 | 97174 | 97220 | 97267 |
| 94 | 97313 | 97359 | 97405 | 97451 | 97497 | 97543 | 97589 | 97635 | 97681 | 97727 |
| 95 | 97772 | 97818 | 97864 | 97909 | 97955 | 98000 | 98046 | 98091 | 98137 | 98182 |
| 96 | 98227 | 98272 | 98318 | 98363 | 98408 | 98453 | 98498 | 98543 | 98588 | 98632 |
| 97 | 98677 | 98722 | 98767 | 98811 | 98856 | 98900 | 98945 | 98989 | 99034 | 99078 |
| 98 | 99123 | 99167 | 99211 | 99255 | 99300 | 99344 | 99388 | 99432 | 99476 | 99520 |
| 99 | 99564 | 99607 | 99651 | 99695 | 99739 | 99782 | 99826 | 99870 | 99913 | 99957 |

TRIGONOMETRIC FORMULAE.**TRIGONOMETRIC FUNCTIONS.**

Let $A = \text{angle } BAC = \text{arc } BF$.
Let radius $AF = AB = AH = 1$.

Then

| | |
|------------------------|-------------------------------|
| $\sin A = BC$ | $\text{versin } A = CF = BE$ |
| $\cos A = AC$ | $\text{covers } A = BK = HL$ |
| $\tan A = DF$ | $\text{exsec } A = BD$ |
| $\cot A = HG$ | $\text{coexsec } A = BG$ |
| $\sec A = AD$ | $\text{chord } A = BF$ |
| $\text{cosec } A = AG$ | $\text{chord } 2A = BI = 2BC$ |

RIGHT-ANGLED TRIANGLES.

In the right-angled triangle ABC ,

Let side $AB = c$, side $AC = b$, and side $BC = a$; let angle $ABC = B$.

Then

$$\sin A = \frac{a}{c} = \cos B \qquad a = c \sin A = b \tan A$$

$$\cos A = \frac{b}{c} = \sin B \qquad b = c \cos A = a \cot A$$

$$\tan A = \frac{a}{b} = \cot B \qquad c = \frac{a}{\sin A} = \frac{b}{\cos A}$$

$$\cot A = \frac{b}{a} = \tan B \qquad a = c \cos B = b \cot B$$

$$\sec A = \frac{c}{b} = \text{cosec } B \qquad b = c \sin B = a \tan B$$

$$\text{cosec } A = \frac{c}{a} = \sec B \qquad c = \frac{a}{\cos B} = \frac{b}{\sin B}$$

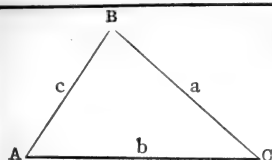
$$\text{vers } A = \frac{c-b}{c} = \text{covers } B \qquad a = \sqrt{(c+b)(c-b)}$$

$$\text{exsec } A = \frac{c-b}{b} = \text{coexsec } B \qquad b = \sqrt{(c+a)(c-a)}$$

$$\text{covers } A = \frac{c-a}{c} = \text{versin } B \qquad c = \sqrt{a^2 + b^2}$$

$$\text{coexsec } A = \frac{c-a}{a} = \text{exsec } B \qquad C = 90^\circ = A + B$$

$$\text{Area} = \frac{ab}{2} = \frac{a}{2} \sqrt{c^2 - a^2} = \frac{a^2 \cot A}{2} = \frac{b^2 \tan A}{2} = \frac{c^2 \sin 2A}{4}$$

**TRIGONOMETRIC FORMULÆ***(Continued).***OBLIQUE TRIANGLES.**

$$s = \frac{1}{2} (a + b + c)$$

| KNOWN | REQUIRED | FORMULÆ |
|------------|-----------------------|---|
| A, B, a | C, b | $C = 180^\circ - (A + B), \quad b = \frac{a}{\sin A} \cdot \sin B,$ |
| | c | $c = \frac{a}{\sin A} \sin (A + B)$ |
| A, a, b | B, C | $\sin B = \frac{\sin A}{a} \cdot b, \quad C = 180^\circ - (A + B),$ |
| | c | $c = \frac{a}{\sin A} \cdot \sin C$ |
| C, a, b | $\frac{1}{2} (A + B)$ | $\frac{1}{2} (A + B) = 90^\circ - \frac{1}{2} C$ |
| | $\frac{1}{2} (A - B)$ | $\tan \frac{1}{2} (A - B) = \frac{a - b}{a + b} \tan \frac{1}{2} (A + B)$ |
| | A, B | $A = \frac{1}{2} (A + B) + \frac{1}{2} (A - B),$ $B = \frac{1}{2} (A + B) - \frac{1}{2} (A - B)$ |
| | c | $c = (a + b) \frac{\cos \frac{1}{2} (A + B)}{\cos \frac{1}{2} (A - B)}$ $= (a - b) \frac{\sin \frac{1}{2} (A + B)}{\sin \frac{1}{2} (A - B)}$ $= \sqrt{a^2 + b^2 - 2ab \cdot \cos C}$ |
| | area | $\text{area} = \frac{1}{2} a b \sin C.$ |
| a, b, c | A | $\sin \frac{1}{2} A = \sqrt{\frac{(s - b)(s - c)}{b c}}$ $\cos \frac{1}{2} A = \sqrt{\frac{s(s - a)}{b c}}$ $\tan \frac{1}{2} A = \sqrt{\frac{(s - b)(s - c)}{s(s - a)}}$ $\sin A = \frac{2 \sqrt{s(s - a)(s - b)(s - c)}}{b c}$ $\text{vers } A = \frac{2(s - b)(s - c)}{b c}$ |
| | area | $\text{area} = \sqrt{s(s - a)(s - b)(s - c)}$ |
| A, B, C, a | area | $\text{area} = \frac{a^2 \sin B \cdot \sin C}{2 \sin A}$ |

TRIGONOMETRIC FORMULÆ—(Continued).
GENERAL.

$$\sin A = \frac{1}{\operatorname{cosec} A} = \sqrt{1 - \cos^2 A} = \tan A \cos A$$

$$= 2 \sin \frac{1}{2} A \cos \frac{1}{2} A = \operatorname{vers} A \cot \frac{1}{2} A$$

$$= \sqrt{\frac{1}{2} \operatorname{vers} 2 A} = \sqrt{\frac{1}{2} (1 - \cos 2 A)}$$

$$\cos A = \frac{1}{\sec A} = \sqrt{1 - \sin^2 A} = \cot A \sin A$$

$$= 1 - \operatorname{vers} A = 2 \cos^2 \frac{1}{2} A - 1 = 1 - 2 \sin^2 \frac{1}{2} A$$

$$= \cos^2 \frac{1}{2} A - \sin^2 \frac{1}{2} A = \sqrt{\frac{1}{2} + \frac{1}{2} \cos 2 A}$$

$$\tan A = \frac{1}{\cot A} = \frac{\sin A}{\cos A} = \sqrt{\sec^2 A - 1}$$

$$= \sqrt{\frac{1}{\cos^2 A} - 1} = \frac{\sqrt{1 - \cos^2 A}}{\cos A} = \frac{\sin 2 A}{1 + \cos 2 A}$$

$$= \frac{1 - \cos 2 A}{\sin 2 A} = \frac{\operatorname{vers} 2 A}{\sin 2 A} = \operatorname{exsec} A \cot \frac{1}{2} A$$

$$\cot A = \frac{1}{\tan A} = \frac{\cos A}{\sin A} = \sqrt{\operatorname{cosec}^2 A - 1}$$

$$= \frac{\sin 2 A}{1 - \cos 2 A} = \frac{\sin 2 A}{\operatorname{vers} 2 A} = \frac{1 + \cos 2 A}{\sin 2 A} = \frac{\tan \frac{1}{2} A}{\operatorname{exsec} A}$$

$$\operatorname{vers} A = 1 - \cos A = \sin A \tan \frac{1}{2} A = 2 \sin^2 \frac{1}{2} A$$

$$= \operatorname{exsec} A \cos A$$

$$\operatorname{exsec} A = \sec A - 1 = \tan A \tan \frac{1}{2} A = \frac{\operatorname{vers} A}{\cos A}$$

$$\sin \frac{1}{2} A = \sqrt{\frac{1 - \cos A}{2}} = \sqrt{\frac{\operatorname{vers} A}{2}}$$

$$\cos \frac{1}{2} A = \sqrt{\frac{1 + \cos A}{2}}$$

$$\tan \frac{1}{2} A = \frac{\tan A}{1 + \sec A} = \operatorname{cosec} A - \cot A = \frac{1 - \cos A}{\sin A} = \sqrt{\frac{1 - \cos A}{1 + \cos A}}$$

$$\cot \frac{1}{2} A = \frac{\sin A}{\operatorname{vers} A} = \frac{1 + \cos A}{\sin A} = \frac{1}{\operatorname{cosec} A - \cot A}$$

$$\operatorname{vers} \frac{1}{2} A = \frac{\frac{1}{2} \operatorname{vers} A}{1 + \sqrt{1 - \frac{1}{2} \operatorname{vers} A}} = \frac{1 - \cos A}{2 + \sqrt{2} (1 + \cos A)}$$

TRIGONOMETRIC FORMULÆ—(Continued).**GENERAL.**

$$\operatorname{exsec} \frac{1}{2} A = \frac{1 - \cos A}{(1 + \cos A) + \sqrt{2(1 + \cos A)}}$$

$$\sin 2 A = 2 \sin A \cos A$$

$$\cos 2 A = 2 \cos^2 A - 1 = \cos^2 A - \sin^2 A = 1 - 2 \sin^2 A$$

$$\tan 2 A = \frac{2 \tan A}{1 - \tan^2 A}$$

$$\cot 2 A = \frac{\cot^2 A - 1}{2 \cot A}$$

$$\operatorname{vers} 2 A = 2 \sin^2 A = 2 \sin A \cos A \tan A$$

$$\operatorname{exsec} 2 A = \frac{2 \tan^2 A}{1 - \tan^2 A}$$

$$\sin 3 A = 3 \sin A - 4 \sin^3 A$$

$$\cos 3 A = 4 \cos^3 A - 3 \cos A$$

$$\tan 3 A = \frac{3 \tan A - \tan^3 A}{1 - 3 \tan^2 A}$$

$$\sin 4 A = 4 \sin A \cos A - 8 \sin^3 A \cos A$$

$$\cos 4 A = 1 - 8 \cos^2 A + 8 \cos^4 A$$

$$\tan 4 A = \frac{4 \tan A - 4 \tan^3 A}{1 - 6 \tan^2 A + \tan^4 A}$$

$$\sin (A+B) = \sin A \cdot \cos B + \sin B \cdot \cos A$$

$$\sin (A-B) = \sin A \cdot \cos B - \sin B \cdot \cos A$$

$$\cos (A+B) = \cos A \cdot \cos B - \sin A \cdot \sin B$$

$$\cos (A-B) = \cos A \cdot \cos B + \sin A \cdot \sin B$$

$$\sin A + \sin B = 2 \sin \frac{1}{2} (A+B) \cos \frac{1}{2} (A-B)$$

$$\sin A - \sin B = 2 \cos \frac{1}{2} (A+B) \sin \frac{1}{2} (A-B)$$

$$\cos A + \cos B = 2 \cos \frac{1}{2} (A+B) \cos \frac{1}{2} (A-B)$$

$$\cos B - \cos A = 2 \sin \frac{1}{2} (A+B) \sin \frac{1}{2} (A-B)$$

$$\sin^2 A - \sin^2 B = \cos^2 B - \cos^2 A = \sin (A+B) \sin (A-B)$$

$$\cos^2 A - \sin^2 B = \cos (A+B) \cos (A-B)$$

$$\tan A + \tan B = \frac{\sin (A+B)}{\cos A \cdot \cos B}$$

$$\tan A - \tan B = \frac{\sin (A-B)}{\cos A \cdot \cos B}$$

| FUNCTION. | QUADRANT SIGN. | | | |
|----------------------------|----------------|-----|-----|-----|
| | 1st | 2nd | 3rd | 4th |
| sine, cosecant, coexsecant | + | + | — | — |
| cosine, secant, exsecant | + | — | — | + |
| tangent, cotangent | + | — | + | — |
| versed sine, covered sine | + | + | + | + |

NATURAL SINES, COSECANTS, TANGENTS, ETC.

| ° | ' | Sine. | Cosecant. | Tangent. | Cotangent. | Secant. | Cosine. | ' | ° |
|---|----|---------|-----------|------------|------------|-----------|----------|----|----|
| 0 | 0 | .000000 | Infinite. | .000000 | Infinite. | 1.00000 | 1.000000 | 0 | 90 |
| | 10 | .002909 | 343.77516 | .002909 | 343.77371 | 1.00000 | .999996 | 50 | |
| | 20 | .005818 | 171.88831 | .005818 | 171.88540 | 1.00002 | .999983 | 40 | |
| | 30 | .008727 | 114.59301 | .008727 | 114.58865 | 1.00004 | .999962 | 30 | |
| | 40 | .011635 | 85.945609 | .011636 | 85.939791 | 1.00007 | .999932 | 20 | |
| | 50 | .014544 | 68.757360 | .014545 | 68.750087 | 1.00011 | .999894 | 10 | |
| 1 | 0 | .017452 | 57.298688 | .017455 | 57.289962 | 1.00015 | .999848 | 0 | 89 |
| | 10 | .020361 | 49.114062 | .020365 | 49.103881 | 1.00021 | .999793 | 50 | |
| | 20 | .023269 | 42.975713 | .023275 | 42.964077 | 1.00027 | .999729 | 40 | |
| | 30 | .026177 | 38.201550 | .026186 | 38.188459 | 1.00034 | .999657 | 30 | |
| | 40 | .029085 | 34.382316 | .029097 | 34.367771 | 1.00042 | .999577 | 20 | |
| | 50 | .031992 | 31.257577 | .032009 | 31.241577 | 1.00051 | .999488 | 10 | |
| 2 | 0 | .034899 | 28.653708 | .034921 | 28.636253 | 1.00061 | .999391 | 0 | 88 |
| | 10 | .037806 | 26.450510 | .037834 | 26.431600 | 1.00072 | .999285 | 50 | |
| | 20 | .040713 | 24.562123 | .040747 | 24.541758 | 1.00083 | .999171 | 40 | |
| | 30 | .043619 | 22.925586 | .043661 | 22.903766 | 1.00095 | .999048 | 30 | |
| | 40 | .046525 | 21.493676 | .046576 | 21.470401 | 1.00108 | .998917 | 20 | |
| | 50 | .049431 | 20.230284 | .049491 | 20.205553 | 1.00122 | .998778 | 10 | |
| 3 | 0 | .052336 | 19.107323 | .052408 | 19.081137 | 1.00137 | .998630 | 0 | 87 |
| | 10 | .055241 | 18.102619 | .055325 | 18.074977 | 1.00153 | .998473 | 50 | |
| | 20 | .058145 | 17.198434 | .058243 | 17.169337 | 1.00169 | .998308 | 40 | |
| | 30 | .061049 | 16.380408 | .061163 | 16.349855 | 1.00187 | .998135 | 30 | |
| | 40 | .063952 | 15.636793 | .064083 | 15.604784 | 1.00205 | .997953 | 20 | |
| | 50 | .066854 | 14.957882 | .067004 | 14.924417 | 1.00224 | .997763 | 10 | |
| 4 | 0 | .069756 | 14.335587 | .069927 | 14.300666 | 1.00244 | .997564 | 0 | 86 |
| | 10 | .072658 | 13.763115 | .072851 | 13.726738 | 1.00265 | .997357 | 50 | |
| | 20 | .075559 | 13.234717 | .075776 | 13.196888 | 1.00287 | .997141 | 40 | |
| | 30 | .078459 | 12.745495 | .078702 | 12.706205 | 1.00309 | .996917 | 30 | |
| | 40 | .081359 | 12.291252 | .081629 | 12.250505 | 1.00333 | .996685 | 20 | |
| | 50 | .084258 | 11.868370 | .084558 | 11.826167 | 1.00357 | .996444 | 10 | |
| 5 | 0 | .087156 | 11.473713 | .087489 | 11.430052 | 1.00382 | .996195 | 0 | 85 |
| | 10 | .090053 | 11.104549 | .090421 | 11.059431 | 1.00408 | .995937 | 50 | |
| | 20 | .092950 | 10.758488 | .093354 | 10.711913 | 1.00435 | .995671 | 40 | |
| | 30 | .095846 | 10.433431 | .096289 | 10.385397 | 1.00463 | .995396 | 30 | |
| | 40 | .098741 | 10.127522 | .099226 | 10.078031 | 1.00491 | .995113 | 20 | |
| | 50 | .101635 | 9.8391227 | .102164 | 9.7881732 | 1.00521 | .994822 | 10 | |
| 6 | 0 | .104528 | 9.5667722 | .105104 | 9.5143645 | 1.00551 | .994522 | 0 | 84 |
| | 10 | .107421 | 9.3091699 | .108046 | 9.2553035 | 1.00582 | .994214 | 50 | |
| | 20 | .110313 | 9.0651512 | .110990 | 9.0098261 | 1.00614 | .993897 | 40 | 83 |
| ° | ' | Cosine. | Secant. | Cotangent. | Tangent. | Cosecant. | Sine. | ' | ° |

For functions from 83°-40' to 90° read from bottom of table upward.

NATURAL SINES, COSECANTS, TANGENTS, ETC.

| ° | ' | Sine. | Cosecant. | Tangent. | Cotangent. | Secant. | Cosine. | ' | ° |
|----|----|---------|-----------|------------|------------|-----------|---------|----|----|
| 6 | 30 | .113203 | 8.8336715 | .113936 | 8.7768874 | 1.00647 | .993572 | 30 | |
| | 40 | .116093 | 8.6137901 | .116883 | 8.5555468 | 1.00681 | .993238 | 20 | |
| | 50 | .118982 | 8.4045586 | .119833 | 8.3449558 | 1.00715 | .992896 | 10 | |
| 7 | 0 | .121869 | 8.2055090 | .122785 | 8.1443464 | 1.00751 | .992546 | 0 | 83 |
| | 10 | .124756 | 8.0156450 | .125738 | 7.9530224 | 1.00787 | .992187 | 50 | |
| | 20 | .127642 | 7.8344335 | .128694 | 7.7703506 | 1.00825 | .991820 | 40 | |
| | 30 | .130526 | 7.6612976 | .131653 | 7.5957541 | 1.00863 | .991445 | 30 | |
| | 40 | .133410 | 7.4957100 | .134613 | 7.4287064 | 1.00902 | .991061 | 20 | |
| | 50 | .136292 | 7.3371909 | .137576 | 7.2687255 | 1.00942 | .990669 | 10 | |
| 8 | 0 | .139173 | 7.1852965 | .140541 | 7.1153697 | 1.00983 | .990268 | 0 | 82 |
| | 10 | .142053 | 7.0396220 | .143508 | 6.9682335 | 1.01024 | .989859 | 50 | |
| | 20 | .144932 | 6.8997942 | .146478 | 6.8269437 | 1.01067 | .989442 | 40 | |
| | 30 | .147809 | 6.7654691 | .149451 | 6.6911562 | 1.01111 | .989016 | 30 | |
| | 40 | .150686 | 6.6363293 | .152426 | 6.5605538 | 1.01155 | .988582 | 20 | |
| | 50 | .153561 | 6.5120812 | .155404 | 6.4348428 | 1.01200 | .988139 | 10 | |
| 9 | 0 | .156434 | 6.3924532 | .158384 | 6.3137515 | 1.01247 | .987688 | 0 | 81 |
| | 10 | .159307 | 6.2771933 | .161368 | 6.1970279 | 1.01294 | .987229 | 50 | |
| | 20 | .162178 | 6.1660674 | .164354 | 6.0844381 | 1.01342 | .986762 | 40 | |
| | 30 | .165048 | 6.0588583 | .167343 | 5.9757644 | 1.01391 | .986286 | 30 | |
| | 40 | .167916 | 5.9553625 | .170334 | 5.8708042 | 1.01440 | .985801 | 20 | |
| | 50 | .170783 | 5.8553921 | .173329 | 5.7693688 | 1.01491 | .985309 | 10 | |
| 10 | 0 | .173648 | 5.7587705 | .176327 | 5.6712818 | 1.01543 | .984808 | 0 | 80 |
| | 10 | .176512 | 5.6653331 | .179328 | 5.5763786 | 1.01595 | .984298 | 50 | |
| | 20 | .179375 | 5.5749258 | .182332 | 5.4845052 | 1.01649 | .983781 | 40 | |
| | 30 | .182236 | 5.4874043 | .185339 | 5.3955172 | 1.01703 | .983255 | 30 | |
| | 40 | .185095 | 5.4026333 | .188359 | 5.3092793 | 1.01758 | .982721 | 20 | |
| | 50 | .187953 | 5.3204860 | .191363 | 5.2256647 | 1.01815 | .982178 | 10 | |
| 11 | 0 | .190809 | 5.2408431 | .194380 | 5.1445540 | 1.01872 | .981627 | 0 | 79 |
| | 10 | .193664 | 5.1635924 | .197401 | 5.0658352 | 1.01930 | .981068 | 50 | |
| | 20 | .196517 | 5.0886284 | .200425 | 4.9894027 | 1.01989 | .980500 | 40 | |
| | 30 | .199368 | 5.0158517 | .203452 | 4.9151570 | 1.02049 | .979925 | 30 | |
| | 40 | .202218 | 4.9451687 | .206483 | 4.8430045 | 1.02110 | .979341 | 20 | |
| | 50 | .205065 | 4.8764907 | .209518 | 4.7728568 | 1.02171 | .978748 | 10 | |
| 12 | 0 | .207912 | 4.8097343 | .212557 | 4.7046301 | 1.02234 | .978148 | 0 | 78 |
| | 10 | .210756 | 4.7448206 | .215599 | 4.6382457 | 1.02298 | .977539 | 50 | |
| | 20 | .213599 | 4.6816748 | .218645 | 4.5736287 | 1.02362 | .976921 | 40 | |
| | 30 | .216440 | 4.6202263 | .221695 | 4.5107085 | 1.02428 | .976296 | 30 | |
| | 40 | .219279 | 4.5604080 | .224748 | 4.4494181 | 1.02494 | .975662 | 20 | |
| | 50 | .222116 | 4.5021565 | .227806 | 4.3896940 | 1.02562 | .975020 | 10 | |
| ° | ' | Cosine. | Secant. | Cotangent. | Tangent. | Cosecant. | Sine. | ' | ° |

For functions from 77°-10' to 83°-30' read from bottom of table upward.

NATURAL SINES, COSECANTS, TANGENTS, ETC.

| ° | ' | Sine. | Cosecant. | Tangent. | Cotangent. | Secant. | Cosine. | ' | ° |
|----|----|---------|-----------|------------|------------|-----------|---------|----|----|
| 13 | 0 | .224951 | 4.4454115 | .230868 | 4.3314759 | 1.02630 | .974370 | 0 | 77 |
| | 10 | .227784 | 4.3901158 | .233934 | 4.2747066 | 1.02700 | .973712 | 50 | |
| | 20 | .230616 | 4.3362150 | .237004 | 4.2193318 | 1.02770 | .973045 | 40 | |
| | 30 | .233445 | 4.2836576 | .240079 | 4.1652998 | 1.02842 | .972370 | 30 | |
| | 40 | .236273 | 4.2323943 | .243158 | 4.1125614 | 1.02914 | .971687 | 20 | |
| | 50 | .239098 | 4.1823785 | .246241 | 4.0610700 | 1.02987 | .970995 | 10 | |
| 14 | 0 | .241922 | 4.1335655 | .249328 | 4.0107809 | 1.03061 | .970296 | 0 | 76 |
| | 10 | .244743 | 4.0859130 | .252420 | 3.9616518 | 1.03137 | .969588 | 50 | |
| | 20 | .247563 | 4.0393804 | .255517 | 3.9136420 | 1.03213 | .968872 | 40 | |
| | 30 | .250380 | 3.9939292 | .258618 | 3.8667131 | 1.03290 | .968148 | 30 | |
| | 40 | .253195 | 3.9495224 | .261723 | 3.8208231 | 1.03368 | .967415 | 20 | |
| | 50 | .256008 | 3.9061250 | .264834 | 3.7759519 | 1.03447 | .966675 | 10 | |
| 15 | 0 | .258819 | 3.8637033 | .267949 | 3.7320508 | 1.03528 | .965926 | 0 | 75 |
| | 10 | .261628 | 3.8222251 | .271069 | 3.6890927 | 1.03609 | .965169 | 50 | |
| | 20 | .264434 | 3.7816596 | .274195 | 3.6470467 | 1.03691 | .964404 | 40 | |
| | 30 | .267238 | 3.7419775 | .277325 | 3.6058835 | 1.03774 | .963630 | 30 | |
| | 40 | .270040 | 3.7031506 | .280460 | 3.5655749 | 1.03858 | .962849 | 20 | |
| | 50 | .272840 | 3.6651518 | .283600 | 3.5260938 | 1.03944 | .962059 | 10 | |
| 16 | 0 | .275637 | 3.6279553 | .286745 | 3.4874144 | 1.04030 | .961262 | 0 | 74 |
| | 10 | .278432 | 3.5915363 | .289896 | 3.4495120 | 1.04117 | .960456 | 50 | |
| | 20 | .281225 | 3.5558710 | .293052 | 3.4123626 | 1.04206 | .959642 | 40 | |
| | 30 | .284015 | 3.5209365 | .296214 | 3.3759434 | 1.04295 | .958820 | 30 | |
| | 40 | .286803 | 3.4867110 | .299380 | 3.3402326 | 1.04385 | .957990 | 20 | |
| | 50 | .289589 | 3.4531735 | .302553 | 3.3052091 | 1.04477 | .957151 | 10 | |
| 17 | 0 | .292372 | 3.4203036 | .305731 | 3.2708526 | 1.04569 | .956305 | 0 | 73 |
| | 10 | .295152 | 3.3880820 | .308914 | 3.2371438 | 1.04663 | .955450 | 50 | |
| | 20 | .297930 | 3.3564900 | .312104 | 3.2040638 | 1.04757 | .954588 | 40 | |
| | 30 | .300706 | 3.3255095 | .315299 | 3.1715948 | 1.04853 | .953717 | 30 | |
| | 40 | .303479 | 3.2951234 | .318500 | 3.1397194 | 1.04950 | .952838 | 20 | |
| | 50 | .306249 | 3.2653149 | .321707 | 3.1084210 | 1.05047 | .951951 | 10 | |
| 18 | 0 | .309017 | 3.2360680 | .324920 | 3.0776835 | 1.05146 | .951057 | 0 | 72 |
| | 10 | .311782 | 3.2073673 | .328139 | 3.0474915 | 1.05246 | .950154 | 50 | |
| | 20 | .314545 | 3.1791978 | .331364 | 3.0178301 | 1.05347 | .949243 | 40 | |
| | 30 | .317305 | 3.1515453 | .334595 | 2.9886850 | 1.05449 | .948324 | 30 | |
| | 40 | .320062 | 3.1243959 | .337833 | 2.9600422 | 1.05552 | .947397 | 20 | |
| | 50 | .322816 | 3.0977363 | .341077 | 2.9318885 | 1.05657 | .946462 | 10 | |
| 19 | 0 | .325568 | 3.0715535 | .344328 | 2.9042109 | 1.05762 | .945519 | 0 | 71 |
| | 10 | .328317 | 3.0458352 | .347585 | 2.8769970 | 1.05869 | .944568 | 50 | |
| | 20 | .331063 | 3.0205693 | .350848 | 2.8502349 | 1.05976 | .943609 | 40 | |
| ° | ' | Cosine. | Secant. | Cotangent. | Tangent. | Cosecant. | Sine. | ' | ° |

For functions from 70°-40' to 77°-0' read from bottom of table upward.

NATURAL SINES, COSECANTS, TANGENTS, ETC.

| ° | ' | Sine. | Cosecant. | Tangent. | Cotangent. | Secant. | Cosine. | ' | ° |
|----|----|---------|-----------|------------|------------|-----------|---------|----|----|
| 19 | 30 | .333807 | 2.9957443 | .354119 | 2.8239129 | 1.06085 | .942641 | 30 | |
| | 40 | .336547 | 2.9713490 | .357396 | 2.7980198 | 1.06195 | .941666 | 20 | |
| | 50 | .339285 | 2.9473724 | .360680 | 2.7725448 | 1.06306 | .940684 | 10 | |
| 20 | 0 | .342020 | 2.9238044 | .363970 | 2.7474774 | 1.06418 | .939693 | 0 | 70 |
| | 10 | .344752 | 2.9006346 | .367268 | 2.7228076 | 1.06531 | .938694 | 50 | |
| | 20 | .347481 | 2.8778532 | .370573 | 2.6985254 | 1.06645 | .937687 | 40 | |
| | 30 | .350207 | 2.8554510 | .373885 | 2.6746215 | 1.06761 | .936672 | 30 | |
| | 40 | .352931 | 2.8334185 | .377204 | 2.6510867 | 1.06878 | .935650 | 20 | |
| | 50 | .355651 | 2.8117471 | .380530 | 2.6279121 | 1.06995 | .934619 | 10 | |
| 21 | 0 | .358368 | 2.7904281 | .383864 | 2.6050891 | 1.07115 | .933580 | 0 | 69 |
| | 10 | .361082 | 2.7694532 | .387205 | 2.5826094 | 1.07235 | .932534 | 50 | |
| | 20 | .363793 | 2.7488144 | .390554 | 2.5604649 | 1.07356 | .931480 | 40 | |
| | 30 | .366501 | 2.7285038 | .393911 | 2.5386479 | 1.07479 | .930418 | 30 | |
| | 40 | .369206 | 2.7085139 | .397275 | 2.5171507 | 1.07602 | .929348 | 20 | |
| | 50 | .371908 | 2.6888374 | .400647 | 2.4959661 | 1.07727 | .928270 | 10 | |
| 22 | 0 | .374607 | 2.6694672 | .404026 | 2.4750869 | 1.07853 | .927184 | 0 | 68 |
| | 10 | .377302 | 2.6503962 | .407414 | 2.4545061 | 1.07981 | .926090 | 50 | |
| | 20 | .379994 | 2.6316180 | .410810 | 2.4342172 | 1.08109 | .924989 | 40 | |
| | 30 | .382683 | 2.6131259 | .414214 | 2.4142136 | 1.08239 | .923880 | 30 | |
| | 40 | .385369 | 2.5949137 | .417626 | 2.3944889 | 1.08370 | .922762 | 20 | |
| | 50 | .388052 | 2.5769753 | .421046 | 2.3750372 | 1.08503 | .921638 | 10 | |
| 23 | 0 | .390731 | 2.5593047 | .424475 | 2.3558524 | 1.08636 | .920505 | 0 | 67 |
| | 10 | .393407 | 2.5418961 | .427912 | 2.3369287 | 1.08771 | .919364 | 50 | |
| | 20 | .396080 | 2.5247440 | .431358 | 2.3182606 | 1.08907 | .918216 | 40 | |
| | 30 | .398749 | 2.5078428 | .434812 | 2.2998425 | 1.09044 | .917060 | 30 | |
| | 40 | .401415 | 2.4911874 | .438276 | 2.2816693 | 1.09183 | .915896 | 20 | |
| | 50 | .404078 | 2.4747726 | .441748 | 2.2637357 | 1.09323 | .914725 | 10 | |
| 24 | 0 | .406737 | 2.4585933 | .445229 | 2.2460368 | 1.09464 | .913545 | 0 | 66 |
| | 10 | .409392 | 2.4426448 | .448719 | 2.2285676 | 1.09606 | .912358 | 50 | |
| | 20 | .412045 | 2.4269222 | .452218 | 2.2113234 | 1.09750 | .911164 | 40 | |
| | 30 | .414693 | 2.4114210 | .455726 | 2.1942997 | 1.09895 | .909961 | 30 | |
| | 40 | .417338 | 2.3961367 | .459244 | 2.1774920 | 1.10041 | .908751 | 20 | |
| | 50 | .419980 | 2.3810650 | .462771 | 2.1608958 | 1.10189 | .907533 | 10 | |
| 25 | 0 | .422618 | 2.3662016 | .466308 | 2.1445069 | 1.10338 | .906308 | 0 | 65 |
| | 10 | .425253 | 2.3515424 | .469854 | 2.1283213 | 1.10488 | .905075 | 50 | |
| | 20 | .427884 | 2.3378083 | .473410 | 2.1123348 | 1.10640 | .903834 | 40 | |
| | 30 | .430511 | 2.3228205 | .476976 | 2.0965436 | 1.10793 | .902585 | 30 | |
| | 40 | .433135 | 2.3087501 | .480551 | 2.0809438 | 1.10947 | .901329 | 20 | |
| | 50 | .435755 | 2.2948685 | .484137 | 2.0655318 | 1.11103 | .900065 | 10 | |
| ° | ' | Cosine. | Secant. | Cotangent. | Tangent. | Cosecant. | Sine. | ' | ° |

For functions from 64°-10' to 70°-30' read from bottom of table upward.

NATURAL SINES, COSECANTS, TANGENTS, ETC.

| ° | ' | Sine. | Cosecant. | Tangent. | Cotangent. | Secant. | Cosine. | ' | ° |
|----|----|---------|-----------|------------|------------|-----------|---------|----|----|
| 26 | 0 | .438371 | 2.2811720 | .487733 | 2.0503038 | 1.11260 | .898794 | 0 | 64 |
| | 10 | .440984 | 2.2676571 | .491339 | 2.0352565 | 1.11419 | .897515 | 50 | |
| | 20 | .443593 | 2.2543204 | .494955 | 2.0203862 | 1.11579 | .896229 | 40 | |
| | 30 | .446198 | 2.2411585 | .498582 | 2.0056897 | 1.11740 | .894934 | 30 | |
| | 40 | .448799 | 2.2281681 | .502219 | 1.9911637 | 1.11903 | .893633 | 20 | |
| | 50 | .451397 | 2.2153460 | .505867 | 1.9768050 | 1.12067 | .892323 | 10 | |
| 27 | 0 | .453990 | 2.2026893 | .509525 | 1.9626105 | 1.12233 | .891007 | 0 | 63 |
| | 10 | .456580 | 2.1901947 | .513195 | 1.9485772 | 1.12400 | .889682 | 50 | |
| | 20 | .459166 | 2.1778595 | .516876 | 1.9347020 | 1.12568 | .888350 | 40 | |
| | 30 | .461749 | 2.1656806 | .520567 | 1.9209821 | 1.12738 | .887011 | 30 | |
| | 40 | .464327 | 2.1536553 | .524270 | 1.9074147 | 1.12910 | .885664 | 20 | |
| | 50 | .466901 | 2.1417808 | .527984 | 1.8939971 | 1.13083 | .884309 | 10 | |
| 28 | 0 | .469472 | 2.1300545 | .531709 | 1.8807265 | 1.13257 | .882948 | 0 | 62 |
| | 10 | .472038 | 2.1184737 | .535447 | 1.8676003 | 1.13433 | .881578 | 50 | |
| | 20 | .474600 | 2.1070359 | .539195 | 1.8546159 | 1.13610 | .880201 | 40 | |
| | 30 | .477159 | 2.0957385 | .542956 | 1.8417708 | 1.13789 | .878817 | 30 | |
| | 40 | .479713 | 2.0845792 | .546728 | 1.8290628 | 1.13970 | .877425 | 20 | |
| | 50 | .482263 | 2.0735556 | .550515 | 1.8164892 | 1.14152 | .876026 | 10 | |
| 29 | 0 | .484810 | 2.0626653 | .554309 | 1.8040478 | 1.14335 | .874620 | 0 | 61 |
| | 10 | .487352 | 2.0519061 | .558118 | 1.7917362 | 1.14521 | .873206 | 50 | |
| | 20 | .489890 | 2.0412757 | .561939 | 1.7795524 | 1.14707 | .871784 | 40 | |
| | 30 | .492424 | 2.0307720 | .565773 | 1.7674940 | 1.14896 | .870356 | 30 | |
| | 40 | .494953 | 2.0203929 | .569619 | 1.7555590 | 1.15085 | .868920 | 20 | |
| | 50 | .497479 | 2.0101362 | .573478 | 1.7437453 | 1.15277 | .867476 | 10 | |
| 30 | 0 | .500000 | 2.0000000 | .577350 | 1.7320508 | 1.15470 | .866025 | 0 | 60 |
| | 10 | .502517 | 1.9899822 | .581235 | 1.7204736 | 1.15665 | .864567 | 50 | |
| | 20 | .505030 | 1.9800810 | .585134 | 1.7090116 | 1.15861 | .863102 | 40 | |
| | 30 | .507538 | 1.9702944 | .589045 | 1.6976631 | 1.16059 | .861629 | 30 | |
| | 40 | .510043 | 1.9606206 | .592970 | 1.6864261 | 1.16259 | .860149 | 20 | |
| | 50 | .512543 | 1.9510577 | .596908 | 1.6752988 | 1.16460 | .858662 | 10 | |
| 31 | 0 | .515038 | 1.9416040 | .600861 | 1.6642795 | 1.16663 | .857167 | 0 | 59 |
| | 10 | .517529 | 1.9322578 | .604827 | 1.6533663 | 1.16868 | .855665 | 50 | |
| | 20 | .520016 | 1.9230173 | .608807 | 1.6425576 | 1.17075 | .854156 | 40 | |
| | 30 | .522499 | 1.9138809 | .612801 | 1.6318517 | 1.17283 | .852640 | 30 | |
| | 40 | .524977 | 1.9048469 | .616809 | 1.6212469 | 1.17493 | .851117 | 20 | |
| | 50 | .527450 | 1.8959138 | .620832 | 1.6107417 | 1.17704 | .849586 | 10 | |
| 32 | 0 | .529919 | 1.8870799 | .624869 | 1.6003345 | 1.17918 | .848048 | 0 | 58 |
| | 10 | .532384 | 1.8783438 | .628921 | 1.5900238 | 1.18133 | .846503 | 50 | |
| | 20 | .534844 | 1.8697040 | .632988 | 1.5798079 | 1.18350 | .844951 | 40 | |
| ° | ' | Cosine. | Secant. | Cotangent. | Tangent. | Cosecant. | Sine. | ' | ° |

For functions from 57°-40' to 64°-0' read from bottom of table upward.

NATURAL SINES, COSECANTS, TANGENTS, ETC.

| ° | ' | Sine. | Cosecant. | Tangent. | Cotangent. | Secant. | Cosine. | ' | ° |
|----|----|---------|-----------|------------|------------|-----------|---------|----|----|
| 32 | 30 | .537300 | 1.8611590 | .637070 | 1.5696856 | 1.18569 | .843391 | 30 | |
| | 40 | .539751 | 1.8527073 | .641167 | 1.5596552 | 1.18790 | .841825 | 20 | |
| | 50 | .542197 | 1.8443476 | .645280 | 1.5497155 | 1.19012 | .840251 | 10 | |
| 33 | 0 | .544639 | 1.8360785 | .649408 | 1.5398650 | 1.19236 | .838671 | 0 | 57 |
| | 10 | .547076 | 1.8278985 | .653551 | 1.5301025 | 1.19463 | .837083 | 50 | |
| | 20 | .549509 | 1.8198065 | .657710 | 1.5204261 | 1.19691 | .835488 | 40 | |
| | 30 | .551937 | 1.8118010 | .661886 | 1.5108352 | 1.19920 | .833886 | 30 | |
| | 40 | .554360 | 1.8038809 | .666077 | 1.5013282 | 1.20152 | .832277 | 20 | |
| | 50 | .556779 | 1.7960449 | .670285 | 1.4919039 | 1.20386 | .830661 | 10 | |
| 34 | 0 | .559193 | 1.7882916 | .674509 | 1.4825610 | 1.20622 | .829038 | 0 | 56 |
| | 10 | .561602 | 1.7806201 | .678749 | 1.4732983 | 1.20859 | .827407 | 50 | |
| | 20 | .564007 | 1.7730290 | .683007 | 1.4641147 | 1.21099 | .825770 | 40 | |
| | 30 | .566406 | 1.7655173 | .687281 | 1.4550090 | 1.21341 | .824126 | 30 | |
| | 40 | .568801 | 1.7580837 | .691573 | 1.4459801 | 1.21584 | .822475 | 20 | |
| | 50 | .571191 | 1.7507273 | .695881 | 1.4370268 | 1.21830 | .820817 | 10 | |
| 35 | 0 | .573576 | 1.7434468 | .700208 | 1.4281480 | 1.22077 | .819152 | 0 | 55 |
| | 10 | .575957 | 1.7362413 | .704552 | 1.4193427 | 1.22327 | .817480 | 50 | |
| | 20 | .578332 | 1.7291096 | .708913 | 1.4106098 | 1.22579 | .815801 | 40 | |
| | 30 | .580703 | 1.7220508 | .713293 | 1.4019483 | 1.22833 | .814116 | 30 | |
| | 40 | .583069 | 1.7150639 | .717691 | 1.3933571 | 1.23089 | .812423 | 20 | |
| | 50 | .585429 | 1.7081478 | .722108 | 1.3848355 | 1.23347 | .810723 | 10 | |
| 36 | 0 | .587785 | 1.7013016 | .726543 | 1.3763810 | 1.23607 | .809017 | 0 | 54 |
| | 10 | .590136 | 1.6945244 | .730996 | 1.3679959 | 1.23869 | .807304 | 50 | |
| | 20 | .592482 | 1.6878151 | .735469 | 1.3596764 | 1.24134 | .805584 | 40 | |
| | 30 | .594823 | 1.6811730 | .739961 | 1.3514224 | 1.24400 | .803857 | 30 | |
| | 40 | .597159 | 1.6745970 | .744472 | 1.3432331 | 1.24669 | .802123 | 20 | |
| | 50 | .599489 | 1.6680864 | .749003 | 1.3351075 | 1.24940 | .800383 | 10 | |
| 37 | 0 | .601815 | 1.6616401 | .753554 | 1.3270448 | 1.25214 | .798636 | 0 | 53 |
| | 10 | .604136 | 1.6552575 | .758125 | 1.3190441 | 1.25489 | .796882 | 50 | |
| | 20 | .606451 | 1.6489378 | .762716 | 1.3111046 | 1.25767 | .795121 | 40 | |
| | 30 | .608761 | 1.6426796 | .767327 | 1.3032254 | 1.26047 | .793353 | 30 | |
| | 40 | .611067 | 1.6364828 | .771959 | 1.2954057 | 1.26330 | .791579 | 20 | |
| | 50 | .613367 | 1.6303462 | .776612 | 1.2876447 | 1.26615 | .789798 | 10 | |
| 38 | 0 | .615661 | 1.6242692 | .781286 | 1.2799416 | 1.26902 | .788011 | 0 | 52 |
| | 10 | .617951 | 1.6182510 | .785981 | 1.2722957 | 1.27191 | .786217 | 50 | |
| | 20 | .620235 | 1.6122908 | .790698 | 1.2647062 | 1.27483 | .784416 | 40 | |
| | 30 | .622515 | 1.6063879 | .795436 | 1.2571723 | 1.27773 | .782608 | 30 | |
| | 40 | .624789 | 1.6005416 | .800196 | 1.2496933 | 1.28075 | .780794 | 20 | |
| | 50 | .627057 | 1.5947511 | .804979 | 1.2422685 | 1.28374 | .778973 | 10 | |
| ° | ' | Cosine. | Secant. | Cotangent. | Tangent. | Cosecant. | Sine. | ' | ° |

For functions from 51°-10' to 57°-30' read from bottom of table upward.

NATURAL SINES, COSECANTS, TANGENTS, ETC.

| ° | ' | Sine. | Cosecant. | Tangent. | Cotangent. | Secant. | Cosine. | ' | ° |
|----|----|---------|-----------|------------|------------|-----------|---------|----|----|
| 39 | 0 | .629320 | 1.5890157 | .809784 | 1.2348972 | 1.28676 | .777146 | 0 | 51 |
| | 10 | .631578 | 1.5833318 | .814612 | 1.2275786 | 1.28980 | .775312 | 50 | |
| | 20 | .633831 | 1.5777077 | .819463 | 1.2203121 | 1.29287 | .773472 | 40 | |
| | 30 | .636078 | 1.5721337 | .824336 | 1.2130970 | 1.29597 | .771625 | 30 | |
| | 40 | .638320 | 1.5666121 | .829234 | 1.2059327 | 1.29909 | .769771 | 20 | |
| | 50 | .640557 | 1.5611424 | .834155 | 1.1988184 | 1.30223 | .767911 | 10 | |
| 40 | 0 | .642788 | 1.5557238 | .839100 | 1.1917536 | 1.30541 | .766044 | 0 | 50 |
| | 10 | .645013 | 1.5503558 | .844069 | 1.1847376 | 1.30861 | .764171 | 50 | |
| | 20 | .647233 | 1.5450378 | .849062 | 1.1777698 | 1.31183 | .762292 | 40 | |
| | 30 | .649448 | 1.5397690 | .854081 | 1.1708496 | 1.31509 | .760406 | 30 | |
| | 40 | .651657 | 1.5345491 | .859124 | 1.1639763 | 1.31837 | .758514 | 20 | |
| | 50 | .653861 | 1.5293773 | .864193 | 1.1571495 | 1.32168 | .756615 | 10 | |
| 41 | 0 | .656059 | 1.5242531 | .869287 | 1.1503684 | 1.32501 | .754710 | 0 | 49 |
| | 10 | .658252 | 1.5191759 | .874407 | 1.1436326 | 1.32838 | .752798 | 50 | |
| | 20 | .660439 | 1.5141452 | .879553 | 1.1369414 | 1.33177 | .750880 | 40 | |
| | 30 | .662620 | 1.5091605 | .884725 | 1.1302944 | 1.33519 | .748956 | 30 | |
| | 40 | .664796 | 1.5042211 | .889924 | 1.1236909 | 1.33864 | .747025 | 20 | |
| | 50 | .666966 | 1.4993267 | .895151 | 1.1171305 | 1.34212 | .745088 | 10 | |
| 42 | 0 | .669131 | 1.4944765 | .900404 | 1.1106125 | 1.34563 | .743145 | 0 | 48 |
| | 10 | .671289 | 1.4896703 | .905685 | 1.1041365 | 1.34917 | .741195 | 50 | |
| | 20 | .673443 | 1.4849073 | .910994 | 1.0977020 | 1.35274 | .739239 | 40 | |
| | 30 | .675590 | 1.4801872 | .916331 | 1.0913085 | 1.35634 | .737277 | 30 | |
| | 40 | .677732 | 1.4755095 | .921697 | 1.0849554 | 1.35997 | .735309 | 20 | |
| | 50 | .679868 | 1.4708736 | .927091 | 1.0786423 | 1.36363 | .733335 | 10 | |
| 43 | 0 | .681998 | 1.4662792 | .932515 | 1.0723687 | 1.36733 | .731354 | 0 | 47 |
| | 10 | .684123 | 1.4617257 | .937968 | 1.0661341 | 1.37105 | .729367 | 50 | |
| | 20 | .686242 | 1.4572127 | .943451 | 1.0599381 | 1.37481 | .727374 | 40 | |
| | 30 | .688355 | 1.4527397 | .948965 | 1.0537801 | 1.37860 | .725374 | 30 | |
| | 40 | .690462 | 1.4483063 | .954508 | 1.0476598 | 1.38242 | .723369 | 20 | |
| | 50 | .692563 | 1.4439120 | .960083 | 1.0415767 | 1.38628 | .721357 | 10 | |
| 44 | 0 | .694658 | 1.4395565 | .965689 | 1.0355303 | 1.39016 | .719340 | 0 | 46 |
| | 10 | .696748 | 1.4352393 | .971326 | 1.0295203 | 1.39409 | .717316 | 50 | |
| | 20 | .698832 | 1.4309602 | .976996 | 1.0235461 | 1.39804 | .715286 | 40 | |
| | 30 | .700909 | 1.4267182 | .982697 | 1.0176074 | 1.40203 | .713251 | 30 | |
| | 40 | .702981 | 1.4225134 | .988432 | 1.0117088 | 1.40606 | .711209 | 20 | |
| | 50 | .705047 | 1.4183454 | .994199 | 1.0058348 | 1.41012 | .709161 | 10 | |
| 45 | 0 | .707107 | 1.4142136 | 1.000000 | 1.0000000 | 1.41421 | .707107 | 0 | 45 |
| ° | ' | Cosine. | Secant. | Cotangent. | Tangent. | Cosecant. | Sine. | ' | ° |

For functions from 45°-0' to 51°-0' read from bottom of table upward.

SQUARES, CUBES, SQUARE ROOTS, CUBE ROOTS AND RECIPROCAL.

| No. | Squares. | Cubes. | Square Roots. | Cube Roots. | Reciprocals. |
|-----|----------|--------|---------------|-------------|--------------|
| 1 | 1 | 1 | 1.0000000 | 1.0000000 | 1.000000000 |
| 2 | 4 | 8 | 1.4142136 | 1.2599210 | .500000000 |
| 3 | 9 | 27 | 1.7320508 | 1.4422496 | .333333333 |
| 4 | 16 | 64 | 2.0000000 | 1.5874011 | .250000000 |
| 5 | 25 | 125 | 2.2360680 | 1.7099759 | .200000000 |
| 6 | 36 | 216 | 2.4494897 | 1.8171206 | .166666667 |
| 7 | 49 | 343 | 2.6457513 | 1.9129312 | .142857143 |
| 8 | 64 | 512 | 2.8284271 | 2.0000000 | .125000000 |
| 9 | 81 | 729 | 3.0000000 | 2.0800837 | .111111111 |
| 10 | 100 | 1000 | 3.1622777 | 2.1544347 | .100000000 |
| 11 | 121 | 1331 | 3.3166248 | 2.2239801 | .090909091 |
| 12 | 144 | 1728 | 3.4641016 | 2.2894286 | .083333333 |
| 13 | 169 | 2197 | 3.6055513 | 2.3513347 | .076923077 |
| 14 | 196 | 2744 | 3.7416574 | 2.4101422 | .071428571 |
| 15 | 225 | 3375 | 3.8729833 | 2.4662121 | .066666667 |
| 16 | 256 | 4096 | 4.0000000 | 2.5198421 | .062500000 |
| 17 | 289 | 4913 | 4.1231056 | 2.5712816 | .058823529 |
| 18 | 324 | 5832 | 4.2426407 | 2.6207414 | .055555556 |
| 19 | 361 | 6859 | 4.3588989 | 2.6684016 | .052631579 |
| 20 | 400 | 8000 | 4.4721360 | 2.7144177 | .050000000 |
| 21 | 441 | 9261 | 4.5825757 | 2.7589243 | .047619048 |
| 22 | 484 | 10648 | 4.6904158 | 2.8020393 | .045454545 |
| 23 | 529 | 12167 | 4.7958315 | 2.8438670 | .043478261 |
| 24 | 576 | 13824 | 4.8989795 | 2.8844991 | .041666667 |
| 25 | 625 | 15625 | 5.0000000 | 2.9240177 | .040000000 |
| 26 | 676 | 17576 | 5.0990195 | 2.9624960 | .038461538 |
| 27 | 729 | 19683 | 5.1961524 | 3.0000000 | .037037037 |
| 28 | 784 | 21952 | 5.2915026 | 3.0365889 | .035714286 |
| 29 | 841 | 24389 | 5.3851648 | 3.0723168 | .034482759 |
| 30 | 900 | 27000 | 5.4772256 | 3.1072325 | .033333333 |
| 31 | 961 | 29791 | 5.5677644 | 3.1413806 | .032258065 |
| 32 | 1024 | 32768 | 5.6568542 | 3.1748021 | .031250000 |
| 33 | 1089 | 35937 | 5.7445626 | 3.2075343 | .030303030 |
| 34 | 1156 | 39304 | 5.8309519 | 3.2396118 | .029411765 |
| 35 | 1225 | 42875 | 5.9160798 | 3.2710663 | .028571429 |
| 36 | 1296 | 46656 | 6.0000000 | 3.3019272 | .027777778 |
| 37 | 1369 | 50653 | 6.0827625 | 3.3322218 | .027027027 |
| 38 | 1444 | 54872 | 6.1644140 | 3.3619754 | .026315789 |
| 39 | 1521 | 59319 | 6.2449980 | 3.3912114 | .025641026 |
| 40 | 1600 | 64000 | 6.3245553 | 3.4199519 | .025000000 |
| 41 | 1681 | 68921 | 6.4031242 | 3.4482172 | .024390244 |
| 42 | 1764 | 74088 | 6.4807407 | 3.4760266 | .023809524 |
| 43 | 1849 | 79507 | 6.5574385 | 3.5033981 | .023255814 |
| 44 | 1936 | 85184 | 6.6332496 | 3.5303483 | .022727273 |
| 45 | 2025 | 91125 | 6.7082039 | 3.5568933 | .022222222 |
| 46 | 2116 | 97336 | 6.7823300 | 3.5830479 | .021739130 |
| 47 | 2209 | 103823 | 6.8556546 | 3.6088261 | .021276596 |
| 48 | 2304 | 110592 | 6.9282032 | 3.6342411 | .020833333 |
| 49 | 2401 | 117649 | 7.0000000 | 3.6593057 | .020408163 |
| 50 | 2500 | 125000 | 7.0710678 | 3.6840314 | .020000000 |
| 51 | 2601 | 132651 | 7.1414284 | 3.7084298 | .019607843 |
| 52 | 2704 | 140608 | 7.2111026 | 3.7325111 | .019230769 |
| 53 | 2809 | 148877 | 7.2801099 | 3.7562858 | .018867925 |
| 54 | 2916 | 157464 | 7.3484692 | 3.7797631 | .018518519 |
| 55 | 3025 | 166375 | 7.4161985 | 3.8029525 | .018181818 |
| 56 | 3136 | 175616 | 7.4833148 | 3.8258624 | .017857143 |
| 57 | 3249 | 185193 | 7.5498344 | 3.8485011 | .017543860 |
| 58 | 3364 | 195112 | 7.6157731 | 3.8708766 | .017241379 |
| 59 | 3481 | 205379 | 7.6811457 | 3.8929965 | .016949153 |

SQUARES, CUBES, SQUARE ROOTS, CUBE ROOTS AND RECIPROCAL.

| No. | Squares. | Cubes. | Square Roots. | Cube Roots. | Reciprocals. |
|-----|----------|---------|---------------|-------------|--------------|
| 60 | 3600 | 216000 | 7.7459667 | 3.9148676 | .016666667 |
| 61 | 3721 | 226981 | 7.8102497 | 3.9364972 | .016393443 |
| 62 | 3844 | 238328 | 7.8740079 | 3.9578915 | .016129032 |
| 63 | 3969 | 250047 | 7.9372539 | 3.9790571 | .015873018 |
| 64 | 4096 | 262144 | 8.0000000 | 4.0000000 | .015625000 |
| 65 | 4225 | 274625 | 8.0622577 | 4.0207256 | .015384615 |
| 66 | 4356 | 287496 | 8.1240384 | 4.0412401 | .015151515 |
| 67 | 4489 | 300763 | 8.1853528 | 4.0615480 | .014925373 |
| 68 | 4624 | 314432 | 8.2462113 | 4.0816551 | .014705882 |
| 69 | 4761 | 328509 | 8.3066239 | 4.1015661 | .014492754 |
| 70 | 4900 | 343000 | 8.3666003 | 4.1212853 | .014285714 |
| 71 | 5041 | 357911 | 8.4261498 | 4.1408178 | .014084507 |
| 72 | 5184 | 373248 | 8.4852814 | 4.1601676 | .013888889 |
| 73 | 5329 | 389017 | 8.5440037 | 4.1793390 | .013698630 |
| 74 | 5476 | 405224 | 8.6023253 | 4.1983364 | .013513514 |
| 75 | 5625 | 421875 | 8.6602540 | 4.2171633 | .013333333 |
| 76 | 5776 | 438976 | 8.7177979 | 4.2358236 | .013157895 |
| 77 | 5929 | 456533 | 8.7749644 | 4.2543210 | .012987013 |
| 78 | 6084 | 474552 | 8.8317609 | 4.2726586 | .012820513 |
| 79 | 6241 | 493039 | 8.8881944 | 4.2908404 | .012658228 |
| 80 | 6400 | 512000 | 8.9442719 | 4.3088695 | .012500000 |
| 81 | 6561 | 531441 | 9.0000000 | 4.3267487 | .012345679 |
| 82 | 6724 | 551368 | 9.0553851 | 4.3444815 | .012195122 |
| 83 | 6889 | 571787 | 9.1104336 | 4.3620707 | .012048193 |
| 84 | 7056 | 592704 | 9.1651514 | 4.3795191 | .011904762 |
| 85 | 7225 | 614125 | 9.2195445 | 4.3968296 | .011764706 |
| 86 | 7396 | 636056 | 9.2736185 | 4.4140049 | .011627907 |
| 87 | 7569 | 658503 | 9.3273791 | 4.4310476 | .011494253 |
| 88 | 7744 | 681472 | 9.3808315 | 4.4479602 | .011363636 |
| 89 | 7921 | 704969 | 9.4339811 | 4.4647451 | .011235955 |
| 90 | 8100 | 729000 | 9.4868330 | 4.4814047 | .011111111 |
| 91 | 8281 | 753571 | 9.5393920 | 4.4979414 | .010989011 |
| 92 | 8464 | 778688 | 9.5916630 | 4.5143574 | .010869565 |
| 93 | 8649 | 804357 | 9.6436508 | 4.5306549 | .010752688 |
| 94 | 8836 | 830584 | 9.6953597 | 4.5468359 | .010638298 |
| 95 | 9025 | 857375 | 9.7467943 | 4.5629026 | .010526316 |
| 96 | 9216 | 884736 | 9.7979590 | 4.5788570 | .010416667 |
| 97 | 9409 | 912673 | 9.8488578 | 4.5947009 | .010309278 |
| 98 | 9604 | 941192 | 9.8994949 | 4.6104363 | .010204082 |
| 99 | 9801 | 970299 | 9.9498744 | 4.6260650 | .010101010 |
| 100 | 10000 | 1000000 | 10.0000000 | 4.6415888 | .010000000 |
| 101 | 10201 | 1030301 | 10.0498756 | 4.6570095 | .009900990 |
| 102 | 10404 | 1061208 | 10.0995049 | 4.6723287 | .009803922 |
| 103 | 10609 | 1092727 | 10.1488916 | 4.6875482 | .009708738 |
| 104 | 10816 | 1124864 | 10.1980390 | 4.7026694 | .009615385 |
| 105 | 11025 | 1157625 | 10.2469508 | 4.7176940 | .009523810 |
| 106 | 11236 | 1191016 | 10.2956301 | 4.7326235 | .009433962 |
| 107 | 11449 | 1225043 | 10.3440804 | 4.7474594 | .009345794 |
| 108 | 11664 | 1259712 | 10.3923048 | 4.7622032 | .009259259 |
| 109 | 11881 | 1295029 | 10.4403065 | 4.7768562 | .009174312 |
| 110 | 12100 | 1331000 | 10.4880885 | 4.7914199 | .009090909 |
| 111 | 12321 | 1367631 | 10.5356538 | 4.8058955 | .009009009 |
| 112 | 12544 | 1404928 | 10.5830052 | 4.8202845 | .008928571 |
| 113 | 12769 | 1442897 | 10.6301458 | 4.8345881 | .008849558 |
| 114 | 12996 | 1481544 | 10.6770783 | 4.8488076 | .008771930 |
| 115 | 13225 | 1520875 | 10.7238053 | 4.8629442 | .008695652 |
| 116 | 13456 | 1560896 | 10.7703296 | 4.8769990 | .008620690 |
| 117 | 13689 | 1601613 | 10.8166538 | 4.8909732 | .008547009 |
| 118 | 13924 | 1643032 | 10.8627805 | 4.9048681 | .008474576 |
| 119 | 14161 | 1685159 | 10.9087121 | 4.9186847 | .008403361 |

SQUARES, CUBES, SQUARE ROOTS, CUBE ROOTS AND RECIPROCAL.

| No. | Squares. | Cubes. | Square Roots. | Cube Roots. | Reciprocals. |
|-----|----------|---------|---------------|-------------|--------------|
| 120 | 14400 | 1728000 | 10.9544512 | 4.9324242 | .008333333 |
| 121 | 14641 | 1771561 | 11.0000000 | 4.9460874 | .008264463 |
| 122 | 14884 | 1815848 | 11.0453610 | 4.9596757 | .008196721 |
| 123 | 15129 | 1860867 | 11.0905365 | 4.9731898 | .008130081 |
| 124 | 15376 | 1906624 | 11.1355287 | 4.9866310 | .008064516 |
| 125 | 15625 | 1953125 | 11.1803399 | 5.0000000 | .008000000 |
| 126 | 15876 | 2000376 | 11.2249722 | 5.0132979 | .007936508 |
| 127 | 16129 | 2048383 | 11.2694277 | 5.0265257 | .007874016 |
| 128 | 16384 | 2097152 | 11.3137085 | 5.0396842 | .007812500 |
| 129 | 16641 | 2146689 | 11.3578167 | 5.0527743 | .007751938 |
| 130 | 16900 | 2197000 | 11.4017543 | 5.0657970 | .007692308 |
| 131 | 17161 | 2248091 | 11.4455231 | 5.0787531 | .007633588 |
| 132 | 17424 | 2299968 | 11.4891253 | 5.0916434 | .007575758 |
| 133 | 17689 | 2352637 | 11.5325626 | 5.1044687 | .007518797 |
| 134 | 17956 | 2406104 | 11.5758369 | 5.1172299 | .007462687 |
| 135 | 18225 | 2460375 | 11.6189500 | 5.1299278 | .007407407 |
| 136 | 18496 | 2515456 | 11.6619038 | 5.1425632 | .007352941 |
| 137 | 18769 | 2571353 | 11.7046999 | 5.1551367 | .007299270 |
| 138 | 19044 | 2628072 | 11.7473401 | 5.1676493 | .007246377 |
| 139 | 19321 | 2685619 | 11.7898261 | 5.1801015 | .007194245 |
| 140 | 19600 | 2744000 | 11.8321596 | 5.1924941 | .007142857 |
| 141 | 19881 | 2803221 | 11.8743421 | 5.2048279 | .007092199 |
| 142 | 20164 | 2863288 | 11.9163753 | 5.2171034 | .007042254 |
| 143 | 20449 | 2924207 | 11.9582607 | 5.2293215 | .006993007 |
| 144 | 20736 | 2985984 | 12.0000000 | 5.2414828 | .006944444 |
| 145 | 21025 | 3048625 | 12.0415946 | 5.2535879 | .006896552 |
| 146 | 21316 | 3112136 | 12.0830460 | 5.2656374 | .0068489315 |
| 147 | 21609 | 3176523 | 12.1243557 | 5.2776321 | .006802721 |
| 148 | 21904 | 3241792 | 12.1655251 | 5.2895725 | .006756757 |
| 149 | 22201 | 3307949 | 12.2065556 | 5.3014592 | .006711409 |
| 150 | 22500 | 3375000 | 12.2474487 | 5.3132928 | .006666667 |
| 151 | 22801 | 3442951 | 12.2882057 | 5.3250740 | .006622517 |
| 152 | 23104 | 3511808 | 12.3288280 | 5.3368033 | .006578947 |
| 153 | 23409 | 3581577 | 12.3693169 | 5.3484812 | .006535948 |
| 154 | 23716 | 3652264 | 12.4096736 | 5.3601084 | .006493506 |
| 155 | 24025 | 3723875 | 12.4498996 | 5.3716854 | .006451613 |
| 156 | 24336 | 3796416 | 12.4899960 | 5.3832126 | .006410256 |
| 157 | 24649 | 3869893 | 12.5299641 | 5.3946907 | .006369427 |
| 158 | 24964 | 3944312 | 12.5698051 | 5.4061202 | .006329114 |
| 159 | 25281 | 4019679 | 12.6095202 | 5.4175015 | .006289308 |
| 160 | 25600 | 4096000 | 12.6491106 | 5.4288352 | .006250000 |
| 161 | 25921 | 4173281 | 12.6885775 | 5.4401218 | .006211180 |
| 162 | 26244 | 4251528 | 12.7279221 | 5.4513618 | .006172840 |
| 163 | 26569 | 4330747 | 12.7671453 | 5.4625556 | .006134969 |
| 164 | 26896 | 4410944 | 12.8062485 | 5.4737037 | .006097561 |
| 165 | 27225 | 4492125 | 12.8452326 | 5.4848066 | .006060606 |
| 166 | 27556 | 4574296 | 12.8840987 | 5.4958647 | .006024096 |
| 167 | 27889 | 4657463 | 12.9228480 | 5.5068784 | .005988024 |
| 168 | 28224 | 4741632 | 12.9614814 | 5.5178484 | .005952381 |
| 169 | 28561 | 4826809 | 13.0000000 | 5.5287748 | .005917160 |
| 170 | 28900 | 4913000 | 13.0384048 | 5.5396582 | .005882353 |
| 171 | 29241 | 5000211 | 13.0766968 | 5.5504991 | .005847953 |
| 172 | 29584 | 5088448 | 13.1148770 | 5.5612978 | .005813953 |
| 173 | 29929 | 5177717 | 13.1529464 | 5.5720546 | .005780347 |
| 174 | 30276 | 5268024 | 13.1909060 | 5.5827702 | .005747126 |
| 175 | 30625 | 5359375 | 13.2287566 | 5.5934447 | .005714286 |
| 176 | 30976 | 5451776 | 13.2664992 | 5.6040787 | .005681818 |
| 177 | 31329 | 5545233 | 13.3041347 | 5.6146724 | .005649718 |
| 178 | 31684 | 5639752 | 13.3416641 | 5.6252263 | .005617978 |
| 179 | 32041 | 5735339 | 13.3790882 | 5.6357408 | .005586592 |

SQUARES, CUBES, SQUARE ROOTS, CUBE ROOTS AND RECIPROCAL.

| No. | Squares. | Cubes. | Square Roots. | Cube Roots. | Reciprocals. |
|-----|----------|----------|---------------|-------------|--------------|
| 180 | 32400 | 5832000 | 13.4164079 | 5.6462162 | .005555556 |
| 181 | 32761 | 5929741 | 13.4536240 | 5.6566528 | .005524862 |
| 182 | 33124 | 6028568 | 13.4907376 | 5.6670511 | .005494506 |
| 183 | 33489 | 6128487 | 13.5277493 | 5.6774114 | .005464481 |
| 184 | 33856 | 6229504 | 13.5646600 | 5.6877340 | .005434783 |
| 185 | 34225 | 6331625 | 13.6014705 | 5.6980192 | .005405405 |
| 186 | 34596 | 6434856 | 13.6381817 | 5.7082675 | .005376344 |
| 187 | 34969 | 6539203 | 13.6747943 | 5.7184791 | .005347594 |
| 188 | 35344 | 6644672 | 13.7113092 | 5.7286543 | .005319149 |
| 189 | 35721 | 6751269 | 13.7477271 | 5.7387936 | .005291005 |
| 190 | 36100 | 6859000 | 13.7840488 | 5.7488971 | .005263158 |
| 191 | 36481 | 6967871 | 13.8202750 | 5.7589652 | .005235602 |
| 192 | 36864 | 7077888 | 13.8564065 | 5.7689982 | .005208333 |
| 193 | 37249 | 7189057 | 13.8924440 | 5.7789966 | .005181347 |
| 194 | 37636 | 7301384 | 13.9283883 | 5.7889604 | .005154639 |
| 195 | 38025 | 7414875 | 13.9642400 | 5.7988900 | .005128205 |
| 196 | 38416 | 7529536 | 14.0000000 | 5.8087857 | .005102041 |
| 197 | 38809 | 7645373 | 14.0356688 | 5.8186479 | .005076142 |
| 198 | 39204 | 7762392 | 14.0712473 | 5.8284767 | .005050505 |
| 199 | 39601 | 7880599 | 14.1067360 | 5.8382725 | .005025126 |
| 200 | 40000 | 8000000 | 14.1421356 | 5.8480355 | .005000000 |
| 201 | 40401 | 8120601 | 14.1774469 | 5.8577660 | .004975124 |
| 202 | 40804 | 8242408 | 14.2126704 | 5.8674643 | .004950495 |
| 203 | 41209 | 8365427 | 14.2478068 | 5.8771307 | .004926108 |
| 204 | 41616 | 8489664 | 14.2828569 | 5.8867653 | .004901961 |
| 205 | 42025 | 8615125 | 14.3178211 | 5.8963685 | .004878049 |
| 206 | 42436 | 8741816 | 14.3527001 | 5.9059406 | .004854369 |
| 207 | 42849 | 8869743 | 14.3874946 | 5.9154817 | .004830918 |
| 208 | 43264 | 8998912 | 14.4222051 | 5.9249921 | .004807692 |
| 209 | 43681 | 9129329 | 14.4568323 | 5.9344721 | .004784689 |
| 210 | 44100 | 9261000 | 14.4913767 | 5.9439220 | .004761905 |
| 211 | 44521 | 9393931 | 14.5258390 | 5.9533418 | .004739336 |
| 212 | 44944 | 9528128 | 14.5602198 | 5.9627320 | .004716981 |
| 213 | 45369 | 9663597 | 14.5945195 | 5.9720926 | .004694836 |
| 214 | 45796 | 9800344 | 14.6287388 | 5.9814240 | .004672897 |
| 215 | 46225 | 9938375 | 14.6628783 | 5.9907264 | .004651163 |
| 216 | 46656 | 10077696 | 14.6969385 | 6.0000000 | .004629630 |
| 217 | 47089 | 10218313 | 14.7309199 | 6.0092450 | .004608295 |
| 218 | 47524 | 10360232 | 14.7648231 | 6.0184617 | .004587156 |
| 219 | 47961 | 10503459 | 14.7986486 | 6.0276502 | .004566210 |
| 220 | 48400 | 10648000 | 14.8323970 | 6.0368107 | .004545455 |
| 221 | 48841 | 10793861 | 14.8660687 | 6.0459435 | .004524887 |
| 222 | 49284 | 10941048 | 14.8996644 | 6.0550489 | .004504505 |
| 223 | 49729 | 11089567 | 14.9331845 | 6.0641270 | .004484305 |
| 224 | 50176 | 11239424 | 14.9666295 | 6.0731779 | .004464286 |
| 225 | 50625 | 11390625 | 15.0000000 | 6.0822020 | .004444444 |
| 226 | 51076 | 11543176 | 15.0332964 | 6.0911994 | .004424779 |
| 227 | 51529 | 11697083 | 15.0665192 | 6.1001702 | .004405286 |
| 228 | 51984 | 11852352 | 15.0996689 | 6.1091147 | .004385965 |
| 229 | 52441 | 12008989 | 15.1327460 | 6.1180332 | .004366612 |
| 230 | 52900 | 12167000 | 15.1657509 | 6.1269257 | .004347826 |
| 231 | 53361 | 12326391 | 15.1986842 | 6.1357924 | .004329004 |
| 232 | 53824 | 12487168 | 15.2315462 | 6.1446337 | .004310345 |
| 233 | 54289 | 12649337 | 15.2643375 | 6.1534495 | .004291845 |
| 234 | 54756 | 12812904 | 15.2970585 | 6.1622401 | .004273504 |
| 235 | 55225 | 12977875 | 15.3297097 | 6.1710058 | .004255319 |
| 236 | 55696 | 13144256 | 15.3622915 | 6.1797466 | .004237288 |
| 237 | 56169 | 13312053 | 15.3948043 | 6.1884628 | .004219409 |
| 238 | 56644 | 13481272 | 15.4272486 | 6.1971544 | .004201681 |
| 239 | 57121 | 13651919 | 15.4596248 | 6.2058218 | .004184100 |

SQUARES, CUBES, SQUARE ROOTS, CUBE ROOTS AND RECIPROCAL.

| No. | Squares. | Cubes. | Square Roots. | Cube Roots. | Reciprocals. |
|-----|----------|----------|---------------|-------------|--------------|
| 240 | 57600 | 13824000 | 15.4919334 | 6.2144650 | .004166667 |
| 241 | 58081 | 13997521 | 15.5241747 | 6.2230843 | .004149378 |
| 242 | 58564 | 14172488 | 15.5563492 | 6.2316797 | .004132231 |
| 243 | 59049 | 14348907 | 15.5884573 | 6.2402515 | .004115226 |
| 244 | 59536 | 14526784 | 15.6204994 | 6.2487998 | .004098361 |
| 245 | 60025 | 14706125 | 15.6524758 | 6.2573248 | .004081633 |
| 246 | 60516 | 14886936 | 15.6843871 | 6.2658266 | .004065041 |
| 247 | 61009 | 15069223 | 15.7162336 | 6.2743054 | .004048583 |
| 248 | 61504 | 15252992 | 15.7480157 | 6.2827613 | .004032258 |
| 249 | 62001 | 15438249 | 15.7797338 | 6.2911946 | .004016064 |
| 250 | 62500 | 15625000 | 15.8113883 | 6.2996053 | .004000000 |
| 251 | 63001 | 15813251 | 15.8429795 | 6.3079935 | .003984064 |
| 252 | 63504 | 16003008 | 15.8745079 | 6.3163596 | .003968254 |
| 253 | 64009 | 16194277 | 15.9059737 | 6.3247035 | .003952569 |
| 254 | 64516 | 16387064 | 15.9373775 | 6.3330256 | .003937008 |
| 255 | 65025 | 16581375 | 15.9687194 | 6.3413257 | .003921569 |
| 256 | 65536 | 16777216 | 16.0000000 | 6.3496042 | .003906250 |
| 257 | 66049 | 16974593 | 16.0312195 | 6.3578611 | .003891051 |
| 258 | 66564 | 17173512 | 16.0623784 | 6.3660968 | .003875969 |
| 259 | 67081 | 17373979 | 16.0934769 | 6.3743111 | .003861004 |
| 260 | 67600 | 17576000 | 16.1245155 | 6.3825043 | .003846154 |
| 261 | 68121 | 17779581 | 16.1554944 | 6.3906765 | .003831418 |
| 262 | 68644 | 17984728 | 16.1864141 | 6.39883279 | .003816794 |
| 263 | 69169 | 18191447 | 16.2172747 | 6.4069585 | .003802281 |
| 264 | 69696 | 18399744 | 16.2480768 | 6.4150687 | .003787879 |
| 265 | 70225 | 18609625 | 16.2788206 | 6.4231583 | .003773585 |
| 266 | 70756 | 18821096 | 16.3095064 | 6.4312276 | .003759398 |
| 267 | 71289 | 19034163 | 16.3401346 | 6.4392767 | .003745318 |
| 268 | 71824 | 19248832 | 16.3707055 | 6.4473057 | .003731343 |
| 269 | 72361 | 19465109 | 16.4012195 | 6.4553148 | .003717472 |
| 270 | 72900 | 19683000 | 16.4316767 | 6.4633041 | .003703704 |
| 271 | 73441 | 19902511 | 16.4620776 | 6.4712736 | .003690037 |
| 272 | 73984 | 20123648 | 16.4924225 | 6.4792236 | .003676471 |
| 273 | 74529 | 20346417 | 16.5227116 | 6.4871541 | .003663004 |
| 274 | 75076 | 20570824 | 16.5529454 | 6.4950653 | .003649635 |
| 275 | 75625 | 20796875 | 16.5831240 | 6.5029572 | .003636364 |
| 276 | 76176 | 21024576 | 16.6132477 | 6.5108300 | .003623188 |
| 277 | 76729 | 21253933 | 16.6433170 | 6.5186839 | .003610108 |
| 278 | 77284 | 21484952 | 16.6733320 | 6.5265189 | .003597122 |
| 279 | 77841 | 21717639 | 16.7032931 | 6.5343351 | .003584229 |
| 280 | 78400 | 21952000 | 16.7332005 | 6.5421326 | .003571429 |
| 281 | 78961 | 22188041 | 16.7630546 | 6.5499116 | .003558719 |
| 282 | 79524 | 22425768 | 16.7928556 | 6.5576722 | .003546099 |
| 283 | 80089 | 22665187 | 16.8226038 | 6.5654144 | .003533569 |
| 284 | 80656 | 22906304 | 16.8522995 | 6.5731385 | .003521127 |
| 285 | 81225 | 23149125 | 16.8819430 | 6.5808443 | .003508772 |
| 286 | 81796 | 23393656 | 16.9115345 | 6.5885323 | .003496503 |
| 287 | 82369 | 23639903 | 16.9410743 | 6.5962023 | .003484321 |
| 288 | 82944 | 23887872 | 16.9705627 | 6.6038545 | .003472222 |
| 289 | 83521 | 24137569 | 17.0000000 | 6.6114890 | .003460208 |
| 290 | 84100 | 24389000 | 17.0293864 | 6.6191060 | .003448276 |
| 291 | 84681 | 24642171 | 17.0587221 | 6.6267054 | .003436426 |
| 292 | 85264 | 24897088 | 17.0880075 | 6.6342874 | .003424658 |
| 293 | 85849 | 25153757 | 17.1172428 | 6.6418522 | .003412969 |
| 294 | 86436 | 25412184 | 17.1464282 | 6.6493998 | .003401361 |
| 295 | 87025 | 25672375 | 17.1755640 | 6.6569302 | .003389831 |
| 296 | 87616 | 25934336 | 17.2046505 | 6.6644437 | .003378378 |
| 297 | 88209 | 26198073 | 17.2336879 | 6.6719403 | .003367003 |
| 298 | 88804 | 26463592 | 17.2626765 | 6.6794200 | .003355705 |
| 299 | 89401 | 26730899 | 17.2916165 | 6.6868831 | .003344482 |

SQUARES, CUBES, SQUARE ROOTS, CUBE ROOTS AND RECIPROCAL.

| No. | Squares. | Cubes. | Square Roots. | Cube Roots. | Reciprocals. |
|-----|----------|----------|---------------|-------------|--------------|
| 300 | 90000 | 27000000 | 17.3205081 | 6.6943295 | .003333333 |
| 301 | 90601 | 27270901 | 17.3493516 | 6.7017593 | .003322259 |
| 302 | 91204 | 27543608 | 17.3781472 | 6.7091729 | .003311258 |
| 303 | 91809 | 27818127 | 17.4068952 | 6.7165700 | .003300330 |
| 304 | 92416 | 28094464 | 17.4355958 | 6.7239508 | .003289474 |
| 305 | 93025 | 28372625 | 17.4642492 | 6.7313155 | .003278689 |
| 306 | 93636 | 28652616 | 17.4928557 | 6.7386641 | .003267974 |
| 307 | 94249 | 28934443 | 17.5214155 | 6.7459967 | .003257329 |
| 308 | 94864 | 29218112 | 17.5499288 | 6.7533134 | .003246753 |
| 309 | 95481 | 29503629 | 17.5783958 | 6.7606143 | .003236246 |
| 310 | 96100 | 29791000 | 17.6068169 | 6.7678995 | .003225806 |
| 311 | 96721 | 30080231 | 17.6351921 | 6.7751690 | .003215434 |
| 312 | 97344 | 30371328 | 17.6635217 | 6.7824229 | .003205128 |
| 313 | 97969 | 30664297 | 17.6918060 | 6.7896613 | .003194888 |
| 314 | 98596 | 30959144 | 17.7200451 | 6.7968844 | .003184713 |
| 315 | 99225 | 31255875 | 17.7482393 | 6.8040921 | .003174603 |
| 316 | 99856 | 31554496 | 17.7763888 | 6.8112847 | .003164557 |
| 317 | 100489 | 31855013 | 17.8044938 | 6.8184620 | .003154574 |
| 318 | 101124 | 32157432 | 17.8325545 | 6.8256242 | .003144654 |
| 319 | 101761 | 32461759 | 17.8605711 | 6.8327714 | .003134796 |
| 320 | 102400 | 32768000 | 17.8885438 | 6.8399037 | .003125000 |
| 321 | 103041 | 33076161 | 17.9164729 | 6.8470213 | .003115265 |
| 322 | 103684 | 33386248 | 17.9443584 | 6.8541240 | .003105590 |
| 323 | 104329 | 33698267 | 17.9722008 | 6.8612120 | .003095975 |
| 324 | 104976 | 34012224 | 18.0000000 | 6.8682855 | .003086420 |
| 325 | 105625 | 34328125 | 18.0277564 | 6.8753443 | .003076923 |
| 326 | 106276 | 34645976 | 18.0554701 | 6.8823888 | .003067485 |
| 327 | 106929 | 34965783 | 18.0831413 | 6.8894188 | .003058104 |
| 328 | 107584 | 35287552 | 18.1107703 | 6.8964345 | .003048780 |
| 329 | 108241 | 35611289 | 18.1383571 | 6.9034359 | .003039514 |
| 330 | 108900 | 35937000 | 18.1659021 | 6.9104232 | .003030303 |
| 331 | 109561 | 36264691 | 18.1934054 | 6.9173964 | .003021148 |
| 332 | 110224 | 36594368 | 18.2208672 | 6.9243556 | .003012048 |
| 333 | 110889 | 36926037 | 18.2482876 | 6.9313008 | .003003003 |
| 334 | 111556 | 37259704 | 18.2756669 | 6.9382321 | .002994012 |
| 335 | 112225 | 37595375 | 18.3030052 | 6.9451496 | .002985075 |
| 336 | 112896 | 37933056 | 18.3303028 | 6.9520533 | .002976190 |
| 337 | 113569 | 38272753 | 18.3575598 | 6.9589434 | .002967359 |
| 338 | 114244 | 38614472 | 18.3847763 | 6.9658198 | .002958580 |
| 339 | 114921 | 38958219 | 18.4119526 | 6.9726826 | .002949853 |
| 340 | 115600 | 39304000 | 18.4390889 | 6.9795321 | .002941176 |
| 341 | 116281 | 39651821 | 18.4661853 | 6.9863681 | .002932551 |
| 342 | 116964 | 40001688 | 18.4932420 | 6.9931906 | .002923977 |
| 343 | 117649 | 40353607 | 18.5202592 | 7.0000000 | .002915452 |
| 344 | 118336 | 40707584 | 18.5472370 | 7.0067962 | .002906977 |
| 345 | 119025 | 41063625 | 18.5741756 | 7.0135791 | .002898551 |
| 346 | 119716 | 41421736 | 18.6010752 | 7.0203490 | .002890173 |
| 347 | 120409 | 41781923 | 18.6279360 | 7.0271058 | .002881844 |
| 348 | 121104 | 42144192 | 18.6547581 | 7.0338497 | .002873563 |
| 349 | 121801 | 42508549 | 18.6815417 | 7.0405806 | .002865330 |
| 350 | 122500 | 42875000 | 18.7082869 | 7.0472987 | .002857143 |
| 351 | 123201 | 43243551 | 18.7349940 | 7.0540041 | .002849003 |
| 352 | 123904 | 43614208 | 18.7616630 | 7.0606967 | .002840909 |
| 353 | 124609 | 43986977 | 18.7882942 | 7.0673767 | .002832861 |
| 354 | 125316 | 44361864 | 18.8148877 | 7.0740440 | .002824859 |
| 355 | 126025 | 44738875 | 18.8414437 | 7.0806988 | .002816901 |
| 356 | 126736 | 45118016 | 18.8679623 | 7.0873411 | .002808989 |
| 357 | 127449 | 45499293 | 18.8944436 | 7.0939709 | .002801120 |
| 358 | 128164 | 45882712 | 18.9208879 | 7.1005885 | .002793296 |
| 359 | 128881 | 46268279 | 18.9472953 | 7.1071937 | .002785515 |

SQUARES, CUBES, SQUARE ROOTS, CUBE ROOTS AND RECIPROCAL.

| No. | Squares. | Cubes. | Square Roots. | Cube Roots. | Reciprocals. |
|-----|----------|----------|---------------|-------------|--------------|
| 360 | 129600 | 46656000 | 18.9736660 | 7.1137866 | .002777778 |
| 361 | 130321 | 47045881 | 19.0000000 | 7.1203674 | .002770083 |
| 362 | 131044 | 47437928 | 19.0262976 | 7.1269360 | .002762431 |
| 363 | 131769 | 47832147 | 19.0525589 | 7.1334925 | .002754821 |
| 364 | 132496 | 48223544 | 19.0787840 | 7.1400370 | .002747253 |
| 365 | 133225 | 48627125 | 19.1049732 | 7.1465695 | .002739726 |
| 366 | 133956 | 49027896 | 19.1311265 | 7.1530901 | .002732240 |
| 367 | 134689 | 49430863 | 19.1572441 | 7.1595988 | .002724796 |
| 368 | 135424 | 49836032 | 19.1833261 | 7.1660957 | .002717391 |
| 369 | 136161 | 50243409 | 19.2093727 | 7.1725809 | .002710027 |
| 370 | 136900 | 50653000 | 19.2353841 | 7.1790544 | .002702703 |
| 371 | 137641 | 51064811 | 19.2613603 | 7.1855162 | .002695418 |
| 372 | 138384 | 51478848 | 19.2873015 | 7.1919663 | .002688172 |
| 373 | 139129 | 51895117 | 19.3132079 | 7.1984050 | .002680965 |
| 374 | 139876 | 52313624 | 19.3390796 | 7.2048322 | .002673797 |
| 375 | 140625 | 52734375 | 19.3649167 | 7.2112479 | .002666667 |
| 376 | 141376 | 53157376 | 19.3907194 | 7.2176522 | .002659574 |
| 377 | 142129 | 53582633 | 19.4164878 | 7.2240450 | .002652520 |
| 378 | 142884 | 54010152 | 19.4422221 | 7.2304268 | .002645503 |
| 379 | 143641 | 54439939 | 19.4679223 | 7.2367972 | .002638522 |
| 380 | 144400 | 54872000 | 19.4935887 | 7.2431565 | .002631579 |
| 381 | 145161 | 55306341 | 19.5192213 | 7.2495045 | .002624672 |
| 382 | 145924 | 55742968 | 19.5448203 | 7.2558415 | .002617801 |
| 383 | 146689 | 56181887 | 19.5703858 | 7.2621675 | .002610966 |
| 384 | 147456 | 56623104 | 19.5959179 | 7.2684824 | .002604167 |
| 385 | 148225 | 57066625 | 19.6214169 | 7.2747864 | .002597403 |
| 386 | 148996 | 57512456 | 19.6468827 | 7.2810794 | .002590674 |
| 387 | 149769 | 57960603 | 19.6723156 | 7.2873617 | .002583979 |
| 388 | 150544 | 58411072 | 19.6977156 | 7.2936330 | .002577320 |
| 389 | 151321 | 58863869 | 19.7230829 | 7.2998936 | .002570694 |
| 390 | 152100 | 59319000 | 19.7484177 | 7.3061436 | .002564103 |
| 391 | 152881 | 59776471 | 19.7737199 | 7.3123828 | .002557545 |
| 392 | 153664 | 60236288 | 19.7989899 | 7.3186114 | .002551020 |
| 393 | 154449 | 60698457 | 19.8242276 | 7.3248295 | .002544529 |
| 394 | 155236 | 61162984 | 19.8494332 | 7.3310369 | .002538071 |
| 395 | 156025 | 61629875 | 19.8746069 | 7.3372339 | .002531646 |
| 396 | 156816 | 62099136 | 19.8997487 | 7.3434205 | .002525253 |
| 397 | 157609 | 62570773 | 19.9248588 | 7.3495966 | .002518892 |
| 398 | 158404 | 63044792 | 19.9499373 | 7.3557624 | .002512563 |
| 399 | 159201 | 63521199 | 19.9749844 | 7.3619178 | .002506266 |
| 400 | 160000 | 64000000 | 20.0000000 | 7.3680630 | .002500000 |
| 401 | 160801 | 64481201 | 20.0249844 | 7.3741979 | .002493766 |
| 402 | 161604 | 64964808 | 20.0499377 | 7.3803227 | .002487562 |
| 403 | 162409 | 65450827 | 20.0748599 | 7.3864373 | .002481390 |
| 404 | 163216 | 65939264 | 20.0997512 | 7.3925418 | .002475248 |
| 405 | 164025 | 66430125 | 20.1246118 | 7.3986363 | .002469136 |
| 406 | 164836 | 66923416 | 20.1494417 | 7.4047206 | .002463054 |
| 407 | 165649 | 67419143 | 20.1742410 | 7.4107950 | .002457002 |
| 408 | 166464 | 67917312 | 20.1990099 | 7.4168595 | .002450980 |
| 409 | 167281 | 68417929 | 20.2237484 | 7.4229142 | .002444988 |
| 410 | 168100 | 68921000 | 20.2484567 | 7.4289589 | .002439024 |
| 411 | 168921 | 69426531 | 20.2731349 | 7.4349938 | .002433090 |
| 412 | 169744 | 69934528 | 20.2977831 | 7.4410189 | .002427184 |
| 413 | 170569 | 70444997 | 20.3224014 | 7.4470342 | .002421308 |
| 414 | 171396 | 70957944 | 20.3469899 | 7.4530399 | .002415459 |
| 415 | 172225 | 71473375 | 20.3715488 | 7.4590359 | .002409639 |
| 416 | 173056 | 71991296 | 20.3960781 | 7.4650223 | .002403846 |
| 417 | 173889 | 72511713 | 20.4205779 | 7.4709991 | .002398082 |
| 418 | 174724 | 73034632 | 20.4450483 | 7.4769664 | .002392344 |
| 419 | 175561 | 73560059 | 20.4694895 | 7.4829242 | .002386635 |

SQUARES, CUBES, SQUARE ROOTS, CUBE ROOTS AND RECIPROCAL.

| No. | Squares. | Cubes. | Square Roots. | Cube Roots. | Reciprocals. |
|-----|----------|-----------|---------------|-------------|--------------|
| 420 | 176400 | 74088000 | 20.4939015 | 7.4888724 | .002380952 |
| 421 | 177241 | 74618461 | 20.5182845 | 7.4948113 | .002375297 |
| 422 | 178084 | 75151448 | 20.5426386 | 7.5007406 | .002369668 |
| 423 | 178929 | 75686967 | 20.5669638 | 7.5066607 | .002364066 |
| 424 | 179776 | 76225024 | 20.5912603 | 7.5125715 | .002358491 |
| 425 | 180625 | 76765625 | 20.6155281 | 7.5184730 | .002352941 |
| 426 | 181476 | 77308776 | 20.6397674 | 7.5243652 | .002347418 |
| 427 | 182329 | 77854483 | 20.6639783 | 7.5302482 | .002341920 |
| 428 | 183184 | 78402752 | 20.6881609 | 7.5361221 | .002336449 |
| 429 | 184041 | 78953589 | 20.7123152 | 7.5419867 | .002331002 |
| 430 | 184900 | 79507000 | 20.7364414 | 7.5478423 | .002325581 |
| 431 | 185761 | 80062991 | 20.7605395 | 7.5536888 | .002320186 |
| 432 | 186624 | 80621568 | 20.7846097 | 7.5595263 | .002314815 |
| 433 | 187489 | 81182737 | 20.8086520 | 7.5653548 | .002309469 |
| 434 | 188356 | 81746504 | 20.8326667 | 7.5711743 | .002304147 |
| 435 | 189225 | 82312875 | 20.8566536 | 7.5769849 | .002298851 |
| 436 | 190096 | 82881856 | 20.8806130 | 7.5827865 | .002293578 |
| 437 | 190969 | 83453453 | 20.9045450 | 7.5885793 | .002288330 |
| 438 | 191844 | 84027672 | 20.9284495 | 7.5943633 | .002283105 |
| 439 | 192721 | 84604519 | 20.9523268 | 7.6001385 | .002277904 |
| 440 | 193600 | 85184000 | 20.9761770 | 7.6059049 | .002272727 |
| 441 | 194481 | 85766121 | 21.0000000 | 7.6116626 | .002267574 |
| 442 | 195364 | 86350888 | 21.0237960 | 7.6174116 | .002262443 |
| 443 | 196249 | 86938307 | 21.0475652 | 7.6231519 | .002257336 |
| 444 | 197136 | 87528384 | 21.0713075 | 7.6288837 | .002252252 |
| 445 | 198025 | 88121125 | 21.0950231 | 7.6346067 | .002247191 |
| 446 | 198916 | 88716536 | 21.1187121 | 7.6403213 | .002242152 |
| 447 | 199809 | 89314623 | 21.1423745 | 7.6460272 | .002237136 |
| 448 | 200704 | 89915392 | 21.1660105 | 7.6517247 | .002232143 |
| 449 | 201601 | 90518849 | 21.1896201 | 7.6574138 | .002227171 |
| 450 | 202500 | 91125000 | 21.2132034 | 7.6630943 | .002222222 |
| 451 | 203401 | 91733851 | 21.2367606 | 7.6687665 | .002217295 |
| 452 | 204304 | 92345408 | 21.2602916 | 7.6744303 | .002212389 |
| 453 | 205209 | 92959677 | 21.2837967 | 7.6800857 | .002207506 |
| 454 | 206116 | 93576664 | 21.3072758 | 7.6857328 | .002202643 |
| 455 | 207025 | 94196375 | 21.3307290 | 7.6913717 | .002197802 |
| 456 | 207936 | 94818816 | 21.3541565 | 7.6970023 | .002192982 |
| 457 | 208849 | 95443993 | 21.3775583 | 7.7026246 | .002188184 |
| 458 | 209764 | 96071912 | 21.4009346 | 7.7082388 | .002183406 |
| 459 | 210681 | 96702579 | 21.4242853 | 7.7138448 | .002178649 |
| 460 | 211600 | 97336000 | 21.4476106 | 7.7194426 | .002173913 |
| 461 | 212521 | 97972181 | 21.4709106 | 7.7250325 | .002169197 |
| 462 | 213444 | 98611128 | 21.4941853 | 7.7306141 | .002164502 |
| 463 | 214369 | 99252847 | 21.5174348 | 7.7361877 | .002159827 |
| 464 | 215296 | 99897344 | 21.5406592 | 7.7417532 | .002155172 |
| 465 | 216225 | 100544625 | 21.5638587 | 7.7473109 | .002150538 |
| 466 | 217156 | 101194696 | 21.5870331 | 7.7528606 | .002145923 |
| 467 | 218089 | 101847563 | 21.6101828 | 7.7584023 | .002141328 |
| 468 | 219024 | 102503232 | 21.6333077 | 7.7639361 | .002136752 |
| 469 | 219961 | 103161709 | 21.6564078 | 7.7694620 | .002132196 |
| 470 | 220900 | 103823000 | 21.6794834 | 7.7749801 | .002127660 |
| 471 | 221841 | 104487111 | 21.7025344 | 7.7804904 | .002123142 |
| 472 | 222784 | 105154048 | 21.7255610 | 7.7859928 | .002118644 |
| 473 | 223729 | 105823817 | 21.7485632 | 7.7914875 | .002114165 |
| 474 | 224676 | 106496424 | 21.7715411 | 7.7969745 | .002109705 |
| 475 | 225625 | 107171875 | 21.7944947 | 7.8024538 | .002105263 |
| 476 | 226576 | 107850176 | 21.8174242 | 7.8079254 | .002100840 |
| 477 | 227529 | 108531333 | 21.8403297 | 7.8133892 | .002096436 |
| 478 | 228484 | 109215352 | 21.8632111 | 7.8188456 | .002092050 |
| 479 | 229441 | 109902239 | 21.8860686 | 7.8242942 | .002087683 |

SQUARES, CUBES, SQUARE ROOTS, CUBE ROOTS AND RECIPROCAL.

| No. | Squares. | Cubes. | Square Roots. | Cube Roots. | Reciprocals. |
|-----|----------|-----------|---------------|-------------|--------------|
| 480 | 230400 | 110592000 | 21.9089023 | 7.8297353 | .002083333 |
| 481 | 231361 | 111284641 | 21.9317122 | 7.8351688 | .002079002 |
| 482 | 232324 | 111980168 | 21.9544984 | 7.8405949 | .002074689 |
| 483 | 233289 | 112678587 | 21.9772610 | 7.8460134 | .002070393 |
| 484 | 234256 | 113379904 | 22.0000000 | 7.8514244 | .002066116 |
| 485 | 235225 | 114084125 | 22.0227155 | 7.8568281 | .002061856 |
| 486 | 236196 | 114791256 | 22.0454077 | 7.8622242 | .002057613 |
| 487 | 237169 | 115501303 | 22.0680765 | 7.8676130 | .002053388 |
| 488 | 238144 | 116214272 | 22.0907220 | 7.8729944 | .002049180 |
| 489 | 239121 | 116930169 | 22.1133444 | 7.8783684 | .002044990 |
| 490 | 240100 | 117649000 | 22.1359436 | 7.8837352 | .002040816 |
| 491 | 241081 | 118370771 | 22.1585198 | 7.8890946 | .002036660 |
| 492 | 242064 | 119095488 | 22.1810730 | 7.8944468 | .002032520 |
| 493 | 243049 | 119823157 | 22.2036033 | 7.8997917 | .002028398 |
| 494 | 244036 | 120553784 | 22.2261108 | 7.9051294 | .002024291 |
| 495 | 245025 | 121287375 | 22.2485955 | 7.9104599 | .002020202 |
| 496 | 246016 | 122023936 | 22.2710575 | 7.9157832 | .002016129 |
| 497 | 247009 | 122763473 | 22.2934968 | 7.9210994 | .002012072 |
| 498 | 248004 | 123505992 | 22.3159136 | 7.9264085 | .002008032 |
| 499 | 249001 | 124251499 | 22.3383079 | 7.9317104 | .002004008 |
| 500 | 250000 | 125000000 | 22.3606798 | 7.9370053 | .002000000 |
| 501 | 251001 | 125751501 | 22.3830293 | 7.9422931 | .001996008 |
| 502 | 252004 | 126506008 | 22.4053565 | 7.9475739 | .001992032 |
| 503 | 253009 | 127263527 | 22.4276615 | 7.9528477 | .001988072 |
| 504 | 254016 | 128024064 | 22.4499443 | 7.9581144 | .001984127 |
| 505 | 255025 | 128787625 | 22.4722051 | 7.9633743 | .001980198 |
| 506 | 256036 | 129554216 | 22.4944438 | 7.9686271 | .001976285 |
| 507 | 257049 | 130323843 | 22.5166605 | 7.9738731 | .001972387 |
| 508 | 258064 | 131096512 | 22.5388553 | 7.9791122 | .001968504 |
| 509 | 259081 | 131872229 | 22.5610283 | 7.9843444 | .001964637 |
| 510 | 260100 | 132651000 | 22.5831796 | 7.9895697 | .001960784 |
| 511 | 261121 | 133432831 | 22.6053091 | 7.9947883 | .001956947 |
| 512 | 262144 | 134217728 | 22.6274170 | 8.0000000 | .001953125 |
| 513 | 263169 | 135005697 | 22.6495033 | 8.0052049 | .001949318 |
| 514 | 264196 | 135796744 | 22.6715681 | 8.0104032 | .001945525 |
| 515 | 265225 | 136590875 | 22.6936114 | 8.0155946 | .001941748 |
| 516 | 266256 | 137388096 | 22.7156334 | 8.0207794 | .001937984 |
| 517 | 267289 | 138188413 | 22.7376340 | 8.0259574 | .001934236 |
| 518 | 268324 | 138991832 | 22.7596134 | 8.0311287 | .001930502 |
| 519 | 269361 | 139798359 | 22.7815715 | 8.0362935 | .001926782 |
| 520 | 270400 | 140608000 | 22.8035085 | 8.0414515 | .001923077 |
| 521 | 271441 | 141420761 | 22.8254244 | 8.0466030 | .001919386 |
| 522 | 272484 | 142236648 | 22.8473193 | 8.0517479 | .001915709 |
| 523 | 273529 | 143055667 | 22.8691933 | 8.0568862 | .001912046 |
| 524 | 274576 | 143877824 | 22.8910463 | 8.0620180 | .001908397 |
| 525 | 275625 | 144703125 | 22.9128785 | 8.0671432 | .001904762 |
| 526 | 276676 | 145531576 | 22.9346899 | 8.0722620 | .001901141 |
| 527 | 277729 | 146363183 | 22.9564806 | 8.0773743 | .001897533 |
| 528 | 278784 | 147197952 | 22.9782506 | 8.0824800 | .001893939 |
| 529 | 279841 | 148035889 | 23.0000000 | 8.0875794 | .001890359 |
| 530 | 280900 | 148877000 | 23.0217289 | 8.0926723 | .001886792 |
| 531 | 281961 | 149721291 | 23.0434372 | 8.0977589 | .001883239 |
| 532 | 283024 | 150568768 | 23.0651252 | 8.1028390 | .001879699 |
| 533 | 284089 | 151419437 | 23.0867928 | 8.1079128 | .001876173 |
| 534 | 285156 | 152273304 | 23.1084400 | 8.1129803 | .001872659 |
| 535 | 286225 | 153130375 | 23.1300670 | 8.1180414 | .001869159 |
| 536 | 287296 | 153990656 | 23.1516738 | 8.1230962 | .001865672 |
| 537 | 288369 | 154854153 | 23.1732605 | 8.1281447 | .001862197 |
| 538 | 289444 | 155720872 | 23.1948270 | 8.1331870 | .001858736 |
| 539 | 290521 | 156590819 | 23.2163735 | 8.1382230 | .001855288 |

SQUARES, CUBES, SQUARE ROOTS, CUBE ROOTS AND RECIPROCAL.

| No. | Squares. | Cubes. | Square Roots. | Cube Roots. | Reciprocals. |
|-----|----------|-----------|---------------|-------------|--------------|
| 540 | 291600 | 157464000 | 23.2379001 | 8.1432529 | .001851852 |
| 541 | 292681 | 158340421 | 23.2594067 | 8.1482765 | .001848429 |
| 542 | 293764 | 159220088 | 23.2808935 | 8.1532939 | .001845018 |
| 543 | 294849 | 160103007 | 23.3023604 | 8.1583051 | .001841621 |
| 544 | 295936 | 160989184 | 23.3238076 | 8.1633102 | .001838235 |
| 545 | 297025 | 161878625 | 23.3452351 | 8.1683092 | .001834862 |
| 546 | 298116 | 162771336 | 23.3666429 | 8.1733020 | .001831502 |
| 547 | 299209 | 163667323 | 23.3880311 | 8.1782888 | .001828154 |
| 548 | 300304 | 164566592 | 23.4093993 | 8.1832695 | .001824818 |
| 549 | 301401 | 165469149 | 23.4307490 | 8.1882441 | .001821494 |
| 550 | 302500 | 166375000 | 23.4520788 | 8.1932127 | .001818182 |
| 551 | 303601 | 167284151 | 23.4733892 | 8.1981753 | .001814882 |
| 552 | 304704 | 168196603 | 23.4946802 | 8.2031319 | .001811594 |
| 553 | 305809 | 169112377 | 23.5159520 | 8.2080825 | .001808318 |
| 554 | 306916 | 170031464 | 23.5372046 | 8.2130271 | .001805054 |
| 555 | 308025 | 170953875 | 23.5584380 | 8.2179657 | .001801802 |
| 556 | 309136 | 171879616 | 23.5796522 | 8.2228985 | .001798561 |
| 557 | 310249 | 172808693 | 23.6008474 | 8.2278254 | .001795332 |
| 558 | 311364 | 173741112 | 23.6220236 | 8.2327463 | .001792115 |
| 559 | 312481 | 174676879 | 23.6431808 | 8.2376614 | .001788909 |
| 560 | 313600 | 175616000 | 23.6643191 | 8.2425706 | .001785714 |
| 561 | 314721 | 176558481 | 23.6854386 | 8.2474740 | .001782531 |
| 562 | 315844 | 177504328 | 23.7065392 | 8.2523715 | .001779359 |
| 563 | 316969 | 178453547 | 23.7276210 | 8.2572633 | .001776199 |
| 564 | 318096 | 179406144 | 23.7486842 | 8.2621492 | .001773050 |
| 565 | 319225 | 180362125 | 23.7697286 | 8.2670294 | .001769912 |
| 566 | 320356 | 181321496 | 23.7907545 | 8.2719039 | .001766784 |
| 567 | 321489 | 182284263 | 23.8117618 | 8.2767726 | .001763668 |
| 568 | 322624 | 183250432 | 23.8327506 | 8.2816355 | .001760563 |
| 569 | 323761 | 184220009 | 23.8537209 | 8.2864928 | .001757469 |
| 570 | 324900 | 185193000 | 23.8746728 | 8.2913444 | .001754386 |
| 571 | 326041 | 186169411 | 23.8956063 | 8.2961903 | .001751313 |
| 572 | 327184 | 187149248 | 23.9165215 | 8.3010304 | .001748252 |
| 573 | 328329 | 188132517 | 23.9374184 | 8.3058651 | .001745201 |
| 574 | 329476 | 189119224 | 23.9582971 | 8.3106941 | .001742160 |
| 575 | 330625 | 190109375 | 23.9791576 | 8.3155175 | .001739130 |
| 576 | 331776 | 191102976 | 24.0000000 | 8.3203353 | .001736111 |
| 577 | 332929 | 192100033 | 24.0208243 | 8.3251475 | .001733102 |
| 578 | 334084 | 193100552 | 24.0416306 | 8.3299542 | .001730104 |
| 579 | 335241 | 194104539 | 24.0624188 | 8.3347553 | .001727116 |
| 580 | 336400 | 195112000 | 24.0831891 | 8.3395509 | .001724138 |
| 581 | 337561 | 196122941 | 24.1039416 | 8.3443410 | .001721170 |
| 582 | 338724 | 197137368 | 24.1246762 | 8.3491256 | .001718213 |
| 583 | 339889 | 198155287 | 24.1453929 | 8.3539047 | .001715266 |
| 584 | 341056 | 199176704 | 24.1660919 | 8.3586784 | .001712329 |
| 585 | 342225 | 200201625 | 24.1867732 | 8.3634466 | .001709402 |
| 586 | 343396 | 201230056 | 24.2074369 | 8.3682095 | .001706485 |
| 587 | 344569 | 202262003 | 24.2280829 | 8.3729668 | .001703578 |
| 588 | 345744 | 203297472 | 24.2487113 | 8.3777188 | .001700680 |
| 589 | 346921 | 204336469 | 24.2693222 | 8.3824653 | .001697793 |
| 590 | 348100 | 205379000 | 24.2899156 | 8.3872065 | .001694915 |
| 591 | 349281 | 206425071 | 24.3104916 | 8.3919423 | .001692047 |
| 592 | 350464 | 207474688 | 24.3310501 | 8.3966729 | .001689189 |
| 593 | 351649 | 208527857 | 24.3515913 | 8.4013981 | .001686341 |
| 594 | 352836 | 209584584 | 24.3721152 | 8.4061180 | .001683502 |
| 595 | 354025 | 210644875 | 24.3926218 | 8.4108326 | .001680672 |
| 596 | 355216 | 211708736 | 24.4131112 | 8.4155419 | .001677852 |
| 597 | 356409 | 212776173 | 24.4335834 | 8.4202460 | .001675042 |
| 598 | 357604 | 213847192 | 24.4540385 | 8.4249448 | .001672241 |
| 599 | 358801 | 214921799 | 24.4744765 | 8.4296383 | .001669449 |

SQUARES, CUBES, SQUARE ROOTS, CUBE ROOTS AND RECIPROCAL.

| No. | Squares. | Cubes. | Square Roots. | Cube Roots. | Reciprocals. |
|-----|----------|-----------|---------------|-------------|--------------|
| 600 | 360000 | 216000000 | 24.4948974 | 8.4343267 | .001666667 |
| 601 | 361201 | 217081801 | 24.5153013 | 8.4390098 | .001663894 |
| 602 | 362404 | 218167208 | 24.5356883 | 8.4436877 | .001661130 |
| 603 | 363609 | 219256227 | 24.5560583 | 8.4483605 | .001658375 |
| 604 | 364816 | 220348864 | 24.5764115 | 8.4530281 | .001655629 |
| 605 | 366025 | 221445125 | 24.5967478 | 8.4576906 | .001652893 |
| 606 | 367236 | 222545016 | 24.6170673 | 8.4623479 | .001650165 |
| 607 | 368449 | 223648543 | 24.6373700 | 8.4670001 | .001647446 |
| 608 | 369664 | 224755712 | 24.6576560 | 8.4716471 | .001644737 |
| 609 | 370881 | 225866529 | 24.6779254 | 8.4762892 | .001642036 |
| 610 | 372100 | 226981000 | 24.6981781 | 8.4809261 | .001639344 |
| 611 | 373321 | 228099131 | 24.7184142 | 8.4855579 | .001636661 |
| 612 | 374544 | 229220928 | 24.7386338 | 8.4901848 | .001633987 |
| 613 | 375769 | 230346397 | 24.7588368 | 8.4948065 | .001631321 |
| 614 | 376996 | 231475544 | 24.7790234 | 8.4994233 | .001628664 |
| 615 | 378225 | 232608375 | 24.7991935 | 8.5040350 | .001626016 |
| 616 | 379456 | 233744896 | 24.8193473 | 8.5086417 | .001623377 |
| 617 | 380689 | 234885113 | 24.8394847 | 8.5132435 | .001620746 |
| 618 | 381924 | 236029032 | 24.8596058 | 8.5178403 | .001618123 |
| 619 | 383161 | 237176659 | 24.8797106 | 8.5224321 | .001615509 |
| 620 | 384400 | 238328000 | 24.8997992 | 8.5270189 | .001612903 |
| 621 | 385641 | 239483061 | 24.9198716 | 8.5316009 | .001610306 |
| 622 | 386884 | 240641848 | 24.9399278 | 8.5361780 | .001607717 |
| 623 | 388129 | 241804367 | 24.9599679 | 8.5407501 | .001605136 |
| 624 | 389376 | 242970624 | 24.9799920 | 8.5453173 | .001602564 |
| 625 | 390625 | 244140625 | 25.0000000 | 8.5498797 | .001600000 |
| 626 | 391876 | 245314376 | 25.0199920 | 8.5544372 | .001597444 |
| 627 | 393129 | 246491883 | 25.0399681 | 8.5589899 | .001594896 |
| 628 | 394384 | 247673152 | 25.0599282 | 8.5635377 | .001592357 |
| 629 | 395641 | 248858189 | 25.0798724 | 8.5680807 | .001589825 |
| 630 | 396900 | 250047000 | 25.0998008 | 8.5726189 | .001587302 |
| 631 | 398161 | 251239591 | 25.1197134 | 8.5771523 | .001584786 |
| 632 | 399424 | 252435968 | 25.1396102 | 8.5816809 | .001582278 |
| 633 | 400689 | 253636137 | 25.1594913 | 8.5862047 | .001579779 |
| 634 | 401956 | 254840104 | 25.1793566 | 8.5907238 | .001577287 |
| 635 | 403225 | 256047875 | 25.1992063 | 8.5952380 | .001574803 |
| 636 | 404496 | 257259456 | 25.2190404 | 8.5997476 | .001572327 |
| 637 | 405769 | 258474853 | 25.2388589 | 8.6042525 | .001569859 |
| 638 | 407044 | 259694072 | 25.2586619 | 8.6087526 | .001567398 |
| 639 | 408321 | 260917119 | 25.2784493 | 8.6132480 | .001564945 |
| 640 | 409600 | 262144000 | 25.2982213 | 8.6177388 | .001562500 |
| 641 | 410881 | 263374721 | 25.3179778 | 8.6222248 | .001560062 |
| 642 | 412164 | 264609288 | 25.3377189 | 8.6267063 | .001557632 |
| 643 | 413449 | 265847707 | 25.3574447 | 8.6311830 | .001555210 |
| 644 | 414736 | 267089984 | 25.3771551 | 8.6356551 | .001552795 |
| 645 | 416025 | 268336125 | 25.3968502 | 8.6401226 | .001550388 |
| 646 | 417316 | 269586136 | 25.4165301 | 8.6445855 | .001547988 |
| 647 | 418609 | 270840023 | 25.4361947 | 8.6490437 | .001545595 |
| 648 | 419904 | 272097792 | 25.4558441 | 8.6534974 | .001543210 |
| 649 | 421201 | 273359449 | 25.4754784 | 8.6579465 | .001540832 |
| 650 | 422500 | 274625000 | 25.4950976 | 8.6623911 | .001538462 |
| 651 | 423801 | 275894451 | 25.5147016 | 8.6668310 | .001536098 |
| 652 | 425104 | 277167808 | 25.5342907 | 8.6712665 | .001533742 |
| 653 | 426409 | 278445077 | 25.5538647 | 8.6756974 | .001531394 |
| 654 | 427716 | 279726264 | 25.5734237 | 8.6801237 | .001529052 |
| 655 | 429025 | 281011375 | 25.5929678 | 8.6845456 | .001526718 |
| 656 | 430336 | 282300416 | 25.6124969 | 8.6889630 | .001524390 |
| 657 | 431649 | 283593393 | 25.6320112 | 8.6933759 | .001522070 |
| 658 | 432964 | 284890312 | 25.6515107 | 8.6977843 | .001519757 |
| 659 | 434281 | 286191179 | 25.6709953 | 8.7021882 | .001517451 |

SQUARES, CUBES, SQUARE ROOTS, CUBE ROOTS AND RECIPROCAL.

| No. | Squares. | Cubes. | Square Roots. | Cube Roots. | Reciprocals. |
|-----|----------|-----------|---------------|-------------|--------------|
| 660 | 435600 | 287496000 | 25.6904652 | 8.7065877 | .001515152 |
| 661 | 436921 | 288804781 | 25.7099203 | 8.7109827 | .001512859 |
| 662 | 438244 | 290117528 | 25.7293607 | 8.7153734 | .001510574 |
| 663 | 439569 | 291434247 | 25.7487864 | 8.7197596 | .001508296 |
| 664 | 440896 | 292754944 | 25.7681975 | 8.7241414 | .001506024 |
| 665 | 442225 | 294079625 | 25.7875939 | 8.7285187 | .001503759 |
| 666 | 443556 | 295408296 | 25.8069758 | 8.7328918 | .001501502 |
| 667 | 444889 | 296740963 | 25.8263431 | 8.7372604 | .001499250 |
| 668 | 446224 | 298077632 | 25.8456960 | 8.7416246 | .001497006 |
| 669 | 447561 | 299418309 | 25.8650343 | 8.7459846 | .001494768 |
| 670 | 448900 | 300763000 | 25.8843582 | 8.7503401 | .001492537 |
| 671 | 450241 | 302111711 | 25.9036677 | 8.7546913 | .001490313 |
| 672 | 451584 | 303464448 | 25.9229628 | 8.7590383 | .001488095 |
| 673 | 452929 | 304821217 | 25.9422435 | 8.7633809 | .001485884 |
| 674 | 454276 | 306182024 | 25.9615100 | 8.7677192 | .001483680 |
| 675 | 455625 | 307546875 | 25.9807621 | 8.7720532 | .001481481 |
| 676 | 456976 | 308915776 | 26.0000000 | 8.7763830 | .001479290 |
| 677 | 458329 | 310288733 | 26.0192237 | 8.7807084 | .001477105 |
| 678 | 459684 | 311665752 | 26.0384331 | 8.7850293 | .001474926 |
| 679 | 461041 | 313046839 | 26.0576284 | 8.7893463 | .001472754 |
| 680 | 462400 | 314432000 | 26.0768096 | 8.7936593 | .001470588 |
| 681 | 463761 | 315821241 | 26.0959767 | 8.7979679 | .001468429 |
| 682 | 465124 | 317214568 | 26.1151297 | 8.8022721 | .001466276 |
| 683 | 466489 | 318611987 | 26.1342687 | 8.8065722 | .001464129 |
| 684 | 467856 | 320013504 | 26.1533937 | 8.8108681 | .001461988 |
| 685 | 469225 | 321419125 | 26.1725047 | 8.8151598 | .001459854 |
| 686 | 470596 | 322828856 | 26.1916017 | 8.8194474 | .001457726 |
| 687 | 471969 | 324242703 | 26.2106848 | 8.8237307 | .001455604 |
| 688 | 473344 | 325660672 | 26.2297541 | 8.8280099 | .001453488 |
| 689 | 474721 | 327082769 | 26.2488095 | 8.8322850 | .001451379 |
| 690 | 476100 | 328509000 | 26.2678511 | 8.8365559 | .001449275 |
| 691 | 477481 | 329939371 | 26.2868789 | 8.8408227 | .001447178 |
| 692 | 478864 | 331373888 | 26.3058929 | 8.8450854 | .001445087 |
| 693 | 480249 | 332812557 | 26.3248932 | 8.8493440 | .001443001 |
| 694 | 481636 | 334255384 | 26.3438797 | 8.8535985 | .001440922 |
| 695 | 483025 | 335702375 | 26.3628527 | 8.8578489 | .001438849 |
| 696 | 484416 | 337153536 | 26.3818119 | 8.8620952 | .001436782 |
| 697 | 485809 | 338608873 | 26.4007576 | 8.8663375 | .001434720 |
| 698 | 487204 | 340068392 | 26.4196896 | 8.8705757 | .001432665 |
| 699 | 488601 | 341532099 | 26.4386081 | 8.8748099 | .001430615 |
| 700 | 490000 | 343000000 | 26.4575131 | 8.8790400 | .001428571 |
| 701 | 491401 | 344472101 | 26.4764046 | 8.8832661 | .001426534 |
| 702 | 492804 | 345948408 | 26.4952826 | 8.8874882 | .001424501 |
| 703 | 494209 | 347428927 | 26.5141472 | 8.8917063 | .001422475 |
| 704 | 495616 | 348913664 | 26.5329983 | 8.8959204 | .001420455 |
| 705 | 497025 | 350402625 | 26.5518361 | 8.9001304 | .001418440 |
| 706 | 498436 | 351895816 | 26.5706605 | 8.9043366 | .001416431 |
| 707 | 499849 | 353393243 | 26.5894716 | 8.9085387 | .001414427 |
| 708 | 501264 | 354894912 | 26.6082694 | 8.9127369 | .001412429 |
| 709 | 502681 | 356400829 | 26.6270539 | 8.9169311 | .001410437 |
| 710 | 504100 | 357911000 | 26.6458252 | 8.9211214 | .001408451 |
| 711 | 505521 | 359425431 | 26.6645833 | 8.9253078 | .001406470 |
| 712 | 506944 | 360944128 | 26.6833281 | 8.9294902 | .001404494 |
| 713 | 508369 | 362467097 | 26.7020598 | 8.9336687 | .001402525 |
| 714 | 509796 | 363994344 | 26.7207784 | 8.9378433 | .001400560 |
| 715 | 511225 | 365525875 | 26.7394839 | 8.9420140 | .001398601 |
| 716 | 512656 | 367061696 | 26.7581763 | 8.9461809 | .001396648 |
| 717 | 514089 | 368601813 | 26.7768557 | 8.9503438 | .001394700 |
| 718 | 515524 | 370146232 | 26.7955220 | 8.9545029 | .001392758 |
| 719 | 516961 | 371694959 | 26.8141754 | 8.9586581 | .001390821 |

SQUARES, CUBES, SQUARE ROOTS, CUBE ROOTS AND RECIPROCAL.

| No. | Squares. | Cubes. | Square Roots. | Cube Roots. | Reciprocals. |
|-----|----------|-----------|---------------|-------------|--------------|
| 720 | 518400 | 373248000 | 26.8328157 | 8.9628095 | .001388889 |
| 721 | 519841 | 374805361 | 26.8514432 | 8.9669570 | .001386963 |
| 722 | 521284 | 376367048 | 26.8700577 | 8.9711007 | .001385042 |
| 723 | 522729 | 377933067 | 26.8886593 | 8.9752406 | .001383126 |
| 724 | 524176 | 379503424 | 26.9072481 | 8.9793766 | .001381215 |
| 725 | 525625 | 381078125 | 26.9258240 | 8.9835089 | .001379310 |
| 726 | 527076 | 382657176 | 26.9443872 | 8.9876373 | .001377410 |
| 727 | 528529 | 384240583 | 26.9629375 | 8.9917620 | .001375516 |
| 728 | 529984 | 385828352 | 26.9814751 | 8.9958829 | .001373626 |
| 729 | 531441 | 387420489 | 27.0000000 | 9.0000000 | .001371742 |
| 730 | 532900 | 389017000 | 27.0185122 | 9.0041134 | .001369863 |
| 731 | 534361 | 390617891 | 27.0370117 | 9.0082229 | .001367989 |
| 732 | 535824 | 392223168 | 27.0554985 | 9.0123288 | .001366120 |
| 733 | 537289 | 393832837 | 27.0739727 | 9.0164309 | .001364256 |
| 734 | 538756 | 395446904 | 27.0924344 | 9.0205293 | .001362398 |
| 735 | 540225 | 397065375 | 27.1108834 | 9.0246239 | .001360544 |
| 736 | 541696 | 398688256 | 27.1293199 | 9.0287149 | .001358696 |
| 737 | 543169 | 400315553 | 27.1477439 | 9.0328021 | .001356852 |
| 738 | 544644 | 401947272 | 27.1661554 | 9.0368857 | .001355014 |
| 739 | 546121 | 403583419 | 27.1845544 | 9.0409655 | .001353180 |
| 740 | 547600 | 405224000 | 27.2029410 | 9.0450417 | .001351351 |
| 741 | 549081 | 406869021 | 27.2213152 | 9.0491142 | .001349528 |
| 742 | 550564 | 408518488 | 27.2396769 | 9.0531831 | .001347709 |
| 743 | 552049 | 410172407 | 27.2580263 | 9.0572482 | .001345895 |
| 744 | 553536 | 411830784 | 27.2763634 | 9.0613098 | .001344086 |
| 745 | 555025 | 413493625 | 27.2946881 | 9.0653677 | .001342282 |
| 746 | 556516 | 415160936 | 27.3130006 | 9.0694220 | .001340483 |
| 747 | 558009 | 416832723 | 27.3313007 | 9.0734726 | .001338688 |
| 748 | 559504 | 418508992 | 27.3495887 | 9.0775197 | .001336898 |
| 749 | 561001 | 420189749 | 27.3678644 | 9.0815631 | .001335113 |
| 750 | 562500 | 421875000 | 27.3861279 | 9.0856030 | .001333333 |
| 751 | 564001 | 423564751 | 27.4043792 | 9.0896392 | .001331558 |
| 752 | 565504 | 425259008 | 27.4226184 | 9.0936719 | .001329787 |
| 753 | 567009 | 426957777 | 27.4408455 | 9.0977010 | .001328021 |
| 754 | 568516 | 428661064 | 27.4590604 | 9.1017265 | .001326260 |
| 755 | 570025 | 430368875 | 27.4772633 | 9.1057485 | .001324503 |
| 756 | 571536 | 432081216 | 27.4954542 | 9.1097669 | .001322751 |
| 757 | 573049 | 433798093 | 27.5136330 | 9.1137818 | .001321004 |
| 758 | 574564 | 435519512 | 27.5317998 | 9.1177931 | .001319261 |
| 759 | 576081 | 437245479 | 27.5499546 | 9.1218010 | .001317523 |
| 760 | 577600 | 438976000 | 27.5680975 | 9.1258053 | .001315789 |
| 761 | 579121 | 440711081 | 27.5862284 | 9.1298061 | .001314060 |
| 762 | 580644 | 442450728 | 27.6043475 | 9.1338034 | .001312336 |
| 763 | 582169 | 444194947 | 27.6224546 | 9.1377971 | .001310616 |
| 764 | 583696 | 445943744 | 27.6405499 | 9.1417874 | .001308901 |
| 765 | 585225 | 447697125 | 27.6586334 | 9.1457742 | .001307190 |
| 766 | 586756 | 449455096 | 27.6767050 | 9.1497576 | .001305483 |
| 767 | 588289 | 451217663 | 27.6947648 | 9.1537375 | .001303781 |
| 768 | 589824 | 452984832 | 27.7128129 | 9.1577139 | .001302083 |
| 769 | 591361 | 454756609 | 27.7308492 | 9.1616869 | .001300390 |
| 770 | 592900 | 456533000 | 27.7488739 | 9.1656565 | .001298701 |
| 771 | 594441 | 458314011 | 27.7668868 | 9.1696225 | .001297017 |
| 772 | 595984 | 460099648 | 27.7848880 | 9.1735852 | .001295337 |
| 773 | 597529 | 461889917 | 27.8028775 | 9.1775445 | .001293661 |
| 774 | 599076 | 463684824 | 27.8208555 | 9.1815003 | .001291990 |
| 775 | 600625 | 465484375 | 27.8388218 | 9.1854527 | .001290323 |
| 776 | 602176 | 467288576 | 27.8567766 | 9.1894018 | .001288660 |
| 777 | 603729 | 469097433 | 27.8747197 | 9.1933474 | .001287001 |
| 778 | 605284 | 470910952 | 27.8926514 | 9.1972897 | .001285347 |
| 779 | 606841 | 472729139 | 27.9105715 | 9.2012286 | .001283697 |

SQUARES, CUBES, SQUARE ROOTS, CUBE ROOTS AND RECIPROCAL.

| No. | Squares. | Cubes. | Square Roots. | Cube Roots. | Reciprocals. |
|-----|----------|-----------|---------------|-------------|--------------|
| 780 | 608400 | 474552000 | 27.9284801 | 9.2051641 | .001282051 |
| 781 | 609961 | 476379541 | 27.9463772 | 9.2090962 | .001280410 |
| 782 | 611524 | 478211768 | 27.9642629 | 9.2130250 | .001278772 |
| 783 | 613089 | 480048687 | 27.9821372 | 9.2169505 | .001277139 |
| 784 | 614656 | 481890304 | 28.0000000 | 9.2208726 | .001275510 |
| 785 | 616225 | 483736625 | 28.0178515 | 9.2247914 | .001273885 |
| 786 | 617796 | 485587656 | 28.0356915 | 9.2287068 | .001272265 |
| 787 | 619369 | 487443403 | 28.0535203 | 9.2326189 | .001270648 |
| 788 | 620944 | 489303872 | 28.0713377 | 9.2365277 | .001269036 |
| 789 | 622521 | 491169069 | 28.0891438 | 9.2404333 | .001267427 |
| 790 | 624100 | 493039000 | 28.1069386 | 9.2443355 | .001265823 |
| 791 | 625681 | 494913671 | 28.1247222 | 9.2482344 | .001264223 |
| 792 | 627264 | 496793088 | 28.1424946 | 9.2521300 | .001262626 |
| 793 | 628849 | 498677257 | 28.1602557 | 9.2560224 | .001261034 |
| 794 | 630436 | 500566184 | 28.1780056 | 9.2599114 | .001259446 |
| 795 | 632025 | 502459875 | 28.1957444 | 9.2637973 | .001257862 |
| 796 | 633616 | 504358336 | 28.2134720 | 9.2676798 | .001256281 |
| 797 | 635209 | 506261573 | 28.2311884 | 9.2715592 | .001254705 |
| 798 | 636804 | 508169592 | 28.2488938 | 9.2754352 | .001253133 |
| 799 | 638401 | 510082399 | 28.2665881 | 9.2793081 | .001251564 |
| 800 | 640000 | 512000000 | 28.2842712 | 9.2831777 | .001250000 |
| 801 | 641601 | 513922401 | 28.3019434 | 9.2870440 | .001248439 |
| 802 | 643204 | 515849608 | 28.3196045 | 9.2909072 | .001246883 |
| 803 | 644809 | 517781627 | 28.3372546 | 9.2947671 | .001245330 |
| 804 | 646416 | 519718464 | 28.3548938 | 9.2986239 | .001243781 |
| 805 | 648025 | 521660125 | 28.3725219 | 9.3024775 | .001242236 |
| 806 | 649636 | 523606616 | 28.3901391 | 9.3063278 | .001240695 |
| 807 | 651249 | 525557943 | 28.4077454 | 9.3101750 | .001239157 |
| 808 | 652864 | 527514112 | 28.4253408 | 9.3140190 | .001237624 |
| 809 | 654481 | 529475129 | 28.4429253 | 9.3178599 | .001236094 |
| 810 | 656100 | 531441000 | 28.4604989 | 9.3216975 | .001234568 |
| 811 | 657721 | 533411731 | 28.4780617 | 9.3255320 | .001233046 |
| 812 | 659344 | 535387328 | 28.4956137 | 9.3293634 | .001231527 |
| 813 | 660969 | 537367797 | 28.5131549 | 9.3331916 | .001230012 |
| 814 | 662596 | 539353144 | 28.5306852 | 9.3370167 | .001228501 |
| 815 | 664225 | 541343375 | 28.5482048 | 9.3408386 | .001226994 |
| 816 | 665856 | 543338496 | 28.5657137 | 9.3446575 | .001225490 |
| 817 | 667489 | 545338513 | 28.5832119 | 9.3484731 | .001223990 |
| 818 | 669124 | 547343432 | 28.6006993 | 9.3522857 | .001222494 |
| 819 | 670761 | 549353259 | 28.6181760 | 9.3560952 | .001221001 |
| 820 | 672400 | 551368000 | 28.6356421 | 9.3599016 | .001219512 |
| 821 | 674041 | 553387661 | 28.6530976 | 9.3637049 | .001218027 |
| 822 | 675684 | 555412248 | 28.6705424 | 9.3675051 | .001216545 |
| 823 | 677329 | 557441767 | 28.6879766 | 9.3713022 | .001215067 |
| 824 | 678976 | 559476224 | 28.7054002 | 9.3750963 | .001213592 |
| 825 | 680625 | 561515625 | 28.7228132 | 9.3788873 | .001212121 |
| 826 | 682276 | 563559976 | 28.7402157 | 9.3826752 | .001210654 |
| 827 | 683929 | 565609283 | 28.7576077 | 9.3864600 | .001209190 |
| 828 | 685584 | 567663552 | 28.7749891 | 9.3902419 | .001207729 |
| 829 | 687241 | 569722789 | 28.7923601 | 9.3940206 | .001206273 |
| 830 | 688900 | 571787000 | 28.8097206 | 9.3977964 | .001204819 |
| 831 | 690561 | 573856191 | 28.8270706 | 9.4015691 | .001203369 |
| 832 | 692224 | 575930368 | 28.8444102 | 9.4053387 | .001201923 |
| 833 | 693889 | 578009537 | 28.8617394 | 9.4091054 | .001200480 |
| 834 | 695556 | 580093704 | 28.8790582 | 9.4128690 | .001199041 |
| 835 | 697225 | 582182875 | 28.8963666 | 9.4166297 | .001197605 |
| 836 | 698896 | 584277056 | 28.9136646 | 9.4203873 | .001196172 |
| 837 | 700569 | 586376253 | 28.9309523 | 9.4241420 | .001194743 |
| 838 | 702244 | 588480472 | 28.9482297 | 9.4278936 | .001193317 |
| 839 | 703921 | 590589719 | 28.9654967 | 9.4316423 | .001191895 |

SQUARES, CUBES, SQUARE ROOTS, CUBE ROOTS AND RECIPROCAL.

| No. | Squares. | Cubes. | Square Roots. | Cube Roots. | Reciprocals. |
|-----|----------|-----------|---------------|-------------|--------------|
| 840 | 705600 | 592704000 | 28.9827535 | 9.4353880 | .001190476 |
| 841 | 707281 | 594823321 | 29.0000000 | 9.4391307 | .001189061 |
| 842 | 708964 | 596947688 | 29.0172363 | 9.4428704 | .001187648 |
| 843 | 710649 | 599077107 | 29.0344323 | 9.4466072 | .001186240 |
| 844 | 712336 | 601211584 | 29.0516781 | 9.4503410 | .001184834 |
| 845 | 714025 | 603351125 | 29.0688837 | 9.4540719 | .001183432 |
| 846 | 715716 | 605495736 | 29.0860791 | 9.4577999 | .001182033 |
| 847 | 717409 | 607645423 | 29.1032644 | 9.4615249 | .001180638 |
| 848 | 719104 | 609800192 | 29.1204396 | 9.4652470 | .001179245 |
| 849 | 720801 | 611960049 | 29.1376046 | 9.4689661 | .001177856 |
| 850 | 722500 | 614125000 | 29.1547595 | 9.4726824 | .001176471 |
| 851 | 724201 | 616295051 | 29.1719043 | 9.4763957 | .001175088 |
| 852 | 725904 | 618470208 | 29.1890390 | 9.4801061 | .001173709 |
| 853 | 727609 | 620650477 | 29.2061637 | 9.4838136 | .001172333 |
| 854 | 729316 | 622835864 | 29.2232784 | 9.4875182 | .001170960 |
| 855 | 731025 | 625026375 | 29.2403830 | 9.4912200 | .001169591 |
| 856 | 732736 | 627222016 | 29.2574777 | 9.4949188 | .001168224 |
| 857 | 734449 | 629422793 | 29.2745623 | 9.4986147 | .001166861 |
| 858 | 736164 | 631628712 | 29.2916370 | 9.5023078 | .001165501 |
| 859 | 737881 | 633839779 | 29.3087018 | 9.5059980 | .001164144 |
| 860 | 739600 | 636056000 | 29.3257566 | 9.5096854 | .001162791 |
| 861 | 741321 | 638277381 | 29.3428015 | 9.5133699 | .001161440 |
| 862 | 743044 | 640503928 | 29.3598365 | 9.5170515 | .001160093 |
| 863 | 744769 | 642735647 | 29.3768616 | 9.5207303 | .001158749 |
| 864 | 746496 | 644972544 | 29.3938769 | 9.5244063 | .001157407 |
| 865 | 748225 | 647214625 | 29.4108823 | 9.5280794 | .001156069 |
| 866 | 749956 | 649461896 | 29.4278779 | 9.5317497 | .001154734 |
| 867 | 751689 | 651714363 | 29.4448637 | 9.5354172 | .001153403 |
| 868 | 753424 | 653972032 | 29.4618397 | 9.5390818 | .001152074 |
| 869 | 755161 | 656234909 | 29.4788059 | 9.5427437 | .001150748 |
| 870 | 756900 | 658503000 | 29.4957624 | 9.5464027 | .001149425 |
| 871 | 758641 | 660776311 | 29.5127091 | 9.5500589 | .001148106 |
| 872 | 760384 | 663054848 | 29.5296461 | 9.5537123 | .001146789 |
| 873 | 762129 | 665338617 | 29.5465734 | 9.5573630 | .001145475 |
| 874 | 763876 | 667627624 | 29.5634910 | 9.5610108 | .001144165 |
| 875 | 765625 | 669921875 | 29.5803989 | 9.5646559 | .001142857 |
| 876 | 767376 | 672221376 | 29.5972972 | 9.5682982 | .001141553 |
| 877 | 769129 | 674526133 | 29.6141858 | 9.5719377 | .001140251 |
| 878 | 770884 | 676836152 | 29.6310648 | 9.5755745 | .001138952 |
| 879 | 772641 | 679151439 | 29.6479342 | 9.5792085 | .001137656 |
| 880 | 774400 | 681472000 | 29.6647939 | 9.5828397 | .001136364 |
| 881 | 776161 | 683797841 | 29.6816442 | 9.5864682 | .001135074 |
| 882 | 777924 | 686128968 | 29.6984848 | 9.5900939 | .001133787 |
| 883 | 779689 | 688465387 | 29.7153159 | 9.5937169 | .001132503 |
| 884 | 781456 | 690807104 | 29.7321375 | 9.5973373 | .001131222 |
| 885 | 783225 | 693154125 | 29.7489496 | 9.6009548 | .001129944 |
| 886 | 784996 | 695506456 | 29.7657521 | 9.6045696 | .001128668 |
| 887 | 786769 | 697864103 | 29.7825452 | 9.6081817 | .001127396 |
| 888 | 788544 | 700227072 | 29.7993289 | 9.6117911 | .001126126 |
| 889 | 790321 | 702595369 | 29.8161030 | 9.6153977 | .001124859 |
| 890 | 792100 | 704969000 | 29.8328678 | 9.6190017 | .001123596 |
| 891 | 793881 | 707347971 | 29.8496231 | 9.6226030 | .001122334 |
| 892 | 795664 | 709732288 | 29.8663690 | 9.6262016 | .001121076 |
| 893 | 797449 | 712121957 | 29.8831056 | 9.6297975 | .001119821 |
| 894 | 799236 | 714516984 | 29.8998328 | 9.6333907 | .001118568 |
| 895 | 801025 | 716917375 | 29.9165506 | 9.6369812 | .001117318 |
| 896 | 802816 | 719323136 | 29.9332591 | 9.6405690 | .001116071 |
| 897 | 804609 | 721734273 | 29.9499583 | 9.6441542 | .001114827 |
| 898 | 806404 | 724150792 | 29.9666481 | 9.6477367 | .001113586 |
| 899 | 808201 | 726572609 | 29.9833287 | 9.6513166 | .001112347 |

SQUARES, CUBES, SQUARE ROOTS, CUBE ROOTS AND RECIPROCAL.

| No. | Squares. | Cubes. | Square Roots. | Cube Roots. | Reciprocals. |
|-----|----------|-----------|---------------|-------------|--------------|
| 900 | 810000 | 729000000 | 30.0000000 | 9.6548938 | .001111111 |
| 901 | 811801 | 731432701 | 30.0166620 | 9.6584684 | .001109878 |
| 902 | 813604 | 733870808 | 30.0333148 | 9.6620403 | .001108647 |
| 903 | 815409 | 736314327 | 30.0499584 | 9.6656096 | .001107420 |
| 904 | 817216 | 738763264 | 30.0665928 | 9.6691762 | .001106195 |
| 905 | 819025 | 741217625 | 30.0832179 | 9.6727403 | .001104972 |
| 906 | 820836 | 743677416 | 30.0998339 | 9.6763017 | .001103753 |
| 907 | 822649 | 746142643 | 30.1164407 | 9.6798604 | .001102536 |
| 908 | 824464 | 748613312 | 30.1330383 | 9.6834166 | .001101322 |
| 909 | 826281 | 751089429 | 30.1496269 | 9.6869701 | .001100110 |
| 910 | 828100 | 753571000 | 30.1662063 | 9.6905211 | .001098901 |
| 911 | 829921 | 756058031 | 30.1827765 | 9.6940694 | .001097695 |
| 912 | 831744 | 758550528 | 30.1993377 | 9.6976151 | .001096491 |
| 913 | 833569 | 761048497 | 30.2158899 | 9.7011583 | .001095290 |
| 914 | 835396 | 763551944 | 30.2324329 | 9.7046989 | .001094092 |
| 915 | 837225 | 766060875 | 30.2489669 | 9.7082369 | .001092896 |
| 916 | 839056 | 768575296 | 30.2654919 | 9.7117723 | .001091703 |
| 917 | 840889 | 771095213 | 30.2820079 | 9.7153051 | .001090513 |
| 918 | 842724 | 773620632 | 30.2985148 | 9.7188354 | .001089325 |
| 919 | 844561 | 776151559 | 30.3150128 | 9.7223631 | .001088139 |
| 920 | 846400 | 778688000 | 30.3315018 | 9.7258883 | .001086957 |
| 921 | 848241 | 781229961 | 30.3479818 | 9.7294109 | .001085776 |
| 922 | 850084 | 783777448 | 30.3644529 | 9.7329309 | .001084599 |
| 923 | 851929 | 786330467 | 30.3809151 | 9.7364484 | .001083424 |
| 924 | 853776 | 788889024 | 30.3973683 | 9.7399634 | .001082251 |
| 925 | 855625 | 791453125 | 30.4138127 | 9.7434758 | .001081081 |
| 926 | 857476 | 794022776 | 30.4302481 | 9.7469857 | .001079914 |
| 927 | 859329 | 796597983 | 30.4466747 | 9.7504930 | .001078749 |
| 928 | 861184 | 799178752 | 30.4630924 | 9.7539979 | .001077586 |
| 929 | 863041 | 801765089 | 30.4795013 | 9.7575002 | .001076426 |
| 930 | 864900 | 804357000 | 30.4959014 | 9.7610001 | .001075269 |
| 931 | 866761 | 806954491 | 30.5122926 | 9.7644974 | .001074114 |
| 932 | 868624 | 809557568 | 30.5286750 | 9.7679922 | .001072961 |
| 933 | 870489 | 812166237 | 30.5450487 | 9.7714845 | .001071811 |
| 934 | 872356 | 814780504 | 30.5614136 | 9.7749743 | .001070664 |
| 935 | 874225 | 817400375 | 30.5777697 | 9.7784616 | .001069519 |
| 936 | 876096 | 820025856 | 30.5941171 | 9.7819466 | .001068376 |
| 937 | 877969 | 822656953 | 30.6104557 | 9.7854288 | .001067236 |
| 938 | 879844 | 825293672 | 30.6267857 | 9.7889087 | .001066098 |
| 939 | 881721 | 827936019 | 30.6431069 | 9.7923861 | .001064963 |
| 940 | 883600 | 830584000 | 30.6594194 | 9.7958611 | .001063830 |
| 941 | 885481 | 833237621 | 30.6757233 | 9.7993336 | .001062699 |
| 942 | 887364 | 835896888 | 30.6920185 | 9.8028036 | .001061571 |
| 943 | 889249 | 838561807 | 30.7083051 | 9.8062711 | .001060445 |
| 944 | 891136 | 841232384 | 30.7245830 | 9.8097362 | .001059322 |
| 945 | 893025 | 843908825 | 30.7408523 | 9.8131989 | .001058201 |
| 946 | 894916 | 846590536 | 30.7571130 | 9.8166591 | .001057082 |
| 947 | 896809 | 849278123 | 30.7733651 | 9.8201169 | .001055966 |
| 948 | 898704 | 851971392 | 30.7896086 | 9.8235723 | .001054852 |
| 949 | 900601 | 854670349 | 30.8058436 | 9.8270252 | .001053741 |
| 950 | 902500 | 857375000 | 30.8220700 | 9.8304757 | .001052632 |
| 951 | 904401 | 860085351 | 30.8382879 | 9.8339238 | .001051525 |
| 952 | 906304 | 862801408 | 30.8544972 | 9.8373695 | .001050420 |
| 953 | 908209 | 865523177 | 30.8706981 | 9.8408127 | .001049318 |
| 954 | 910116 | 868250664 | 30.8868904 | 9.8442536 | .001048218 |
| 955 | 912025 | 870983875 | 30.9030743 | 9.8476920 | .001047120 |
| 956 | 913936 | 873722816 | 30.9192497 | 9.8511280 | .001046025 |
| 957 | 915849 | 876467493 | 30.9354166 | 9.8545617 | .001044932 |
| 958 | 917764 | 879217912 | 30.9515751 | 9.8579929 | .001043841 |
| 959 | 919681 | 881974079 | 30.9677251 | 9.8614218 | .001042753 |

SQUARES, CUBES, SQUARE ROOTS, CUBE ROOTS AND RECIPROCAL.

| No. | Squares. | Cubes. | Square Roots. | Cube Roots. | Reciprocals. |
|------|----------|------------|---------------|-------------|--------------|
| 960 | 921600 | 884736000 | 30.9838668 | 9.8648483 | .001041667 |
| 961 | 923521 | 887503681 | 31.0000000 | 9.8682724 | .001040583 |
| 962 | 925444 | 890277128 | 31.0161248 | 9.8716941 | .001039501 |
| 963 | 927369 | 893056347 | 31.0322413 | 9.8751135 | .001038422 |
| 964 | 929296 | 895841344 | 31.0483494 | 9.8785305 | .001037344 |
| 965 | 931225 | 898632125 | 31.0644491 | 9.8819451 | .001036269 |
| 966 | 933156 | 901428696 | 31.0805405 | 9.8853574 | .001035197 |
| 967 | 935089 | 904231063 | 31.0966236 | 9.8887673 | .001034126 |
| 968 | 937024 | 907039232 | 31.1126984 | 9.8921749 | .001033058 |
| 969 | 938961 | 909853209 | 31.1287648 | 9.8955801 | .001031992 |
| 970 | 940900 | 912673000 | 31.1448230 | 9.8989830 | .001030928 |
| 971 | 942841 | 915498611 | 31.1608729 | 9.9023835 | .001029866 |
| 972 | 944784 | 918330048 | 31.1769145 | 9.9057817 | .001028807 |
| 973 | 946729 | 921167317 | 31.1929479 | 9.9091776 | .001027749 |
| 974 | 948676 | 924010424 | 31.2089731 | 9.9125712 | .001026694 |
| 975 | 950625 | 926859375 | 31.2249900 | 9.9159624 | .001025641 |
| 976 | 952576 | 929714176 | 31.2409987 | 9.9193513 | .001024590 |
| 977 | 954529 | 932574833 | 31.2569992 | 9.9227379 | .001023541 |
| 978 | 956484 | 935441352 | 31.2729915 | 9.9261222 | .001022495 |
| 979 | 958441 | 938313739 | 31.2889757 | 9.9295042 | .001021450 |
| 980 | 960400 | 941192000 | 31.3049517 | 9.9328839 | .001020408 |
| 981 | 962361 | 944076141 | 31.3209195 | 9.9362613 | .001019363 |
| 982 | 964324 | 946966168 | 31.3368792 | 9.9396363 | .001018330 |
| 983 | 966289 | 949862087 | 31.3528308 | 9.9430092 | .001017294 |
| 984 | 968256 | 952763904 | 31.3687743 | 9.9463797 | .001016260 |
| 985 | 970225 | 955671625 | 31.3847097 | 9.9497479 | .001015228 |
| 986 | 972196 | 958585256 | 31.4006369 | 9.9531138 | .001014199 |
| 987 | 974169 | 961504803 | 31.4165561 | 9.9564775 | .001013171 |
| 988 | 976144 | 964430272 | 31.4324673 | 9.9598389 | .001012146 |
| 989 | 978121 | 967361669 | 31.4483704 | 9.9631981 | .001011122 |
| 990 | 980100 | 970299000 | 31.4642654 | 9.9665549 | .001010101 |
| 991 | 982081 | 973242271 | 31.4801525 | 9.9699095 | .001009082 |
| 992 | 984064 | 976191488 | 31.4960315 | 9.9732619 | .001008065 |
| 993 | 986049 | 979146657 | 31.5119025 | 9.9766120 | .001007049 |
| 994 | 988036 | 982107784 | 31.5277655 | 9.9799599 | .001006036 |
| 995 | 990025 | 985074875 | 31.5436206 | 9.9833055 | .001005025 |
| 996 | 992016 | 988047936 | 31.5594677 | 9.9866488 | .001004016 |
| 997 | 994009 | 991026973 | 31.5753068 | 9.9899900 | .001003009 |
| 998 | 996004 | 994011992 | 31.5911380 | 9.9933289 | .001002004 |
| 999 | 998001 | 997002999 | 31.6069613 | 9.9966656 | .001001001 |
| 1000 | 1000000 | 1000000000 | 31.6227766 | 10.0000000 | .001000000 |
| 1001 | 1002001 | 1003003001 | 31.6385840 | 10.0033322 | .0009990010 |
| 1002 | 1004004 | 1006012008 | 31.6543836 | 10.0066622 | .0009980040 |
| 1003 | 1006009 | 1009027027 | 31.6701752 | 10.0099899 | .0009970090 |
| 1004 | 1008016 | 1012048064 | 31.6859590 | 10.0133155 | .0009960159 |
| 1005 | 1010025 | 1015075125 | 31.7017349 | 10.0166389 | .0009950249 |
| 1006 | 1012036 | 1018108216 | 31.7175030 | 10.0199601 | .0009940358 |
| 1007 | 1014049 | 1021147343 | 31.7332633 | 10.0232791 | .0009930487 |
| 1008 | 1016064 | 1024192512 | 31.7490157 | 10.0265958 | .0009920635 |
| 1009 | 1018081 | 1027243729 | 31.7647603 | 10.0299104 | .0009910803 |
| 1010 | 1020100 | 1030301000 | 31.7804972 | 10.0332228 | .0009900990 |
| 1011 | 1022121 | 1033364331 | 31.7962262 | 10.0365330 | .0009891197 |
| 1012 | 1024144 | 1036433728 | 31.8119474 | 10.0398410 | .0009881423 |
| 1013 | 1026169 | 1039509197 | 31.8276609 | 10.0431469 | .0009871668 |
| 1014 | 1028196 | 1042590744 | 31.8433666 | 10.0464506 | .0009861933 |
| 1015 | 1030225 | 1045678375 | 31.8590646 | 10.0497521 | .0009852217 |
| 1016 | 1032256 | 1048772096 | 31.8747549 | 10.0530514 | .0009842520 |
| 1017 | 1034289 | 1051871913 | 31.8904374 | 10.0563485 | .0009832842 |
| 1018 | 1036324 | 1054977832 | 31.9061123 | 10.0596435 | .0009823183 |
| 1019 | 1038361 | 1058089859 | 31.9217794 | 10.0629364 | .0009813543 |

SQUARES OF NUMBERS AND FRACTIONAL INTERVALS.

| Fraction | 0 | 1 | 2 | 3 | 4 | 5 |
|------------------------------------|---------|---------|---------|----------|----------|----------|
| 0 | .000000 | 1.00000 | 4.00000 | 9.00000 | 16.00000 | 25.00000 |
| $\frac{1}{64}$.. | .000244 | 1.03149 | 4.06274 | 9.09399 | 16.12524 | 25.15649 |
| $\frac{2}{64}$ $\frac{1}{32}$.. | .000977 | 1.06348 | 4.12598 | 9.18848 | 16.25098 | 25.31348 |
| $\frac{3}{64}$.. | .002197 | 1.09595 | 4.18970 | 9.28345 | 16.37720 | 25.47095 |
| $\frac{4}{64}$ $\frac{1}{16}$.. | .003906 | 1.12891 | 4.25391 | 9.37891 | 16.50391 | 25.62891 |
| $\frac{5}{64}$.. | .006104 | 1.16235 | 4.31860 | 9.47485 | 16.63110 | 25.78735 |
| $\frac{6}{64}$ $\frac{3}{32}$.. | .008789 | 1.19629 | 4.38379 | 9.57129 | 16.75879 | 25.94629 |
| $\frac{7}{64}$.. | .011963 | 1.23071 | 4.44946 | 9.66821 | 16.88596 | 26.10571 |
| $\frac{8}{64}$ $\frac{1}{8}$.. | .015625 | 1.26563 | 4.51563 | 9.76563 | 17.01563 | 26.26563 |
| $\frac{9}{64}$.. | .019775 | 1.30103 | 4.58228 | 9.86353 | 17.14478 | 26.42603 |
| $\frac{10}{64}$ $\frac{5}{32}$.. | .024414 | 1.33691 | 4.64941 | 9.96191 | 17.27441 | 26.58691 |
| $\frac{11}{64}$.. | .029541 | 1.37329 | 4.71704 | 10.05079 | 17.40454 | 26.74829 |
| $\frac{12}{64}$ $\frac{3}{16}$.. | .035156 | 1.41016 | 4.78516 | 10.16016 | 17.53516 | 26.91016 |
| $\frac{13}{64}$.. | .041260 | 1.44751 | 4.85376 | 10.26001 | 17.66626 | 27.07251 |
| $\frac{14}{64}$ $\frac{7}{32}$.. | .047852 | 1.48535 | 4.92285 | 10.36035 | 17.79785 | 27.23535 |
| $\frac{15}{64}$.. | .054932 | 1.52368 | 4.99243 | 10.46118 | 17.92993 | 27.39868 |
| $\frac{16}{64}$ $\frac{1}{4}$.. | .062500 | 1.56250 | 5.06250 | 10.56250 | 18.06250 | 27.56250 |
| $\frac{17}{64}$.. | .070557 | 1.60131 | 5.13306 | 10.66431 | 18.19556 | 27.72681 |
| $\frac{18}{64}$ $\frac{9}{32}$.. | .079102 | 1.64160 | 5.20410 | 10.76560 | 18.32910 | 27.89160 |
| $\frac{19}{64}$.. | .088135 | 1.68188 | 5.27563 | 10.86938 | 18.46313 | 28.05638 |
| $\frac{20}{64}$ $\frac{5}{16}$.. | .097656 | 1.72266 | 5.34766 | 10.97266 | 18.59766 | 28.22266 |
| $\frac{21}{64}$.. | .107666 | 1.76392 | 5.42017 | 11.07642 | 18.73267 | 28.38892 |
| $\frac{22}{64}$ $\frac{11}{32}$.. | .118164 | 1.80566 | 5.49316 | 11.18066 | 18.86816 | 28.55566 |
| $\frac{23}{64}$.. | .129150 | 1.84790 | 5.56665 | 11.28540 | 19.00415 | 28.72290 |
| $\frac{24}{64}$ $\frac{3}{8}$.. | .140625 | 1.89063 | 5.64063 | 11.39063 | 19.14063 | 28.89063 |
| $\frac{25}{64}$.. | .152588 | 1.93384 | 5.71509 | 11.49634 | 19.27759 | 29.05884 |
| $\frac{26}{64}$ $\frac{13}{32}$.. | .165039 | 1.97754 | 5.79004 | 11.60254 | 19.41504 | 29.22754 |
| $\frac{27}{64}$.. | .177979 | 2.02173 | 5.86548 | 11.70923 | 19.55298 | 29.39673 |
| $\frac{28}{64}$ $\frac{7}{16}$.. | .191406 | 2.06641 | 5.94141 | 11.81641 | 19.69141 | 29.56641 |
| $\frac{29}{64}$.. | .205322 | 2.11157 | 6.01782 | 11.92407 | 19.83032 | 29.73657 |
| $\frac{30}{64}$ $\frac{15}{32}$.. | .219727 | 2.15723 | 6.09473 | 12.03223 | 19.96973 | 29.90723 |
| $\frac{31}{64}$.. | .234619 | 2.20337 | 6.17212 | 12.14037 | 20.10962 | 30.07837 |
| $\frac{32}{64}$ $\frac{1}{2}$.. | .250000 | 2.25000 | 6.25000 | 12.25000 | 20.25000 | 30.25000 |
| $\frac{33}{64}$.. | .265869 | 2.29712 | 6.32837 | 12.35962 | 20.39037 | 30.42212 |
| $\frac{34}{64}$ $\frac{17}{32}$.. | .282227 | 2.34473 | 6.40723 | 12.46973 | 20.53223 | 30.59473 |
| $\frac{35}{64}$.. | .299072 | 2.39282 | 6.48657 | 12.58032 | 20.67407 | 30.76782 |
| $\frac{36}{64}$ $\frac{9}{16}$.. | .316406 | 2.44141 | 6.56641 | 12.69141 | 20.81641 | 30.94141 |
| $\frac{37}{64}$.. | .334229 | 2.49048 | 6.64673 | 12.80298 | 20.95923 | 31.11548 |
| $\frac{38}{64}$ $\frac{19}{32}$.. | .352539 | 2.54004 | 6.72754 | 12.91504 | 21.10254 | 31.29004 |
| $\frac{39}{64}$.. | .371338 | 2.59009 | 6.80884 | 13.02759 | 21.24634 | 31.46509 |
| $\frac{40}{64}$ $\frac{5}{8}$.. | .390625 | 2.64063 | 6.89063 | 13.14063 | 21.39063 | 31.64063 |
| $\frac{41}{64}$.. | .410400 | 2.69165 | 6.97290 | 13.25415 | 21.53540 | 31.81665 |
| $\frac{42}{64}$ $\frac{21}{32}$.. | .430664 | 2.74316 | 7.05566 | 13.36816 | 21.68066 | 31.99316 |
| $\frac{43}{64}$.. | .451416 | 2.79517 | 7.13892 | 13.48267 | 21.82642 | 32.17017 |
| $\frac{44}{64}$ $\frac{11}{16}$.. | .472656 | 2.84766 | 7.22266 | 13.59766 | 21.97266 | 32.34766 |
| $\frac{45}{64}$.. | .494385 | 2.90063 | 7.30688 | 13.71313 | 22.11938 | 32.52563 |
| $\frac{46}{64}$ $\frac{23}{32}$.. | .516602 | 2.95410 | 7.39160 | 13.82910 | 22.26660 | 32.70410 |
| $\frac{47}{64}$.. | .539307 | 3.00806 | 7.47681 | 13.94556 | 22.41431 | 32.88306 |

SQUARES OF NUMBERS AND FRACTIONAL INTERVALS.

| Fraction | 6 | 7 | 8 | 9 | 10 | 11 |
|-----------------|----------|----------|----------|----------|-----------|-----------|
| 0 | 36.00000 | 49.00000 | 64.00000 | 81.00000 | 100.00000 | 121.00000 |
| $\frac{1}{64}$ | 36.18774 | 49.21899 | 64.25024 | 81.28140 | 100.31274 | 121.34399 |
| $\frac{2}{64}$ | 36.37598 | 49.43848 | 64.50098 | 81.56348 | 100.62593 | 121.68848 |
| $\frac{3}{64}$ | 36.56470 | 49.65845 | 64.75220 | 81.84595 | 100.93970 | 122.03345 |
| $\frac{4}{64}$ | 36.75391 | 49.87891 | 65.00391 | 82.12891 | 101.25391 | 122.37891 |
| $\frac{5}{64}$ | 36.94360 | 50.09985 | 65.25610 | 82.41235 | 101.56860 | 122.72485 |
| $\frac{6}{64}$ | 37.13379 | 50.32129 | 65.50879 | 82.69629 | 101.88379 | 123.07129 |
| $\frac{7}{64}$ | 37.32446 | 50.54221 | 65.76196 | 82.98071 | 102.19946 | 123.41821 |
| $\frac{8}{64}$ | 37.51563 | 50.76563 | 66.01563 | 83.26563 | 102.51563 | 123.76563 |
| $\frac{9}{64}$ | 37.70728 | 50.98853 | 66.26978 | 83.55103 | 102.83228 | 124.11353 |
| $\frac{10}{64}$ | 37.89941 | 51.21191 | 66.52441 | 83.83691 | 103.14941 | 124.46191 |
| $\frac{11}{64}$ | 38.09204 | 51.43579 | 66.77954 | 84.12329 | 103.46704 | 124.81079 |
| $\frac{12}{64}$ | 38.28516 | 51.66016 | 67.03516 | 84.41016 | 103.78516 | 125.16016 |
| $\frac{13}{64}$ | 38.47876 | 51.88501 | 67.29126 | 84.69751 | 104.10376 | 125.51001 |
| $\frac{14}{64}$ | 38.67285 | 52.11035 | 67.54785 | 84.98535 | 104.42285 | 125.86035 |
| $\frac{15}{64}$ | 38.86743 | 52.33618 | 67.80493 | 85.27368 | 104.74243 | 126.21118 |
| $\frac{16}{64}$ | 39.06250 | 52.56250 | 68.06250 | 85.56250 | 105.06250 | 126.56250 |
| $\frac{17}{64}$ | 39.25806 | 52.78931 | 68.32056 | 85.85181 | 105.38306 | 126.91431 |
| $\frac{18}{64}$ | 39.45410 | 53.01660 | 68.57910 | 86.14160 | 105.70410 | 127.26660 |
| $\frac{19}{64}$ | 39.65063 | 53.24438 | 68.83813 | 86.43188 | 106.02563 | 127.61938 |
| $\frac{20}{64}$ | 39.84766 | 53.47266 | 69.09766 | 86.72266 | 106.34766 | 127.97266 |
| $\frac{21}{64}$ | 40.04517 | 53.70142 | 69.35767 | 87.01392 | 106.67017 | 128.32642 |
| $\frac{22}{64}$ | 40.24316 | 53.93066 | 69.61816 | 87.30566 | 106.99316 | 128.68066 |
| $\frac{23}{64}$ | 40.44165 | 54.16040 | 69.87915 | 87.59790 | 107.31665 | 129.03540 |
| $\frac{24}{64}$ | 40.64063 | 54.39063 | 70.14063 | 87.89063 | 107.64063 | 129.39063 |
| $\frac{25}{64}$ | 40.84009 | 54.62134 | 70.40269 | 88.18384 | 107.96509 | 129.74634 |
| $\frac{26}{64}$ | 41.04004 | 54.85254 | 70.66504 | 88.47764 | 108.29004 | 130.10254 |
| $\frac{27}{64}$ | 41.24048 | 55.08423 | 70.92798 | 88.77173 | 108.61548 | 130.45923 |
| $\frac{28}{64}$ | 41.44141 | 55.31641 | 71.19141 | 89.06641 | 108.94141 | 130.81641 |
| $\frac{29}{64}$ | 41.64282 | 55.54907 | 71.45532 | 89.36157 | 109.26782 | 131.17407 |
| $\frac{30}{64}$ | 41.84473 | 55.78223 | 71.71973 | 89.65723 | 109.59473 | 131.53223 |
| $\frac{31}{64}$ | 42.04712 | 56.01587 | 71.98462 | 89.95337 | 109.92212 | 131.89087 |
| $\frac{32}{64}$ | 42.25000 | 56.25000 | 72.25000 | 90.25000 | 110.25000 | 132.25000 |
| $\frac{33}{64}$ | 42.45337 | 56.48462 | 72.51587 | 90.54712 | 110.57837 | 132.60962 |
| $\frac{34}{64}$ | 42.65723 | 56.71973 | 72.78223 | 90.84473 | 110.90723 | 132.96973 |
| $\frac{35}{64}$ | 42.86157 | 56.95532 | 73.04907 | 91.14282 | 111.23657 | 133.33032 |
| $\frac{36}{64}$ | 43.06641 | 57.19141 | 73.31641 | 91.44141 | 111.56641 | 133.69141 |
| $\frac{37}{64}$ | 43.27173 | 57.42798 | 73.58423 | 91.74048 | 111.89673 | 134.05298 |
| $\frac{38}{64}$ | 43.47754 | 57.66504 | 73.85254 | 92.04004 | 112.22754 | 134.41504 |
| $\frac{39}{64}$ | 43.68384 | 57.90259 | 74.12134 | 92.34009 | 112.55884 | 134.77759 |
| $\frac{40}{64}$ | 43.89063 | 58.14063 | 74.39063 | 92.64063 | 112.89063 | 135.14063 |
| $\frac{41}{64}$ | 44.09790 | 58.37915 | 74.66040 | 92.94165 | 113.22290 | 135.50415 |
| $\frac{42}{64}$ | 44.30566 | 58.61816 | 74.93066 | 93.24316 | 113.55566 | 135.86816 |
| $\frac{43}{64}$ | 44.51392 | 58.85767 | 75.20142 | 93.54517 | 113.88892 | 136.23267 |
| $\frac{44}{64}$ | 44.72266 | 59.09766 | 75.47266 | 93.84766 | 114.22266 | 136.59766 |
| $\frac{45}{64}$ | 44.93183 | 59.33813 | 75.74438 | 94.15063 | 114.55683 | 136.96313 |
| $\frac{46}{64}$ | 45.14160 | 59.57910 | 76.01660 | 94.45410 | 114.89160 | 137.32910 |
| $\frac{47}{64}$ | 45.35181 | 59.82056 | 76.28931 | 94.75806 | 115.22681 | 137.69556 |

SQUARES OF NUMBERS AND FRACTIONAL INTERVALS.

| Fraction | 0 | 1 | 2 | 3 | 4 | 5 |
|----------------------------------|----------|----------|----------|----------|----------|----------|
| $\frac{.49}{64}$ $\frac{3}{4}$ | .562500 | 3.06250 | 7.56250 | 14.06250 | 22.56250 | 33.06250 |
| $\frac{.54}{64}$ $\frac{25}{32}$ | .586182 | 3.11743 | 7.64868 | 14.17993 | 22.71118 | 33.24243 |
| $\frac{.59}{64}$ $\frac{3}{8}$ | .610352 | 3.17285 | 7.73535 | 14.29785 | 22.86035 | 33.42285 |
| $\frac{.64}{64}$ $\frac{1}{2}$ | .635010 | 3.22876 | 7.82251 | 14.41626 | 23.01001 | 33.60376 |
| $\frac{.69}{64}$ $\frac{13}{16}$ | .660156 | 3.28516 | 7.91016 | 14.53516 | 23.16016 | 33.78516 |
| $\frac{.74}{64}$ $\frac{27}{32}$ | .685791 | 3.34204 | 7.99829 | 14.65454 | 23.31079 | 33.96704 |
| $\frac{.79}{64}$ $\frac{3}{4}$ | .711914 | 3.39941 | 8.08691 | 14.77441 | 23.46191 | 34.14941 |
| $\frac{.84}{64}$ $\frac{1}{2}$ | .738525 | 3.45728 | 8.17603 | 14.89478 | 23.61353 | 34.33228 |
| $\frac{.89}{64}$ $\frac{7}{8}$ | .765625 | 3.51563 | 8.26563 | 15.01563 | 23.76563 | 34.51563 |
| $\frac{.94}{64}$ $\frac{29}{32}$ | .793213 | 3.57446 | 8.35571 | 15.13696 | 23.91821 | 34.69946 |
| $\frac{.99}{64}$ $\frac{3}{4}$ | .821289 | 3.63379 | 8.44629 | 15.25879 | 24.07129 | 34.88379 |
| $\frac{.1}{64}$ $\frac{1}{2}$ | .849854 | 3.69360 | 8.53735 | 15.38110 | 24.22485 | 35.06860 |
| $\frac{.15}{64}$ $\frac{15}{16}$ | .878906 | 3.75391 | 8.62891 | 15.50391 | 24.37891 | 35.25391 |
| $\frac{.2}{64}$ $\frac{3}{4}$ | .908447 | 3.81470 | 8.72095 | 15.62720 | 24.53345 | 35.43970 |
| $\frac{.25}{64}$ $\frac{31}{32}$ | .938477 | 3.87598 | 8.81348 | 15.75098 | 24.68848 | 35.62598 |
| $\frac{.3}{64}$ $\frac{1}{2}$ | .968994 | 3.93774 | 8.90649 | 15.87524 | 24.84399 | 35.81274 |
| Fraction | 12 | 13 | 14 | 15 | 16 | 17 |
| $\frac{.35}{32}$ $\frac{0}{1}$ | 144.0000 | 169.0000 | 196.0000 | 225.0000 | 256.0000 | 289.0000 |
| $\frac{.4}{32}$ $\frac{1}{16}$ | 144.7510 | 169.8135 | 196.8760 | 225.9385 | 257.0010 | 290.0635 |
| $\frac{.45}{32}$ $\frac{3}{16}$ | 145.5039 | 170.6289 | 197.7539 | 226.8789 | 258.0039 | 291.1289 |
| $\frac{.5}{32}$ $\frac{1}{8}$ | 146.2588 | 171.4463 | 198.6338 | 227.8213 | 259.0088 | 292.1963 |
| $\frac{.55}{32}$ $\frac{5}{16}$ | 147.0156 | 172.2656 | 199.5156 | 228.7656 | 260.0156 | 293.2656 |
| $\frac{.6}{32}$ $\frac{3}{8}$ | 147.7744 | 173.0869 | 200.3994 | 229.7119 | 261.0244 | 294.3369 |
| $\frac{.65}{32}$ $\frac{7}{16}$ | 148.5352 | 173.9102 | 201.2852 | 230.6602 | 262.0352 | 295.4102 |
| $\frac{.7}{32}$ $\frac{1}{2}$ | 149.2979 | 174.7354 | 202.1725 | 231.6104 | 263.0479 | 296.4854 |
| $\frac{.75}{32}$ $\frac{9}{16}$ | 150.0625 | 175.5625 | 203.0625 | 232.5625 | 264.0625 | 297.5625 |
| $\frac{.8}{32}$ $\frac{5}{8}$ | 150.8291 | 176.3916 | 203.9541 | 233.5166 | 265.0791 | 298.6416 |
| $\frac{.85}{32}$ $\frac{11}{16}$ | 151.5977 | 177.2227 | 204.8477 | 234.4727 | 266.0977 | 299.7227 |
| $\frac{.9}{32}$ $\frac{3}{4}$ | 152.3682 | 178.0557 | 205.7432 | 235.4307 | 267.1182 | 300.8057 |
| $\frac{.95}{32}$ $\frac{7}{8}$ | 153.1406 | 178.8906 | 206.6406 | 236.3906 | 268.1406 | 301.8906 |
| $\frac{.1}{32}$ $\frac{15}{16}$ | 153.9150 | 179.7275 | 207.5400 | 237.3525 | 269.1650 | 302.9775 |
| $\frac{.15}{32}$ $\frac{1}{2}$ | 154.6914 | 180.5664 | 208.4414 | 238.3164 | 270.1914 | 304.0664 |
| $\frac{.2}{32}$ $\frac{9}{16}$ | 155.4697 | 181.4072 | 209.3447 | 239.2822 | 271.2197 | 305.1572 |
| $\frac{.25}{32}$ $\frac{5}{8}$ | 156.2500 | 182.2500 | 210.2500 | 240.2500 | 272.2500 | 306.2500 |
| $\frac{.3}{32}$ $\frac{11}{16}$ | 157.0322 | 183.0947 | 211.1572 | 241.2197 | 273.2822 | 307.3447 |
| $\frac{.35}{32}$ $\frac{3}{4}$ | 157.8164 | 183.9414 | 212.0664 | 242.1914 | 274.3164 | 308.4414 |
| $\frac{.4}{32}$ $\frac{7}{8}$ | 158.6025 | 184.7900 | 212.9775 | 243.1650 | 275.3525 | 309.5400 |
| $\frac{.45}{32}$ $\frac{15}{16}$ | 159.3906 | 185.6406 | 213.8906 | 244.1406 | 276.3906 | 310.6406 |
| $\frac{.5}{32}$ $\frac{1}{2}$ | 160.1807 | 186.4932 | 214.8057 | 245.1182 | 277.4307 | 311.7432 |
| $\frac{.55}{32}$ $\frac{9}{16}$ | 160.9727 | 187.3477 | 215.7227 | 246.0977 | 278.4727 | 312.8477 |
| $\frac{.6}{32}$ $\frac{5}{8}$ | 161.7666 | 188.2041 | 216.6416 | 247.0791 | 279.5166 | 313.9541 |
| $\frac{.65}{32}$ $\frac{11}{16}$ | 162.5625 | 189.0625 | 217.5625 | 248.0625 | 280.5625 | 315.0625 |
| $\frac{.7}{32}$ $\frac{3}{4}$ | 163.3604 | 189.9229 | 218.4854 | 249.0479 | 281.6104 | 316.1729 |
| $\frac{.75}{32}$ $\frac{7}{8}$ | 164.1602 | 190.7852 | 219.4102 | 250.0352 | 282.6602 | 317.2852 |
| $\frac{.8}{32}$ $\frac{15}{16}$ | 164.9619 | 191.6494 | 220.3369 | 251.0244 | 283.7119 | 318.3994 |
| $\frac{.85}{32}$ $\frac{1}{2}$ | 165.7656 | 192.5156 | 221.2656 | 252.0156 | 284.7656 | 319.5156 |
| $\frac{.9}{32}$ $\frac{9}{16}$ | 166.5713 | 193.3838 | 222.1963 | 253.0088 | 285.8213 | 320.6338 |
| $\frac{.95}{32}$ $\frac{5}{8}$ | 167.3789 | 194.2639 | 223.1289 | 254.0039 | 286.8789 | 321.7539 |
| $\frac{.1}{32}$ $\frac{11}{16}$ | 168.1885 | 195.1260 | 224.0636 | 255.0010 | 287.9385 | 322.8760 |

SQUARES OF NUMBERS AND FRACTIONAL INTERVALS.

| Fraction | 6 | 7 | 8 | 9 | 10 | 11 |
|-----------------|----------|----------|----------|----------|-----------|-----------|
| $\frac{3}{4}$ | 45.56250 | 60.06250 | 76.56250 | 95.06250 | 115.56250 | 138.06250 |
| $\frac{5}{8}$ | 45.77368 | 60.30493 | 76.83618 | 95.36743 | 115.89868 | 138.42993 |
| $\frac{1}{2}$ | 45.98535 | 60.54785 | 77.11035 | 95.67285 | 116.23535 | 138.79785 |
| $\frac{3}{8}$ | 46.19751 | 60.79126 | 77.38501 | 95.97876 | 116.57251 | 139.16626 |
| $\frac{1}{4}$ | 46.41016 | 61.03516 | 77.66016 | 96.28516 | 116.91016 | 139.53516 |
| $\frac{5}{16}$ | 46.62329 | 61.27954 | 77.93579 | 96.59204 | 117.24829 | 139.90454 |
| $\frac{3}{16}$ | 46.83691 | 61.52441 | 78.21191 | 96.89941 | 117.58691 | 140.27441 |
| $\frac{1}{8}$ | 47.05103 | 61.76978 | 78.48853 | 97.20728 | 117.92603 | 140.64478 |
| $\frac{5}{8}$ | 47.26563 | 62.01563 | 78.76563 | 97.51563 | 118.26563 | 141.01563 |
| $\frac{3}{4}$ | 47.48071 | 62.26196 | 79.04321 | 97.82446 | 118.60571 | 141.38696 |
| $\frac{7}{8}$ | 47.69629 | 62.50879 | 79.32129 | 98.13379 | 118.94629 | 141.75879 |
| $\frac{15}{16}$ | 47.91235 | 62.75610 | 79.59985 | 98.44360 | 119.28735 | 142.13110 |
| $\frac{1}{2}$ | 48.12891 | 63.00391 | 79.87891 | 98.75391 | 119.62891 | 142.50391 |
| $\frac{5}{8}$ | 48.34595 | 63.25220 | 80.15845 | 99.06470 | 119.97095 | 142.87720 |
| $\frac{3}{4}$ | 48.56348 | 63.50098 | 80.43848 | 99.37598 | 120.31348 | 143.25098 |
| $\frac{7}{8}$ | 48.78149 | 63.75024 | 80.71899 | 99.68774 | 120.65649 | 143.62524 |

| Fraction | 18 | 19 | 20 | 21 | 22 | 23 |
|-----------------|----------|----------|----------|----------|----------|----------|
| 0 | 324.0000 | 361.0000 | 400.0000 | 441.0000 | 484.0000 | 529.0000 |
| $\frac{1}{32}$ | 325.1260 | 362.1885 | 401.2510 | 442.3135 | 485.3760 | 530.4385 |
| $\frac{1}{16}$ | 326.2539 | 363.3789 | 402.5039 | 443.6289 | 486.7539 | 531.8789 |
| $\frac{3}{32}$ | 327.3838 | 364.5713 | 403.7588 | 444.9463 | 488.1338 | 533.3213 |
| $\frac{1}{8}$ | 328.5156 | 365.7656 | 405.0156 | 446.2656 | 489.5156 | 534.7656 |
| $\frac{5}{32}$ | 329.6494 | 366.9619 | 406.2744 | 447.5869 | 490.8994 | 536.2119 |
| $\frac{3}{16}$ | 330.7852 | 368.1602 | 407.5352 | 448.9102 | 492.2852 | 537.6602 |
| $\frac{7}{32}$ | 331.9229 | 369.3604 | 408.7979 | 450.2354 | 493.6729 | 539.1104 |
| $\frac{1}{4}$ | 333.0625 | 370.5625 | 410.0625 | 451.5625 | 495.0625 | 540.5625 |
| $\frac{5}{16}$ | 334.2041 | 371.7666 | 411.3291 | 452.8916 | 496.4541 | 542.0166 |
| $\frac{3}{8}$ | 335.3477 | 372.9727 | 412.5977 | 454.2227 | 497.8477 | 543.4727 |
| $\frac{7}{16}$ | 336.4932 | 374.1807 | 413.8682 | 455.5557 | 499.2432 | 544.9307 |
| $\frac{1}{2}$ | 337.6406 | 375.3906 | 415.1406 | 456.8906 | 500.6406 | 546.3906 |
| $\frac{5}{8}$ | 338.7900 | 376.6025 | 416.4150 | 458.2275 | 502.0400 | 547.8525 |
| $\frac{3}{4}$ | 339.9414 | 377.8164 | 417.6914 | 459.5664 | 503.4414 | 549.3164 |
| $\frac{7}{8}$ | 341.0947 | 379.0322 | 418.9697 | 460.9072 | 504.8447 | 550.7822 |
| $\frac{15}{16}$ | 342.2500 | 380.2500 | 420.2500 | 462.2500 | 506.2500 | 552.2500 |
| $\frac{1}{2}$ | 343.4072 | 381.4697 | 421.5322 | 463.5947 | 507.6572 | 553.7197 |
| $\frac{5}{8}$ | 344.5664 | 382.6914 | 422.8164 | 464.9414 | 509.0664 | 555.1914 |
| $\frac{3}{4}$ | 345.7275 | 383.9150 | 424.1025 | 466.2900 | 510.4775 | 556.6650 |
| $\frac{7}{8}$ | 346.8906 | 385.1406 | 425.3906 | 467.6406 | 511.8906 | 558.1406 |
| $\frac{15}{16}$ | 348.0557 | 386.3682 | 426.6807 | 468.9932 | 513.3057 | 559.6182 |
| $\frac{1}{2}$ | 349.2227 | 387.5977 | 427.9727 | 470.3477 | 514.7227 | 561.0977 |
| $\frac{5}{8}$ | 350.3916 | 388.8291 | 429.2666 | 471.7041 | 516.1416 | 562.5791 |
| $\frac{3}{4}$ | 351.5625 | 390.0625 | 430.5625 | 473.0625 | 517.5625 | 564.0625 |
| $\frac{7}{8}$ | 352.7354 | 391.2979 | 431.8604 | 474.4229 | 518.9854 | 565.5479 |
| $\frac{15}{16}$ | 353.9102 | 392.5352 | 433.1602 | 475.7852 | 520.4102 | 567.0352 |
| $\frac{1}{2}$ | 355.0869 | 393.7744 | 434.4619 | 477.1494 | 521.8369 | 568.5244 |
| $\frac{5}{8}$ | 356.2656 | 395.0156 | 435.7656 | 478.5156 | 523.2656 | 570.0156 |
| $\frac{3}{4}$ | 357.4463 | 396.2588 | 437.0713 | 479.8838 | 524.6963 | 571.5088 |
| $\frac{7}{8}$ | 358.6289 | 397.5039 | 438.3789 | 481.2539 | 526.1289 | 573.0039 |
| $\frac{15}{16}$ | 359.8135 | 398.7510 | 439.6885 | 482.6260 | 527.5635 | 574.5010 |

SQUARES OF NUMBERS AND FRACTIONAL INTERVALS.

| No. | 0 | $\frac{1}{8}$ | $\frac{1}{4}$ | $\frac{3}{8}$ | $\frac{1}{2}$ | $\frac{5}{8}$ | $\frac{3}{4}$ | $\frac{7}{8}$ |
|-----|------|---------------|---------------|---------------|---------------|---------------|---------------|---------------|
| 24 | 576 | 582.0156 | 588.0625 | 594.1406 | 600.25 | 606.3906 | 612.5625 | 618.7656 |
| 25 | 625 | 631.2656 | 637.5625 | 643.8906 | 650.25 | 656.6406 | 663.0625 | 669.5156 |
| 26 | 676 | 682.5156 | 689.0625 | 695.6406 | 702.25 | 708.8906 | 715.5625 | 722.2656 |
| 27 | 729 | 735.7656 | 742.5625 | 749.3906 | 756.25 | 763.1406 | 770.0625 | 777.0156 |
| 28 | 784 | 791.0156 | 798.0625 | 805.1406 | 812.25 | 819.3906 | 826.5625 | 833.7656 |
| 29 | 841 | 848.2656 | 855.5625 | 862.8906 | 870.25 | 877.6406 | 885.0625 | 892.5156 |
| 30 | 900 | 907.5156 | 915.0625 | 922.6406 | 930.25 | 937.8906 | 945.5625 | 953.2656 |
| 31 | 961 | 968.7656 | 976.5625 | 984.3906 | 992.25 | 1000.1406 | 1008.0625 | 1016.0156 |
| 32 | 1024 | 1032.0156 | 1040.0625 | 1048.1406 | 1056.25 | 1064.3906 | 1072.5625 | 1080.7656 |
| 33 | 1089 | 1097.2656 | 1105.5625 | 1113.8906 | 1122.25 | 1130.6406 | 1139.0625 | 1147.5156 |
| 34 | 1156 | 1164.5156 | 1173.0625 | 1181.6406 | 1190.25 | 1198.8906 | 1207.5625 | 1216.2656 |
| 35 | 1225 | 1233.7656 | 1242.5625 | 1251.3906 | 1260.25 | 1269.1406 | 1278.0625 | 1287.0156 |
| 36 | 1296 | 1305.0156 | 1314.0625 | 1323.1406 | 1332.25 | 1341.3906 | 1350.5625 | 1359.7656 |
| 37 | 1369 | 1378.2656 | 1387.5625 | 1396.8906 | 1406.25 | 1415.6406 | 1425.0625 | 1434.5156 |
| 38 | 1444 | 1453.5156 | 1463.0625 | 1472.6406 | 1482.25 | 1491.8906 | 1501.5625 | 1511.2656 |
| 39 | 1521 | 1530.7656 | 1540.5625 | 1550.3906 | 1560.25 | 1570.1406 | 1580.0625 | 1590.0156 |
| 40 | 1600 | 1610.0156 | 1620.0625 | 1630.1406 | 1640.25 | 1650.3906 | 1660.5625 | 1670.7656 |
| 41 | 1681 | 1691.2656 | 1701.5625 | 1711.8906 | 1722.25 | 1732.6406 | 1743.0625 | 1753.5156 |
| 42 | 1764 | 1774.5156 | 1785.0625 | 1795.6406 | 1806.25 | 1816.8906 | 1827.5625 | 1838.2656 |
| 43 | 1849 | 1859.7656 | 1870.5625 | 1881.3906 | 1892.25 | 1903.1406 | 1914.0625 | 1925.0156 |
| 44 | 1936 | 1947.0156 | 1958.0625 | 1969.1406 | 1980.25 | 1991.3906 | 2002.5625 | 2013.7656 |
| 45 | 2025 | 2036.2656 | 2047.5625 | 2058.8906 | 2070.25 | 2081.6406 | 2093.0625 | 2104.5156 |
| 46 | 2116 | 2127.5156 | 2139.0625 | 2150.6406 | 2162.25 | 2173.8906 | 2185.5625 | 2197.2656 |
| 47 | 2209 | 2220.7656 | 2232.5625 | 2244.3906 | 2256.25 | 2268.1406 | 2280.0625 | 2292.0156 |
| 48 | 2304 | 2316.0156 | 2328.0625 | 2340.1406 | 2352.25 | 2364.3906 | 2376.5625 | 2388.7656 |
| 49 | 2401 | 2413.2656 | 2425.5625 | 2437.8906 | 2450.25 | 2462.6406 | 2475.0625 | 2487.5156 |
| 50 | 2500 | 2512.5156 | 2525.0625 | 2537.6406 | 2550.25 | 2562.8906 | 2575.5625 | 2588.2656 |
| 51 | 2601 | 2613.7656 | 2626.5625 | 2639.3906 | 2652.25 | 2665.1406 | 2678.0625 | 2691.0156 |
| 52 | 2704 | 2717.0156 | 2730.0625 | 2743.1406 | 2756.25 | 2769.3906 | 2782.5625 | 2795.7656 |
| 53 | 2809 | 2822.2656 | 2835.5625 | 2848.8906 | 2862.25 | 2875.6406 | 2889.0625 | 2902.5156 |
| 54 | 2916 | 2929.5156 | 2943.0625 | 2956.6406 | 2970.25 | 2983.8906 | 2997.5625 | 3011.2656 |
| 55 | 3025 | 3038.7656 | 3052.5625 | 3066.3906 | 3080.25 | 3094.1406 | 3108.0625 | 3122.0156 |
| 56 | 3136 | 3150.0156 | 3164.0625 | 3178.1406 | 3192.25 | 3206.3906 | 3220.5625 | 3234.7656 |
| 57 | 3249 | 3263.2656 | 3277.5625 | 3291.8906 | 3306.25 | 3320.6406 | 3335.0625 | 3349.5156 |
| 58 | 3364 | 3378.5156 | 3393.0625 | 3407.6406 | 3422.25 | 3436.8906 | 3451.5625 | 3466.2656 |
| 59 | 3481 | 3495.7656 | 3510.5625 | 3525.3906 | 3540.25 | 3555.1406 | 3570.0625 | 3585.0156 |
| 60 | 3600 | 3615.0156 | 3630.0625 | 3645.1406 | 3660.25 | 3675.3906 | 3690.5625 | 3705.7656 |
| 61 | 3721 | 3736.2656 | 3751.5625 | 3766.8906 | 3782.25 | 3797.6406 | 3813.0625 | 3828.5156 |
| 62 | 3844 | 3859.5156 | 3875.0625 | 3890.6406 | 3906.25 | 3921.8906 | 3937.5625 | 3953.2656 |
| 63 | 3969 | 3984.7656 | 4000.5625 | 4016.3906 | 4032.25 | 4048.1406 | 4064.0625 | 4080.0156 |
| 64 | 4096 | 4112.0156 | 4128.0625 | 4144.1406 | 4160.25 | 4176.3906 | 4192.5625 | 4208.7656 |
| 65 | 4225 | 4241.2656 | 4257.5625 | 4273.8906 | 4290.25 | 4306.6406 | 4323.0625 | 4339.5156 |
| 66 | 4356 | 4372.5156 | 4389.0625 | 4405.6406 | 4422.25 | 4438.8906 | 4455.5625 | 4472.2656 |
| 67 | 4489 | 4505.7656 | 4522.5625 | 4539.3906 | 4556.25 | 4573.1406 | 4590.0625 | 4607.0156 |
| 68 | 4624 | 4641.0156 | 4658.0625 | 4675.1406 | 4692.25 | 4709.3906 | 4726.5625 | 4743.7656 |
| 69 | 4761 | 4778.2656 | 4795.5625 | 4812.8906 | 4830.25 | 4847.6406 | 4865.0625 | 4882.5156 |
| 70 | 4900 | 4917.5156 | 4935.0625 | 4952.6406 | 4970.25 | 4987.8906 | 5005.5625 | 5023.2656 |

CUBES OF NUMBERS AND FRACTIONAL INTERVALS.

| Fraction | 0 | 1 | 2 | 3 | 4 | 5 |
|-----------------|-----------|-----------|-----------|----------|-----------|-----------|
| 0 | 0.000000 | 1.000000 | 8.000000 | 27.00000 | 64.00000 | 125.00000 |
| $\frac{1}{32}$ | .030518 | 1.036710 | 8.380890 | 27.85257 | 65.51175 | 127.35843 |
| $\frac{2}{32}$ | .062444 | 1.199463 | 8.773682 | 28.72290 | 67.04712 | 129.74634 |
| $\frac{3}{32}$ | .095297 | 1.308441 | 9.178558 | 29.61118 | 68.60629 | 132.16391 |
| $\frac{4}{32}$ | .109531 | 1.423828 | 9.595703 | 30.51758 | 70.18945 | 134.61133 |
| $\frac{5}{32}$ | .0038147 | 1.545807 | 10.025299 | 31.44229 | 71.79678 | 137.08878 |
| $\frac{6}{32}$ | .0065918 | 1.674561 | 10.467529 | 32.38550 | 73.42847 | 139.59644 |
| $\frac{7}{32}$ | .0104675 | 1.810272 | 10.922577 | 33.34738 | 75.08469 | 142.13449 |
| $\frac{8}{32}$ | .0156250 | 1.953125 | 11.390625 | 34.32813 | 76.76563 | 144.70313 |
| $\frac{9}{32}$ | .0222473 | 2.103302 | 11.871857 | 35.32791 | 78.47147 | 147.30252 |
| $\frac{10}{32}$ | .0305176 | 2.260986 | 12.366455 | 36.34692 | 80.20239 | 149.93286 |
| $\frac{11}{32}$ | .0406189 | 2.426351 | 12.874603 | 37.38535 | 81.95859 | 152.59433 |
| $\frac{12}{32}$ | .0527344 | 2.599609 | 13.396484 | 38.44336 | 83.74023 | 155.28711 |
| $\frac{13}{32}$ | .0670471 | 2.780914 | 13.932281 | 39.52115 | 85.54752 | 158.01138 |
| $\frac{14}{32}$ | .0837402 | 2.970459 | 14.482178 | 40.61890 | 87.38052 | 160.76733 |
| $\frac{15}{32}$ | .1029968 | 3.168427 | 15.049356 | 41.73679 | 89.23972 | 163.55515 |
| $\frac{16}{32}$ | .1250000 | 3.375000 | 15.625000 | 42.87500 | 91.12500 | 166.37500 |
| $\frac{17}{32}$ | .1499329 | 3.590363 | 16.218292 | 44.03372 | 93.03665 | 169.22708 |
| $\frac{18}{32}$ | .1779785 | 3.814697 | 16.826416 | 45.21313 | 94.97485 | 172.11157 |
| $\frac{19}{32}$ | .2093201 | 4.048187 | 17.449554 | 46.41342 | 96.93979 | 175.02866 |
| $\frac{20}{32}$ | .2441406 | 4.291016 | 18.087891 | 47.63477 | 98.93164 | 177.97852 |
| $\frac{21}{32}$ | .2826233 | 4.543365 | 18.741608 | 48.87735 | 100.95059 | 180.96133 |
| $\frac{22}{32}$ | .3249512 | 4.805420 | 19.410889 | 50.14136 | 102.99683 | 183.97729 |
| $\frac{23}{32}$ | .3713074 | 5.077362 | 20.095917 | 51.42697 | 105.07053 | 187.02658 |
| $\frac{24}{32}$ | .4218750 | 5.359375 | 20.796875 | 52.73438 | 107.17188 | 190.10938 |
| $\frac{25}{32}$ | .4768372 | 5.651642 | 21.513947 | 54.06375 | 109.30106 | 193.22536 |
| $\frac{26}{32}$ | .5363770 | 5.954346 | 22.247314 | 55.41528 | 111.45825 | 196.37622 |
| $\frac{27}{32}$ | .6006775 | 6.267670 | 22.997162 | 56.78915 | 113.64365 | 199.56064 |
| $\frac{28}{32}$ | .6699219 | 6.591797 | 23.763672 | 58.18555 | 115.85742 | 202.77930 |
| $\frac{29}{32}$ | .7442932 | 6.926910 | 24.547028 | 59.60464 | 118.09976 | 206.03238 |
| $\frac{30}{32}$ | .8239746 | 7.273193 | 25.347412 | 61.04663 | 120.37085 | 209.32007 |
| $\frac{31}{32}$ | .9091492 | 7.630829 | 26.165009 | 62.51169 | 122.67087 | 212.64255 |
| Fraction | 6 | 7 | 8 | 9 | 10 | 11 |
| 0 | 216.00000 | 343.00000 | 512.00000 | 729.0000 | 1000.0000 | 1331.0000 |
| $\frac{1}{32}$ | 219.39261 | 347.61429 | 518.02347 | 736.6201 | 1009.4043 | 1342.3760 |
| $\frac{2}{32}$ | 222.82056 | 352.26978 | 524.09399 | 744.2932 | 1018.8674 | 1353.8167 |
| $\frac{3}{32}$ | 226.28403 | 356.96654 | 530.21176 | 752.0194 | 1028.3895 | 1365.3221 |
| $\frac{4}{32}$ | 229.78320 | 361.70508 | 536.37695 | 759.7988 | 1037.9707 | 1376.8926 |
| $\frac{5}{32}$ | 233.31827 | 366.48526 | 542.58975 | 767.6317 | 1047.6112 | 1388.5232 |
| $\frac{6}{32}$ | 236.88940 | 371.30737 | 548.85034 | 775.5183 | 1057.3113 | 1400.2292 |
| $\frac{7}{32}$ | 240.49680 | 376.17160 | 555.15891 | 783.4587 | 1067.0710 | 1411.9958 |
| $\frac{8}{32}$ | 244.14063 | 381.07813 | 561.51563 | 791.4531 | 1076.8906 | 1423.8231 |
| $\frac{9}{32}$ | 247.82108 | 386.02713 | 567.92068 | 799.5017 | 1086.7703 | 1435.7263 |
| $\frac{10}{32}$ | 251.53833 | 391.01830 | 574.37427 | 807.6047 | 1096.7102 | 1447.6907 |
| $\frac{11}{32}$ | 255.29257 | 396.05331 | 580.87656 | 815.7623 | 1106.7105 | 1459.7213 |
| $\frac{12}{32}$ | 259.08398 | 401.13086 | 587.42773 | 823.9746 | 1116.7715 | 1471.8184 |
| $\frac{13}{32}$ | 262.91275 | 406.25162 | 594.02798 | 832.2418 | 1126.8932 | 1483.9821 |
| $\frac{14}{32}$ | 266.77905 | 411.41577 | 600.67749 | 840.5642 | 1137.0759 | 1496.2126 |
| $\frac{15}{32}$ | 270.68307 | 416.62350 | 607.37643 | 848.9419 | 1147.3198 | 1508.5102 |

CUBES OF NUMBERS AND FRACTIONAL INTERVALS.

| Fraction | 6 | 7 | 8 | 9 | 10 | 11 |
|--------------------------------|-----------|-----------|-----------|-----------|-----------|-----------|
| $\frac{1}{32}$ $\frac{1}{2}$ | 274.62500 | 421.87500 | 614.12500 | 857.3750 | 1157.6250 | 1520.8750 |
| $\frac{1}{32}$ $\frac{1}{4}$ | 278.60501 | 427.17044 | 620.92337 | 865.8638 | 1167.9917 | 1533.3072 |
| $\frac{1}{32}$ $\frac{3}{8}$ | 282.62329 | 432.51001 | 627.77173 | 874.4084 | 1178.4202 | 1545.8069 |
| $\frac{1}{32}$ $\frac{1}{2}$ | 286.68002 | 437.89389 | 634.67026 | 883.0091 | 1188.9105 | 1558.3774 |
| $\frac{1}{32}$ $\frac{5}{8}$ | 290.77539 | 443.32227 | 641.61914 | 891.6660 | 1199.4629 | 1571.0098 |
| $\frac{1}{32}$ $\frac{3}{4}$ | 294.90958 | 448.79532 | 648.61856 | 900.3793 | 1210.0775 | 1583.7133 |
| $\frac{1}{32}$ $\frac{1}{2}$ | 299.08276 | 454.31323 | 655.66870 | 909.1491 | 1220.7546 | 1596.4851 |
| $\frac{1}{32}$ $\frac{3}{4}$ | 303.29514 | 459.87619 | 662.76974 | 917.9758 | 1231.4943 | 1609.3254 |
| $\frac{1}{32}$ $\frac{3}{4}$ | 307.54688 | 465.48438 | 669.92188 | 926.8594 | 1242.2969 | 1622.2344 |
| $\frac{1}{32}$ $\frac{13}{16}$ | 311.83817 | 471.13797 | 677.12527 | 935.8001 | 1253.1624 | 1635.2122 |
| $\frac{1}{32}$ $\frac{1}{2}$ | 316.16919 | 476.83716 | 684.38013 | 944.7981 | 1264.0911 | 1648.2590 |
| $\frac{1}{32}$ $\frac{1}{2}$ | 320.54013 | 482.58212 | 691.68661 | 953.8536 | 1275.0831 | 1661.3751 |
| $\frac{1}{32}$ $\frac{7}{8}$ | 324.95117 | 488.37305 | 699.04492 | 962.9668 | 1286.1387 | 1674.5505 |
| $\frac{1}{32}$ $\frac{15}{16}$ | 329.40250 | 494.21011 | 706.45523 | 972.1378 | 1297.2580 | 1687.8156 |
| $\frac{1}{32}$ $\frac{1}{2}$ | 333.89429 | 500.09351 | 713.91772 | 981.3669 | 1308.4412 | 1701.1404 |
| $\frac{1}{32}$ $\frac{1}{2}$ | 338.42673 | 506.02341 | 721.43259 | 990.6543 | 1319.6884 | 1714.5351 |
| Fraction | 12 | 13 | 14 | 15 | 16 | 17 |
| $\frac{1}{16}$ 0 | 1728.0000 | 2197.0000 | 2744.0000 | 3375.0000 | 4096.0000 | 4913.0000 |
| $\frac{1}{16}$ $\frac{1}{8}$ | 1755.1409 | 2228.8401 | 2780.9143 | 3417.3635 | 4144.1877 | 4967.3870 |
| $\frac{1}{16}$ $\frac{1}{4}$ | 1782.5645 | 2260.9863 | 2818.1582 | 3460.0801 | 4192.7520 | 5022.1738 |
| $\frac{1}{16}$ $\frac{1}{2}$ | 1810.2722 | 2293.4402 | 2855.7332 | 3503.1511 | 4241.6941 | 5077.3621 |
| $\frac{1}{16}$ $\frac{1}{4}$ | 1838.2656 | 2326.2031 | 2893.6406 | 3546.5781 | 4291.0156 | 5132.9531 |
| $\frac{1}{16}$ $\frac{3}{8}$ | 1866.5461 | 2359.2766 | 2931.8821 | 3590.3625 | 4340.7180 | 5188.9485 |
| $\frac{1}{16}$ $\frac{1}{2}$ | 1895.1152 | 2392.6621 | 2970.4590 | 3634.5059 | 4390.8027 | 5245.3496 |
| $\frac{1}{16}$ $\frac{1}{2}$ | 1923.9744 | 2426.3611 | 3009.3728 | 3679.0095 | 4441.2712 | 5302.1580 |
| $\frac{1}{16}$ $\frac{1}{2}$ | 1953.1250 | 2460.3750 | 3048.6250 | 3723.8750 | 4492.1250 | 5359.3750 |
| $\frac{1}{16}$ $\frac{5}{8}$ | 1982.5686 | 2494.7053 | 3088.2170 | 3769.1038 | 4543.3555 | 5417.0022 |
| $\frac{1}{16}$ $\frac{3}{4}$ | 2012.3066 | 2529.3535 | 3128.1504 | 3814.6973 | 4594.9941 | 5475.0410 |
| $\frac{1}{16}$ $\frac{1}{2}$ | 2042.3406 | 2564.3210 | 3168.4265 | 3860.6570 | 4647.0125 | 5533.4929 |
| $\frac{1}{16}$ $\frac{3}{4}$ | 2072.6719 | 2599.6094 | 3209.0469 | 3906.9844 | 4699.4219 | 5592.3594 |
| $\frac{1}{16}$ $\frac{1}{2}$ | 2103.3020 | 2635.2200 | 3250.0129 | 3953.6809 | 4752.2239 | 5651.6418 |
| $\frac{1}{16}$ $\frac{7}{8}$ | 2134.2324 | 2671.1543 | 3291.3262 | 4000.7480 | 4805.4199 | 5711.3418 |
| $\frac{1}{16}$ $\frac{1}{2}$ | 2165.4646 | 2707.4138 | 3332.9880 | 4048.1873 | 4859.0115 | 5771.4607 |
| Fraction | 18 | 19 | 20 | 21 | 22 | 23 |
| $\frac{1}{16}$ 0 | 5832.0000 | 6859.0000 | 8000.0000 | 9261.000 | 10648.000 | 12167.000 |
| $\frac{1}{16}$ $\frac{1}{8}$ | 5892.9612 | 6926.9104 | 8075.2346 | 9343.934 | 10739.008 | 12266.457 |
| $\frac{1}{16}$ $\frac{1}{4}$ | 5954.3457 | 6995.2676 | 8150.9395 | 9427.361 | 10830.533 | 12366.455 |
| $\frac{1}{16}$ $\frac{1}{2}$ | 6016.1550 | 7064.0730 | 8227.1160 | 9511.284 | 10922.577 | 12466.995 |
| $\frac{1}{16}$ $\frac{1}{4}$ | 6078.3906 | 7133.3281 | 8303.7656 | 9595.703 | 11015.141 | 12568.078 |
| $\frac{1}{16}$ $\frac{3}{8}$ | 6141.0540 | 7203.0344 | 8380.8899 | 9680.620 | 11108.226 | 12669.706 |
| $\frac{1}{16}$ $\frac{1}{2}$ | 6204.1465 | 7273.1934 | 8458.4902 | 9766.037 | 11201.834 | 12771.881 |
| $\frac{1}{16}$ $\frac{1}{2}$ | 6267.6697 | 7343.8064 | 8536.5681 | 9851.955 | 11295.957 | 12874.603 |
| $\frac{1}{16}$ $\frac{1}{2}$ | 6331.6250 | 7414.8750 | 8615.1250 | 9938.375 | 11390.625 | 12977.875 |
| $\frac{1}{16}$ $\frac{5}{8}$ | 6396.0139 | 7486.4006 | 8694.1624 | 10025.299 | 11485.311 | 13081.698 |
| $\frac{1}{16}$ $\frac{3}{4}$ | 6460.8379 | 7558.3848 | 8773.6816 | 10112.729 | 11581.525 | 13186.072 |
| $\frac{1}{16}$ $\frac{1}{2}$ | 6526.0984 | 7630.8289 | 8853.6843 | 10200.655 | 11677.770 | 13291.001 |
| $\frac{1}{16}$ $\frac{3}{4}$ | 6591.7969 | 7703.7344 | 8934.1719 | 10289.109 | 11774.547 | 13396.484 |
| $\frac{1}{16}$ $\frac{1}{2}$ | 6657.9348 | 7777.1028 | 9015.1458 | 10378.054 | 11871.857 | 13502.625 |
| $\frac{1}{16}$ $\frac{7}{8}$ | 6724.5137 | 7850.9355 | 9096.6074 | 10467.529 | 11969.701 | 13609.123 |
| $\frac{1}{16}$ $\frac{1}{2}$ | 6791.5349 | 7925.2341 | 9178.5583 | 10557.508 | 12068.082 | 13716.281 |

CUBES OF NUMBERS AND FRACTIONAL INTERVALS.

| No | 0 | $\frac{1}{8}$ | $\frac{1}{4}$ | $\frac{3}{8}$ | $\frac{1}{2}$ | $\frac{5}{8}$ | $\frac{3}{4}$ | $\frac{7}{8}$ |
|----|--------|---------------|---------------|---------------|---------------|---------------|---------------|---------------|
| 24 | 13824 | 14041.127 | 14260.516 | 14482.178 | 14706.125 | 14932.369 | 15160.922 | 15391.796 |
| 25 | 15625 | 15860.549 | 16098.453 | 16338.725 | 16581.375 | 16826.416 | 17073.859 | 17323.717 |
| 26 | 17576 | 17830.721 | 18087.891 | 18347.521 | 18609.625 | 18874.213 | 19141.297 | 19410.889 |
| 27 | 19683 | 19957.643 | 20234.828 | 20514.568 | 20796.875 | 21081.760 | 21369.234 | 21659.311 |
| 28 | 21952 | 22247.315 | 22545.266 | 22845.865 | 23149.125 | 23455.057 | 23763.672 | 24074.982 |
| 29 | 24389 | 24705.736 | 25025.203 | 25347.412 | 25672.375 | 26000.104 | 26330.609 | 26663.904 |
| 30 | 27000 | 27338.908 | 27680.641 | 28025.209 | 28372.625 | 28722.900 | 29076.047 | 29432.076 |
| 31 | 29791 | 30152.830 | 30517.578 | 30885.256 | 31255.875 | 31629.447 | 32005.984 | 32385.498 |
| 32 | 32768 | 33153.502 | 33542.016 | 33933.553 | 34328.125 | 34725.744 | 35126.422 | 35530.170 |
| 33 | 35937 | 36346.924 | 36759.953 | 37176.100 | 37595.375 | 38017.791 | 38443.359 | 38872.092 |
| 34 | 39304 | 39739.096 | 40177.391 | 40618.896 | 41063.625 | 41511.588 | 41962.797 | 42417.264 |
| 35 | 42875 | 43336.018 | 43800.328 | 44267.943 | 44738.875 | 45213.135 | 45690.734 | 46171.686 |
| 36 | 46656 | 47143.689 | 47634.766 | 48129.240 | 48627.125 | 49128.432 | 49633.172 | 50141.357 |
| 37 | 50653 | 51168.111 | 51686.703 | 52208.787 | 52734.375 | 53263.479 | 53796.109 | 54332.279 |
| 38 | 54872 | 55415.283 | 55962.141 | 56512.584 | 57066.625 | 57624.275 | 58185.547 | 58750.451 |
| 39 | 59319 | 59891.205 | 60467.078 | 61046.631 | 61629.875 | 62216.822 | 62807.484 | 63401.873 |
| 40 | 64000 | 64601.877 | 65207.516 | 65816.928 | 66430.125 | 67047.119 | 67667.922 | 68292.545 |
| 41 | 68921 | 69553.299 | 70189.453 | 70829.475 | 71473.375 | 72121.166 | 72772.859 | 73428.467 |
| 42 | 74088 | 74751.471 | 75418.891 | 76090.272 | 76765.625 | 77444.963 | 78128.297 | 78815.639 |
| 43 | 79507 | 80202.393 | 80901.828 | 81605.318 | 82312.875 | 83024.510 | 83740.234 | 84460.061 |
| 44 | 85184 | 85912.065 | 86644.266 | 87380.615 | 88121.125 | 88865.807 | 89614.672 | 90367.732 |
| 45 | 91125 | 91886.486 | 92652.203 | 93422.162 | 94196.375 | 94974.854 | 95757.609 | 96544.654 |
| 46 | 97336 | 98131.658 | 98931.641 | 99735.959 | 100544.63 | 101357.65 | 102175.05 | 102996.83 |
| 47 | 103823 | 104653.58 | 105488.58 | 106328.01 | 107171.87 | 108020.20 | 108872.98 | 109730.25 |
| 48 | 110592 | 111458.25 | 112329.02 | 113204.30 | 114084.12 | 114968.49 | 115857.42 | 116750.92 |
| 49 | 117649 | 118551.67 | 119458.95 | 120370.85 | 121287.37 | 122208.54 | 123134.36 | 124064.84 |
| 50 | 125000 | 125939.85 | 126884.39 | 127833.65 | 128787.62 | 129746.34 | 130709.80 | 131678.01 |
| 51 | 132651 | 133628.77 | 134611.33 | 135598.69 | 136590.87 | 137587.88 | 138589.73 | 139596.44 |
| 52 | 140608 | 141624.44 | 142645.77 | 143671.99 | 144703.12 | 145739.18 | 146780.17 | 147826.11 |
| 53 | 148877 | 149932.86 | 150993.70 | 152059.54 | 153130.37 | 154206.23 | 155287.11 | 156373.03 |
| 54 | 157464 | 158560.03 | 159661.14 | 160767.33 | 161878.62 | 162995.03 | 164116.55 | 165243.20 |
| 55 | 166375 | 167511.96 | 168654.08 | 169801.38 | 170953.87 | 172111.57 | 173274.48 | 174442.62 |
| 56 | 175616 | 176794.63 | 177978.52 | 179167.68 | 180362.12 | 181561.87 | 182766.92 | 183977.29 |
| 57 | 185193 | 186414.05 | 187640.45 | 188872.22 | 190109.37 | 191351.92 | 192599.86 | 193853.22 |
| 58 | 196112 | 196376.22 | 197645.89 | 198921.02 | 200201.62 | 201487.71 | 202779.30 | 204076.39 |
| 59 | 205379 | 206687.14 | 208000.83 | 209320.07 | 210644.87 | 211975.26 | 213311.23 | 214652.81 |
| 60 | 216000 | 217352.81 | 218711.27 | 220075.37 | 221445.12 | 222820.56 | 224201.67 | 225588.48 |
| 61 | 226981 | 228379.24 | 229783.20 | 231192.91 | 232608.38 | 234029.60 | 235456.61 | 236889.40 |
| 62 | 238328 | 239772.41 | 241222.64 | 242678.71 | 244140.63 | 245608.40 | 247082.05 | 248561.58 |
| 63 | 250047 | 251538.33 | 253035.58 | 254538.76 | 256047.88 | 257562.95 | 259083.98 | 260611.00 |
| 64 | 262144 | 263683.00 | 265228.02 | 266779.05 | 268336.13 | 269899.24 | 271468.42 | 273043.67 |
| 65 | 274625 | 276212.42 | 277805.95 | 279405.60 | 281011.38 | 282623.29 | 284241.36 | 285865.59 |
| 66 | 287496 | 289132.60 | 290775.39 | 292424.40 | 294079.63 | 295741.09 | 297408.80 | 299082.76 |
| 67 | 300763 | 302449.52 | 304142.33 | 305841.44 | 307546.88 | 309258.63 | 310976.73 | 312701.19 |
| 68 | 314432 | 316169.19 | 317912.77 | 319662.74 | 321419.13 | 323181.93 | 324951.17 | 326726.86 |
| 69 | 328509 | 330297.61 | 332092.70 | 333894.29 | 335702.37 | 337516.98 | 339338.11 | 341165.78 |
| 70 | 343000 | 344840.78 | 346688.14 | 348542.08 | 350402.61 | 352269.77 | 354143.55 | 356023.95 |

VALUES FOR COMBINATIONS OF π ($\pi = 3.14159265359$).

| Combination. | Values for n . | | | | |
|---------------------------------|------------------|-----------|-----------|-----------|------------|
| | 1 | 2 | 3 | 4 | 5 |
| $n\pi$ | 3.141593 | 6.283185 | 9.424778 | 12.566371 | 15.707963 |
| $\frac{n\pi}{4}$ | .785398 | 1.570796 | 2.356194 | 3.141593 | 3.926991 |
| $\frac{n\pi}{6}$ | .523599 | 1.047196 | 1.570796 | 2.094395 | 2.617994 |
| $\frac{n\pi}{8}$ | .392699 | .785398 | 1.178097 | 1.570796 | 1.963495 |
| $\frac{n\pi}{16}$ | .196350 | .392699 | .589049 | .785398 | .981748 |
| $\frac{n\pi}{32}$ | .098175 | .196350 | .294524 | .392699 | .490874 |
| $\frac{n\pi}{64}$ | .049087 | .098175 | .147262 | .196350 | .245437 |
| $\frac{\pi}{n}$ | 3.141593 | 1.570796 | 1.047198 | .785398 | .628319 |
| $\frac{n}{\pi}$ | .318310 | .636620 | .954930 | 1.273240 | 1.591549 |
| $\frac{n}{\pi} 90^\circ$ | .034907 | .017453 | .011636 | .008727 | .006981 |
| $\frac{n}{\pi} 90^\circ$ | 28.647890 | 57.295780 | 85.943670 | 114.59156 | 143.239450 |
| π^n | 3.141593 | 9.869604 | 31.006277 | 97.409091 | 306.01979 |
| $\frac{1}{\pi^n}$ | .318310 | .101321 | .032252 | .010266 | .003268 |
| $\frac{1}{\sqrt[n]{\pi}}$ | 3.141593 | 1.772454 | 1.464592 | 1.331335 | 1.257274 |
| $\frac{1}{\sqrt[n]{\pi}}$ | .318310 | .564190 | .682784 | .751126 | .795371 |
| $n\pi^2$ | 9.869604 | 19.739209 | 29.608813 | 39.478418 | 49.348022 |
| $\frac{n}{\pi^2}$ | .101321 | .202642 | .303963 | .405284 | .506605 |
| $\sqrt{n\pi}$ | 1.772454 | 2.506628 | 3.069980 | 3.544908 | 3.963328 |
| $\sqrt{\frac{n}{\pi}}$ | .564190 | .797885 | .977205 | 1.128379 | 1.261566 |
| $n\sqrt{\pi}$ | 1.772454 | 3.544908 | 5.317362 | 7.089815 | 8.862269 |
| $\frac{n}{\sqrt{\pi}}$ | .564190 | 1.128379 | 1.692569 | 2.256785 | 2.820948 |
| $n\pi^3$ | 31.006277 | 62.012553 | 93.018830 | 124.02511 | 155.03138 |
| $\frac{n}{\pi^3}$ | .032252 | .064503 | .096755 | .129006 | .161258 |
| $\sqrt[3]{n\pi}$ | 1.464592 | 1.845270 | 2.112469 | 2.324895 | 2.504417 |
| $\sqrt[3]{\frac{n}{\pi}}$ | .682784 | .860254 | .984745 | 1.086351 | 1.167544 |
| $n\sqrt[3]{\pi}$ | 1.464592 | 2.929184 | 4.393776 | 5.858368 | 7.322959 |
| $\frac{n}{\sqrt[3]{\pi}}$ | .682784 | 1.365568 | 2.048352 | 2.731136 | 3.413920 |
| $n\pi^4$ | 97.409091 | 194.81818 | 292.22727 | 389.63636 | 487.04545 |
| $\frac{n}{\pi^4}$ | .010266 | .020532 | .030797 | .041063 | .051329 |
| $\sqrt[4]{n\pi}$ | 1.331335 | 1.563233 | 1.752136 | 1.882793 | 1.990811 |
| $\sqrt[4]{\frac{n}{\pi}}$ | .751126 | .893244 | .988537 | 1.062252 | 1.123195 |

VALUES FOR COMBINATIONS OF π ($\pi = 3.14159265359$).

| Values for n. | | | | Combination. |
|---------------|-----------|-----------|-----------|---------------------------------|
| 6 | 7 | 8 | 9 | |
| 18.849556 | 21.991149 | 25.132741 | 28.274334 | $n\pi$ |
| 4.712389 | 5.497737 | 6.283185 | 7.068593 | $\frac{n\pi}{4}$ |
| 3.141593 | 3.665191 | 4.188790 | 4.712330 | $\frac{n\pi}{6}$ |
| 2.356194 | 2.748894 | 3.141593 | 3.534292 | $\frac{n\pi}{8}$ |
| 1.178097 | 1.374447 | 1.570796 | 1.767146 | $\frac{n\pi}{16}$ |
| .589049 | .687223 | .785398 | .883573 | $\frac{n\pi}{32}$ |
| .294524 | .343612 | .392699 | .441786 | $\frac{n\pi}{64}$ |
| .523599 | .448790 | .392699 | .349066 | $\frac{\pi}{n}$ |
| 1.909359 | 2.228169 | 2.546479 | 2.864789 | $\frac{n}{\pi}$ |
| .005818 | .004987 | .004363 | .003879 | $\frac{\pi}{n 90^\circ}$ |
| 171.88738 | 200.53523 | 229.18312 | 257.84101 | $\frac{n 90^\circ}{\pi}$ |
| 961.38937 | 3020.1938 | 9488.5331 | 29809.108 | π^n |
| .001040 | .000331 | .000103 | .000034 | $\frac{1}{\pi^n}$ |
| 1.210203 | 1.177664 | 1.153835 | 1.136635 | $\sqrt[n]{\pi}$ |
| .826307 | .849139 | .866675 | .880564 | $\frac{1}{\sqrt[n]{\pi}}$ |
| 59.217626 | 69.087231 | 79.956835 | 89.826440 | $n\pi^2$ |
| .607926 | .709247 | .810563 | .911880 | $\frac{n}{\pi^2}$ |
| 4.341608 | 4.689471 | 5.013257 | 5.317362 | $\sqrt{n\pi}$ |
| 1.381977 | 1.492705 | 1.595769 | 1.692569 | $\sqrt{\frac{n}{\pi}}$ |
| 10.634723 | 12.407177 | 14.179631 | 15.952085 | $n\sqrt{\pi}$ |
| 3.385138 | 3.949327 | 4.513517 | 5.077705 | $\frac{n}{\sqrt{\pi}}$ |
| 186.03766 | 217.04394 | 248.05021 | 279.05649 | $n\pi^3$ |
| .193509 | .225761 | .258013 | .290264 | $\frac{n}{\pi^3}$ |
| 2.661340 | 2.801663 | 2.929184 | 3.046474 | $\sqrt[3]{n\pi}$ |
| 1.240701 | 1.306189 | 1.365563 | 1.420248 | $\sqrt[3]{\frac{n}{\pi}}$ |
| 8.787551 | 10.252143 | 11.716735 | 13.181327 | $n\sqrt[3]{\pi}$ |
| 4.096704 | 4.779489 | 5.462273 | 6.145057 | $\frac{n}{\sqrt[3]{\pi}}$ |
| 584.45455 | 681.86364 | 779.27273 | 876.68182 | $n\pi^4$ |
| .061596 | .071862 | .082128 | .092394 | $\frac{n}{\pi^4}$ |
| 2.083553 | 2.165519 | 2.239030 | 2.305940 | $\sqrt[4]{n\pi}$ |
| 1.175575 | 1.221763 | 1.263237 | 1.300988 | $\sqrt[4]{\frac{n}{\pi}}$ |

MENSURATION.**LENGTH.**

Circumference of circle = diameter $\times 3.1416$.

Diameter of circle = circumference $\times 0.3183$.

Side of square of equal periphery as circle = diameter $\times 0.7854$.

Diameter of circle of equal periphery as square = side $\times 1.2732$.

Side of an inscribed square = diameter of circle $\times 0.7071$.

Diameter of circle circumscribed about square = side $\times 1.4142$.

Circumference of circle whose diameter is 1 =

$$\pi = 3.14159265$$

$$\log. \pi = 0.4971499$$

$$\sqrt{\pi} = 1.772454$$

$$\pi^2 = 9.869604$$

$$r = \frac{c^2}{8v} + \frac{v}{2}$$

$$x = \sqrt{r^2 - (r + o - v)^2}$$

$$v = r - \sqrt{r^2 - \frac{c^2}{4}} = \frac{c}{2} \tan \frac{A}{4} = 2r \sin^2 \frac{A}{4} = r + o - \sqrt{r^2 - x^2}$$

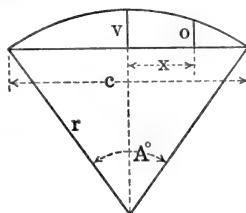
$$c = 2\sqrt{2vr - v^2} = 2r \sin \frac{A}{2}$$

$$\text{Length of arc} = \frac{\pi r A^\circ}{180} = .0174533 r A^\circ$$

$$\text{Angle } A^\circ = \frac{180 \times \text{arc}}{\pi r} = \frac{57.29578 \times \text{arc}}{r}$$

$$\cos \frac{A}{2} = \frac{c^2 - 4v^2}{c^2 + 4v^2}$$

$$\text{For division of circle into } n \text{ parts, } c = 2r \sin \frac{180^\circ}{n}$$



$$\frac{1}{\pi} = 0.318310$$

$$\frac{1}{\pi^2} = 0.101321$$

$$\sqrt{\frac{1}{\pi}} = 0.564190$$

$$o = \sqrt{r^2 - x^2} - (r - v)$$

MENSURATION—(Continued).**AREA.**

Triangle = base \times half perpendicular height.

Parallelogram = base \times perpendicular height.

Trapezoid = half the sum of the parallel sides \times perpendicular height.

Trapezium, found by dividing into two triangles.

Circle = diameter squared $\times 0.7854$; or, = circumference squared $\times 0.07958$.

Sector of circle = length of arc \times half radius.

Segment of circle = area of sector of equal radius — triangle when segment is less, and + triangle when segment is greater than the semicircle; also for flat segments very nearly =

$$\frac{4v}{3} \sqrt{0.388 v^2 + \frac{c^2}{4}}$$

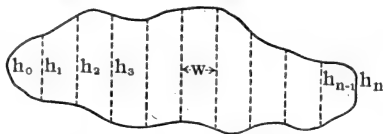
Side of square of equal area as circle = diameter $\times 0.8862$; also, = circumference $\times 0.2821$.

Diameter of circle of equal area as square = side $\times 1.1284$.

Parabola = base $\times \frac{2}{3}$ height.

Ellipse = long diameter \times short diameter $\times 0.7854$.

Regular polygon = sum of sides \times half perpendicular distance from center to sides.

APPROXIMATE AREA OF IRREGULAR FIGURE.

Divide figure into n strips by equidistant parallel ordinates, h_0, h_1, h_2 , etc.

Then by

Simpson's Rule, (n must be even)

$$\text{Area} = \frac{w}{3} [(h_0 + h_n) + 4(h_1 + h_3 + \dots h_{n-1}) + 2(h_2 + h_4 + \dots h_{n-2})]$$

Durand's Rule

$$\text{Area} = w[0.4(h_0 + h_n) + 1.1(h_1 + h_{n-1}) + (h_2 + h_3 + \dots h_{n-2})]$$

Trapezoidal Rule

$$\text{Area} = w [\frac{1}{2}(h_0 + h_n) + (h_1 + h_2 + h_3 + \dots h_{n-1})]$$

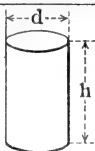
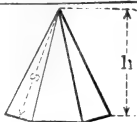
RELATIONS IN CIRCULAR SEGMENTS

| Central Angle Degrees | Area Radius ² | Chord Radius | Height Radius | Arc Radius | Central Angle Degrees | Area Radius ² | Chord Radius | Height Radius | Arc Radius |
|-----------------------------|-----------------------------|-----------------|------------------|---------------|-----------------------------|-----------------------------|-----------------|------------------|---------------|
| 1 | .0440 | .017 | .040 | .017 | 46 | .04176 | .781 | .0795 | .803 |
| 2 | .0335 | .035 | .015 | .035 | 47 | .04448 | .797 | .0829 | .820 |
| 3 | .0412 | .052 | .034 | .052 | 48 | .04731 | .813 | .0865 | .838 |
| 4 | .0428 | .070 | .061 | .070 | 49 | .05025 | .829 | .0900 | .855 |
| 5 | .0455 | .087 | .095 | .087 | 50 | .05331 | .845 | .0937 | .873 |
| 6 | .0496 | .105 | .0014 | .105 | 51 | .05649 | .861 | .0974 | .890 |
| 7 | .00015 | .122 | .0019 | .122 | 52 | .05978 | .877 | .1012 | .908 |
| 8 | .00023 | .140 | .0024 | .140 | 53 | .06319 | .892 | .1051 | .925 |
| 9 | .00032 | .157 | .0031 | .157 | 54 | .06673 | .908 | .1090 | .942 |
| 10 | .00044 | .174 | .0038 | .175 | 55 | .07039 | .923 | .1130 | .960 |
| 11 | .00059 | .192 | .0046 | .192 | 56 | .07417 | .939 | .1171 | .977 |
| 12 | .00076 | .209 | .0055 | .209 | 57 | .07808 | .954 | .1212 | .995 |
| 13 | .00097 | .226 | .0064 | .227 | 58 | .08212 | .970 | .1254 | 1.012 |
| 14 | .00121 | .244 | .0075 | .244 | 59 | .08629 | .985 | .1296 | 1.030 |
| 15 | .00149 | .261 | .0086 | .262 | 60 | .09059 | 1.000 | .1340 | 1.047 |
| 16 | .00181 | .278 | .0097 | .279 | 61 | .09502 | 1.015 | .1384 | 1.065 |
| 17 | .00217 | .296 | .0110 | .297 | 62 | .09958 | 1.030 | .1428 | 1.082 |
| 18 | .00257 | .313 | .0123 | .314 | 63 | .10428 | 1.045 | .1474 | 1.100 |
| 19 | .00302 | .330 | .0137 | .332 | 64 | .10911 | 1.060 | .1520 | 1.117 |
| 20 | .00352 | .347 | .0152 | .349 | 65 | .11408 | 1.075 | .1566 | 1.134 |
| 21 | .00408 | .364 | .0167 | .367 | 66 | .11919 | 1.089 | .1613 | 1.152 |
| 22 | .00468 | .382 | .0184 | .384 | 67 | .12443 | 1.104 | .1661 | 1.169 |
| 23 | .00535 | .399 | .0201 | .401 | 68 | .12982 | 1.118 | .1710 | 1.187 |
| 24 | .00607 | .416 | .0219 | .419 | 69 | .13535 | 1.133 | .1759 | 1.204 |
| 25 | .00686 | .433 | .0237 | .436 | 70 | .14102 | 1.147 | .1808 | 1.222 |
| 26 | .00771 | .450 | .0256 | .454 | 71 | .14683 | 1.161 | .1859 | 1.239 |
| 27 | .00862 | .467 | .0276 | .471 | 72 | .15279 | 1.176 | .1910 | 1.257 |
| 28 | .00961 | .484 | .0297 | .489 | 73 | .15889 | 1.190 | .1961 | 1.274 |
| 29 | .01067 | .501 | .0319 | .506 | 74 | .16514 | 1.204 | .2014 | 1.292 |
| 30 | .01180 | .518 | .0341 | .524 | 75 | .17154 | 1.218 | .2066 | 1.309 |
| 31 | .01301 | .534 | .0364 | .541 | 76 | .17808 | 1.231 | .2120 | 1.326 |
| 32 | .01429 | .551 | .0387 | .559 | 77 | .18477 | 1.245 | .2174 | 1.344 |
| 33 | .01566 | .568 | .0412 | .576 | 78 | .19160 | 1.259 | .2229 | 1.361 |
| 34 | .01711 | .585 | .0437 | .593 | 79 | .19859 | 1.272 | .2284 | 1.379 |
| 35 | .01864 | .601 | .0463 | .611 | 80 | .20573 | 1.286 | .2340 | 1.396 |
| 36 | .02027 | .618 | .0489 | .628 | 81 | .21301 | 1.299 | .2396 | 1.414 |
| 37 | .02198 | .635 | .0517 | .646 | 82 | .22045 | 1.312 | .2453 | 1.431 |
| 38 | .02378 | .651 | .0545 | .663 | 83 | .22804 | 1.325 | .2510 | 1.449 |
| 39 | .02568 | .668 | .0574 | .681 | 84 | .23578 | 1.338 | .2569 | 1.466 |
| 40 | .02767 | .684 | .0603 | .698 | 85 | .24367 | 1.351 | .2627 | 1.484 |
| 41 | .02976 | .700 | .0633 | .716 | 86 | .25171 | 1.364 | .2686 | 1.501 |
| 42 | .03195 | .717 | .0664 | .733 | 87 | .25990 | 1.377 | .2746 | 1.518 |
| 43 | .03425 | .733 | .0696 | .750 | 88 | .26825 | 1.389 | .2807 | 1.536 |
| 44 | .03664 | .749 | .0728 | .768 | 89 | .27677 | 1.402 | .2867 | 1.553 |
| 45 | .03915 | .765 | .0761 | .785 | 90 | .28540 | 1.414 | .2929 | 1.571 |

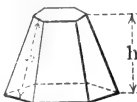
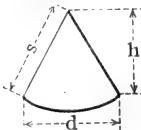
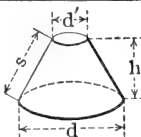
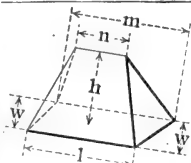
RELATIONS IN CIRCULAR SEGMENTS

| Central Angle Degrees | Area Radius ² | Chord Radius | Height Radius | Arc Radius | Central Angle Degrees | Area Radius ² | Chord Radius | Height Radius | Arc Radius |
|-----------------------------|-----------------------------|-----------------|------------------|---------------|-----------------------------|-----------------------------|-----------------|------------------|---------------|
| 91 | .2942 | 1.427 | .2991 | 1.588 | 136 | .8395 | 1.854 | .6254 | 2.374 |
| 92 | .3032 | 1.439 | .3053 | 1.606 | 137 | .8545 | 1.861 | .6335 | 2.391 |
| 93 | .3123 | 1.451 | .3116 | 1.623 | 138 | .8697 | 1.867 | .6416 | 2.409 |
| 94 | .3215 | 1.463 | .3180 | 1.641 | 139 | .8850 | 1.873 | .6498 | 2.426 |
| 95 | .3309 | 1.475 | .3244 | 1.658 | 140 | .9003 | 1.879 | .6580 | 2.443 |
| 96 | .3405 | 1.486 | .3309 | 1.676 | 141 | .9158 | 1.885 | .6662 | 2.461 |
| 97 | .3502 | 1.498 | .3374 | 1.693 | 142 | .9313 | 1.891 | .6744 | 2.478 |
| 98 | .3601 | 1.509 | .3439 | 1.710 | 143 | .9470 | 1.897 | .6827 | 2.496 |
| 99 | .3701 | 1.521 | .3506 | 1.728 | 144 | .9627 | 1.902 | .6910 | 2.513 |
| 100 | .3803 | 1.532 | .3572 | 1.745 | 145 | .9786 | 1.907 | .6993 | 2.531 |
| 101 | .3906 | 1.543 | .3639 | 1.763 | 146 | .9945 | 1.913 | .7076 | 2.548 |
| 102 | .4010 | 1.554 | .3707 | 1.780 | 147 | 1.0105 | 1.918 | .7160 | 2.566 |
| 103 | .4117 | 1.565 | .3775 | 1.798 | 148 | 1.0265 | 1.923 | .7244 | 2.583 |
| 104 | .4224 | 1.576 | .3843 | 1.815 | 149 | 1.0427 | 1.927 | .7328 | 2.601 |
| 105 | .4333 | 1.587 | .3912 | 1.833 | 150 | 1.0590 | 1.932 | .7412 | 2.618 |
| 106 | .4444 | 1.597 | .3982 | 1.850 | 151 | 1.0753 | 1.936 | .7496 | 2.635 |
| 107 | .4556 | 1.608 | .4052 | 1.868 | 152 | 1.0917 | 1.941 | .7581 | 2.653 |
| 108 | .4669 | 1.618 | .4122 | 1.885 | 153 | 1.1082 | 1.945 | .7666 | 2.670 |
| 109 | .4784 | 1.628 | .4193 | 1.902 | 154 | 1.1247 | 1.949 | .7750 | 2.688 |
| 110 | .4901 | 1.638 | .4264 | 1.920 | 155 | 1.1413 | 1.953 | .7836 | 2.705 |
| 111 | .5019 | 1.648 | .4336 | 1.937 | 156 | 1.1580 | 1.956 | .7921 | 2.723 |
| 112 | .5138 | 1.658 | .4408 | 1.955 | 157 | 1.1747 | 1.960 | .8006 | 2.740 |
| 113 | .5259 | 1.668 | .4481 | 1.972 | 158 | 1.1915 | 1.963 | .8092 | 2.758 |
| 114 | .5381 | 1.677 | .4554 | 1.990 | 159 | 1.2083 | 1.967 | .8178 | 2.775 |
| 115 | .5504 | 1.687 | .4627 | 2.007 | 160 | 1.2252 | 1.970 | .8264 | 2.793 |
| 116 | .5629 | 1.696 | .4701 | 2.025 | 161 | 1.2422 | 1.973 | .8350 | 2.810 |
| 117 | .5755 | 1.705 | .4775 | 2.042 | 162 | 1.2592 | 1.975 | .8436 | 2.827 |
| 118 | .5883 | 1.714 | .4850 | 2.059 | 163 | 1.2763 | 1.978 | .8522 | 2.845 |
| 119 | .6012 | 1.723 | .4925 | 2.077 | 164 | 1.2933 | 1.981 | .8608 | 2.862 |
| 120 | .6142 | 1.732 | .5000 | 2.094 | 165 | 1.3105 | 1.983 | .8695 | 2.880 |
| 121 | .6273 | 1.741 | .5076 | 2.112 | 166 | 1.3277 | 1.985 | .8781 | 2.897 |
| 122 | .6406 | 1.749 | .5152 | 2.129 | 167 | 1.3449 | 1.987 | .8868 | 2.915 |
| 123 | .6540 | 1.758 | .5228 | 2.147 | 168 | 1.3621 | 1.989 | .8955 | 2.932 |
| 124 | .6676 | 1.766 | .5305 | 2.164 | 169 | 1.3794 | 1.991 | .9042 | 2.950 |
| 125 | .6812 | 1.774 | .5383 | 2.182 | 170 | 1.3967 | 1.992 | .9128 | 2.967 |
| 126 | .6950 | 1.782 | .5460 | 2.199 | 171 | 1.4140 | 1.994 | .9215 | 2.985 |
| 127 | .7090 | 1.790 | .5538 | 2.217 | 172 | 1.4314 | 1.995 | .9302 | 3.002 |
| 128 | .7230 | 1.798 | .5616 | 2.234 | 173 | 1.4488 | 1.996 | .9390 | 3.019 |
| 129 | .7372 | 1.805 | .5695 | 2.251 | 174 | 1.4662 | 1.997 | .9477 | 3.037 |
| 130 | .7514 | 1.813 | .5774 | 2.269 | 175 | 1.4836 | 1.998 | .9564 | 3.054 |
| 131 | .7658 | 1.820 | .5853 | 2.286 | 176 | 1.5010 | 1.999 | .9651 | 3.072 |
| 132 | .7803 | 1.827 | .5933 | 2.304 | 177 | 1.5185 | 1.999 | .9738 | 3.089 |
| 133 | .7950 | 1.834 | .6013 | 2.321 | 178 | 1.5359 | 2.000 | .9825 | 3.107 |
| 134 | .8097 | 1.841 | .6093 | 2.339 | 179 | 1.5533 | 2.000 | .9913 | 3.124 |
| 135 | .8245 | 1.848 | .6173 | 2.356 | 180 | 1.5708 | 2.000 | 1.0000 | 3.142 |

SURFACES AND VOLUMES OF SOLIDS.

**CYLINDER**Convex Surface = πdh Total Surface = $\pi dh + \frac{\pi d^2}{2}$ Volume = $\frac{\pi d^2 h}{4}$ Volume Cylinder, right or oblique, = area of section at right angles to sides \times length of side.**PRISM**Lateral Surface = $h \times$ Base PerimeterTotal Surface = Lateral Surface + $(2 \times$ Base Area)Volume = $h \times$ Base Area**PYRAMID**Lateral Surface = $\frac{s}{2} \times$ Base Perimeter

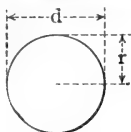
Total Surface = Lateral Surface + Base Area

Volume = $\frac{h}{3} \times$ Base AreaCenter of Gravity = $\frac{h}{4}$, above base**FRUSTUM OF PYRAMID**Lateral Surface = $s(\text{Top} + \text{Base Perimeters}) \div 2$ If $a =$ top area and $A =$ base area,Total Surface = Lateral Surface + $(a + A)$ Volume = $h(a + A + \sqrt{aA}) \div 3$ Center of Gravity above base = $\frac{h}{4} \left(\frac{3a + A + 2\sqrt{aA}}{a + A + \sqrt{aA}} \right)$ **CONE**Convex Surface = $\frac{\pi}{2} ds = \frac{\pi d}{4} \sqrt{d^2 + 4h^2}$ Total Surface = Convex Surface + $\frac{\pi d^2}{4}$ Volume = $\frac{\pi}{12} d^2 h = \frac{\pi}{24} d^2 \sqrt{4s^2 - d^2}$ Center of Gravity above base = $\frac{h}{4}$ **FRUSTUM OF CONE**Convex Surface = $\frac{\pi s}{2} (d + d') = \frac{\pi}{4} (d + d') \sqrt{4h^2 + (d - d')^2}$ Total Surface = $\frac{\pi s}{2} (d + d') + \frac{\pi}{4} (d^2 + d'^2)$ Volume = $\frac{\pi h}{12} (d^2 + dd' + d'^2)$ Center of Gravity above base = $\frac{h(d^2 + 2dd' + 3d'^2)}{4(d^2 + dd' + d'^2)}$ **WEDGE**

Surface = Sum of surfaces of bounding planes

Volume = $\frac{wh}{6} (l + m + n)$

SURFACES AND VOLUMES OF SOLIDS.

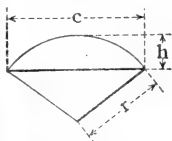
**SPHERE**

$$\text{Surface} = \pi d^2 = 4\pi r^2$$

$$\text{Volume} = \frac{\pi d^3}{6} = \frac{4}{3}\pi r^3$$

Side of an equal cube = diameter of sphere $\times 0.806$
 Length of an equal cylinder = diameter of sphere $\times 0.6667$

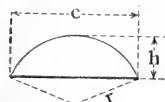
Center of Gravity of Half Sphere
 $= \frac{3}{8}r$ above spherical center

**SPHERICAL SECTOR**

$$\text{Total Surface} = \frac{\pi r}{2}(4h + c)$$

$$\text{Volume} = \frac{2}{3}\pi r^2 h = \frac{2}{3}\pi r^2 \left(r - \sqrt{r^2 - \frac{c^2}{4}} \right)$$

Center of Gravity $= \frac{3}{4} \left(r - \frac{h}{2} \right)$
 above center of sphere

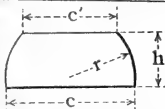
**SPHERICAL SEGMENT**

$$\text{Spherical Surface} = 2\pi r h = \pi(c^2 + 4h^2) \div 4$$

$$\text{Total Surface} = \text{Spherical Surface} + (\pi c^2 \div 4)$$

$$\text{Volume} = \pi h^2(3r - h) \div 3 = \pi h(3c^2 + 4h^2) \div 24$$

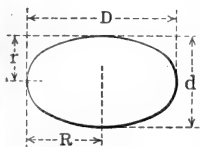
Center of gravity above base of segment
 $= h(4r - h) \div 4(3r - h)$

**SPHERICAL ZONE**

$$\text{Convex Surface} = 2\pi r h$$

$$\text{Total Surface} = 2\pi r h + \frac{\pi}{4}(c^2 + c'^2)$$

$$\text{Volume} = \frac{\pi h}{24}(3c^2 + 3c'^2 + 4h^2)$$

**ELLIPSOID (I. Revolution about transverse axis)**

$$\text{Surface} = 2\pi r \left[r + R \left(\frac{\sin^{-1} e}{e} \right) \right]$$

$$\text{Volume} = \frac{4}{3}\pi R r^2$$

ELLIPSOID (II. Revolution about conjugate axis)

$$\text{Surface} = \pi \left[2R^2 + \frac{2.302r^2}{e} \log \left(\frac{1+e}{1-e} \right) \right]$$

$$\text{Volume} = \frac{4}{3}\pi R^2 r \quad \text{Where } e = \frac{\sqrt{R^2 - r^2}}{R}$$

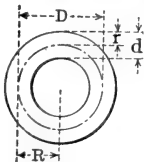
**PARABOLOID**

$$\text{Convex Surface} = \frac{\pi r}{6h^2} \left[(r^2 + 4h^2)^{3/2} - r^3 \right]$$

$$\text{Total Surface} = \text{Convex Surface} + \pi r^2$$

$$\text{Volume} = \frac{\pi r^2 h}{2} \quad \text{Center of Gravity} = \frac{h}{3} \text{ above base}$$

SURFACES AND VOLUMES OF SOLIDS

**CIRCULAR RING (TORUS)**

D & R = Mean Diameter and Mean Radius, respectively, of Ring

d & r = Mean Diameter and Mean Radius, respectively, of Section

$$\text{Surface} = \pi^2 D d = 4\pi^2 R r$$

$$\text{Volume} = 2\pi^2 R r^2 = \frac{\pi^2}{4} D d^2$$

**PRISMOID**

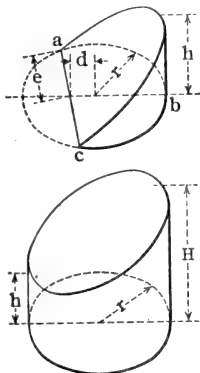
End faces are in parallel planes.

$$\text{Volume} = \frac{1}{6}(A + A' + 4M), \text{ where}$$

1 = perpendicular distance between ends

A, A' = areas of ends

M = area of mid section, parallel to ends

**UNGULAS FROM RIGHT CIRCULAR CYLINDER**

(As formed by cutting plane oblique to base)

I. Base, abc, less than semicircle;

Convex Surface

$$= h(2re - (d \times \text{length arc abc})) + (r - d)$$

$$\text{Volume} = h(\frac{2}{3}e^3 - (d \times \text{area base abc})) + (r - d)$$

II. Base, abc, = semicircle;

Convex Surface = $2rh$

$$\text{Volume} = \frac{2}{3}r^2h$$

III. Base, abc, greater than semicircle (figure);

Convex Surface

$$= h(2re + (d \times \text{length arc abc})) + (r + d)$$

$$\text{Volume} = h(\frac{2}{3}e^3 + (d \times \text{area base abc})) + (r + d)$$

IV. Base, abc, = circle, oblique plane touching circumference.

Convex Surface = πrh

$$\text{Volume} = \frac{1}{2}\pi r^2h$$

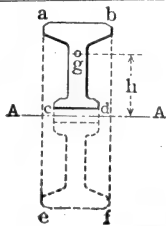
V. Base, abc, = circle, oblique plane entirely above (figure).

Convex Surface = $2\pi r$

$$\times \frac{1}{2}(h, \text{minimum} + H, \text{maximum})$$

$$\text{Volume} = \pi r^2 \times \frac{1}{2}(h, \text{minimum}$$

$$+ H, \text{maximum})$$

**ANY SOLID OF REVOLUTION**

Let abcd represent the generating section about axis A-A of solid abef.

Let g at distance h from A-A be the center of gravity of abcd.

Let α° be the angular amount of generating revolution.

Then

Total Surface of solid abef

$$= (2\pi h\alpha + 360) \times \text{perimeter abcd}$$

$$\text{Volume of solid abef} = (\frac{2\pi h\alpha + 360}{360}) \times \text{area abcd}$$

$$\text{For complete revolution } (2\pi h\alpha + 360) = 2\pi h$$

MINUTES AND SECONDS EXPRESSED AS DECIMALS OF A DEGREE

| Minutes | 0 | 10 | 20 | 30 | 40 | 50 |
|---------|--------|--------|--------|--------|--------|--------|
| 0 | | .16667 | .33333 | .50000 | .66667 | .83333 |
| 1 | .01667 | .18333 | .35000 | .51667 | .68333 | .85000 |
| 2 | .03333 | .20000 | .36667 | .53333 | .70000 | .86667 |
| 3 | .05000 | .21667 | .38333 | .55000 | .71667 | .88333 |
| 4 | .06667 | .23333 | .40000 | .56667 | .73333 | .90000 |
| 5 | .08333 | .25000 | .41667 | .58333 | .75000 | .91667 |
| 6 | .10000 | .26667 | .43333 | .60000 | .76667 | .93333 |
| 7 | .11667 | .28333 | .45000 | .61667 | .78333 | .95000 |
| 8 | .13333 | .30000 | .46667 | .63333 | .80000 | .96667 |
| 9 | .15000 | .31667 | .48333 | .65000 | .81667 | .98333 |
| Seconds | 0 | 10 | 20 | 30 | 40 | 50 |
| 0 | | .00278 | .00556 | .00833 | .01111 | .01389 |
| 1 | .00028 | .00306 | .00583 | .00861 | .01139 | .01417 |
| 2 | .00056 | .00333 | .00611 | .00889 | .01167 | .01444 |
| 3 | .00083 | .00361 | .00639 | .00917 | .01194 | .01472 |
| 4 | .00111 | .00389 | .00667 | .00944 | .01222 | .01500 |
| 5 | .00139 | .00417 | .00694 | .00972 | .01250 | .01528 |
| 6 | .00167 | .00444 | .00722 | .01000 | .01278 | .01556 |
| 7 | .00194 | .00472 | .00750 | .01028 | .01306 | .01583 |
| 8 | .00222 | .00500 | .00778 | .01056 | .01333 | .01611 |
| 9 | .00250 | .00528 | .00806 | .01083 | .01361 | .01639 |

DECIMALS OF A DEGREE EXPRESSED AS MINUTES OR SECONDS

| Degree | .00 Min. (Sec.) | .10 Min. (Sec.) | .20 Min. (Sec.) | .30 Min. (Sec.) | .40 Min. (Sec.) |
|--------|--------------------|--------------------|--------------------|--------------------|--------------------|
| .00 | | 6.0 (360) | 12.0 (720) | 18.0 (1080) | 24.0 (1440) |
| .01 | .6 (36) | 6.6 (396) | 12.6 (756) | 18.6 (1116) | 24.6 (1476) |
| .02 | 1.2 (72) | 7.2 (432) | 13.2 (792) | 19.2 (1152) | 25.2 (1512) |
| .03 | 1.8 (108) | 7.8 (468) | 13.8 (828) | 19.8 (1188) | 25.8 (1548) |
| .04 | 2.4 (144) | 8.4 (504) | 14.4 (864) | 20.4 (1224) | 26.4 (1584) |
| .05 | 3.0 (180) | 9.0 (540) | 15.0 (900) | 21.0 (1260) | 27.0 (1620) |
| .06 | 3.6 (216) | 9.6 (576) | 15.6 (936) | 21.6 (1296) | 27.6 (1656) |
| .07 | 4.2 (252) | 10.2 (612) | 16.2 (972) | 22.2 (1332) | 28.2 (1692) |
| .08 | 4.8 (288) | 10.8 (648) | 16.8 (1008) | 22.8 (1368) | 28.8 (1728) |
| .09 | 5.4 (324) | 11.4 (684) | 17.4 (1044) | 23.4 (1404) | 29.4 (1764) |
| Degree | .50 Min. (Sec.) | .60 Min. (Sec.) | .70 Min. (Sec.) | .80 Min. (Sec.) | .90 Min. (Sec.) |
| .00 | 30.0 (1800) | 36.0 (2160) | 42.0 (2520) | 48.0 (2880) | 54.0 (3240) |
| .01 | 30.6 (1836) | 36.6 (2196) | 42.6 (2556) | 48.6 (2916) | 54.6 (3276) |
| .02 | 31.2 (1872) | 37.2 (2232) | 43.2 (2592) | 49.2 (2952) | 55.2 (3312) |
| .03 | 31.8 (1908) | 37.8 (2268) | 43.8 (2628) | 49.8 (2988) | 55.8 (3348) |
| .04 | 32.4 (1944) | 38.4 (2304) | 44.4 (2664) | 50.4 (3024) | 56.4 (3384) |
| .05 | 33.0 (1980) | 39.0 (2340) | 45.0 (2700) | 51.0 (3060) | 57.0 (3420) |
| .06 | 33.6 (2016) | 39.6 (2376) | 45.6 (2736) | 51.6 (3096) | 57.6 (3456) |
| .07 | 34.2 (2052) | 40.2 (2412) | 46.2 (2772) | 52.2 (3132) | 58.2 (3492) |
| .08 | 34.8 (2088) | 40.8 (2448) | 46.8 (2808) | 52.8 (3168) | 58.8 (3528) |
| .09 | 35.4 (2124) | 41.4 (2484) | 47.4 (2844) | 53.4 (3204) | 59.4 (3564) |

WEIGHTS AND MEASURES.**AVOIRDUPOIS WEIGHT.****United States and British.**

| Grains. | Drams. | Ounces. | Pounds. | Hundred-weight. | Gross Tons. |
|-----------|---------|---------|---------|-----------------|-------------|
| 1. | .03657 | .002286 | .000143 | .00000128 | .000000064 |
| 27.34375 | 1. | .0625 | .003906 | .00003488 | .000001744 |
| 437.5 | 16. | 1. | .0625 | .00055804 | .00002790 |
| 7000. | 256. | 16. | 1. | .0089286 | .0004464 |
| 784000. | 28672. | 1792. | 112. | 1. | .05 |
| 15680000. | 573440. | 35840. | 2240. | 20. | 1. |

1 pound avoirdupois = 1.215278 pounds troy.

1 net ton = 2000 pounds = .892857 gross ton.

TROY WEIGHT.**United States and British.**

| Grains. | Pennyweight. | Ounces. | Pounds. |
|---------|--------------|----------|----------|
| 1 | .041667 | .0020833 | .0001736 |
| 24 | 1. | .05 | .0041667 |
| 480 | 20. | 1. | .0833333 |
| 5760 | 240. | 12. | 1. |

1 pound troy = .822857 pound avoirdupois.

175 ounces troy = 192 ounces avoirdupois.

APOTHECARIES' WEIGHT.**United States and British.**

| Grains. | Scruples. | Drams. | Ounces. | Pounds. |
|---------|-----------|---------|----------|------------|
| 1 | .05 | .016667 | .0020833 | .000173611 |
| 20 | 1. | .333333 | .0416667 | .0034722 |
| 60 | 3. | 1. | .125 | .0104167 |
| 480 | 24. | 8. | 1. | .0833333 |
| 5760 | 288. | 96. | 12. | 1. |

The pound, ounce and grain are the same as in troy weight.

The avoirdupois grain = troy grain = apothecaries' grain.

WEIGHTS AND MEASURES—Continued.**LINEAR MEASURE.****United States and British.**

| Inches. | Feet. | Yards. | Rods. | Furlongs. | Miles. |
|---------|--------|--------|----------|-----------|-----------|
| 1 | .08333 | .02778 | .0050505 | .00012626 | .00001578 |
| 12 | 1. | .33333 | .0606061 | .00151515 | .00018939 |
| 36 | 3. | 1. | .1818182 | .00454545 | .00056818 |
| 198 | 16.5 | 5.5 | 1. | .025 | .003125 |
| 7920 | 660. | 220. | 40. | 1. | .125 |
| 63360 | 5280. | 1760. | 320. | 8. | 1. |

ROPE AND CABLE MEASURE.

1 inch = .111111 span = .013889 fathom = .0001157 cable's length.

1 span = 9 inches = .125 fathom = .00104167 cable's length.

1 fathom = 6 feet = 8 spans = 72 inches = .008333 cable's length.

1 cable's length = 120 fathoms = 720 feet = 960 spans = 8640 inches.

NAUTICAL MEASURE.

1 nautical mile, as adopted by the United States Coast and Geodetic Survey, equals the length of one minute of arc of a great circle of a sphere whose surface equals that of the earth = 6080.204 feet = 1.1516 statute miles.

1 league = 3 nautical miles = 18240.613 feet.

GUNTER'S CHAIN.

1 link = 7.92 inches = .01 chain = .000125 mile.

1 chain = 100 links = 66 feet = 4 rods = .0125 mile.

1 mile = 80 chains = 8000 links.

SQUARE OR LAND MEASURE.**United States and British.**

| Square Inches. | Square Feet. | Square Yards. | Square Rods. | Acres. | Square Miles. |
|----------------|--------------|---------------|--------------|----------|---------------|
| 1 | .000944 | .0007716 | | | |
| 144 | 1. | .111111 | | | |
| 1296 | 9.0 | 1. | .03306 | .0002066 | |
| 39204 | 272.25 | 30.25 | 1. | .00625 | .0000977 |
| 6272640 | 43500. | 4840. | 160. | 1. | .0015625 |
| | 27878400. | 3097600. | 102400. | 640. | 1. |

1 square rod = 40 square rods.

1 acre = 4 square rods.

1 square acre = 208.71 feet square.

WEIGHTS AND MEASURES—Continued.**CUBIC OR SOLID MEASURE.****United States and British.**

1 cubic inch = .0005787 cubic foot = .000021433 cubic yard.

1 cubic foot = 1728 cubic inches = .03703704 cubic yard.

1 cubic yard = 27 cubic feet = 46656 cubic inches.

1 cord of wood = 128 cubic feet = 4 feet by 4 feet by 8 feet.

1 perch of masonry = 24.75 cubic feet = 16.5 feet by 1.5 feet by 1 foot. It is usually taken as 25 cubic feet.

DRY MEASURE.**United States only.**

| Pints. | Quarts. | Gallons. | Pecks. | Bushels | Cubic Inches. |
|--------|---------|----------|--------|---------|---------------|
| 1 | .50 | .125 | .0625 | .015625 | 33.6003125 |
| 2 | 1. | .25 | .125 | .03125 | 67.200625 |
| 8 | 4. | 1. | .05 | .125 | 268.8025 |
| 16 | 8. | 2. | 1. | .25 | 537.605 |
| 64 | 32. | 8. | 4. | 1. | 2150.42 |

1 heaped bushel = 1.25 struck bushel, and the cone must be not less than 6 inches high.

LIQUID MEASURE.**United States only.**

| Gills. | Pints. | Quarts. | Gallons. | Barrels. | Cubic Inches. |
|--------|--------|---------|----------|----------|---------------|
| 1 | .25 | .125 | .03125 | .000992 | 7.21875 |
| 4 | 1. | .5 | .125 | .003968 | 28.875 |
| 8 | 2. | 1. | .25 | .007937 | 57.75 |
| 32 | 8. | 4. | 1. | .031746 | 231. |
| 1008 | 252. | 128. | 31.5 | 1. | 7276.5 |

The British imperial gallon = 277.410 cubic inches or 10 pounds avoirdupois of pure water at 62° F. and barometer at 30 inches.

The British imperial gallon = 1.20091 United States gallons.

1 fluid drachm = 60 minims = .125 fluid ounce = .0078125 pint.

1 fluid ounce = 480 minims = 8 drachms = .0625 pint.

WEIGHTS AND MEASURES—Concluded.**METRIC SYSTEM.****Measures of Length, Capacity and Weight.**

| LENGTH. | Kilometre. | Hecto- metre. | Decametre. | Metre. | Decimetre. | Centimetre. | Millimetre. |
|-----------|---------------------------|--------------------------------|--------------------------------|----------------------------|---------------------------------|---|--|
| CAPACITY. | Kilolitre or Stere. | Hectolitre or Decistere. | Decalitre or Centistere. | Litre or Millistere. | Decilitre. | Centilitre. | Millilitre. |
| WEIGHT. | Kilo- gramme. | Hecto- gramme. | Deca- gramme. | Gramme. | Deci- gramme. | Centi- gramme. | Milli- gramme. |
| | 1 | 10 1 | 100 10 1 | 1000 100 10 1 | 10000 1000 100 10 1 | 100000 10000 1000 100 10 1 | 1000000 100000 10000 1000 100 10 1 |
| | | | | .1 .01 .001 | .1 .01 | .1 | |

1 myriametre = 10 kilometres = 10000 metres.

1 tonne = 1000 kilogrammes = 100 quintals = 10 myriagrammes.

1 gramme = weight of 1 cubic centimetre of distilled water at its maximum density at sea level in latitude of Paris and barometer at 760 millimetres.

1 litre = 1 cubic decimetre.

METRIC SYSTEM.**Square or Surface Measure.**

| Square Kilometre. | Square Hectometre or Hectare. | Square Decametre or Are. | Square Metre or Centiare. | Square Decimetre. | Square Centimetre. | Square Millimetre. |
|----------------------|-------------------------------------|--|---|--|-------------------------------------|------------------------------|
| 1 | 100 1 .01 .0001 .000001 | 10000 100 1 .01 .0001 .000001 | 1000000 10000 100 1 .01 .0001 .000001 | 1000000 10000 100 1 .01 .0001 | 1000000 10000 100 1 .01 | 1000000 10000 100 1 |

1 square myriametre = 100 square kilometres = 100 000 000 square metres.

METRIC SYSTEM.**Cubic Measure.**

| Cubic Decametre. | Cubic Metre. | Cubic Decimetre. | Cubic Centimetre. | Cubic Millimetre. |
|------------------------------------|--|---|--|------------------------------------|
| 1 .001 .000001 .000000001 | 1000 1 .001 .000001 .000000001 | 1000000 1000 1 .001 .000001 | 1000000000 1000000 1000 1 .001 | 1000000000 1000000 1000 1 |

1 cubic metre = 1 kilolitre = 1 stere.

TABLES FOR CONVERTING UNITED STATES WEIGHTS AND MEASURES.

CUSTOMARY TO METRIC.

Weights.

See Page 590

| No. | Grains to Milligrammes. | Troy Ounces to Grammes. | Avoirdupois Ounces to Grammes. | Avoirdupois Pounds to Kilogrammes. Page 582 | Net Tons of 2000 Pounds to Tonnes. | Gross Tons of 2240 Pounds to Tonnes. |
|-----|-------------------------------|-------------------------------|--------------------------------------|--|--|--|
| 1 | 64.79892 | 31.10348 | 28.34953 | .45359 | .90718 | 1.01605 |
| 2 | 129.59784 | 62.20696 | 56.69905 | .90718 | 1.81437 | 2.03209 |
| 3 | 194.39675 | 93.31044 | 85.04858 | 1.36078 | 2.72155 | 3.04814 |
| 4 | 259.19567 | 124.41392 | 113.39811 | 1.81437 | 3.62874 | 4.06419 |
| 5 | 323.99459 | 155.51740 | 141.74763 | 2.26796 | 4.53592 | 5.08024 |
| 6 | 388.79351 | 186.62088 | 170.09716 | 2.72155 | 5.44311 | 6.09628 |
| 7 | 453.59243 | 217.72437 | 198.44669 | 3.17515 | 6.35029 | 7.11233 |
| 8 | 518.39135 | 248.82785 | 226.79621 | 3.62874 | 7.25748 | 8.12838 |
| 9 | 583.19026 | 279.93133 | 255.14574 | 4.08233 | 8.16466 | 9.14442 |

1 Avoirdupois Pound = 453.5924277 Grammes.

Linear Measure.

| No. | 64ths of an Inch to Millimetres. Page 450 | Inches to Centimetres. Page 568 | Feet to Metres. Page 574 | Yards to Metres. | Statute Miles to Kilometres. | Nautical Miles to Kilometres. |
|-----|--|--|-----------------------------------|------------------------|------------------------------------|-------------------------------------|
| 1 | .39688 | 2.54001 | .304801 | .914402 | 1.60935 | 1.85325 |
| 2 | .79375 | 5.08001 | .609601 | 1.828804 | 3.21869 | 3.70650 |
| 3 | 1.19063 | 7.62002 | .914402 | 2.743205 | 4.82804 | 5.55975 |
| 4 | 1.58750 | 10.16002 | 1.219202 | 3.657607 | 6.43739 | 7.41300 |
| 5 | 1.98438 | 12.70003 | 1.524003 | 4.572009 | 8.04674 | 9.26625 |
| 6 | 2.38125 | 15.24003 | 1.828804 | 5.486411 | 9.65608 | 11.11950 |
| 7 | 2.77813 | 17.78004 | 2.133604 | 6.400813 | 11.26543 | 12.97275 |
| 8 | 3.17501 | 20.32004 | 2.438405 | 7.315215 | 12.87478 | 14.82600 |
| 9 | 3.57188 | 22.86005 | 2.743205 | 8.229616 | 14.48412 | 16.67925 |

1 Nautical Mile = 1853.25 Metres.

1 Gunter's Chain = 20.1168 Metres.

1 Fathom = 1.829 Metres.

TABLES FOR CONVERTING UNITED STATES WEIGHTS AND MEASURES.

METRIC TO CUSTOMARY.

Weights.

See Page 590

| No. | Milligrammes to Grains. | Grammes to Troy Ounces. | Grammes to Avoirdupois Ounces. | Kilogrammes to Avoirdupois Pounds. Page 586 | Tonnes to Net Tons of 2000 Pounds. | Tonnes to Gross Tons of 2240 Pounds. |
|-----|-------------------------------|-------------------------------|--------------------------------------|--|--|--|
| 1 | .01543 | .03215 | .03527 | 2.20462 | 1.10231 | .98421 |
| 2 | .03086 | .06430 | .07055 | 4.40924 | 2.20462 | 1.96841 |
| 3 | .04630 | .09645 | .10582 | 6.61387 | 3.30693 | 2.95262 |
| 4 | .06173 | .12860 | .14110 | 8.81849 | 4.40924 | 3.93682 |
| 5 | .07716 | .16075 | .17637 | 11.02311 | 5.51156 | 4.92103 |
| 6 | .09259 | .19290 | .21164 | 13.22773 | 6.61387 | 5.90524 |
| 7 | .10803 | .22506 | .24692 | 15.43236 | 7.71618 | 6.88944 |
| 8 | .12346 | .25721 | .28219 | 17.63698 | 8.81849 | 7.87365 |
| 9 | .13889 | .28936 | .31747 | 19.84160 | 9.92080 | 8.85785 |

1 Kilogramme = 15432.35639 Grains.

Linear Measure.

| No. | Millimetres to 64ths of an Inch. | Centimetres to Inches. Page 570 | Metres to Feet. Page 578 | Metres to Yards. | Kilometres to Statute Miles. | Kilometres to Nautical Miles. |
|-----|--|--|-----------------------------------|------------------------|------------------------------------|-------------------------------------|
| 1 | 2.51968 | .39370 | 3.280833 | 1.093611 | .62137 | .53959 |
| 2 | 5.03936 | .78740 | 6.561667 | 2.187222 | 1.24274 | 1.07919 |
| 3 | 7.55904 | 1.18110 | 9.842500 | 3.280833 | 1.86411 | 1.61878 |
| 4 | 10.07872 | 1.57480 | 13.123333 | 4.374444 | 2.48548 | 2.15837 |
| 5 | 12.59840 | 1.96850 | 16.404167 | 5.468056 | 3.10685 | 2.69796 |
| 6 | 15.11808 | 2.36220 | 19.685000 | 6.561667 | 3.72822 | 3.23756 |
| 7 | 17.63776 | 2.75590 | 22.965833 | 7.655278 | 4.34959 | 3.77715 |
| 8 | 20.15744 | 3.14960 | 26.246667 | 8.748889 | 4.97096 | 4.31674 |
| 9 | 22.67712 | 3.54330 | 29.527500 | 9.842500 | 5.59233 | 4.85633 |

TABLES FOR CONVERTING UNITED STATES WEIGHTS AND MEASURES.

CUSTOMARY TO METRIC.

Square Measure.

| No. | Square Inches to Square Centimetres. | Square Feet to Square Metres. | Square Yards to Square Metres. | Acres to Hectares. | Square Miles to Square Kilometres. |
|-----|--|-------------------------------------|--------------------------------------|--------------------------|--|
| 1 | 6.45163 | .09290 | .83613 | .40470 | 2.59000 |
| 2 | 12.90325 | .18581 | 1.67226 | .80939 | 5.18000 |
| 3 | 19.35488 | .27871 | 2.50839 | 1.21409 | 7.77000 |
| 4 | 25.80650 | .37161 | 3.34452 | 1.61879 | 10.35999 |
| 5 | 32.25813 | .46452 | 4.18065 | 2.02349 | 12.94999 |
| 6 | 38.70975 | .55742 | 5.01679 | 2.42818 | 15.53999 |
| 7 | 45.16138 | .65032 | 5.85292 | 2.83288 | 18.12999 |
| 8 | 51.61300 | .74323 | 6.68905 | 3.23758 | 20.71999 |
| 9 | 58.06463 | .83613 | 7.52518 | 3.64228 | 23.30999 |

1 Square Statute Mile = 259.00 Hectares.

Cubic Measure

| No. | Cubic Inches to Cubic Centimetres. | Cubic Inches to Cubic Decimetres. | Cubic Feet to Cubic Metres. | Cubic Yards to Cubic Metres. |
|-----|--|---|-----------------------------------|------------------------------------|
| 1 | 16.38716 | .01639 | .02832 | .76456 |
| 2 | 32.77432 | .03277 | .05663 | 1.52912 |
| 3 | 49.16148 | .04916 | .08495 | 2.29368 |
| 4 | 65.54864 | .06555 | .11327 | 3.05824 |
| 5 | 81.93580 | .08194 | .14159 | 3.82280 |
| 6 | 98.32296 | .09832 | .16990 | 4.58736 |
| 7 | 114.71013 | .11471 | .19822 | 5.35192 |
| 8 | 131.09729 | .13110 | .22654 | 6.11648 |
| 9 | 147.48445 | .14748 | .25485 | 6.88104 |

TABLES FOR CONVERTING UNITED STATES WEIGHTS AND MEASURES.

METRIC TO CUSTOMARY.

Square Measure.

| No. | Square Centi- metres to Square Inches. | Square Metres to Square Feet. | Square Metres to Square Yards. | Hectares to Acres. | Square Kilo- metres to Square Miles. |
|-----|--|-------------------------------------|--------------------------------------|--------------------------|--|
| 1 | .15500 | 10.76387 | 1.19599 | 2.47104 | .38610 |
| 2 | .31000 | 21.52773 | 2.39197 | 4.94209 | .77220 |
| 3 | .46500 | 32.29160 | 3.58796 | 7.41313 | 1.15830 |
| 4 | .62000 | 43.05547 | 4.78394 | 9.88418 | 1.54440 |
| 5 | .77500 | 53.81934 | 5.97993 | 12.35522 | 1.93050 |
| 6 | .93000 | 64.58320 | 7.17591 | 14.82626 | 2.31660 |
| 7 | 1.08500 | 75.34707 | 8.37190 | 17.29731 | 2.70270 |
| 8 | 1.24000 | 86.11094 | 9.56788 | 19.76835 | 3.08880 |
| 9 | 1.39500 | 96.87481 | 10.76387 | 22.23940 | 3.47490 |

1 Hectare = .003861 Square Statute Mile.

Cubic Measure

| No. | Cubic Centimetres to Cubic Inches. | Cubic Decimetres to Cubic Inches. | Cubic Metres to Cubic Feet. | Cubic Metres to Cubic Yards. |
|-----|--|---|-----------------------------------|------------------------------------|
| 1 | .06102 | 61.02338 | 35.31445 | 1.30794 |
| 2 | .12205 | 122.04676 | 70.62891 | 2.61589 |
| 3 | .18307 | 183.07013 | 105.94336 | 3.92383 |
| 4 | .24409 | 244.09351 | 141.25782 | 5.23177 |
| 5 | .30512 | 305.11689 | 176.57227 | 6.53971 |
| 6 | .36614 | 366.14027 | 211.88673 | 7.84766 |
| 7 | .42716 | 427.16365 | 247.20118 | 9.15560 |
| 8 | .48819 | 488.18702 | 282.51564 | 10.46354 |
| 9 | .54921 | 549.21040 | 317.83009 | 11.77149 |

TABLES FOR CONVERTING UNITED STATES WEIGHTS AND MEASURES.

CUSTOMARY TO METRIC.

Capacity Measures.

| No. | Liquid Quarts to Litres. | Gallons to Litres. | Gallons to Cubic Metres. | Busbels to Hectolitres. | Fluid Drachms to Millilitres or Cubic Centimetres. | Fluid Ounces to Millilitres or Cubic Centimetres. |
|-----|--------------------------------|--------------------------|--------------------------------|-------------------------------|---|--|
| 1 | .94636 | 3.78543 | .00379 | .35239 | 3.69671 | 29.57370 |
| 2 | 1.89272 | 7.57087 | .00757 | .70479 | 7.39343 | 59.14741 |
| 3 | 2.83908 | 11.35630 | .01136 | 1.05718 | 11.09014 | 88.72111 |
| 4 | 3.78543 | 15.14174 | .01514 | 1.40957 | 14.78685 | 118.29482 |
| 5 | 4.73179 | 18.92717 | .01893 | 1.76196 | 18.48357 | 147.86852 |
| 6 | 5.67815 | 22.71260 | .02271 | 2.11436 | 22.18028 | 177.44222 |
| 7 | 6.62451 | 26.49804 | .02650 | 2.46675 | 25.87699 | 207.01593 |
| 8 | 7.57087 | 30.28347 | .03028 | 2.81914 | 29.57370 | 236.58963 |
| 9 | 8.51723 | 34.06891 | .03407 | 3.17154 | 33.27042 | 266.16334 |

Miscellaneous.

| No. | Pounds per Lineal Foot to Kilogrammes per Lineal Metre. | Pounds per Square Inch to Kilogrammes per Square Centimetre. | Pounds per Square Foot to Kilogrammes per Square Metre. | Pounds per Cubic Foot to Kilogrammes per Cubic Metre. | Foot-Pounds to Kilogramme- Metres | United States Horsepower to Metric Horsepower. |
|-----|---|--|---|---|--|---|
| 1 | 1.48816 | .07031 | 4.88241 | 16.01837 | .13826 | 1.01387 |
| 2 | 2.97632 | .14061 | 9.76482 | 32.03674 | .27651 | 2.02775 |
| 3 | 4.46448 | .21092 | 14.64723 | 48.05510 | .41477 | 3.04162 |
| 4 | 5.95264 | .28123 | 19.52963 | 64.07348 | .55302 | 4.05549 |
| 5 | 7.44081 | .35153 | 24.41204 | 80.09185 | .69128 | 5.06937 |
| 6 | 8.92897 | .42184 | 29.29445 | 96.11021 | .82953 | 6.08324 |
| 7 | 10.41713 | .49215 | 34.17686 | 112.12858 | .96779 | 7.09711 |
| 8 | 11.90529 | .56245 | 39.05927 | 128.14695 | 1.10604 | 8.11098 |
| 9 | 13.39345 | .63276 | 43.94168 | 144.16532 | 1.24430 | 9.12486 |

TABLES FOR CONVERTING UNITED STATES WEIGHTS AND MEASURES.

METRIC TO CUSTOMARY.

Capacity Measures.

| No. | Litres to Fluid Quarts. | Litres to Gallons. | Cubic Metres to Gallons. | Hectolitres to Bushels. | Millilitres or Cubic Centi- metres to Fluid Drachms. | Millilitres or Cubic Centi- metres to Fluid Ounces. |
|-----|-------------------------------|--------------------------|--------------------------------|-------------------------------|---|--|
| 1 | 1.05668 | .26417 | 264.17047 | 2.83774 | .27051 | .03381 |
| 2 | 2.11336 | .52834 | 528.34093 | 5.67548 | .54102 | .06763 |
| 3 | 3.17005 | .79251 | 792.51140 | 8.51323 | .81153 | .10144 |
| 4 | 4.22673 | 1.05668 | 1056.68187 | 11.35097 | 1.08204 | .13526 |
| 5 | 5.28341 | 1.32085 | 1320.85234 | 14.18871 | 1.35255 | .16907 |
| 6 | 6.34009 | 1.58502 | 1585.02280 | 17.02645 | 1.62306 | .20288 |
| 7 | 7.39677 | 1.84919 | 1849.19327 | 19.86420 | 1.89357 | .23670 |
| 8 | 8.45345 | 2.11336 | 2113.36374 | 22.70194 | 2.16408 | .27051 |
| 9 | 9.51014 | 2.37753 | 2377.53420 | 25.53968 | 2.43460 | .30432 |

Miscellaneous.

| No. | Kilogrammes per Lineal Metre to Pounds per Lineal Foot. | Kilogrammes per Square Centimetre to Pounds per Square Inch. | Kilogrammes per Square Metre to Pounds per Square Foot. | Kilogrammes per Cubic Metre to Pounds per Cubic Foot. | Kilogramme- Metres to Foot-Pounds. | Metric Horsepower to United States Horsepower. |
|-----|---|--|---|---|---|---|
| 1 | .67197 | 14.22340 | .20482 | .06243 | 7.23300 | .98632 |
| 2 | 1.34393 | 28.44680 | .40963 | .12486 | 14.46600 | 1.97264 |
| 3 | 2.01590 | 42.67020 | .61445 | .18728 | 21.69899 | 2.95895 |
| 4 | 2.68787 | 56.89359 | .81927 | .24971 | 28.93199 | 3.94527 |
| 5 | 3.35984 | 71.11699 | 1.02408 | .31214 | 36.16499 | 4.93159 |
| 6 | 4.03180 | 85.34039 | 1.22890 | .37457 | 43.39799 | 5.91791 |
| 7 | 4.70377 | 99.56379 | 1.43372 | .43700 | 50.63098 | 6.90423 |
| 8 | 5.37574 | 113.78719 | 1.63854 | .49943 | 57.86398 | 7.89054 |
| 9 | 6.04770 | 128.01059 | 1.84335 | .56185 | 65.09698 | 8.87686 |

EQUIVALENTS OF INCHES IN MILLIMETRES.**FRACTIONS OF AN INCH ADVANCING BY 32nds.**Page 450 shows values for each $\frac{1}{16}$ to 1 inch.

Conversion Factor: 1 inch=25.40005 millimetres.

| Inches | 0" | 1" | 2" | 3" | 4" | 5" |
|-----------------------|--------|--------|--------|---------|---------|---------|
| 0 | | 25.400 | 50.800 | 76.200 | 101.600 | 127.000 |
| $\frac{1}{32}$ | .794 | 26.194 | 51.594 | 76.994 | 102.394 | 127.794 |
| .. $\frac{1}{16}$.. | 1.588 | 26.988 | 52.388 | 77.788 | 103.188 | 128.588 |
| $\frac{3}{32}$ | 2.381 | 27.781 | 53.181 | 78.581 | 103.981 | 129.382 |
| $\frac{1}{8}$ | 3.175 | 28.575 | 53.975 | 79.375 | 104.775 | 130.175 |
| $\frac{5}{32}$ | 3.969 | 29.369 | 54.769 | 80.169 | 105.569 | 130.969 |
| .. $\frac{3}{16}$.. | 4.763 | 30.163 | 55.563 | 80.963 | 106.363 | 131.763 |
| $\frac{7}{32}$ | 5.556 | 30.956 | 56.356 | 81.756 | 107.156 | 132.557 |
| $\frac{1}{4}$ | 6.350 | 31.750 | 57.150 | 82.550 | 107.950 | 133.350 |
| $\frac{9}{32}$ | 7.144 | 32.544 | 57.944 | 83.344 | 108.744 | 134.144 |
| .. $\frac{5}{16}$.. | 7.938 | 33.338 | 58.738 | 84.138 | 109.538 | 134.938 |
| $\frac{11}{32}$ | 8.731 | 34.131 | 59.531 | 84.931 | 110.331 | 135.732 |
| $\frac{3}{8}$ | 9.525 | 34.925 | 60.325 | 85.725 | 111.125 | 136.525 |
| $\frac{13}{32}$ | 10.319 | 35.719 | 61.119 | 86.519 | 111.919 | 137.319 |
| .. $\frac{7}{16}$.. | 11.113 | 36.513 | 61.913 | 87.313 | 112.713 | 138.113 |
| $\frac{15}{32}$ | 11.906 | 37.306 | 62.706 | 88.106 | 113.506 | 138.907 |
| $\frac{1}{2}$ | 12.700 | 38.100 | 63.500 | 88.900 | 114.300 | 139.700 |
| $\frac{17}{32}$ | 13.494 | 38.894 | 64.294 | 89.694 | 115.094 | 140.494 |
| .. $\frac{9}{16}$.. | 14.288 | 39.688 | 65.088 | 90.488 | 115.888 | 141.288 |
| $\frac{19}{32}$ | 15.081 | 40.481 | 65.881 | 91.281 | 116.681 | 142.082 |
| $\frac{5}{8}$ | 15.875 | 41.275 | 66.675 | 92.075 | 117.475 | 142.875 |
| $\frac{21}{32}$ | 16.669 | 42.069 | 67.469 | 92.869 | 118.269 | 143.669 |
| .. $\frac{11}{16}$.. | 17.463 | 42.863 | 68.263 | 93.663 | 119.063 | 144.463 |
| $\frac{23}{32}$ | 18.256 | 43.656 | 69.056 | 94.456 | 119.856 | 145.257 |
| $\frac{3}{4}$ | 19.050 | 44.450 | 69.850 | 95.250 | 120.650 | 146.050 |
| $\frac{25}{32}$ | 19.844 | 45.244 | 70.644 | 96.044 | 121.444 | 146.844 |
| .. $\frac{13}{16}$.. | 20.638 | 46.038 | 71.438 | 96.838 | 122.238 | 147.638 |
| $\frac{27}{32}$ | 21.431 | 46.831 | 72.231 | 97.631 | 123.031 | 148.432 |
| $\frac{7}{8}$ | 22.225 | 47.625 | 73.025 | 98.425 | 123.825 | 149.225 |
| $\frac{29}{32}$ | 23.019 | 48.419 | 73.819 | 99.219 | 124.619 | 150.019 |
| .. $\frac{15}{16}$.. | 23.813 | 49.213 | 74.613 | 100.013 | 125.413 | 150.813 |
| $\frac{31}{32}$ | 24.606 | 50.006 | 75.406 | 100.806 | 126.206 | 151.607 |

12 Inches=304.8006 Millimetres.

EQUIVALENTS OF INCHES IN MILLIMETRES.

(Continued)

| Inches | 6" | 7" | 8" | 9" | 10" | 11" |
|-----------------------|---------|---------|---------|---------|---------|---------|
| 0 | 152.400 | 177.800 | 203.200 | 228.601 | 254.001 | 279.401 |
| $\frac{1}{32}$ | 153.194 | 178.594 | 203.994 | 229.394 | 254.794 | 280.194 |
| $\frac{1}{16}$ | 153.988 | 179.388 | 204.788 | 230.188 | 255.588 | 280.988 |
| $\frac{3}{32}$ | 154.782 | 180.182 | 205.582 | 230.982 | 256.382 | 281.782 |
| $\frac{1}{8}$ | 155.575 | 180.975 | 206.375 | 231.775 | 257.176 | 282.576 |
| $\frac{5}{32}$ | 156.369 | 181.769 | 207.169 | 232.569 | 257.969 | 283.369 |
| $\frac{3}{16}$ | 157.163 | 182.563 | 207.963 | 233.363 | 258.763 | 284.163 |
| $\frac{7}{32}$ | 157.957 | 183.357 | 208.757 | 234.157 | 259.557 | 284.957 |
| $\frac{1}{4}$ | 158.750 | 184.150 | 209.550 | 234.950 | 260.351 | 285.751 |
| $\frac{9}{32}$ | 159.544 | 184.944 | 210.344 | 235.744 | 261.144 | 286.544 |
| $\frac{5}{16}$ | 160.338 | 185.738 | 211.138 | 236.538 | 261.938 | 287.338 |
| $\frac{11}{32}$ | 161.132 | 186.532 | 211.932 | 237.332 | 262.732 | 288.132 |
| $\frac{3}{8}$ | 161.925 | 187.325 | 212.725 | 238.125 | 263.526 | 288.926 |
| $\frac{13}{32}$ | 162.719 | 188.119 | 213.519 | 238.919 | 264.319 | 289.719 |
| $\frac{7}{16}$ | 163.513 | 188.913 | 214.313 | 239.713 | 265.113 | 290.513 |
| $\frac{15}{32}$ | 164.307 | 189.707 | 215.107 | 240.507 | 265.907 | 291.307 |
| $\frac{1}{2}$ | 165.100 | 190.500 | 215.900 | 241.300 | 266.701 | 292.101 |
| $\frac{17}{32}$ | 165.894 | 191.294 | 216.694 | 242.094 | 267.494 | 292.894 |
| $\frac{9}{16}$ | 166.688 | 192.088 | 217.488 | 242.888 | 268.288 | 293.688 |
| $\frac{19}{32}$ | 167.482 | 192.882 | 218.282 | 243.682 | 269.082 | 294.482 |
| $\frac{5}{8}$ | 168.275 | 193.675 | 219.075 | 244.475 | 269.876 | 295.276 |
| $\frac{21}{32}$ | 169.069 | 194.469 | 219.869 | 245.269 | 270.669 | 296.069 |
| $\frac{11}{16}$ | 169.863 | 195.263 | 220.663 | 246.063 | 271.463 | 296.863 |
| $\frac{23}{32}$ | 170.657 | 196.057 | 221.457 | 246.857 | 272.257 | 297.657 |
| $\frac{3}{4}$ | 171.450 | 196.850 | 222.250 | 247.650 | 273.051 | 298.451 |
| $\frac{25}{32}$ | 172.244 | 197.644 | 223.044 | 248.444 | 273.844 | 299.244 |
| $\frac{13}{16}$ | 173.038 | 198.438 | 223.838 | 249.238 | 274.638 | 300.038 |
| $\frac{27}{32}$ | 173.832 | 199.232 | 224.632 | 250.032 | 275.432 | 300.832 |
| $\frac{7}{8}$ | 174.625 | 200.025 | 225.425 | 250.825 | 276.226 | 301.626 |
| $\frac{29}{32}$ | 175.419 | 200.819 | 226.219 | 251.619 | 277.019 | 302.419 |
| $\frac{15}{16}$ | 176.213 | 201.613 | 227.013 | 252.413 | 277.813 | 303.213 |
| $\frac{31}{32}$ | 177.007 | 202.407 | 227.807 | 253.207 | 278.607 | 304.007 |

12 Inches=304.8006 Millimetres.

EQUIVALENTS OF MILLIMETRES IN INCHES.

Conversion Factor: 1 millimetre = .03937 inch.

| Millimetres | 0 | 100 | 200 | 300 | 400 |
|-------------|-------|-------|-------|--------|--------|
| 0 | .000 | 3.937 | 7.874 | 11.811 | 15.748 |
| 1 | .039 | 3.976 | 7.913 | 11.850 | 15.788 |
| 2 | .079 | 4.016 | 7.953 | 11.890 | 15.827 |
| 3 | .118 | 4.055 | 7.992 | 11.929 | 15.866 |
| 4 | .157 | 4.095 | 8.032 | 11.969 | 15.906 |
| 5 | .197 | 4.134 | 8.071 | 12.008 | 15.945 |
| 6 | .236 | 4.173 | 8.110 | 12.047 | 15.984 |
| 7 | .276 | 4.213 | 8.150 | 12.087 | 16.024 |
| 8 | .315 | 4.252 | 8.189 | 12.126 | 16.063 |
| 9 | .354 | 4.291 | 8.228 | 12.165 | 16.103 |
| 10 | .394 | 4.331 | 8.268 | 12.205 | 16.142 |
| 11 | .433 | 4.370 | 8.307 | 12.244 | 16.181 |
| 12 | .472 | 4.409 | 8.347 | 12.284 | 16.221 |
| 13 | .512 | 4.449 | 8.386 | 12.323 | 16.260 |
| 14 | .551 | 4.488 | 8.425 | 12.362 | 16.299 |
| 15 | .591 | 4.528 | 8.465 | 12.402 | 16.339 |
| 16 | .630 | 4.567 | 8.504 | 12.441 | 16.378 |
| 17 | .669 | 4.606 | 8.543 | 12.480 | 16.417 |
| 18 | .709 | 4.646 | 8.583 | 12.520 | 16.457 |
| 19 | .748 | 4.685 | 8.622 | 12.559 | 16.496 |
| 20 | .787 | 4.724 | 8.661 | 12.599 | 16.536 |
| 21 | .827 | 4.764 | 8.701 | 12.638 | 16.575 |
| 22 | .866 | 4.803 | 8.740 | 12.677 | 16.614 |
| 23 | .906 | 4.843 | 8.780 | 12.717 | 16.654 |
| 24 | .945 | 4.882 | 8.819 | 12.756 | 16.693 |
| 25 | .984 | 4.921 | 8.858 | 12.795 | 16.732 |
| 26 | 1.024 | 4.961 | 8.898 | 12.835 | 16.772 |
| 27 | 1.063 | 5.000 | 8.937 | 12.874 | 16.811 |
| 28 | 1.102 | 5.039 | 8.976 | 12.913 | 16.851 |
| 29 | 1.142 | 5.079 | 9.016 | 12.953 | 16.890 |
| 30 | 1.181 | 5.118 | 9.055 | 12.992 | 16.929 |
| 31 | 1.220 | 5.158 | 9.095 | 13.032 | 16.969 |
| 32 | 1.260 | 5.197 | 9.134 | 13.071 | 17.008 |
| 33 | 1.299 | 5.236 | 9.173 | 13.110 | 17.047 |
| 34 | 1.339 | 5.276 | 9.213 | 13.150 | 17.087 |
| 35 | 1.378 | 5.315 | 9.252 | 13.189 | 17.126 |
| 36 | 1.417 | 5.354 | 9.291 | 13.228 | 17.166 |
| 37 | 1.457 | 5.394 | 9.331 | 13.268 | 17.205 |
| 38 | 1.496 | 5.433 | 9.370 | 13.307 | 17.244 |
| 39 | 1.535 | 5.472 | 9.410 | 13.347 | 17.284 |
| 40 | 1.575 | 5.512 | 9.449 | 13.386 | 17.323 |
| 41 | 1.614 | 5.551 | 9.488 | 13.425 | 17.362 |
| 42 | 1.654 | 5.591 | 9.528 | 13.465 | 17.402 |
| 43 | 1.693 | 5.630 | 9.567 | 13.504 | 17.441 |
| 44 | 1.732 | 5.669 | 9.606 | 13.543 | 17.480 |
| 45 | 1.772 | 5.709 | 9.646 | 13.583 | 17.520 |
| 46 | 1.811 | 5.748 | 9.685 | 13.622 | 17.559 |
| 47 | 1.850 | 5.787 | 9.724 | 13.662 | 17.599 |
| 48 | 1.890 | 5.827 | 9.764 | 13.701 | 17.638 |
| 49 | 1.929 | 5.866 | 9.803 | 13.740 | 17.677 |

EQUIVALENTS OF MILLIMETRES IN INCHES.

(Continued)

| Millimetres | 0 | 100 | 200 | 300 | 400 |
|-------------|-------|-------|--------|--------|--------|
| 50 | 1.969 | 5.906 | 9.843 | 13.780 | 17.717 |
| 51 | 2.008 | 5.945 | 9.882 | 13.819 | 17.756 |
| 52 | 2.047 | 5.984 | 9.921 | 13.858 | 17.795 |
| 53 | 2.087 | 6.024 | 9.961 | 13.898 | 17.835 |
| 54 | 2.126 | 6.063 | 10.000 | 13.937 | 17.874 |
| 55 | 2.165 | 6.102 | 10.039 | 13.977 | 17.914 |
| 56 | 2.205 | 6.142 | 10.079 | 14.016 | 17.953 |
| 57 | 2.244 | 6.181 | 10.118 | 14.055 | 17.992 |
| 58 | 2.283 | 6.221 | 10.158 | 14.095 | 18.032 |
| 59 | 2.323 | 6.260 | 10.197 | 14.134 | 18.071 |
| 60 | 2.362 | 6.299 | 10.236 | 14.173 | 18.110 |
| 61 | 2.402 | 6.339 | 10.276 | 14.213 | 18.150 |
| 62 | 2.441 | 6.378 | 10.315 | 14.252 | 18.189 |
| 63 | 2.480 | 6.417 | 10.354 | 14.291 | 18.229 |
| 64 | 2.520 | 6.457 | 10.394 | 14.331 | 18.268 |
| 65 | 2.559 | 6.496 | 10.433 | 14.370 | 18.307 |
| 66 | 2.598 | 6.535 | 10.473 | 14.410 | 18.347 |
| 67 | 2.638 | 6.575 | 10.512 | 14.449 | 18.386 |
| 68 | 2.677 | 6.614 | 10.551 | 14.488 | 18.425 |
| 69 | 2.717 | 6.654 | 10.591 | 14.528 | 18.465 |
| 70 | 2.756 | 6.693 | 10.630 | 14.567 | 18.504 |
| 71 | 2.795 | 6.732 | 10.669 | 14.606 | 18.543 |
| 72 | 2.835 | 6.772 | 10.709 | 14.646 | 18.583 |
| 73 | 2.874 | 6.811 | 10.748 | 14.685 | 18.622 |
| 74 | 2.913 | 6.850 | 10.787 | 14.725 | 18.662 |
| 75 | 2.953 | 6.890 | 10.827 | 14.764 | 18.701 |
| 76 | 2.992 | 6.929 | 10.866 | 14.803 | 18.740 |
| 77 | 3.032 | 6.969 | 10.906 | 14.843 | 18.780 |
| 78 | 3.071 | 7.008 | 10.945 | 14.882 | 18.819 |
| 79 | 3.110 | 7.047 | 10.984 | 14.921 | 18.858 |
| 80 | 3.150 | 7.087 | 11.024 | 14.961 | 18.898 |
| 81 | 3.189 | 7.126 | 11.063 | 15.000 | 18.937 |
| 82 | 3.228 | 7.165 | 11.102 | 15.040 | 18.977 |
| 83 | 3.268 | 7.205 | 11.142 | 15.079 | 19.016 |
| 84 | 3.307 | 7.244 | 11.181 | 15.118 | 19.055 |
| 85 | 3.346 | 7.284 | 11.221 | 15.158 | 19.095 |
| 86 | 3.386 | 7.323 | 11.260 | 15.197 | 19.134 |
| 87 | 3.425 | 7.362 | 11.299 | 15.236 | 19.173 |
| 88 | 3.465 | 7.402 | 11.339 | 15.276 | 19.213 |
| 89 | 3.504 | 7.441 | 11.378 | 15.315 | 19.252 |
| 90 | 3.543 | 7.480 | 11.417 | 15.354 | 19.292 |
| 91 | 3.583 | 7.520 | 11.457 | 15.394 | 19.331 |
| 92 | 3.622 | 7.559 | 11.496 | 15.433 | 19.370 |
| 93 | 3.661 | 7.598 | 11.536 | 15.473 | 19.410 |
| 94 | 3.701 | 7.638 | 11.575 | 15.512 | 19.449 |
| 95 | 3.740 | 7.677 | 11.614 | 15.551 | 19.488 |
| 96 | 3.780 | 7.717 | 11.654 | 15.591 | 19.528 |
| 97 | 3.819 | 7.756 | 11.693 | 15.630 | 19.567 |
| 98 | 3.858 | 7.795 | 11.732 | 15.669 | 19.606 |
| 99 | 3.898 | 7.835 | 11.772 | 15.709 | 19.646 |

EQUIVALENTS OF MILLIMETRES IN INCHES.

(Continued)

| Millimetres | 500 | 600 | 700 | 800 | 900 |
|-------------|--------|--------|--------|--------|--------|
| 0 | 19.685 | 23.622 | 27.559 | 31.496 | 35.433 |
| 1 | 19.725 | 23.662 | 27.599 | 31.536 | 35.473 |
| 2 | 19.764 | 23.701 | 27.638 | 31.575 | 35.512 |
| 3 | 19.803 | 23.740 | 27.677 | 31.614 | 35.552 |
| 4 | 19.843 | 23.780 | 27.717 | 31.654 | 35.591 |
| 5 | 19.882 | 23.819 | 27.756 | 31.693 | 35.630 |
| 6 | 19.921 | 23.858 | 27.796 | 31.733 | 35.670 |
| 7 | 19.961 | 23.898 | 27.835 | 31.772 | 35.709 |
| 8 | 20.000 | 23.937 | 27.874 | 31.811 | 35.748 |
| 9 | 20.040 | 23.977 | 27.914 | 31.851 | 35.788 |
| 10 | 20.079 | 24.016 | 27.953 | 31.890 | 35.827 |
| 11 | 20.118 | 24.055 | 27.992 | 31.929 | 35.866 |
| 12 | 20.158 | 24.095 | 28.032 | 31.969 | 35.906 |
| 13 | 20.197 | 24.134 | 28.071 | 32.008 | 35.945 |
| 14 | 20.236 | 24.173 | 28.110 | 32.048 | 35.985 |
| 15 | 20.276 | 24.213 | 28.150 | 32.087 | 36.024 |
| 16 | 20.315 | 24.252 | 28.189 | 32.126 | 36.063 |
| 17 | 20.355 | 24.292 | 28.229 | 32.166 | 36.103 |
| 18 | 20.394 | 24.331 | 28.268 | 32.205 | 36.142 |
| 19 | 20.433 | 24.370 | 28.307 | 32.244 | 36.181 |
| 20 | 20.473 | 24.410 | 28.347 | 32.284 | 36.221 |
| 21 | 20.512 | 24.449 | 28.386 | 32.323 | 36.260 |
| 22 | 20.551 | 24.488 | 28.425 | 32.362 | 36.300 |
| 23 | 20.591 | 24.528 | 28.465 | 32.402 | 36.339 |
| 24 | 20.630 | 24.567 | 28.504 | 32.441 | 36.378 |
| 25 | 20.669 | 24.607 | 28.544 | 32.481 | 36.418 |
| 26 | 20.709 | 24.646 | 28.583 | 32.520 | 36.457 |
| 27 | 20.748 | 24.685 | 28.622 | 32.559 | 36.496 |
| 28 | 20.788 | 24.725 | 28.662 | 32.599 | 36.536 |
| 29 | 20.827 | 24.764 | 28.701 | 32.638 | 36.575 |
| 30 | 20.866 | 24.803 | 28.740 | 32.677 | 36.615 |
| 31 | 20.906 | 24.843 | 28.780 | 32.717 | 36.654 |
| 32 | 20.945 | 24.882 | 28.819 | 32.756 | 36.693 |
| 33 | 20.984 | 24.921 | 28.859 | 32.796 | 36.733 |
| 34 | 21.024 | 24.961 | 28.898 | 32.835 | 36.772 |
| 35 | 21.063 | 25.000 | 28.937 | 32.874 | 36.811 |
| 36 | 21.103 | 25.040 | 28.977 | 32.914 | 36.851 |
| 37 | 21.142 | 25.079 | 29.016 | 32.953 | 36.890 |
| 38 | 21.181 | 25.118 | 29.055 | 32.992 | 36.929 |
| 39 | 21.221 | 25.158 | 29.095 | 33.032 | 36.969 |
| 40 | 21.260 | 25.197 | 29.134 | 33.071 | 37.008 |
| 41 | 21.299 | 25.236 | 29.173 | 33.111 | 37.048 |
| 42 | 21.339 | 25.276 | 29.213 | 33.150 | 37.087 |
| 43 | 21.378 | 25.315 | 29.252 | 33.189 | 37.126 |
| 44 | 21.418 | 25.355 | 29.292 | 33.229 | 37.166 |
| 45 | 21.457 | 25.394 | 29.331 | 33.268 | 37.205 |
| 46 | 21.496 | 25.433 | 29.370 | 33.307 | 37.244 |
| 47 | 21.536 | 25.473 | 29.410 | 33.347 | 37.284 |
| 48 | 21.575 | 25.512 | 29.449 | 33.386 | 37.323 |
| 49 | 21.614 | 25.551 | 29.488 | 33.425 | 37.363 |

EQUIVALENTS OF MILLIMETRES IN INCHES.

(Continued)

| Millimetres | 500 | 600 | 700 | 800 | 900 |
|-------------|--------|--------|--------|--------|--------|
| 50 | 21.654 | 25.591 | 29.528 | 33.465 | 37.402 |
| 51 | 21.693 | 25.630 | 29.567 | 33.504 | 37.441 |
| 52 | 21.732 | 25.670 | 29.607 | 33.544 | 37.481 |
| 53 | 21.772 | 25.709 | 29.646 | 33.583 | 37.520 |
| 54 | 21.811 | 25.748 | 29.685 | 33.622 | 37.559 |
| 55 | 21.851 | 25.788 | 29.725 | 33.662 | 37.599 |
| 56 | 21.890 | 25.827 | 29.764 | 33.701 | 37.638 |
| 57 | 21.929 | 25.866 | 29.803 | 33.740 | 37.677 |
| 58 | 21.969 | 25.906 | 29.843 | 33.780 | 37.717 |
| 59 | 22.008 | 25.945 | 29.882 | 33.819 | 37.756 |
| 60 | 22.047 | 25.984 | 29.922 | 33.859 | 37.796 |
| 61 | 22.087 | 26.024 | 29.961 | 33.898 | 37.835 |
| 62 | 22.126 | 26.063 | 30.000 | 33.937 | 37.874 |
| 63 | 22.166 | 26.103 | 30.040 | 33.977 | 37.914 |
| 64 | 22.205 | 26.142 | 30.079 | 34.016 | 37.953 |
| 65 | 22.244 | 26.181 | 30.118 | 34.055 | 37.992 |
| 66 | 22.284 | 26.221 | 30.158 | 34.095 | 38.032 |
| 67 | 22.323 | 26.260 | 30.197 | 34.134 | 38.071 |
| 68 | 22.362 | 26.299 | 30.236 | 34.174 | 38.111 |
| 69 | 22.402 | 26.339 | 30.276 | 34.213 | 38.150 |
| 70 | 22.441 | 26.378 | 30.315 | 34.252 | 38.189 |
| 71 | 22.481 | 26.418 | 30.355 | 34.292 | 38.229 |
| 72 | 22.520 | 26.457 | 30.394 | 34.331 | 38.268 |
| 73 | 22.559 | 26.496 | 30.433 | 34.370 | 38.307 |
| 74 | 22.599 | 26.536 | 30.473 | 34.410 | 38.347 |
| 75 | 22.638 | 26.575 | 30.512 | 34.449 | 38.386 |
| 76 | 22.677 | 26.614 | 30.551 | 34.488 | 38.426 |
| 77 | 22.717 | 26.654 | 30.591 | 34.528 | 38.465 |
| 78 | 22.756 | 26.693 | 30.630 | 34.567 | 38.504 |
| 79 | 22.795 | 26.733 | 30.670 | 34.607 | 38.544 |
| 80 | 22.835 | 26.772 | 30.709 | 34.646 | 38.583 |
| 81 | 22.874 | 26.811 | 30.748 | 34.685 | 38.622 |
| 82 | 22.914 | 26.851 | 30.788 | 34.725 | 38.662 |
| 83 | 22.953 | 26.890 | 30.827 | 34.764 | 38.701 |
| 84 | 22.992 | 26.929 | 30.866 | 34.803 | 38.741 |
| 85 | 23.032 | 26.969 | 30.906 | 34.843 | 38.780 |
| 86 | 23.071 | 27.008 | 30.945 | 34.882 | 38.819 |
| 87 | 23.110 | 27.047 | 30.985 | 34.922 | 38.859 |
| 88 | 23.150 | 27.087 | 31.024 | 34.961 | 38.898 |
| 89 | 23.189 | 27.126 | 31.063 | 35.000 | 38.937 |
| 90 | 23.229 | 27.166 | 31.103 | 35.040 | 38.977 |
| 91 | 23.268 | 27.205 | 31.142 | 35.079 | 39.016 |
| 92 | 23.307 | 27.244 | 31.181 | 35.118 | 39.055 |
| 93 | 23.347 | 27.284 | 31.221 | 35.158 | 39.095 |
| 94 | 23.385 | 27.323 | 31.260 | 35.197 | 39.134 |
| 95 | 23.424 | 27.362 | 31.299 | 35.237 | 39.174 |
| 96 | 23.464 | 27.402 | 31.339 | 35.276 | 39.213 |
| 97 | 23.503 | 27.441 | 31.378 | 35.315 | 39.252 |
| 98 | 23.543 | 27.481 | 31.418 | 35.355 | 39.292 |
| 99 | 23.582 | 27.520 | 31.457 | 35.394 | 39.331 |

EQUIVALENTS OF FEET IN METRES.

Conversion Factor: 1 foot = 0.3048006096 metre.

| Feet | 0 | 100 | 200 | 300 | 400 |
|------|----------|----------|----------|-----------|-----------|
| 0 | | 30.48006 | 60.96012 | 91.44018 | 121.92024 |
| 1 | .30480 | 30.78486 | 61.26492 | 91.74498 | 122.22504 |
| 2 | .60960 | 31.08966 | 61.56972 | 92.04978 | 122.52985 |
| 3 | .91440 | 31.39446 | 61.87452 | 92.35458 | 122.83465 |
| 4 | 1.21920 | 31.69926 | 62.17932 | 92.65939 | 123.13945 |
| 5 | 1.52400 | 32.00406 | 62.48412 | 92.96419 | 123.44425 |
| 6 | 1.82880 | 32.30886 | 62.78893 | 93.26899 | 123.74905 |
| 7 | 2.13360 | 32.61367 | 63.09373 | 93.57379 | 124.05385 |
| 8 | 2.43840 | 32.91347 | 63.39853 | 93.87859 | 124.35865 |
| 9 | 2.74321 | 33.22327 | 63.70333 | 94.18339 | 124.66345 |
| 10 | 3.04801 | 33.52807 | 64.00813 | 94.48819 | 124.96825 |
| 11 | 3.35281 | 33.83287 | 64.31293 | 94.79299 | 125.27305 |
| 12 | 3.65761 | 34.13767 | 64.61773 | 95.09779 | 125.57785 |
| 13 | 3.96241 | 34.44247 | 64.92253 | 95.40259 | 125.88265 |
| 14 | 4.26721 | 34.74727 | 65.22733 | 95.70739 | 126.18745 |
| 15 | 4.57201 | 35.05207 | 65.53213 | 96.01219 | 126.49225 |
| 16 | 4.87681 | 35.35687 | 65.83693 | 96.31699 | 126.79705 |
| 17 | 5.18161 | 35.66167 | 66.14173 | 96.62179 | 127.10185 |
| 18 | 5.48641 | 35.96647 | 66.44653 | 96.92659 | 127.40665 |
| 19 | 5.79121 | 36.27127 | 66.75133 | 97.23139 | 127.71145 |
| 20 | 6.09601 | 36.57607 | 67.05613 | 97.53620 | 128.01626 |
| 21 | 6.40081 | 36.88087 | 67.36093 | 97.84100 | 128.32106 |
| 22 | 6.70561 | 37.18567 | 67.66574 | 98.14580 | 128.62586 |
| 23 | 7.01041 | 37.49047 | 67.97054 | 98.45060 | 128.93066 |
| 24 | 7.31521 | 37.79528 | 68.27534 | 98.75540 | 129.23546 |
| 25 | 7.62002 | 38.10008 | 68.58014 | 99.06020 | 129.54026 |
| 26 | 7.92482 | 38.40488 | 68.88494 | 99.36500 | 129.84506 |
| 27 | 8.22962 | 38.70968 | 69.18974 | 99.66980 | 130.14986 |
| 28 | 8.53442 | 39.01448 | 69.49454 | 99.97460 | 130.45466 |
| 29 | 8.83922 | 39.31928 | 69.79934 | 100.27940 | 130.75946 |
| 30 | 9.14402 | 39.62408 | 70.10414 | 100.58420 | 131.06426 |
| 31 | 9.44882 | 39.92888 | 70.40894 | 100.88900 | 131.36906 |
| 32 | 9.75362 | 40.23368 | 70.71374 | 101.19380 | 131.67386 |
| 33 | 10.05842 | 40.53848 | 71.01854 | 101.49860 | 131.97866 |
| 34 | 10.36322 | 40.84328 | 71.32334 | 101.80340 | 132.28346 |
| 35 | 10.66802 | 41.14808 | 71.62814 | 102.10820 | 132.58827 |
| 36 | 10.97282 | 41.45288 | 71.93294 | 102.41300 | 132.89307 |
| 37 | 11.27762 | 41.75768 | 72.23774 | 102.71781 | 133.19787 |
| 38 | 11.58242 | 42.06248 | 72.54255 | 103.02261 | 133.50267 |
| 39 | 11.88722 | 42.36728 | 72.84735 | 103.32741 | 133.80747 |
| 40 | 12.19202 | 42.67209 | 73.15215 | 103.63221 | 134.11227 |
| 41 | 12.49682 | 42.97689 | 73.45695 | 103.93701 | 134.41707 |
| 42 | 12.80163 | 43.28169 | 73.76175 | 104.24181 | 134.72187 |
| 43 | 13.10643 | 43.58649 | 74.06655 | 104.54661 | 135.02667 |
| 44 | 13.41123 | 43.89129 | 74.37135 | 104.85141 | 135.33147 |
| 45 | 13.71603 | 44.19609 | 74.67615 | 105.15621 | 135.63627 |
| 46 | 14.02083 | 44.50089 | 74.98095 | 105.46101 | 135.94107 |
| 47 | 14.32563 | 44.80569 | 75.28575 | 105.76581 | 136.24587 |
| 48 | 14.63043 | 45.11049 | 75.59055 | 106.07061 | 136.55067 |
| 49 | 14.93523 | 45.41529 | 75.89535 | 106.37541 | 136.85547 |

1 inch = .02540 metre. 2 inches = .05080 metre. 3 inches = .07620 metre.

EQUIVALENTS OF FEET IN METRES.

(Continued)

| Feet | 0 | 100 | 200 | 300 | 400 |
|------|----------|----------|----------|-----------|-----------|
| 50 | 15.24003 | 45.72009 | 76.20015 | 106.68021 | 137.16027 |
| 51 | 15.54483 | 46.02489 | 76.50495 | 106.98501 | 137.46507 |
| 52 | 15.84963 | 46.32969 | 76.80975 | 107.28981 | 137.76988 |
| 53 | 16.15443 | 46.63449 | 77.11455 | 107.59462 | 138.07468 |
| 54 | 16.45923 | 46.93929 | 77.41935 | 107.89942 | 138.37948 |
| 55 | 16.76403 | 47.24409 | 77.72416 | 108.20422 | 138.68428 |
| 56 | 17.06883 | 47.54890 | 78.02896 | 108.50902 | 138.98908 |
| 57 | 17.37363 | 47.85370 | 78.33376 | 108.81382 | 139.29388 |
| 58 | 17.67844 | 48.15850 | 78.63856 | 109.11862 | 139.59868 |
| 59 | 17.98324 | 48.46330 | 78.94336 | 109.42342 | 139.90348 |
| 60 | 18.28804 | 48.76810 | 79.24816 | 109.72822 | 140.20828 |
| 61 | 18.59284 | 49.07290 | 79.55296 | 110.03302 | 140.51308 |
| 62 | 18.89764 | 49.37770 | 79.85776 | 110.33782 | 140.81788 |
| 63 | 19.20244 | 49.68250 | 80.16256 | 110.64262 | 141.12268 |
| 64 | 19.50724 | 49.98730 | 80.46736 | 110.94742 | 141.42748 |
| 65 | 19.81204 | 50.29210 | 80.77216 | 111.25222 | 141.73228 |
| 66 | 20.11684 | 50.59690 | 81.07696 | 111.55702 | 142.03708 |
| 67 | 20.42164 | 50.90170 | 81.38176 | 111.86182 | 142.34188 |
| 68 | 20.72644 | 51.20650 | 81.68656 | 112.16662 | 142.64669 |
| 69 | 21.03124 | 51.51130 | 81.99136 | 112.47142 | 142.95149 |
| 70 | 21.33604 | 51.81610 | 82.29616 | 112.77623 | 143.25629 |
| 71 | 21.64084 | 52.12090 | 82.60097 | 113.08103 | 143.56109 |
| 72 | 21.94564 | 52.42570 | 82.90577 | 113.38583 | 143.86589 |
| 73 | 22.25044 | 52.73051 | 83.21057 | 113.69063 | 144.17069 |
| 74 | 22.55525 | 53.03531 | 83.51537 | 113.99543 | 144.47549 |
| 75 | 22.86005 | 53.34011 | 83.82017 | 114.30023 | 144.78029 |
| 76 | 23.16485 | 53.64491 | 84.12497 | 114.60503 | 145.08509 |
| 77 | 23.46965 | 53.94971 | 84.42977 | 114.90983 | 145.38989 |
| 78 | 23.77445 | 54.25451 | 84.73457 | 115.21463 | 145.69469 |
| 79 | 24.07925 | 54.55931 | 85.03937 | 115.51943 | 145.99949 |
| 80 | 24.38405 | 54.86411 | 85.34417 | 115.82423 | 146.30429 |
| 81 | 24.68885 | 55.16891 | 85.64897 | 116.12903 | 146.60909 |
| 82 | 24.99365 | 55.47371 | 85.95377 | 116.43383 | 146.91389 |
| 83 | 25.29845 | 55.77851 | 86.25857 | 116.73863 | 147.21869 |
| 84 | 25.60325 | 56.08331 | 86.56337 | 117.04343 | 147.52350 |
| 85 | 25.90805 | 56.38811 | 86.86817 | 117.34823 | 147.82830 |
| 86 | 26.21285 | 56.69291 | 87.17297 | 117.65303 | 148.13310 |
| 87 | 26.51765 | 56.99771 | 87.47777 | 117.95783 | 148.43790 |
| 88 | 26.82245 | 57.30251 | 87.78258 | 118.26264 | 148.74270 |
| 89 | 27.12725 | 57.60732 | 88.08738 | 118.56744 | 149.04750 |
| 90 | 27.43205 | 57.91212 | 88.39218 | 118.87224 | 149.35230 |
| 91 | 27.73686 | 58.21692 | 88.69698 | 119.17704 | 149.65710 |
| 92 | 28.04166 | 58.52172 | 89.00178 | 119.48184 | 149.96190 |
| 93 | 28.34646 | 58.82652 | 89.30658 | 119.78664 | 150.26670 |
| 94 | 28.65126 | 59.13132 | 89.61138 | 120.09144 | 150.57150 |
| 95 | 28.95606 | 59.43612 | 89.91618 | 120.39624 | 150.87630 |
| 96 | 29.26086 | 59.74092 | 90.22098 | 120.70104 | 151.18110 |
| 97 | 29.56566 | 60.04572 | 90.52578 | 121.00584 | 151.48590 |
| 98 | 29.87046 | 60.35052 | 90.83058 | 121.31064 | 151.79070 |
| 99 | 30.17526 | 60.65532 | 91.13538 | 121.61544 | 152.09550 |

4 inches=.10160 metre. 5 inches=.12700 metre. 6 inches=.15240 metre.

EQUIVALENTS OF FEET IN METRES.

(Continued)

| Feet | 500 | 600 | 700 | 800 | 900 |
|------|-----------|-----------|-----------|-----------|-----------|
| 0 | 152.40030 | 182.88037 | 213.36043 | 243.84049 | 274.32055 |
| 1 | 152.70511 | 183.18517 | 213.66523 | 244.14523 | 274.62535 |
| 2 | 153.00991 | 183.48997 | 213.97003 | 244.45009 | 274.93015 |
| 3 | 153.31471 | 183.79477 | 214.27483 | 244.75489 | 275.23495 |
| 4 | 153.61951 | 184.09957 | 214.57963 | 245.05969 | 275.53975 |
| 5 | 153.92431 | 184.40437 | 214.88443 | 245.36449 | 275.84455 |
| 6 | 154.22911 | 184.70917 | 215.18923 | 245.66929 | 276.14935 |
| 7 | 154.53391 | 185.01397 | 215.49403 | 245.97409 | 276.45415 |
| 8 | 154.83871 | 185.31877 | 215.79883 | 246.27889 | 276.75895 |
| 9 | 155.14351 | 185.62357 | 216.10363 | 246.58369 | 277.06375 |
| 10 | 155.44831 | 185.92837 | 216.40843 | 246.88849 | 277.36855 |
| 11 | 155.75311 | 186.23317 | 216.71323 | 247.19329 | 277.67335 |
| 12 | 156.05791 | 186.53797 | 217.01803 | 247.49809 | 277.97815 |
| 13 | 156.36271 | 186.84277 | 217.32283 | 247.80290 | 278.28295 |
| 14 | 156.66751 | 187.14757 | 217.62764 | 248.10770 | 278.58775 |
| 15 | 156.97231 | 187.45237 | 217.93244 | 248.41250 | 278.89255 |
| 16 | 157.27711 | 187.75717 | 218.23724 | 248.71730 | 279.19735 |
| 17 | 157.58192 | 188.06198 | 218.54204 | 249.02210 | 279.50215 |
| 18 | 157.88672 | 188.36678 | 218.84684 | 249.32690 | 279.80695 |
| 19 | 158.19152 | 188.67158 | 219.15164 | 249.63170 | 280.11175 |
| 20 | 158.49632 | 188.97638 | 219.45644 | 249.93650 | 280.41655 |
| 21 | 158.80112 | 189.28118 | 219.76124 | 250.24130 | 280.72135 |
| 22 | 159.10592 | 189.58598 | 220.06604 | 250.54610 | 281.02615 |
| 23 | 159.41072 | 189.89078 | 220.37084 | 250.85090 | 281.33095 |
| 24 | 159.71552 | 190.19558 | 220.67564 | 251.15570 | 281.63575 |
| 25 | 160.02032 | 190.50038 | 220.98044 | 251.46050 | 281.94055 |
| 26 | 160.32512 | 190.80518 | 221.28524 | 251.76530 | 282.24535 |
| 27 | 160.62992 | 191.10998 | 221.59004 | 252.07010 | 282.55015 |
| 28 | 160.93472 | 191.41478 | 221.89484 | 252.37490 | 282.85495 |
| 29 | 161.23952 | 191.71958 | 222.19964 | 252.67971 | 283.15975 |
| 30 | 161.54432 | 192.02438 | 222.50445 | 252.98451 | 283.46455 |
| 31 | 161.84912 | 192.32918 | 222.80925 | 253.28931 | 283.76935 |
| 32 | 162.15392 | 192.63398 | 223.11405 | 253.59411 | 284.07415 |
| 33 | 162.45872 | 192.93878 | 223.41885 | 253.89891 | 284.37895 |
| 34 | 162.76353 | 193.24359 | 223.72365 | 254.20371 | 284.68375 |
| 35 | 163.06833 | 193.54839 | 224.02845 | 254.50851 | 284.98855 |
| 36 | 163.37313 | 193.85319 | 224.33325 | 254.81331 | 285.29335 |
| 37 | 163.67793 | 194.15799 | 224.63805 | 255.11811 | 285.59815 |
| 38 | 163.98273 | 194.46279 | 224.94285 | 255.42291 | 285.90295 |
| 39 | 164.28753 | 194.76759 | 225.24765 | 255.72771 | 286.20775 |
| 40 | 164.59233 | 195.07239 | 225.55245 | 256.03251 | 286.51255 |
| 41 | 164.89713 | 195.37719 | 225.85725 | 256.33731 | 286.81735 |
| 42 | 165.20193 | 195.68199 | 226.16205 | 256.64211 | 287.12215 |
| 43 | 165.50673 | 195.98679 | 226.46685 | 256.94691 | 287.42695 |
| 44 | 165.81153 | 196.29159 | 226.77165 | 257.25171 | 287.73175 |
| 45 | 166.11633 | 196.59639 | 227.07645 | 257.55652 | 288.03655 |
| 46 | 166.42113 | 196.90119 | 227.38125 | 257.86132 | 288.34135 |
| 47 | 166.72593 | 197.20599 | 227.68605 | 258.16612 | 288.64615 |
| 48 | 167.03073 | 197.51080 | 227.99086 | 258.47092 | 288.95095 |
| 49 | 167.33553 | 197.81560 | 228.29566 | 258.77572 | 289.25575 |

7 inches=.17780 metre. 8 inches=.20320 metre. 9 inches=.22860 metre.

EQUIVALENTS OF FEET IN METRES.

(Continued)

| Feet | 500 | 600 | 700 | 800 | 900 |
|------|-----------|-----------|-----------|-----------|-----------|
| 50 | 167.64034 | 198.12040 | 228.60046 | 259.08052 | 289.56058 |
| 51 | 167.94514 | 198.42520 | 228.90526 | 259.38532 | 289.86538 |
| 52 | 168.24994 | 198.73000 | 229.21006 | 259.69012 | 290.17018 |
| 53 | 168.55474 | 199.03480 | 229.51486 | 259.99492 | 290.47498 |
| 54 | 168.85954 | 199.33960 | 229.81966 | 260.29972 | 290.77978 |
| 55 | 169.16434 | 199.64440 | 230.12446 | 260.60452 | 291.08458 |
| 56 | 169.46914 | 199.94920 | 230.42926 | 260.90932 | 291.38938 |
| 57 | 169.77394 | 200.25400 | 230.73406 | 261.21412 | 291.69418 |
| 58 | 170.07874 | 200.55880 | 231.03886 | 261.51892 | 291.99898 |
| 59 | 170.38354 | 200.86360 | 231.34366 | 261.82372 | 292.30378 |
| 60 | 170.68834 | 201.16840 | 231.64846 | 262.12852 | 292.60859 |
| 61 | 170.99314 | 201.47320 | 231.95326 | 262.43332 | 292.91339 |
| 62 | 171.29794 | 201.77800 | 232.25806 | 262.73813 | 293.21819 |
| 63 | 171.60274 | 202.08280 | 232.56287 | 263.04293 | 293.52299 |
| 64 | 171.90754 | 202.38760 | 232.86767 | 263.34773 | 293.82779 |
| 65 | 172.21234 | 202.69241 | 233.17247 | 263.65253 | 294.13259 |
| 66 | 172.51715 | 202.99721 | 233.47727 | 263.95733 | 294.43739 |
| 67 | 172.82195 | 203.30201 | 233.78207 | 264.26213 | 294.74219 |
| 68 | 173.12675 | 203.60681 | 234.08687 | 264.56693 | 295.04699 |
| 69 | 173.43155 | 203.91161 | 234.39167 | 264.87173 | 295.35179 |
| 70 | 173.73635 | 204.21641 | 234.69647 | 265.17653 | 295.65659 |
| 71 | 174.04115 | 204.52121 | 235.00127 | 265.48133 | 295.96139 |
| 72 | 174.34595 | 204.82601 | 235.30607 | 265.78613 | 296.26619 |
| 73 | 174.65075 | 205.13081 | 235.61087 | 266.09093 | 296.57099 |
| 74 | 174.95555 | 205.43561 | 235.91567 | 266.39573 | 296.87579 |
| 75 | 175.26035 | 205.74041 | 236.22047 | 266.70053 | 297.18059 |
| 76 | 175.56515 | 206.04521 | 236.52527 | 267.00533 | 297.48539 |
| 77 | 175.86995 | 206.35001 | 236.83007 | 267.31013 | 297.79020 |
| 78 | 176.17475 | 206.65481 | 237.13487 | 267.61493 | 298.09500 |
| 79 | 176.47955 | 206.95961 | 237.43967 | 267.91974 | 298.39980 |
| 80 | 176.78435 | 207.26441 | 237.74448 | 268.22454 | 298.70460 |
| 81 | 177.08915 | 207.56922 | 238.04928 | 268.52934 | 299.00940 |
| 82 | 177.39395 | 207.87402 | 238.35408 | 268.83414 | 299.31420 |
| 83 | 177.69876 | 208.17882 | 238.65888 | 269.13894 | 299.61900 |
| 84 | 178.00356 | 208.48362 | 238.96368 | 269.44374 | 299.92380 |
| 85 | 178.30836 | 208.78842 | 239.26848 | 269.74854 | 300.22860 |
| 86 | 178.61316 | 209.09322 | 239.57328 | 270.05334 | 300.53340 |
| 87 | 178.91796 | 209.39802 | 239.87808 | 270.35814 | 300.83820 |
| 88 | 179.22276 | 209.70282 | 240.18288 | 270.66294 | 301.14300 |
| 89 | 179.52756 | 210.00762 | 240.48768 | 270.96774 | 301.44780 |
| 90 | 179.83236 | 210.31242 | 240.79248 | 271.27254 | 301.75260 |
| 91 | 180.13716 | 210.61722 | 241.09728 | 271.57734 | 302.05740 |
| 92 | 180.44196 | 210.92202 | 241.40208 | 271.88214 | 302.36220 |
| 93 | 180.74676 | 211.22682 | 241.70688 | 272.18694 | 302.66701 |
| 94 | 181.05156 | 211.53162 | 242.01168 | 272.49174 | 302.97181 |
| 95 | 181.35636 | 211.83642 | 242.31648 | 272.79655 | 303.27661 |
| 96 | 181.66116 | 212.14122 | 242.62129 | 273.10135 | 303.58141 |
| 97 | 181.96596 | 212.44602 | 242.92609 | 273.40615 | 303.88621 |
| 98 | 182.27076 | 212.75082 | 243.23089 | 273.71095 | 304.19101 |
| 99 | 182.57557 | 213.05563 | 243.53569 | 274.01575 | 304.49581 |

10 inches=.25400 metre. 11 inches=.27940 metre. 12 inches=.30480 metre.

EQUIVALENTS OF METRES IN FEET.

Conversion factor: 1 metre=3.28083333 feet.

| Metres | 0 | 100 | 200 | 300 | 400 |
|--------|-----------|-----------|-----------|-------------|-------------|
| 0 | | 328.08333 | 656.16667 | 984.25000 | 1,312.33333 |
| 1 | 3.28083 | 331.36417 | 659.44750 | 987.53083 | 1,315.61417 |
| 2 | 6.56167 | 334.64500 | 662.72833 | 990.81167 | 1,318.89500 |
| 3 | 9.84250 | 337.92583 | 666.00917 | 994.09250 | 1,322.17583 |
| 4 | 13.12333 | 341.20667 | 669.29000 | 997.37333 | 1,325.45667 |
| 5 | 16.40417 | 344.48750 | 672.57083 | 1,000.65417 | 1,328.73750 |
| 6 | 19.68500 | 347.76833 | 675.85167 | 1,003.93500 | 1,332.01833 |
| 7 | 22.96583 | 351.04917 | 679.13250 | 1,007.21583 | 1,335.29917 |
| 8 | 26.24667 | 354.33000 | 682.41333 | 1,010.49667 | 1,338.58000 |
| 9 | 29.52750 | 357.61083 | 685.69417 | 1,013.77750 | 1,341.86083 |
| 10 | 32.80833 | 360.89167 | 688.97500 | 1,017.05833 | 1,345.14167 |
| 11 | 36.08917 | 364.17250 | 692.25583 | 1,020.33917 | 1,348.42250 |
| 12 | 39.37000 | 367.45333 | 695.53667 | 1,023.62000 | 1,351.70333 |
| 13 | 42.65083 | 370.73417 | 698.81750 | 1,026.90083 | 1,354.98417 |
| 14 | 45.93167 | 374.01500 | 702.09833 | 1,030.18167 | 1,358.26500 |
| 15 | 49.21250 | 377.29583 | 705.37917 | 1,033.46250 | 1,361.54583 |
| 16 | 52.49333 | 380.57667 | 708.66000 | 1,036.74333 | 1,364.82667 |
| 17 | 55.77417 | 383.85750 | 711.94083 | 1,040.02417 | 1,368.10750 |
| 18 | 59.05500 | 387.13833 | 715.22167 | 1,043.30500 | 1,371.38833 |
| 19 | 62.33583 | 390.41917 | 718.50250 | 1,046.58583 | 1,374.66917 |
| 20 | 65.61667 | 393.70000 | 721.78333 | 1,049.86667 | 1,377.95000 |
| 21 | 68.89750 | 396.98083 | 725.06417 | 1,053.14750 | 1,381.23083 |
| 22 | 72.17833 | 400.26167 | 728.34500 | 1,056.42833 | 1,384.51167 |
| 23 | 75.45917 | 403.54250 | 731.62583 | 1,059.70917 | 1,387.79250 |
| 24 | 78.74000 | 406.82333 | 734.90667 | 1,062.99000 | 1,391.07333 |
| 25 | 82.02083 | 410.10417 | 738.18750 | 1,066.27083 | 1,394.35417 |
| 26 | 85.30167 | 413.38500 | 741.46833 | 1,069.55167 | 1,397.63500 |
| 27 | 88.58250 | 416.66583 | 744.74917 | 1,072.83250 | 1,400.91583 |
| 28 | 91.86333 | 419.94667 | 748.03000 | 1,076.11333 | 1,404.19667 |
| 29 | 95.14417 | 423.22750 | 751.31083 | 1,079.39417 | 1,407.47750 |
| 30 | 98.42500 | 426.50833 | 754.59167 | 1,082.67500 | 1,410.75833 |
| 31 | 101.70583 | 429.78917 | 757.87250 | 1,085.95583 | 1,414.03917 |
| 32 | 104.98667 | 433.07000 | 761.15333 | 1,089.23667 | 1,417.32000 |
| 33 | 108.26750 | 436.35083 | 764.43417 | 1,092.51750 | 1,420.60083 |
| 34 | 111.54833 | 439.63167 | 767.71500 | 1,095.79833 | 1,423.88167 |
| 35 | 114.82917 | 442.91250 | 770.99583 | 1,099.07917 | 1,427.16250 |
| 36 | 118.11000 | 446.19333 | 774.27667 | 1,102.36000 | 1,430.44333 |
| 37 | 121.39083 | 449.47417 | 777.55750 | 1,105.64083 | 1,433.72417 |
| 38 | 124.67167 | 452.75500 | 780.83833 | 1,108.92167 | 1,437.00500 |
| 39 | 127.95250 | 456.03583 | 784.11917 | 1,112.20250 | 1,440.28583 |
| 40 | 131.23333 | 459.31667 | 787.40000 | 1,115.48333 | 1,443.56667 |
| 41 | 134.51417 | 462.59750 | 790.68083 | 1,118.76417 | 1,446.84750 |
| 42 | 137.79500 | 465.87833 | 793.96167 | 1,122.04500 | 1,450.12833 |
| 43 | 141.07583 | 469.15917 | 797.24250 | 1,125.32583 | 1,453.40917 |
| 44 | 144.35667 | 472.44000 | 800.52333 | 1,128.60667 | 1,456.69000 |
| 45 | 147.63750 | 475.72083 | 803.80417 | 1,131.88750 | 1,459.97083 |
| 46 | 150.91833 | 479.00167 | 807.08500 | 1,135.16833 | 1,463.25167 |
| 47 | 154.19917 | 482.28250 | 810.36583 | 1,138.44917 | 1,466.53250 |
| 48 | 157.48000 | 485.56333 | 813.64667 | 1,141.73000 | 1,469.81333 |
| 49 | 160.76083 | 488.84417 | 816.92750 | 1,145.01083 | 1,473.09417 |

EQUIVALENTS OF METRES IN FEET.

(Continued)

| Metres | 0 | 100 | 200 | 300 | 400 |
|--------|-----------|-----------|-----------|-------------|-------------|
| 50 | 164.04167 | 492.12500 | 820.20833 | 1,148.29167 | 1,476.37500 |
| 51 | 167.32250 | 495.40583 | 823.45917 | 1,151.57250 | 1,479.65583 |
| 52 | 170.60333 | 498.68667 | 826.77000 | 1,154.85333 | 1,482.93667 |
| 53 | 173.88417 | 501.96750 | 830.05083 | 1,158.13417 | 1,486.21750 |
| 54 | 177.16500 | 505.24833 | 833.33167 | 1,161.41500 | 1,489.49833 |
| 55 | 180.44583 | 508.52917 | 836.61250 | 1,164.69583 | 1,492.77917 |
| 56 | 183.72667 | 511.81000 | 839.89333 | 1,167.97667 | 1,496.06000 |
| 57 | 187.00750 | 515.09083 | 843.17417 | 1,171.25750 | 1,499.34083 |
| 58 | 190.28833 | 518.37167 | 846.45500 | 1,174.53833 | 1,502.62167 |
| 59 | 193.56917 | 521.65250 | 849.73583 | 1,177.81917 | 1,505.90250 |
| 60 | 196.85000 | 524.93333 | 853.01667 | 1,181.10000 | 1,509.18333 |
| 61 | 200.13083 | 528.21417 | 856.29750 | 1,184.38083 | 1,512.46417 |
| 62 | 203.41167 | 531.49500 | 859.57833 | 1,187.66167 | 1,515.74500 |
| 63 | 206.69250 | 534.77583 | 862.85917 | 1,190.94250 | 1,519.02583 |
| 64 | 209.97333 | 538.05667 | 866.14000 | 1,194.22333 | 1,522.30667 |
| 65 | 213.25417 | 541.33750 | 869.42083 | 1,197.50417 | 1,525.58750 |
| 66 | 216.53500 | 544.61833 | 872.70167 | 1,200.78500 | 1,528.86833 |
| 67 | 219.81583 | 547.89917 | 875.98250 | 1,204.06583 | 1,532.14917 |
| 68 | 223.09667 | 551.18000 | 879.26333 | 1,207.34667 | 1,535.43000 |
| 69 | 226.37750 | 554.46083 | 882.54417 | 1,210.62750 | 1,538.71083 |
| 70 | 229.65833 | 557.74167 | 885.82500 | 1,213.90833 | 1,541.99167 |
| 71 | 232.93917 | 561.02250 | 889.10583 | 1,217.18917 | 1,545.27250 |
| 72 | 236.22000 | 564.30333 | 892.38667 | 1,220.47000 | 1,548.55333 |
| 73 | 239.50083 | 567.58417 | 895.66750 | 1,223.75083 | 1,551.83417 |
| 74 | 242.78167 | 570.86500 | 898.94833 | 1,227.03167 | 1,555.11500 |
| 75 | 246.06250 | 574.14583 | 902.22917 | 1,230.31250 | 1,558.39583 |
| 76 | 249.34333 | 577.42667 | 905.51000 | 1,233.59333 | 1,561.67667 |
| 77 | 252.62417 | 580.70750 | 908.79083 | 1,236.87417 | 1,564.95750 |
| 78 | 255.90500 | 583.98833 | 912.07167 | 1,240.15500 | 1,568.23833 |
| 79 | 259.18583 | 587.26917 | 915.35250 | 1,243.43583 | 1,571.51917 |
| 80 | 262.46667 | 590.55000 | 918.63333 | 1,246.71667 | 1,574.80000 |
| 81 | 265.74750 | 593.83083 | 921.91417 | 1,249.99750 | 1,578.08083 |
| 82 | 269.02833 | 597.11167 | 925.19500 | 1,253.27833 | 1,581.36167 |
| 83 | 272.30917 | 600.39250 | 928.47583 | 1,256.55917 | 1,584.64250 |
| 84 | 275.59000 | 603.67333 | 931.75667 | 1,259.84000 | 1,587.92333 |
| 85 | 278.87083 | 606.95417 | 935.03750 | 1,263.12083 | 1,591.20417 |
| 86 | 282.15167 | 610.23500 | 938.31833 | 1,266.40167 | 1,594.48500 |
| 87 | 285.43250 | 613.51583 | 941.59917 | 1,269.68250 | 1,597.76583 |
| 88 | 288.71333 | 616.79667 | 944.88000 | 1,272.96333 | 1,601.04667 |
| 89 | 291.99417 | 620.07750 | 948.16083 | 1,276.24417 | 1,604.32750 |
| 90 | 295.27500 | 623.35833 | 951.44167 | 1,279.52500 | 1,607.60833 |
| 91 | 298.55583 | 626.63917 | 954.72250 | 1,282.80583 | 1,610.88917 |
| 92 | 301.83667 | 629.92000 | 958.00333 | 1,286.08667 | 1,614.17000 |
| 93 | 305.11750 | 633.20083 | 961.28417 | 1,289.36750 | 1,617.45083 |
| 94 | 308.39833 | 636.48167 | 964.56500 | 1,292.64833 | 1,620.73167 |
| 95 | 311.67917 | 639.76250 | 967.84583 | 1,295.92917 | 1,624.01250 |
| 96 | 314.96000 | 643.04333 | 971.12667 | 1,299.21000 | 1,627.29333 |
| 97 | 318.24083 | 646.32417 | 974.40750 | 1,302.49083 | 1,630.57417 |
| 98 | 321.52167 | 649.60500 | 977.68833 | 1,305.77167 | 1,633.85500 |
| 99 | 324.80250 | 652.88583 | 980.96917 | 1,309.05250 | 1,637.13583 |

EQUIVALENTS OF METRES IN FEET.

(Continued)

| Metres | 500 | 600 | 700 | 800 | 900 |
|--------|-------------|-------------|-------------|-------------|-------------|
| 0 | 1,640.41667 | 1,968.50000 | 2,296.58333 | 2,624.66667 | 2,952.75000 |
| 1 | 1,643.69760 | 1,971.78083 | 2,299.86417 | 2,627.94750 | 2,956.03083 |
| 2 | 1,646.97833 | 1,975.06167 | 2,303.14500 | 2,631.22833 | 2,959.31167 |
| 3 | 1,650.25917 | 1,978.34250 | 2,306.42583 | 2,634.50917 | 2,962.59250 |
| 4 | 1,653.54000 | 1,981.62333 | 2,309.70667 | 2,637.79000 | 2,965.87333 |
| 5 | 1,656.82083 | 1,984.90417 | 2,312.98750 | 2,641.07083 | 2,969.15417 |
| 6 | 1,660.10167 | 1,988.18500 | 2,316.26833 | 2,644.35167 | 2,972.43500 |
| 7 | 1,663.38250 | 1,991.46583 | 2,319.54917 | 2,647.63250 | 2,975.71583 |
| 8 | 1,666.66333 | 1,994.74667 | 2,322.83000 | 2,650.91333 | 2,978.99667 |
| 9 | 1,669.94417 | 1,998.02750 | 2,326.11083 | 2,654.19417 | 2,982.27750 |
| 10 | 1,673.22500 | 2,001.30833 | 2,329.39167 | 2,657.47500 | 2,985.55833 |
| 11 | 1,676.50583 | 2,004.58917 | 2,332.67250 | 2,660.75583 | 2,988.83917 |
| 12 | 1,679.78667 | 2,007.87000 | 2,335.95333 | 2,664.03667 | 2,992.12000 |
| 13 | 1,683.06750 | 2,011.15083 | 2,339.23417 | 2,667.31750 | 2,995.40083 |
| 14 | 1,686.34833 | 2,014.43167 | 2,342.51500 | 2,670.59833 | 2,998.68167 |
| 15 | 1,689.62917 | 2,017.71250 | 2,345.79583 | 2,673.87917 | 3,001.96250 |
| 16 | 1,692.91000 | 2,020.99333 | 2,349.07667 | 2,677.16000 | 3,005.24333 |
| 17 | 1,696.19083 | 2,024.27417 | 2,352.35750 | 2,680.44083 | 3,008.52417 |
| 18 | 1,699.47167 | 2,027.55500 | 2,355.63833 | 2,683.72167 | 3,011.80500 |
| 19 | 1,702.75250 | 2,030.83583 | 2,358.91917 | 2,687.00250 | 3,015.08583 |
| 20 | 1,706.03333 | 2,034.11667 | 2,362.20000 | 2,690.28333 | 3,018.36667 |
| 21 | 1,709.31417 | 2,037.39750 | 2,365.48083 | 2,693.56417 | 3,021.64750 |
| 22 | 1,712.59500 | 2,040.67833 | 2,368.76167 | 2,696.84500 | 3,024.92833 |
| 23 | 1,715.87583 | 2,043.95917 | 2,372.04250 | 2,700.12583 | 3,028.20917 |
| 24 | 1,719.15667 | 2,047.24000 | 2,375.32333 | 2,703.40667 | 3,031.49000 |
| 25 | 1,722.43750 | 2,050.52083 | 2,378.60417 | 2,706.68750 | 3,034.77083 |
| 26 | 1,725.71833 | 2,053.80167 | 2,381.88500 | 2,709.96833 | 3,038.05167 |
| 27 | 1,728.99917 | 2,057.08250 | 2,385.16583 | 2,713.24917 | 3,041.33250 |
| 28 | 1,732.28000 | 2,060.36333 | 2,388.44667 | 2,716.53000 | 3,044.61333 |
| 29 | 1,735.56083 | 2,063.64417 | 2,391.72750 | 2,719.81083 | 3,047.89417 |
| 30 | 1,738.84167 | 2,066.92500 | 2,395.00833 | 2,723.09167 | 3,051.17500 |
| 31 | 1,742.12250 | 2,070.20583 | 2,398.28917 | 2,726.37250 | 3,054.45583 |
| 32 | 1,745.40333 | 2,073.48667 | 2,401.57000 | 2,729.65333 | 3,057.73667 |
| 33 | 1,748.68417 | 2,076.76750 | 2,404.85083 | 2,732.93417 | 3,061.01750 |
| 34 | 1,751.96500 | 2,080.04833 | 2,408.13167 | 2,736.21500 | 3,064.29833 |
| 35 | 1,755.24583 | 2,083.32917 | 2,411.41250 | 2,739.49583 | 3,067.57917 |
| 36 | 1,758.52667 | 2,086.61000 | 2,414.69333 | 2,742.77667 | 3,070.86000 |
| 37 | 1,761.80750 | 2,089.89083 | 2,417.97417 | 2,746.05750 | 3,074.14083 |
| 38 | 1,765.08833 | 2,093.17167 | 2,421.25500 | 2,749.33833 | 3,077.42167 |
| 39 | 1,768.36917 | 2,096.45250 | 2,424.53583 | 2,752.61917 | 3,080.70250 |
| 40 | 1,771.65000 | 2,099.73333 | 2,427.81667 | 2,755.90000 | 3,083.98333 |
| 41 | 1,774.93083 | 2,103.01417 | 2,431.09750 | 2,759.18083 | 3,087.26417 |
| 42 | 1,778.21167 | 2,106.29500 | 2,434.37833 | 2,762.46167 | 3,090.54500 |
| 43 | 1,781.49250 | 2,109.57583 | 2,437.65917 | 2,765.74250 | 3,093.82583 |
| 44 | 1,784.77333 | 2,112.85667 | 2,440.94000 | 2,769.02333 | 3,097.10667 |
| 45 | 1,788.05417 | 2,116.13750 | 2,444.22083 | 2,772.30417 | 3,100.38750 |
| 46 | 1,791.33500 | 2,119.41833 | 2,447.50167 | 2,775.58500 | 3,103.66833 |
| 47 | 1,794.61583 | 2,122.69917 | 2,450.78250 | 2,778.86583 | 3,106.94917 |
| 48 | 1,797.89667 | 2,125.98000 | 2,454.06333 | 2,782.14667 | 3,110.23000 |
| 49 | 1,801.17750 | 2,129.26083 | 2,457.34417 | 2,785.42750 | 3,113.51083 |

EQUIVALENTS OF METRES IN FEET.

(Continued)

| Metres | 500 | 600 | 700 | 800 | 900 |
|--------|-------------|-------------|-------------|-------------|-------------|
| 50 | 1,804.45833 | 2,132.54167 | 2,460.62500 | 2,788.70833 | 3,116.79167 |
| 51 | 1,807.73917 | 2,135.82250 | 2,463.90583 | 2,791.98917 | 3,120.07250 |
| 52 | 1,811.02000 | 2,139.10333 | 2,467.18667 | 2,795.27000 | 3,123.35333 |
| 53 | 1,814.30083 | 2,142.38417 | 2,470.46750 | 2,798.55083 | 3,126.63417 |
| 54 | 1,817.58167 | 2,145.66500 | 2,473.74833 | 2,801.83167 | 3,129.91500 |
| 55 | 1,820.86250 | 2,148.94583 | 2,477.02917 | 2,805.11250 | 3,133.19583 |
| 56 | 1,824.14333 | 2,152.22667 | 2,480.31000 | 2,808.39333 | 3,136.47667 |
| 57 | 1,827.42417 | 2,155.50750 | 2,483.59083 | 2,811.67417 | 3,139.75750 |
| 58 | 1,830.70500 | 2,158.78833 | 2,486.87167 | 2,814.95500 | 3,143.03833 |
| 59 | 1,833.98583 | 2,162.06917 | 2,490.15250 | 2,818.23583 | 3,146.31917 |
| 60 | 1,837.26667 | 2,165.35000 | 2,493.43333 | 2,821.51667 | 3,149.60000 |
| 61 | 1,840.54750 | 2,168.63083 | 2,496.71417 | 2,824.79750 | 3,152.88083 |
| 62 | 1,843.82833 | 2,171.91167 | 2,499.99500 | 2,828.07833 | 3,156.16167 |
| 63 | 1,847.10917 | 2,175.19250 | 2,503.27583 | 2,831.35917 | 3,159.44250 |
| 64 | 1,850.39000 | 2,178.47333 | 2,506.55667 | 2,834.64000 | 3,162.72333 |
| 65 | 1,853.67083 | 2,181.75417 | 2,509.83750 | 2,837.92083 | 3,166.00417 |
| 66 | 1,856.95167 | 2,185.03500 | 2,513.11833 | 2,841.20167 | 3,169.28500 |
| 67 | 1,860.23250 | 2,188.31583 | 2,516.39917 | 2,844.48250 | 3,172.56583 |
| 68 | 1,863.51333 | 2,191.59667 | 2,519.68000 | 2,847.76333 | 3,175.84667 |
| 69 | 1,866.79417 | 2,194.87750 | 2,522.96083 | 2,851.04417 | 3,179.12750 |
| 70 | 1,870.07500 | 2,198.15833 | 2,526.24167 | 2,854.32500 | 3,182.40833 |
| 71 | 1,873.35583 | 2,201.43917 | 2,529.52250 | 2,857.60583 | 3,185.68917 |
| 72 | 1,876.63667 | 2,204.72000 | 2,532.80333 | 2,860.88667 | 3,188.97000 |
| 73 | 1,879.91750 | 2,208.00083 | 2,536.08417 | 2,864.16750 | 3,192.25083 |
| 74 | 1,883.19833 | 2,211.28167 | 2,539.36500 | 2,867.44833 | 3,195.53167 |
| 75 | 1,886.47917 | 2,214.56250 | 2,542.64583 | 2,870.72917 | 3,198.81250 |
| 76 | 1,889.76000 | 2,217.84333 | 2,545.92667 | 2,874.01000 | 3,202.09333 |
| 77 | 1,893.04083 | 2,221.12417 | 2,549.20750 | 2,877.29083 | 3,205.37417 |
| 78 | 1,896.32167 | 2,224.40500 | 2,552.48833 | 2,880.57167 | 3,208.65500 |
| 79 | 1,899.60250 | 2,227.68583 | 2,555.76917 | 2,883.85250 | 3,211.93583 |
| 80 | 1,902.88333 | 2,230.96667 | 2,559.05000 | 2,887.13333 | 3,215.21667 |
| 81 | 1,906.16417 | 2,234.24750 | 2,562.33083 | 2,890.41417 | 3,218.49750 |
| 82 | 1,909.44500 | 2,237.52833 | 2,565.61167 | 2,893.69500 | 3,221.77833 |
| 83 | 1,912.72583 | 2,240.80917 | 2,568.89250 | 2,896.97583 | 3,225.05917 |
| 84 | 1,916.00667 | 2,244.09000 | 2,572.17333 | 2,900.25667 | 3,228.34000 |
| 85 | 1,919.28750 | 2,247.37083 | 2,575.45417 | 2,903.53750 | 3,231.62083 |
| 86 | 1,922.56833 | 2,250.65167 | 2,578.73500 | 2,906.81833 | 3,234.90167 |
| 87 | 1,925.84917 | 2,253.93250 | 2,582.01583 | 2,910.09917 | 3,238.18250 |
| 88 | 1,929.13000 | 2,257.21333 | 2,585.29667 | 2,913.38000 | 3,241.46333 |
| 89 | 1,932.41083 | 2,260.49417 | 2,588.57750 | 2,916.66083 | 3,244.74417 |
| 90 | 1,935.69167 | 2,263.77500 | 2,591.85833 | 2,919.94167 | 3,248.02500 |
| 91 | 1,938.97250 | 2,267.05583 | 2,595.13917 | 2,923.22250 | 3,251.30583 |
| 92 | 1,942.25333 | 2,270.33667 | 2,598.42000 | 2,926.50333 | 3,254.58667 |
| 93 | 1,945.53417 | 2,273.61750 | 2,601.70083 | 2,929.78417 | 3,257.86750 |
| 94 | 1,948.81500 | 2,276.89833 | 2,604.98167 | 2,933.06500 | 3,261.14833 |
| 95 | 1,952.09583 | 2,280.17917 | 2,608.26250 | 2,936.34583 | 3,264.42917 |
| 96 | 1,955.37667 | 2,283.46000 | 2,611.54333 | 2,939.62667 | 3,267.71000 |
| 97 | 1,958.65750 | 2,286.74083 | 2,614.82417 | 2,942.90750 | 3,270.99083 |
| 98 | 1,961.93833 | 2,290.02167 | 2,618.10500 | 2,946.18833 | 3,274.27167 |
| 99 | 1,965.21917 | 2,293.30250 | 2,621.38583 | 2,949.46917 | 3,277.55250 |

EQUIVALENTS OF AVOIRDUPOIS POUNDS IN KILOGRAMS.

Conversion Factor: 1 avoirdupois pound = 0.4535924277 kilogram.

| Pounds | 0 | 100 | 200 | 300 | 400 |
|--------|----------|----------|-----------|-----------|-----------|
| 0 | | 45.35924 | 90.71849 | 136.07773 | 181.43697 |
| 1 | .45359 | 45.81284 | 91.17208 | 136.53132 | 181.89056 |
| 2 | .90718 | 46.26643 | 91.62567 | 136.98491 | 182.34416 |
| 3 | 1.36078 | 46.72002 | 92.07926 | 137.43851 | 182.79775 |
| 4 | 1.81437 | 47.17361 | 92.53286 | 137.89210 | 183.25134 |
| 5 | 2.26796 | 47.62720 | 92.98645 | 138.34569 | 183.70493 |
| 6 | 2.72155 | 48.08080 | 93.44004 | 138.79928 | 184.15853 |
| 7 | 3.17515 | 48.53439 | 93.89363 | 139.25288 | 184.61212 |
| 8 | 3.62874 | 48.98798 | 94.34722 | 139.70647 | 185.06571 |
| 9 | 4.08233 | 49.44157 | 94.80082 | 140.16006 | 185.51930 |
| 10 | 4.53592 | 49.89517 | 95.25441 | 140.61365 | 185.97290 |
| 11 | 4.98952 | 50.34876 | 95.70800 | 141.06725 | 186.42649 |
| 12 | 5.44311 | 50.80235 | 96.16159 | 141.52084 | 186.88008 |
| 13 | 5.89670 | 51.25594 | 96.61519 | 141.97443 | 187.33367 |
| 14 | 6.35029 | 51.70954 | 97.06878 | 142.42802 | 187.78727 |
| 15 | 6.80389 | 52.16313 | 97.52237 | 142.88161 | 188.24086 |
| 16 | 7.25748 | 52.61672 | 97.97596 | 143.33521 | 188.69445 |
| 17 | 7.71107 | 53.07031 | 98.42956 | 143.78880 | 189.14804 |
| 18 | 8.16466 | 53.52391 | 98.88315 | 144.24239 | 189.60163 |
| 19 | 8.61826 | 53.97750 | 99.33674 | 144.69598 | 190.05523 |
| 20 | 9.07185 | 54.43109 | 99.79033 | 145.14958 | 190.50882 |
| 21 | 9.52544 | 54.88468 | 100.24393 | 145.60317 | 190.96241 |
| 22 | 9.97903 | 55.33828 | 100.69752 | 146.05676 | 191.41600 |
| 23 | 10.43263 | 55.79187 | 101.15111 | 146.51035 | 191.86960 |
| 24 | 10.88622 | 56.24546 | 101.60470 | 146.96395 | 192.32319 |
| 25 | 11.33981 | 56.69905 | 102.05830 | 147.41754 | 192.77678 |
| 26 | 11.79340 | 57.15265 | 102.51189 | 147.87113 | 193.23037 |
| 27 | 12.24700 | 57.60624 | 102.96548 | 148.32472 | 193.68397 |
| 28 | 12.70059 | 58.05983 | 103.41907 | 148.77832 | 194.13756 |
| 29 | 13.15418 | 58.51342 | 103.87267 | 149.23191 | 194.59115 |
| 30 | 13.60777 | 58.96702 | 104.32626 | 149.68550 | 195.04474 |
| 31 | 14.06137 | 59.42061 | 104.77985 | 150.13909 | 195.49834 |
| 32 | 14.51496 | 59.87420 | 105.23344 | 150.59269 | 195.95193 |
| 33 | 14.96855 | 60.32779 | 105.68704 | 151.04628 | 196.40552 |
| 34 | 15.42214 | 60.78139 | 106.14063 | 151.49987 | 196.85911 |
| 35 | 15.87573 | 61.23498 | 106.59422 | 151.95346 | 197.31271 |
| 36 | 16.32933 | 61.68857 | 107.04781 | 152.40706 | 197.76630 |
| 37 | 16.78292 | 62.14216 | 107.50141 | 152.86065 | 198.21989 |
| 38 | 17.23651 | 62.59576 | 107.95500 | 153.31424 | 198.67348 |
| 39 | 17.69010 | 63.04935 | 108.40859 | 153.76783 | 199.12708 |
| 40 | 18.14370 | 63.50294 | 108.86218 | 154.22143 | 199.58067 |
| 41 | 18.59729 | 63.95653 | 109.31578 | 154.67502 | 200.03426 |
| 42 | 19.05088 | 64.41012 | 109.76937 | 155.12861 | 200.48785 |
| 43 | 19.50447 | 64.86372 | 110.22296 | 155.58220 | 200.94145 |
| 44 | 19.95807 | 65.31731 | 110.67655 | 156.03580 | 201.39504 |
| 45 | 20.41166 | 65.77090 | 111.13014 | 156.48939 | 201.84863 |
| 46 | 20.86525 | 66.22449 | 111.58374 | 156.94298 | 202.30222 |
| 47 | 21.31884 | 66.67809 | 112.03733 | 157.39657 | 202.75582 |
| 48 | 21.77244 | 67.13168 | 112.49092 | 157.85016 | 203.20941 |
| 49 | 22.22603 | 67.58527 | 112.94451 | 158.30376 | 203.66300 |

1 oz. = .028350 kg. 2 oz. = .056699 kg. 3 oz. = .085049 kg. 4 oz. = .113398 kg.

EQUIVALENTS OF AVOIRDUPOIS POUNDS IN KILOGRAMS.

(Continued)

| Pounds | 0 | 100 | 200 | 300 | 400 |
|--------|----------|----------|-----------|-----------|-----------|
| 50 | 22.67962 | 68.03886 | 113.39811 | 158.75735 | 204.11659 |
| 51 | 23.13321 | 68.49246 | 113.85170 | 159.21094 | 204.57018 |
| 52 | 23.58681 | 68.94605 | 114.30529 | 159.66453 | 205.02378 |
| 53 | 24.04040 | 69.39964 | 114.75888 | 160.11813 | 205.47737 |
| 54 | 24.49399 | 69.85323 | 115.21248 | 160.57172 | 205.93096 |
| 55 | 24.94758 | 70.30683 | 115.66607 | 161.02531 | 206.38455 |
| 56 | 25.40118 | 70.76042 | 116.11966 | 161.47890 | 206.83815 |
| 57 | 25.85477 | 71.21401 | 116.57325 | 161.93250 | 207.29174 |
| 58 | 26.30836 | 71.66760 | 117.02685 | 162.38609 | 207.74533 |
| 59 | 26.76195 | 72.12120 | 117.48044 | 162.83968 | 208.19892 |
| 60 | 27.21555 | 72.57479 | 117.93403 | 163.29327 | 208.65252 |
| 61 | 27.66914 | 73.02838 | 118.38762 | 163.74687 | 209.10611 |
| 62 | 28.12273 | 73.48197 | 118.84122 | 164.20046 | 209.55970 |
| 63 | 28.57632 | 73.93557 | 119.29481 | 164.65405 | 210.01329 |
| 64 | 29.02992 | 74.38916 | 119.74840 | 165.10764 | 210.46689 |
| 65 | 29.48351 | 74.84275 | 120.20199 | 165.56124 | 210.92048 |
| 66 | 29.93710 | 75.29634 | 120.65559 | 166.01483 | 211.37407 |
| 67 | 30.39069 | 75.74994 | 121.10918 | 166.46842 | 211.82766 |
| 68 | 30.84429 | 76.20353 | 121.56277 | 166.92201 | 212.28126 |
| 69 | 31.29788 | 76.65712 | 122.01636 | 167.37561 | 212.73485 |
| 70 | 31.75147 | 77.11071 | 122.46996 | 167.82920 | 213.18844 |
| 71 | 32.20506 | 77.56431 | 122.92355 | 168.28279 | 213.64203 |
| 72 | 32.65865 | 78.01790 | 123.37714 | 168.73638 | 214.09563 |
| 73 | 33.11225 | 78.47149 | 123.83073 | 169.18998 | 214.54922 |
| 74 | 33.56584 | 78.92509 | 124.28433 | 169.64357 | 215.00281 |
| 75 | 34.01943 | 79.37867 | 124.73792 | 170.09716 | 215.45640 |
| 76 | 34.47302 | 79.83227 | 125.19151 | 170.55075 | 215.91000 |
| 77 | 34.92662 | 80.28586 | 125.64510 | 171.00435 | 216.36359 |
| 78 | 35.38021 | 80.73945 | 126.09869 | 171.45794 | 216.81718 |
| 79 | 35.83380 | 81.19304 | 126.55229 | 171.91153 | 217.27077 |
| 80 | 36.28739 | 81.64664 | 127.00588 | 172.36512 | 217.72437 |
| 81 | 36.74099 | 82.10023 | 127.45947 | 172.81871 | 218.17796 |
| 82 | 37.19458 | 82.55382 | 127.91306 | 173.27231 | 218.63155 |
| 83 | 37.64817 | 83.00741 | 128.36666 | 173.72590 | 219.08514 |
| 84 | 38.10176 | 83.46101 | 128.82025 | 174.17949 | 219.53874 |
| 85 | 38.55536 | 83.91460 | 129.27384 | 174.63308 | 219.99233 |
| 86 | 39.00895 | 84.36819 | 129.72743 | 175.08668 | 220.44592 |
| 87 | 39.46254 | 84.82178 | 130.18103 | 175.54027 | 220.89951 |
| 88 | 39.91613 | 85.27538 | 130.63462 | 175.99386 | 221.35310 |
| 89 | 40.36973 | 85.72897 | 131.08821 | 176.44745 | 221.80670 |
| 90 | 40.82332 | 86.18256 | 131.54180 | 176.90105 | 222.26029 |
| 91 | 41.27691 | 86.63615 | 131.99540 | 177.35464 | 222.71388 |
| 92 | 41.73050 | 87.08975 | 132.44899 | 177.80823 | 223.16747 |
| 93 | 42.18410 | 87.54334 | 132.90258 | 178.26182 | 223.62107 |
| 94 | 42.63769 | 87.99693 | 133.35617 | 178.71542 | 224.07466 |
| 95 | 43.09128 | 88.45052 | 133.80977 | 179.16901 | 224.52825 |
| 96 | 43.54487 | 88.90412 | 134.26336 | 179.62260 | 224.98184 |
| 97 | 43.99847 | 89.35771 | 134.71695 | 180.07619 | 225.43544 |
| 98 | 44.45206 | 89.81130 | 135.17054 | 180.52979 | 225.88903 |
| 99 | 44.90565 | 90.26489 | 135.62414 | 180.98338 | 226.34262 |

5 oz.=.141748 kg. 6 oz.=.170997 kg. 7 oz.=.198447 kg. 8 oz.=.226796 kg.

EQUIVALENTS OF AVOIRDUPOIS POUNDS IN KILOGRAMS.

(Continued)

| Pounds | 500 | 600 | 700 | 800 | 900 |
|--------|-----------|-----------|-----------|-----------|-----------|
| 0 | 226.79621 | 272.15546 | 317.51470 | 362.87394 | 408.23318 |
| 1 | 227.24981 | 272.60905 | 317.96829 | 363.32753 | 408.68678 |
| 2 | 227.70340 | 273.06264 | 318.42188 | 363.78113 | 409.14037 |
| 3 | 228.15699 | 273.51623 | 318.87548 | 364.23472 | 409.59396 |
| 4 | 228.61058 | 273.96983 | 319.32907 | 364.68831 | 410.04755 |
| 5 | 229.06418 | 274.42342 | 319.78266 | 365.14190 | 410.50115 |
| 6 | 229.51777 | 274.87701 | 320.23625 | 365.59550 | 410.95474 |
| 7 | 229.97136 | 275.33060 | 320.68985 | 366.04909 | 411.40833 |
| 8 | 230.42495 | 275.78420 | 321.14344 | 366.50268 | 411.86192 |
| 9 | 230.87855 | 276.23779 | 321.59703 | 366.95627 | 412.31552 |
| 10 | 231.33214 | 276.69138 | 322.05062 | 367.40987 | 412.76911 |
| 11 | 231.78573 | 277.14497 | 322.50422 | 367.86346 | 413.22270 |
| 12 | 232.23932 | 277.59857 | 322.95781 | 368.31705 | 413.67629 |
| 13 | 232.69292 | 278.05216 | 323.41140 | 368.77064 | 414.12989 |
| 14 | 233.14651 | 278.50575 | 323.86499 | 369.22424 | 414.58348 |
| 15 | 233.60010 | 278.95934 | 324.31859 | 369.67783 | 415.03707 |
| 16 | 234.05369 | 279.41294 | 324.77218 | 370.13142 | 415.49066 |
| 17 | 234.50729 | 279.86653 | 325.22577 | 370.58501 | 415.94426 |
| 18 | 234.96088 | 280.32012 | 325.67936 | 371.03861 | 416.39785 |
| 19 | 235.41447 | 280.77371 | 326.13296 | 371.49220 | 416.85144 |
| 20 | 235.86806 | 281.22731 | 326.58655 | 371.94579 | 417.30503 |
| 21 | 236.32165 | 281.68090 | 327.04014 | 372.39938 | 417.75863 |
| 22 | 236.77525 | 282.13449 | 327.49373 | 372.85298 | 418.21222 |
| 23 | 237.22884 | 282.58808 | 327.94733 | 373.30657 | 418.66581 |
| 24 | 237.68243 | 283.04167 | 328.40092 | 373.76016 | 419.11940 |
| 25 | 238.13602 | 283.49527 | 328.85451 | 374.21375 | 419.57300 |
| 26 | 238.58962 | 283.94886 | 329.30810 | 374.66735 | 420.02659 |
| 27 | 239.04321 | 284.40245 | 329.76169 | 375.12094 | 420.48018 |
| 28 | 239.49680 | 284.85604 | 330.21529 | 375.57453 | 420.93377 |
| 29 | 239.95039 | 285.30964 | 330.66888 | 376.02812 | 421.38737 |
| 30 | 240.40399 | 285.76323 | 331.12247 | 376.48171 | 421.84096 |
| 31 | 240.85758 | 286.21682 | 331.57606 | 376.93531 | 422.29455 |
| 32 | 241.31117 | 286.67041 | 332.02966 | 377.38890 | 422.74814 |
| 33 | 241.76476 | 287.12401 | 332.48325 | 377.84249 | 423.20174 |
| 34 | 242.21836 | 287.57760 | 332.93684 | 378.29608 | 423.65533 |
| 35 | 242.67195 | 288.03119 | 333.39043 | 378.74968 | 424.10892 |
| 36 | 243.12554 | 288.48478 | 333.84403 | 379.20327 | 424.56251 |
| 37 | 243.57913 | 288.93838 | 334.29762 | 379.65686 | 425.01610 |
| 38 | 244.03273 | 289.39197 | 334.75121 | 380.11045 | 425.46970 |
| 39 | 244.48632 | 289.84556 | 335.20480 | 380.56405 | 425.92329 |
| 40 | 244.93991 | 290.29915 | 335.65840 | 381.01764 | 426.37688 |
| 41 | 245.39350 | 290.75275 | 336.11199 | 381.47123 | 426.83047 |
| 42 | 245.84710 | 291.20634 | 336.56558 | 381.92482 | 427.28407 |
| 43 | 246.30069 | 291.65993 | 337.01917 | 382.37842 | 427.73766 |
| 44 | 246.75428 | 292.11352 | 337.47277 | 382.83201 | 428.19125 |
| 45 | 247.20787 | 292.56712 | 337.92636 | 383.28560 | 428.64484 |
| 46 | 247.66147 | 293.02071 | 338.37995 | 383.73919 | 429.09844 |
| 47 | 248.11506 | 293.47430 | 338.83354 | 384.19279 | 429.55203 |
| 48 | 248.56865 | 293.92789 | 339.28714 | 384.64638 | 430.00562 |
| 49 | 249.02224 | 294.38149 | 339.74073 | 385.09997 | 430.45921 |

9 oz. = .255146 kg. 10 oz. = .283495 kg. 11 oz. = .311845 kg. 12 oz. = .340194 kg.

EQUIVALENTS OF AVOIRDUPOIS POUNDS IN KILOGRAMS.

(Continued)

| Pounds | 500 | 600 | 700 | 800 | 900 |
|--------|-----------|-----------|-----------|-----------|-----------|
| 50 | 249.47584 | 294.83508 | 340.19432 | 385.55356 | 430.91281 |
| 51 | 249.92943 | 295.28867 | 340.64791 | 386.00716 | 431.36640 |
| 52 | 250.38302 | 295.74226 | 341.10151 | 386.46075 | 431.81999 |
| 53 | 250.83661 | 296.19586 | 341.55510 | 386.91434 | 432.27358 |
| 54 | 251.29020 | 296.64945 | 342.00869 | 387.36793 | 432.72718 |
| 55 | 251.74380 | 297.10304 | 342.46228 | 387.82153 | 433.18077 |
| 56 | 252.19739 | 297.55663 | 342.91588 | 388.27512 | 433.63436 |
| 57 | 252.65098 | 298.01022 | 343.36947 | 388.72871 | 434.08795 |
| 58 | 253.10457 | 298.46382 | 343.82306 | 389.18230 | 434.54155 |
| 59 | 253.55817 | 298.91741 | 344.27665 | 389.63590 | 434.99514 |
| 60 | 254.01176 | 299.37100 | 344.73025 | 390.08949 | 435.44873 |
| 61 | 254.46535 | 299.82459 | 345.18384 | 390.54308 | 435.90232 |
| 62 | 254.91894 | 300.27819 | 345.63743 | 390.99667 | 436.35592 |
| 63 | 255.37254 | 300.73178 | 346.09102 | 391.45027 | 436.80951 |
| 64 | 255.82613 | 301.18537 | 346.54461 | 391.90386 | 437.26310 |
| 65 | 256.27972 | 301.63896 | 346.99821 | 392.35745 | 437.71669 |
| 66 | 256.73331 | 302.09256 | 347.45180 | 392.81104 | 438.17029 |
| 67 | 257.18691 | 302.54615 | 347.90539 | 393.26463 | 438.62388 |
| 68 | 257.64050 | 302.99974 | 348.35898 | 393.71823 | 439.07747 |
| 69 | 258.09409 | 303.45333 | 348.81258 | 394.17182 | 439.53106 |
| 70 | 258.54768 | 303.90693 | 349.26617 | 394.62541 | 439.98465 |
| 71 | 259.00128 | 304.36052 | 349.71976 | 395.07900 | 440.43825 |
| 72 | 259.45487 | 304.81411 | 350.17335 | 395.53260 | 440.89184 |
| 73 | 259.90846 | 305.26770 | 350.62695 | 395.98619 | 441.34543 |
| 74 | 260.36205 | 305.72130 | 351.08054 | 396.43978 | 441.79902 |
| 75 | 260.81565 | 306.17489 | 351.53413 | 396.89337 | 442.25262 |
| 76 | 261.26924 | 306.62848 | 351.98772 | 397.34697 | 442.70621 |
| 77 | 261.72283 | 307.08207 | 352.44132 | 397.80056 | 443.15980 |
| 78 | 262.17642 | 307.53567 | 352.89491 | 398.25415 | 443.61339 |
| 79 | 262.63002 | 307.98926 | 353.34850 | 398.70774 | 444.06699 |
| 80 | 263.08361 | 308.44285 | 353.80209 | 399.16134 | 444.52058 |
| 81 | 263.53720 | 308.89644 | 354.25569 | 399.61493 | 444.97417 |
| 82 | 263.99079 | 309.35004 | 354.70928 | 400.06852 | 445.42776 |
| 83 | 264.44439 | 309.80363 | 355.16287 | 400.52211 | 445.88136 |
| 84 | 264.89798 | 310.25722 | 355.61646 | 400.97571 | 446.33495 |
| 85 | 265.35157 | 310.71081 | 356.07006 | 401.42930 | 446.78854 |
| 86 | 265.80516 | 311.16441 | 356.52365 | 401.88289 | 447.24213 |
| 87 | 266.25876 | 311.61800 | 356.97724 | 402.33648 | 447.69573 |
| 88 | 266.71235 | 312.07159 | 357.43083 | 402.79008 | 448.14932 |
| 89 | 267.16594 | 312.52518 | 357.88443 | 403.24367 | 448.60291 |
| 90 | 267.61953 | 312.97878 | 358.33802 | 403.69726 | 449.05650 |
| 91 | 268.07312 | 313.43237 | 358.79161 | 404.15085 | 449.51010 |
| 92 | 268.52672 | 313.88596 | 359.24520 | 404.60445 | 449.96369 |
| 93 | 268.98031 | 314.33955 | 359.69880 | 405.05804 | 450.41728 |
| 94 | 269.43390 | 314.79314 | 360.15239 | 405.51163 | 450.87087 |
| 95 | 269.88749 | 315.24674 | 360.60598 | 405.96522 | 451.32447 |
| 96 | 270.34109 | 315.70033 | 361.05957 | 406.41882 | 451.77806 |
| 97 | 270.79468 | 316.15392 | 361.51316 | 406.87241 | 452.23165 |
| 98 | 271.24827 | 316.60751 | 361.96676 | 407.32600 | 452.68524 |
| 99 | 271.70186 | 317.06111 | 362.42035 | 407.77959 | 453.13884 |

13 oz. = .368544 kg. 14 oz. = .396893 kg. 15 oz. = .425243 kg. 16 oz. = .453593 kg.

EQUIVALENTS OF KILOGRAMS IN AVOIRDUPOIS POUNDS.

Conversion factor: 1 kilogram = 2.204622341 avoirdupois pounds.

| Kilos | 0 | 100 | 200 | 300 | 400 |
|-------|----------|----------|----------|----------|----------|
| 0 | | 220.4622 | 440.9245 | 661.3867 | 881.8489 |
| 1 | 2.2046 | 222.6669 | 443.1291 | 663.5913 | 884.0536 |
| 2 | 4.4092 | 224.8715 | 445.3337 | 665.7959 | 886.2582 |
| 3 | 6.6139 | 227.0761 | 447.5383 | 668.0006 | 888.4628 |
| 4 | 8.8185 | 229.2807 | 449.7430 | 670.2052 | 890.6674 |
| 5 | 11.0231 | 231.4853 | 451.9476 | 672.4098 | 892.8720 |
| 6 | 13.2277 | 233.6900 | 454.1522 | 674.6144 | 895.0767 |
| 7 | 15.4324 | 235.8946 | 456.3568 | 676.8191 | 897.2813 |
| 8 | 17.6370 | 238.0992 | 458.5614 | 679.0237 | 899.4859 |
| 9 | 19.8416 | 240.3038 | 460.7661 | 681.2283 | 901.6905 |
| 10 | 22.0462 | 242.5085 | 462.9707 | 683.4329 | 903.8952 |
| 11 | 24.2508 | 244.7131 | 465.1753 | 685.6375 | 906.0998 |
| 12 | 26.4555 | 246.9177 | 467.3799 | 687.8422 | 908.3044 |
| 13 | 28.6601 | 249.1223 | 469.5846 | 690.0468 | 910.5090 |
| 14 | 30.8647 | 251.3269 | 471.7892 | 692.2514 | 912.7136 |
| 15 | 33.0693 | 253.5316 | 473.9938 | 694.4560 | 914.9183 |
| 16 | 35.2740 | 255.7362 | 476.1984 | 696.6607 | 917.1229 |
| 17 | 37.4786 | 257.9408 | 478.4030 | 698.8653 | 919.3275 |
| 18 | 39.6832 | 260.1454 | 480.6077 | 701.0699 | 921.5321 |
| 19 | 41.8878 | 262.3501 | 482.8123 | 703.2745 | 923.7368 |
| 20 | 44.0924 | 264.5547 | 485.0169 | 705.4791 | 925.9414 |
| 21 | 46.2971 | 266.7593 | 487.2215 | 707.6838 | 928.1460 |
| 22 | 48.5017 | 268.9639 | 489.4262 | 709.8884 | 930.3506 |
| 23 | 50.7063 | 271.1685 | 491.6308 | 712.0930 | 932.5553 |
| 24 | 52.9109 | 273.3732 | 493.8354 | 714.2976 | 934.7599 |
| 25 | 55.1156 | 275.5778 | 496.0400 | 716.5023 | 936.9645 |
| 26 | 57.3202 | 277.7824 | 498.2446 | 718.7069 | 939.1691 |
| 27 | 59.5248 | 279.9870 | 500.4493 | 720.9115 | 941.3737 |
| 28 | 61.7294 | 282.1917 | 502.6539 | 723.1161 | 943.5784 |
| 29 | 63.9340 | 284.3963 | 504.8585 | 725.3208 | 945.7830 |
| 30 | 66.1387 | 286.6009 | 507.0631 | 727.5254 | 947.9876 |
| 31 | 68.3433 | 288.8055 | 509.2678 | 729.7300 | 950.1922 |
| 32 | 70.5479 | 291.0101 | 511.4724 | 731.9346 | 952.3969 |
| 33 | 72.7525 | 293.2148 | 513.6770 | 734.1392 | 954.6015 |
| 34 | 74.9572 | 295.4194 | 515.8816 | 736.3439 | 956.8061 |
| 35 | 77.1618 | 297.6240 | 518.0863 | 738.5485 | 959.0107 |
| 36 | 79.3664 | 299.8286 | 520.2909 | 740.7531 | 961.2153 |
| 37 | 81.5710 | 302.0333 | 522.4955 | 742.9577 | 963.4200 |
| 38 | 83.7756 | 304.2379 | 524.7001 | 745.1624 | 965.6246 |
| 39 | 85.9803 | 306.4425 | 526.9047 | 747.3670 | 967.8292 |
| 40 | 88.1849 | 308.6471 | 529.1094 | 749.5716 | 970.0338 |
| 41 | 90.3895 | 310.8518 | 531.3140 | 751.7762 | 972.2385 |
| 42 | 92.5941 | 313.0564 | 533.5186 | 753.9808 | 974.4431 |
| 43 | 94.7988 | 315.2610 | 535.7232 | 756.1855 | 976.6477 |
| 44 | 97.0034 | 317.4656 | 537.9279 | 758.3901 | 978.8523 |
| 45 | 99.2080 | 319.6702 | 540.1325 | 760.5947 | 981.0569 |
| 46 | 101.4126 | 321.8749 | 542.3371 | 762.7993 | 983.2616 |
| 47 | 103.6173 | 324.0795 | 544.5417 | 765.0040 | 985.4662 |
| 48 | 105.8219 | 326.2841 | 546.7463 | 767.2086 | 987.6708 |
| 49 | 108.0265 | 328.4887 | 548.9510 | 769.4132 | 989.8754 |

EQUIVALENTS OF KILOGRAMS IN
AVOIRDUPOIS POUNDS.

(Continued)

| Kilos | 0 | 100 | 200 | 300 | 400 |
|-------|----------|----------|----------|----------|------------|
| 50 | 110.2311 | 330.6934 | 551.1556 | 771.6178 | 992.0801 |
| 51 | 112.4357 | 332.8980 | 553.3602 | 773.8224 | 994.2847 |
| 52 | 114.6404 | 335.1026 | 555.5648 | 776.0271 | 996.4893 |
| 53 | 116.8450 | 337.3072 | 557.7695 | 778.2317 | 998.6939 |
| 54 | 119.0496 | 339.5118 | 559.9741 | 780.4363 | 1,000.8985 |
| 55 | 121.2542 | 341.7165 | 562.1787 | 782.6409 | 1,003.1032 |
| 56 | 123.4589 | 343.9211 | 564.3833 | 784.8456 | 1,005.3078 |
| 57 | 125.6636 | 346.1257 | 566.5879 | 787.0502 | 1,007.5124 |
| 58 | 127.8681 | 348.3303 | 568.7926 | 789.2548 | 1,009.7170 |
| 59 | 130.0727 | 350.5350 | 570.9972 | 791.4594 | 1,011.9217 |
| 60 | 132.3773 | 352.7396 | 573.2018 | 793.6640 | 1,014.1263 |
| 61 | 134.4820 | 354.9442 | 575.4064 | 795.8687 | 1,016.3309 |
| 62 | 136.6866 | 357.1488 | 577.6111 | 798.0733 | 1,018.5355 |
| 63 | 138.8912 | 359.3534 | 579.8157 | 800.2779 | 1,020.7401 |
| 64 | 141.0958 | 361.5581 | 582.0203 | 802.4825 | 1,022.9448 |
| 65 | 143.3005 | 363.7627 | 584.2249 | 804.6872 | 1,025.1494 |
| 66 | 145.5051 | 365.9673 | 586.4295 | 806.8918 | 1,027.3540 |
| 67 | 147.7097 | 368.1719 | 588.6342 | 809.0964 | 1,029.5586 |
| 68 | 149.9143 | 370.3766 | 590.8388 | 811.3010 | 1,031.7633 |
| 69 | 152.1189 | 371.5812 | 593.0434 | 813.5056 | 1,033.9679 |
| 70 | 154.3236 | 374.7858 | 595.2480 | 815.7103 | 1,036.1725 |
| 71 | 156.5282 | 376.9904 | 597.4527 | 817.9149 | 1,038.3771 |
| 72 | 158.7328 | 379.1950 | 599.6573 | 820.1195 | 1,040.5817 |
| 73 | 160.9374 | 381.3997 | 601.8619 | 822.3241 | 1,042.7864 |
| 74 | 163.1421 | 383.6043 | 604.0665 | 824.5288 | 1,044.9910 |
| 75 | 165.3467 | 385.8089 | 606.2711 | 826.7334 | 1,047.1956 |
| 76 | 167.5513 | 388.0135 | 608.4758 | 828.9380 | 1,049.4002 |
| 77 | 169.7559 | 390.2182 | 610.6804 | 831.1426 | 1,051.6049 |
| 78 | 171.9605 | 392.4228 | 612.8850 | 833.3472 | 1,053.8095 |
| 79 | 174.1652 | 394.6274 | 615.0896 | 835.5519 | 1,056.0141 |
| 80 | 176.3698 | 396.8320 | 617.2943 | 837.7565 | 1,058.2187 |
| 81 | 178.5744 | 399.0366 | 619.4989 | 839.9611 | 1,060.4233 |
| 82 | 180.7790 | 401.2413 | 621.7035 | 842.1657 | 1,062.6280 |
| 83 | 182.9837 | 403.4459 | 623.9081 | 844.3704 | 1,064.8326 |
| 84 | 185.1883 | 405.6505 | 626.1127 | 846.5750 | 1,067.0372 |
| 85 | 187.3929 | 407.8551 | 628.3174 | 848.7796 | 1,069.2418 |
| 86 | 189.5975 | 410.0598 | 630.5220 | 850.9842 | 1,071.4465 |
| 87 | 191.8021 | 412.2644 | 632.7266 | 853.1888 | 1,073.6511 |
| 88 | 194.0068 | 414.4690 | 634.9312 | 855.3935 | 1,075.8557 |
| 89 | 196.2114 | 416.6736 | 637.1359 | 857.5981 | 1,078.0603 |
| 90 | 198.4160 | 418.8782 | 639.3405 | 859.8027 | 1,080.2649 |
| 91 | 200.6206 | 421.0829 | 641.5451 | 862.0073 | 1,082.4696 |
| 92 | 202.8253 | 423.2875 | 643.7497 | 864.2120 | 1,084.6742 |
| 93 | 205.0299 | 425.4921 | 645.9543 | 866.4166 | 1,086.8788 |
| 94 | 207.2345 | 427.6967 | 648.1590 | 868.6212 | 1,089.0834 |
| 95 | 209.4391 | 429.9014 | 650.3636 | 870.8258 | 1,091.2881 |
| 96 | 211.6437 | 432.1060 | 652.5682 | 873.0304 | 1,093.4927 |
| 97 | 213.8484 | 434.3106 | 654.7728 | 875.2351 | 1,095.6973 |
| 98 | 216.0530 | 436.5152 | 656.9775 | 877.4397 | 1,097.9019 |
| 99 | 218.2576 | 438.7198 | 659.1821 | 879.6443 | 1,100.1065 |

EQUIVALENTS OF KILOGRAMS IN AVOIRDUPOIS POUNDS.

(Continued)

| Kilos | 500 | 600 | 700 | 800 | 900 |
|-------|------------|------------|------------|------------|------------|
| 0 | 1,102.3112 | 1,322.7734 | 1,543.2356 | 1,763.6979 | 1,984.1601 |
| 1 | 1,104.5158 | 1,324.9780 | 1,545.4403 | 1,765.9025 | 1,986.3647 |
| 2 | 1,106.7204 | 1,327.1826 | 1,547.6449 | 1,768.1071 | 1,988.5694 |
| 3 | 1,108.9250 | 1,329.3873 | 1,549.8495 | 1,770.3117 | 1,990.7740 |
| 4 | 1,111.1297 | 1,331.5919 | 1,552.0541 | 1,172.5164 | 1,992.9786 |
| 5 | 1,113.3343 | 1,333.7965 | 1,554.2588 | 1,774.7210 | 1,995.1832 |
| 6 | 1,115.5389 | 1,336.0011 | 1,556.4634 | 1,776.9256 | 1,997.3878 |
| 7 | 1,117.7435 | 1,338.2058 | 1,558.6680 | 1,779.1302 | 1,999.5925 |
| 8 | 1,119.9481 | 1,340.4104 | 1,560.8726 | 1,781.3349 | 2,001.7971 |
| 9 | 1,122.1528 | 1,342.6150 | 1,563.0772 | 1,783.5395 | 2,004.0017 |
| 10 | 1,124.3574 | 1,344.8196 | 1,565.2819 | 1,785.7441 | 2,006.2063 |
| 11 | 1,126.5620 | 1,347.0243 | 1,567.4865 | 1,787.9487 | 2,008.4110 |
| 12 | 1,128.7666 | 1,349.2289 | 1,569.6911 | 1,790.1533 | 2,010.6156 |
| 13 | 1,130.9713 | 1,351.4335 | 1,571.8957 | 1,792.3580 | 2,012.8202 |
| 14 | 1,133.1759 | 1,353.6381 | 1,574.1004 | 1,794.5626 | 2,015.0248 |
| 15 | 1,135.3805 | 1,355.8427 | 1,576.3050 | 1,796.7672 | 2,017.2294 |
| 16 | 1,137.5851 | 1,358.0474 | 1,578.5096 | 1,798.9718 | 2,019.4341 |
| 17 | 1,139.7898 | 1,360.2520 | 1,580.7142 | 1,801.1765 | 2,021.6387 |
| 18 | 1,141.9944 | 1,362.4566 | 1,582.9188 | 1,803.3811 | 2,023.8433 |
| 19 | 1,144.1990 | 1,364.6612 | 1,585.1235 | 1,805.5857 | 2,026.0479 |
| 20 | 1,146.4036 | 1,366.8659 | 1,587.3281 | 1,807.7903 | 2,028.2526 |
| 21 | 1,148.6082 | 1,369.0705 | 1,589.5327 | 1,809.9949 | 2,030.4572 |
| 22 | 1,150.8129 | 1,371.2751 | 1,591.7373 | 1,812.1996 | 2,032.6618 |
| 23 | 1,153.0175 | 1,373.4797 | 1,593.9420 | 1,814.4042 | 2,034.8664 |
| 24 | 1,155.2221 | 1,375.6843 | 1,596.1466 | 1,816.6088 | 2,037.0710 |
| 25 | 1,157.4267 | 1,377.8890 | 1,598.3512 | 1,818.8134 | 2,039.2757 |
| 26 | 1,159.6314 | 1,380.0936 | 1,600.5558 | 1,821.0181 | 2,041.4803 |
| 27 | 1,161.8360 | 1,382.2982 | 1,602.7604 | 1,823.2227 | 2,043.6849 |
| 28 | 1,164.0406 | 1,384.5028 | 1,604.9651 | 1,825.4273 | 2,045.8895 |
| 29 | 1,166.2452 | 1,386.7075 | 1,607.1697 | 1,827.6319 | 2,048.0942 |
| 30 | 1,168.4498 | 1,388.9121 | 1,609.3743 | 1,829.8365 | 2,050.2988 |
| 31 | 1,170.6545 | 1,391.1167 | 1,611.5789 | 1,832.0412 | 2,052.5034 |
| 32 | 1,172.8591 | 1,393.3213 | 1,613.7836 | 1,834.2458 | 2,054.7080 |
| 33 | 1,175.0637 | 1,395.5259 | 1,615.9882 | 1,836.4504 | 2,056.9126 |
| 34 | 1,177.2683 | 1,397.7306 | 1,618.1928 | 1,838.6550 | 2,059.1173 |
| 35 | 1,179.4730 | 1,399.9352 | 1,620.3974 | 1,840.8597 | 2,061.3219 |
| 36 | 1,181.6776 | 1,402.1398 | 1,622.6020 | 1,843.0643 | 2,063.5265 |
| 37 | 1,183.8822 | 1,404.3444 | 1,624.8067 | 1,845.2689 | 2,065.7311 |
| 38 | 1,186.0868 | 1,406.5491 | 1,627.0113 | 1,847.4735 | 2,067.9358 |
| 39 | 1,188.2914 | 1,408.7537 | 1,629.2159 | 1,849.6781 | 2,070.1404 |
| 40 | 1,190.4961 | 1,410.9583 | 1,631.4205 | 1,851.8828 | 2,072.3450 |
| 41 | 1,192.7007 | 1,413.1629 | 1,633.6252 | 1,854.0874 | 2,074.5496 |
| 42 | 1,194.9053 | 1,415.3675 | 1,635.8298 | 1,856.2920 | 2,076.7542 |
| 43 | 1,197.1099 | 1,417.5722 | 1,638.0344 | 1,858.4966 | 2,078.9589 |
| 44 | 1,199.3146 | 1,419.7768 | 1,640.2390 | 1,860.7013 | 2,081.1635 |
| 45 | 1,201.5192 | 1,421.9814 | 1,642.4436 | 1,862.9059 | 2,083.3681 |
| 46 | 1,203.7238 | 1,424.1860 | 1,644.6483 | 1,865.1105 | 2,085.5727 |
| 47 | 1,205.9284 | 1,426.3907 | 1,646.8529 | 1,867.3151 | 2,087.7774 |
| 48 | 1,208.1330 | 1,428.5953 | 1,649.0575 | 1,869.5197 | 2,089.9820 |
| 49 | 1,210.3377 | 1,430.7999 | 1,651.2621 | 1,871.7244 | 2,092.1866 |

EQUIVALENTS OF KILOGRAMS IN
AVOIRDUPOIS POUNDS.

(Continued)

| Kilos | 500 | 600 | 700 | 800 | 900 |
|-------|------------|------------|------------|------------|------------|
| 50 | 1,212.5423 | 1,433.0045 | 1,653.4668 | 1,873.9290 | 2,094.3912 |
| 51 | 1,214.7469 | 1,435.2091 | 1,655.6714 | 1,876.1336 | 2,096.5958 |
| 52 | 1,216.9515 | 1,437.4138 | 1,657.8760 | 1,878.3382 | 2,098.8005 |
| 53 | 1,219.1562 | 1,439.6184 | 1,660.0806 | 1,880.5429 | 2,101.0051 |
| 54 | 1,221.3608 | 1,441.8230 | 1,662.2852 | 1,882.7475 | 2,103.2097 |
| 55 | 1,223.5654 | 1,444.0276 | 1,664.4899 | 1,884.9521 | 2,105.4143 |
| 56 | 1,225.7700 | 1,446.2323 | 1,666.6945 | 1,887.1567 | 2,107.6190 |
| 57 | 1,227.9746 | 1,448.4369 | 1,668.8991 | 1,889.3613 | 2,109.8236 |
| 58 | 1,230.1793 | 1,450.6415 | 1,671.1037 | 1,891.5660 | 2,112.0282 |
| 59 | 1,232.3839 | 1,452.8461 | 1,673.3084 | 1,893.7706 | 2,114.2328 |
| 60 | 1,234.5885 | 1,455.0507 | 1,675.5130 | 1,895.9752 | 2,116.4374 |
| 61 | 1,236.7931 | 1,457.2554 | 1,677.7176 | 1,898.1798 | 2,118.6421 |
| 62 | 1,238.9978 | 1,459.4600 | 1,679.9222 | 1,900.3845 | 2,120.8467 |
| 63 | 1,241.2024 | 1,461.6646 | 1,682.1268 | 1,902.5891 | 2,123.0513 |
| 64 | 1,243.4070 | 1,463.8692 | 1,684.3315 | 1,904.7937 | 2,125.2559 |
| 65 | 1,245.6116 | 1,466.0739 | 1,686.5361 | 1,906.9983 | 2,127.4606 |
| 66 | 1,247.8162 | 1,468.2785 | 1,688.7407 | 1,909.2029 | 2,129.6652 |
| 67 | 1,250.0209 | 1,470.4831 | 1,690.9453 | 1,911.4076 | 2,131.8698 |
| 68 | 1,252.2255 | 1,472.6877 | 1,693.1500 | 1,913.6122 | 2,134.0744 |
| 69 | 1,254.4301 | 1,474.8923 | 1,695.3546 | 1,915.8168 | 2,136.2790 |
| 70 | 1,256.6347 | 1,477.0970 | 1,697.5592 | 1,918.0214 | 2,138.4837 |
| 71 | 1,258.8394 | 1,479.3016 | 1,699.7638 | 1,920.2261 | 2,140.6883 |
| 72 | 1,261.0440 | 1,481.5062 | 1,701.9684 | 1,922.4307 | 2,142.8929 |
| 73 | 1,263.2486 | 1,483.7108 | 1,704.1731 | 1,924.6353 | 2,145.0975 |
| 74 | 1,265.4532 | 1,485.9155 | 1,706.3777 | 1,926.8399 | 2,147.3022 |
| 75 | 1,267.6578 | 1,488.1201 | 1,708.5823 | 1,929.0445 | 2,149.5068 |
| 76 | 1,269.8625 | 1,490.3247 | 1,710.7869 | 1,931.2492 | 2,151.7114 |
| 77 | 1,272.0671 | 1,492.5293 | 1,712.9916 | 1,933.4538 | 2,153.9160 |
| 78 | 1,274.2717 | 1,494.7339 | 1,715.1962 | 1,935.6584 | 2,156.1206 |
| 79 | 1,276.4763 | 1,496.9386 | 1,717.4008 | 1,937.8630 | 2,158.3253 |
| 80 | 1,278.6810 | 1,499.1432 | 1,719.6054 | 1,940.0677 | 2,160.5299 |
| 81 | 1,280.8856 | 1,501.3478 | 1,721.8100 | 1,942.2723 | 2,162.7345 |
| 82 | 1,283.0902 | 1,503.5524 | 1,724.0147 | 1,944.4769 | 2,164.9391 |
| 83 | 1,285.2948 | 1,505.7571 | 1,726.2193 | 1,946.6815 | 2,167.1438 |
| 84 | 1,287.4994 | 1,507.9617 | 1,728.4239 | 1,948.8861 | 2,169.3484 |
| 85 | 1,289.7041 | 1,510.1663 | 1,730.6285 | 1,951.0908 | 2,171.5530 |
| 86 | 1,291.9087 | 1,512.3709 | 1,732.8332 | 1,953.2954 | 2,173.7576 |
| 87 | 1,294.1133 | 1,514.5755 | 1,735.0378 | 1,955.5000 | 2,175.9623 |
| 88 | 1,296.3179 | 1,516.7802 | 1,737.2424 | 1,957.7046 | 2,178.1669 |
| 89 | 1,298.5226 | 1,518.9848 | 1,739.4470 | 1,959.9093 | 2,180.3715 |
| 90 | 1,300.7272 | 1,521.1894 | 1,741.6516 | 1,962.1139 | 2,182.5761 |
| 91 | 1,302.9318 | 1,523.3940 | 1,743.8563 | 1,964.3185 | 2,184.7807 |
| 92 | 1,305.1364 | 1,525.5987 | 1,746.0609 | 1,966.5231 | 2,186.9854 |
| 93 | 1,307.3410 | 1,527.8033 | 1,748.2655 | 1,968.7278 | 2,189.1900 |
| 94 | 1,309.5457 | 1,530.0079 | 1,750.4701 | 1,970.9324 | 2,191.3946 |
| 95 | 1,311.7503 | 1,532.2125 | 1,752.6748 | 1,973.1370 | 2,193.5992 |
| 96 | 1,313.9549 | 1,534.4171 | 1,754.8794 | 1,975.3416 | 2,195.8039 |
| 97 | 1,316.1595 | 1,536.6218 | 1,757.0840 | 1,977.5462 | 2,198.0085 |
| 98 | 1,318.3642 | 1,538.8264 | 1,759.2886 | 1,979.7509 | 2,200.2131 |
| 99 | 1,320.5688 | 1,541.0310 | 1,761.4933 | 1,981.9555 | 2,202.4177 |

COMPARISON OF THE VARIOUS TONS AND POUNDS IN USE IN THE UNITED STATES.

(See Pages 562, 563, 582, 586)

| Troy Pounds | Avoirdupois Pounds | Kilograms | Short Tons | Long Tons | Metric Tons |
|-------------|--------------------|-----------|-------------|-------------|-------------|
| 1 | .822 857 | .373 24 | .000 411 43 | .000 367 35 | .000 373 24 |
| 2 | 1.645 71 | .746 48 | .000 822 86 | .000 734 69 | .000 746 48 |
| 3 | 2.468 57 | 1.119 73 | .001 234 29 | .001 102 04 | .001 119 73 |
| 4 | 3.291 43 | 1.492 97 | .001 645 71 | .001 469 39 | .001 492 97 |
| 5 | 4.114 29 | 1.866 21 | .002 057 14 | .001 836 73 | .001 866 21 |
| 6 | 4.937 14 | 2.239 45 | .002 468 57 | .002 204 08 | .002 239 45 |
| 7 | 5.760 00 | 2.612 69 | .002 880 00 | .002 571 43 | .002 612 69 |
| 8 | 6.582 86 | 2.985 93 | .003 291 43 | .002 938 78 | .002 985 93 |
| 9 | 7.405 71 | 3.359 18 | .003 702 86 | .003 306 12 | .003 359 18 |
| 1.215 28 | 1 | .453 59 | .0005 | .000 446 43 | .000 453 59 |
| 2.430 56 | 2 | .907 18 | .0010 | .000 892 86 | .000 907 18 |
| 3.645 83 | 3 | 1.360 78 | .0015 | .001 339 29 | .001 360 78 |
| 4.861 11 | 4 | 1.814 37 | .0020 | .001 785 71 | .001 814 37 |
| 6.076 39 | 5 | 2.267 96 | .0025 | .002 232 14 | .002 267 96 |
| 7.291 67 | 6 | 2.721 55 | .0030 | .002 678 57 | .002 721 55 |
| 8.506 94 | 7 | 3.175 15 | .0035 | .003 125 00 | .003 175 15 |
| 9.722 22 | 8 | 3.628 74 | .0040 | .003 571 43 | .003 628 74 |
| 10.937 50 | 9 | 4.082 33 | .0045 | .004 017 86 | .004 082 33 |
| 2.679 23 | 2.204 62 | 1 | .001 102 31 | .000 984 21 | .001 |
| 5.358 46 | 4.409 24 | 2 | .002 204 62 | .001 968 41 | .002 |
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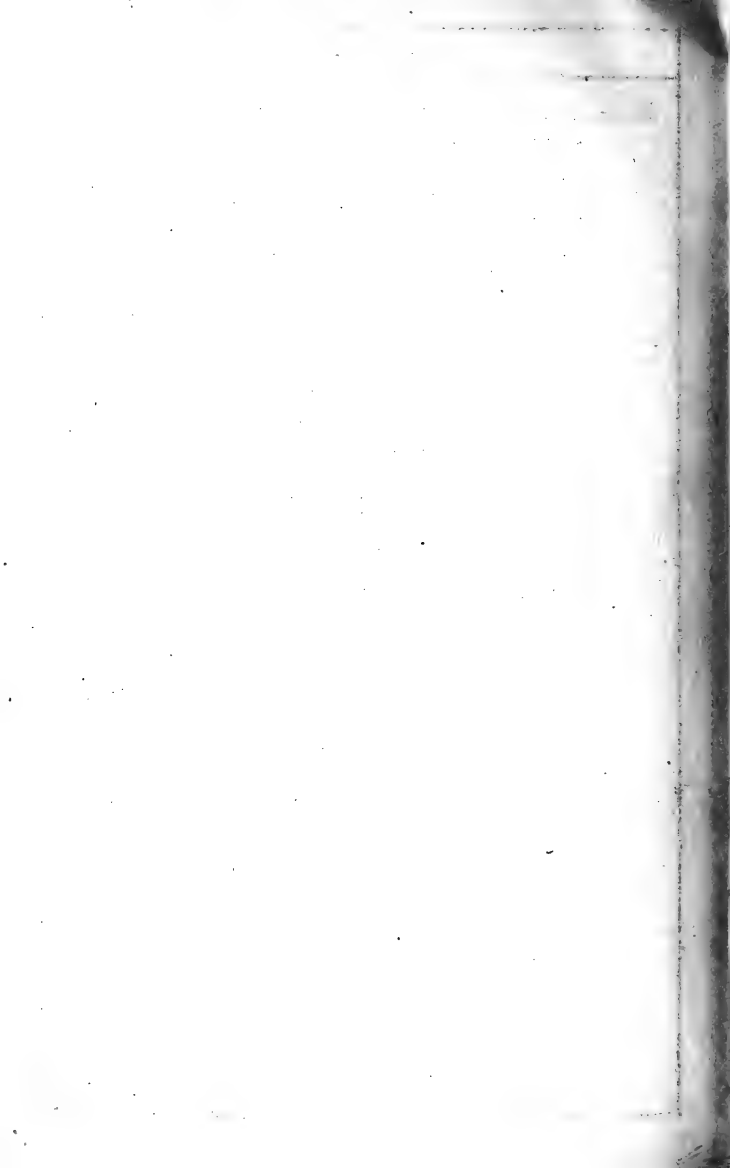
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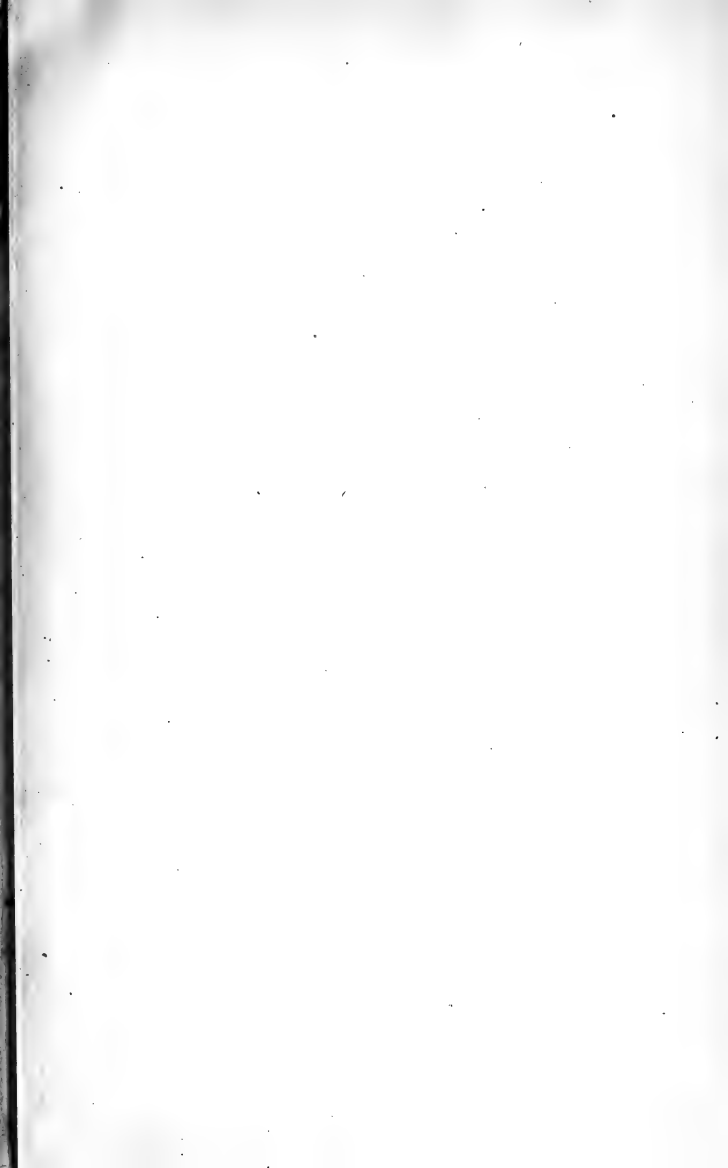
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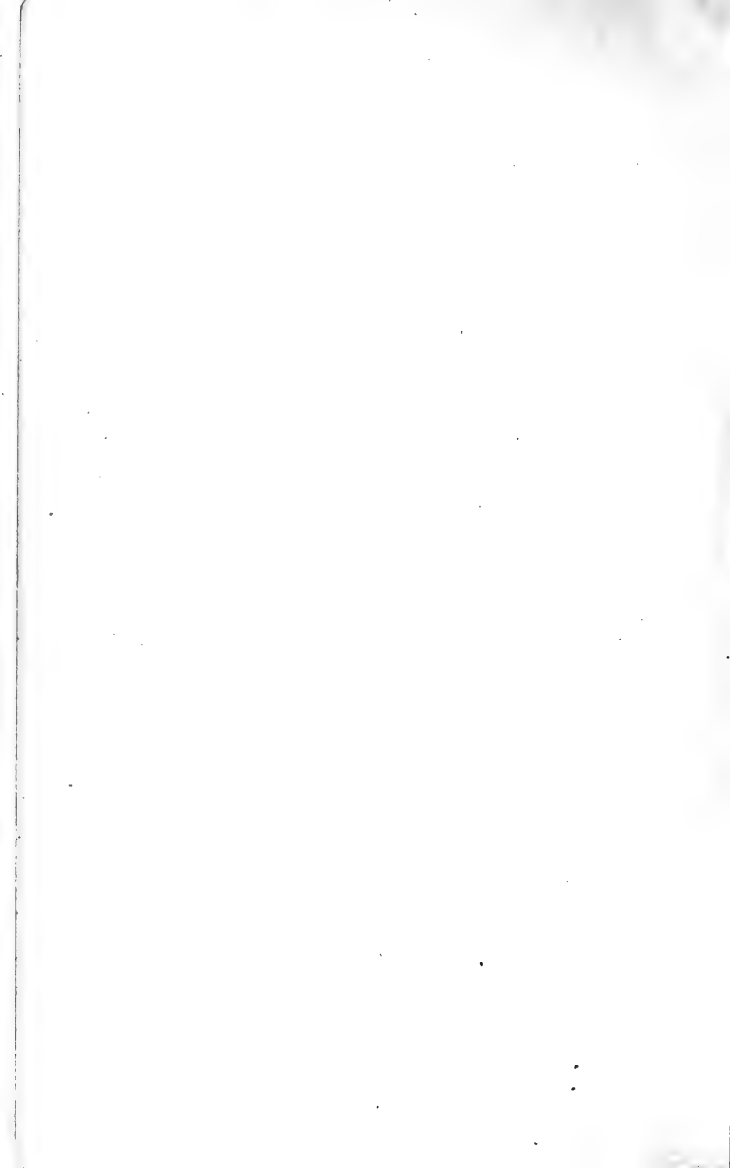
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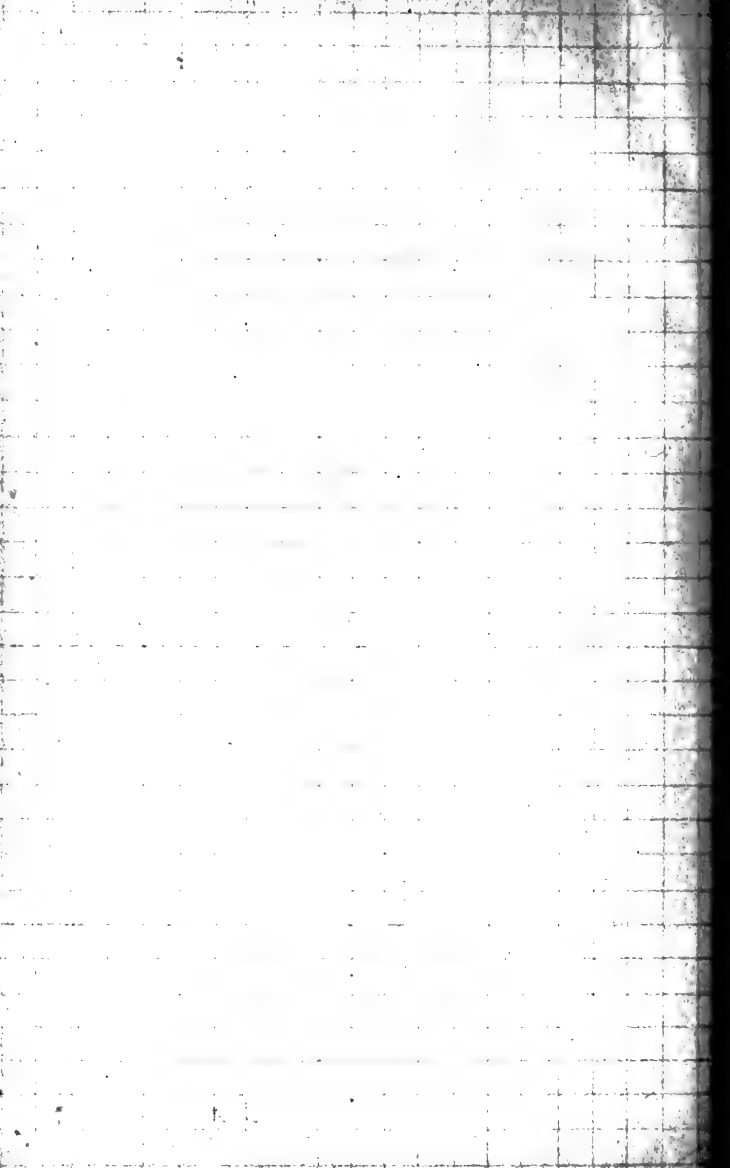
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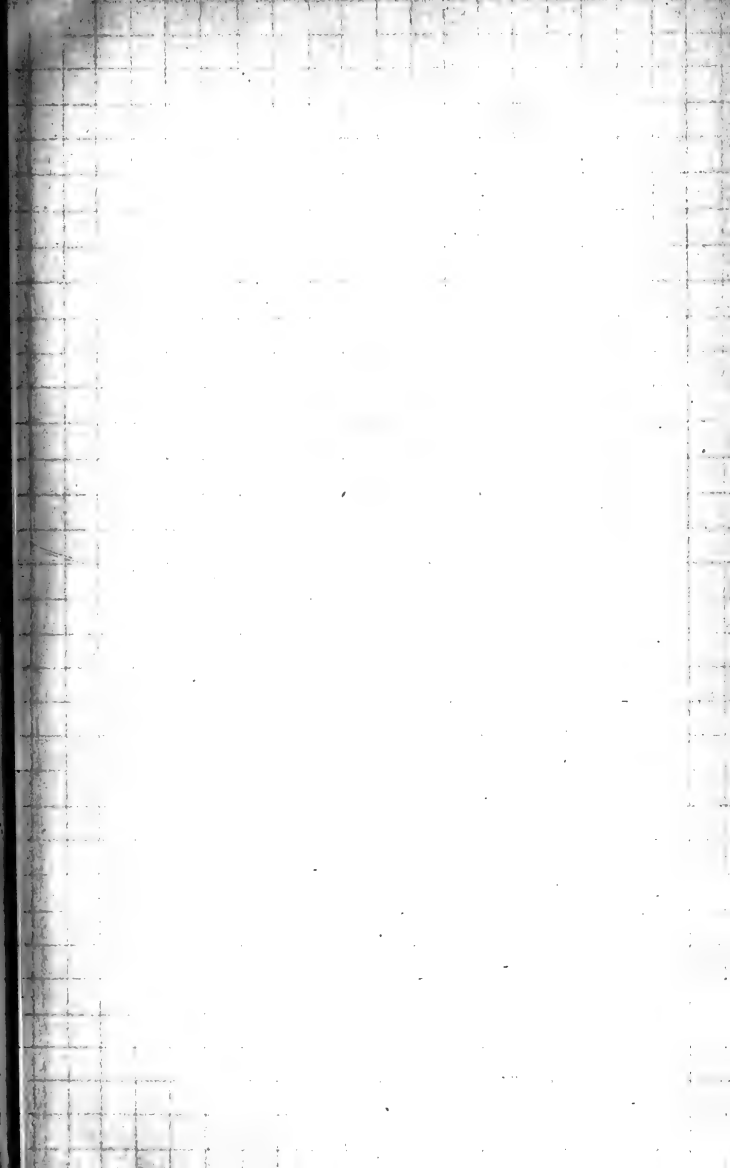
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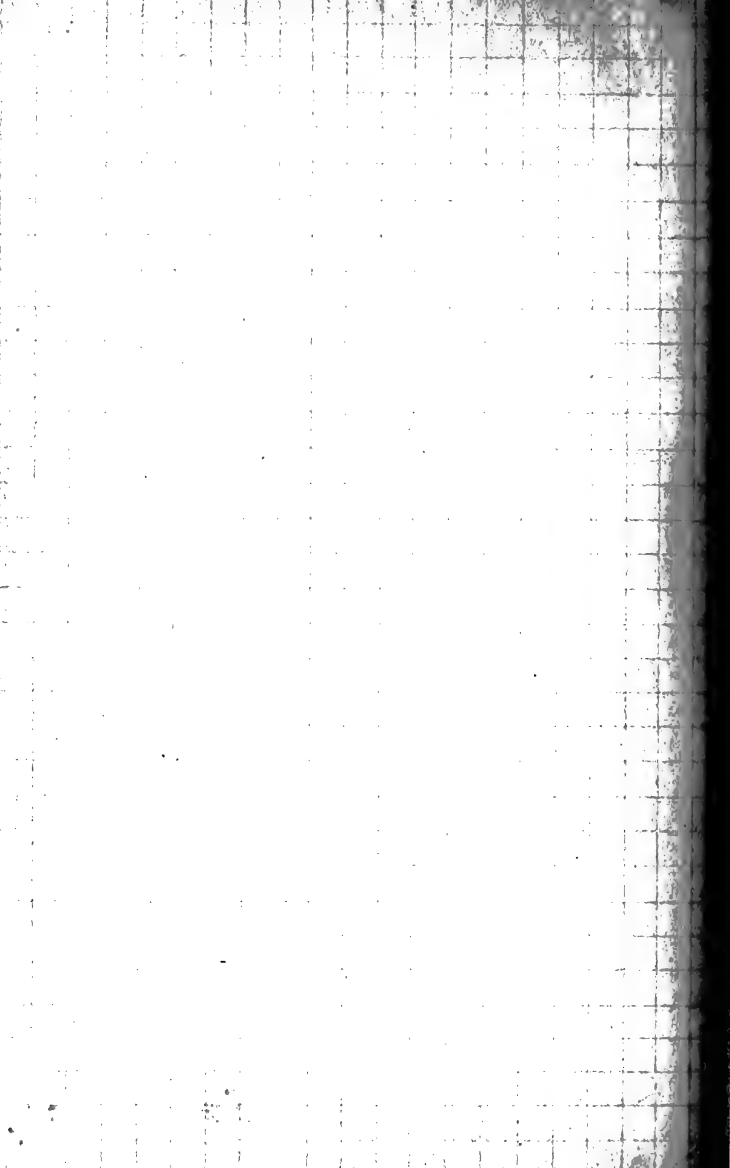


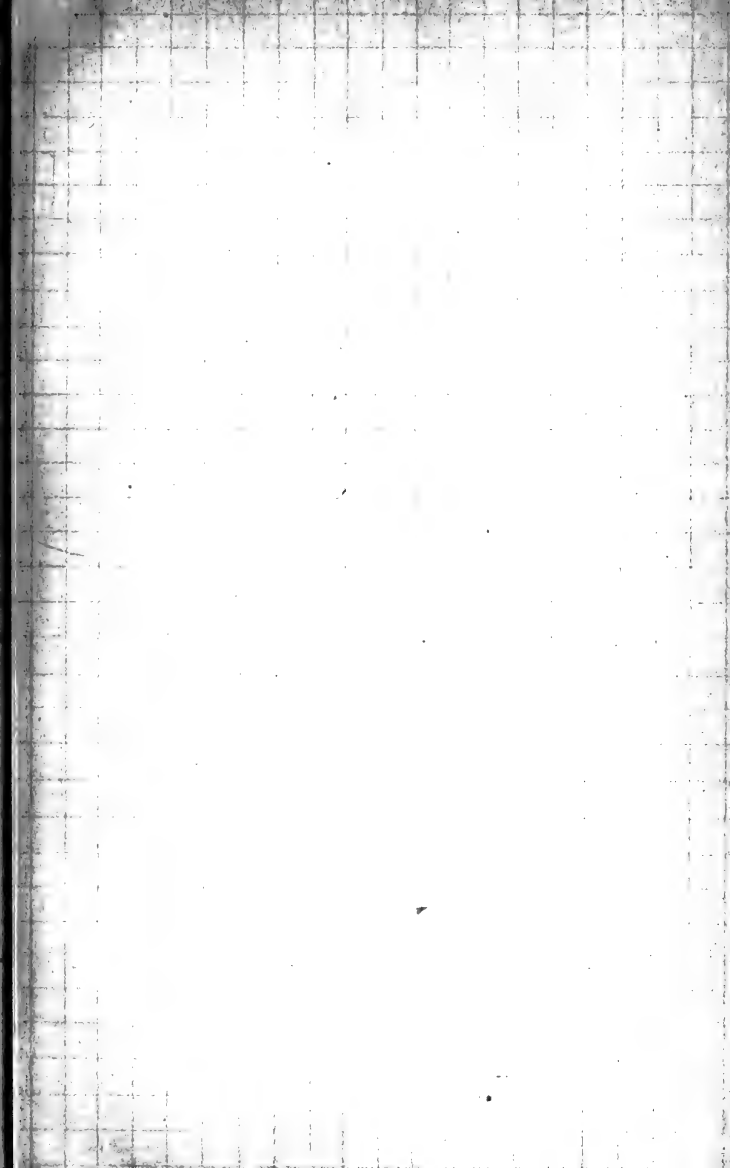


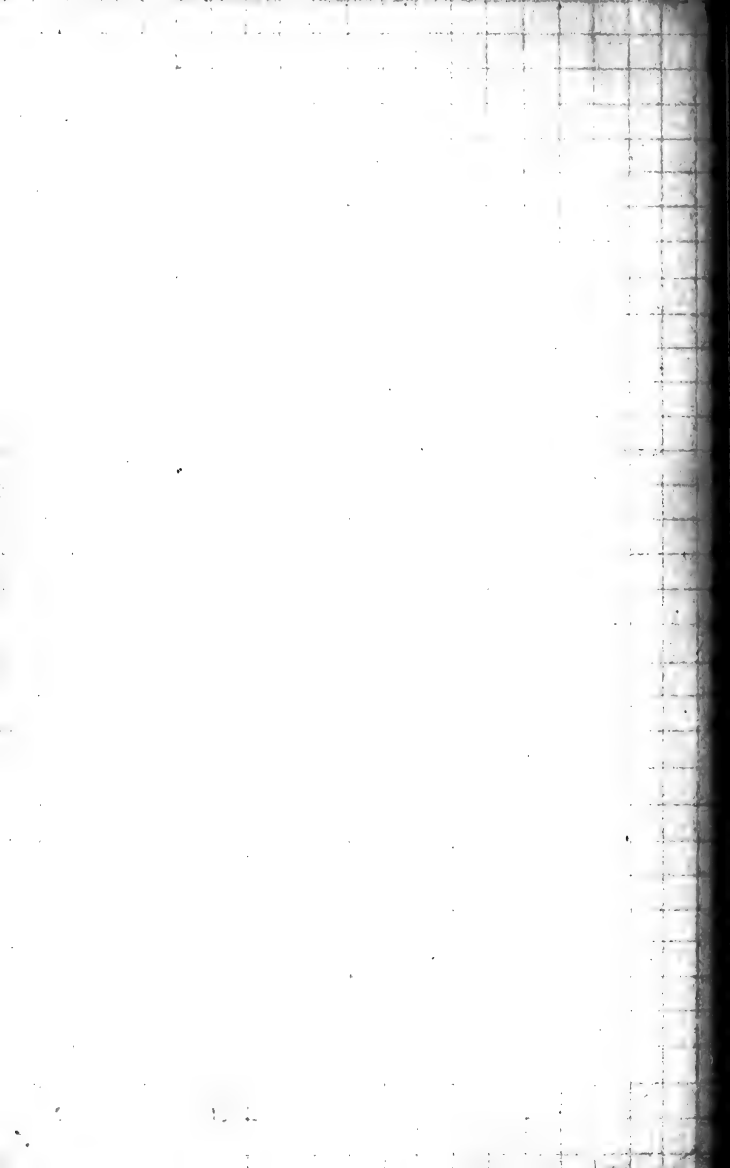


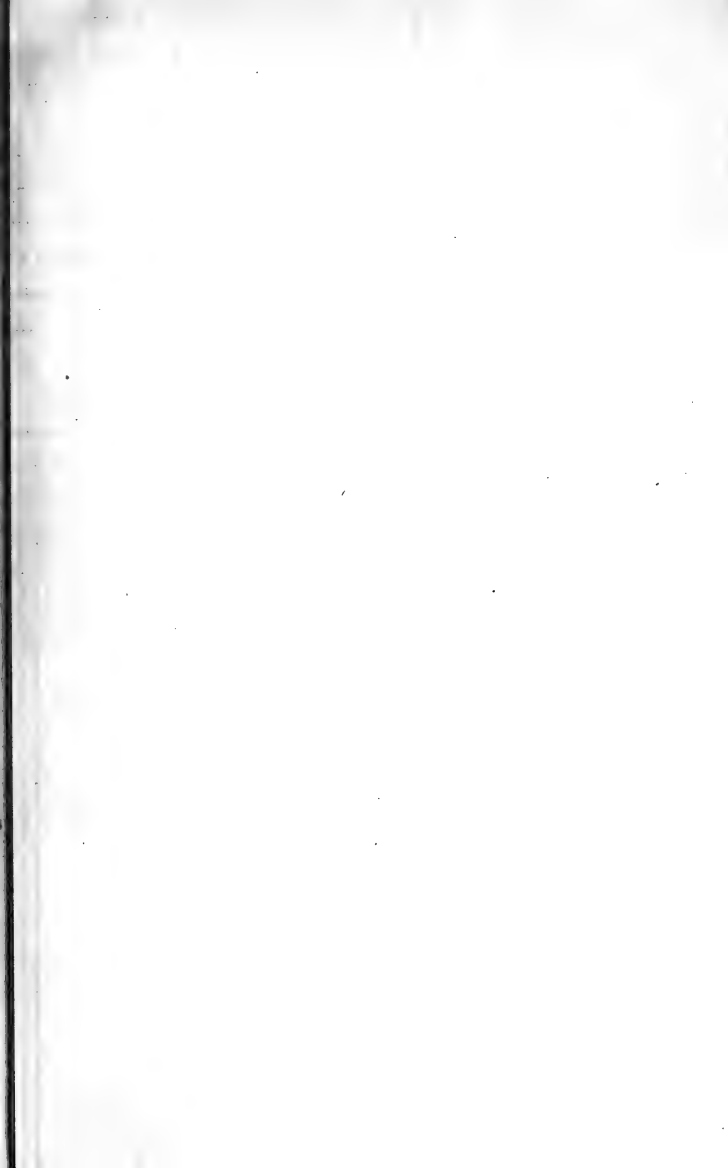


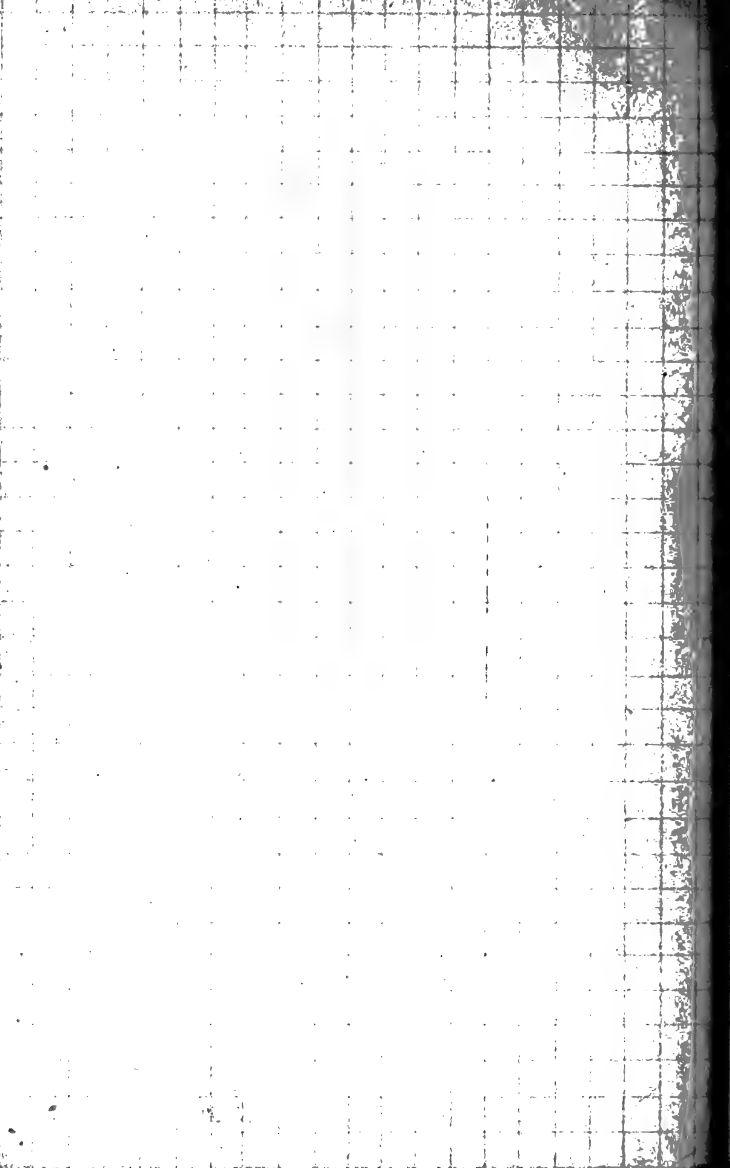


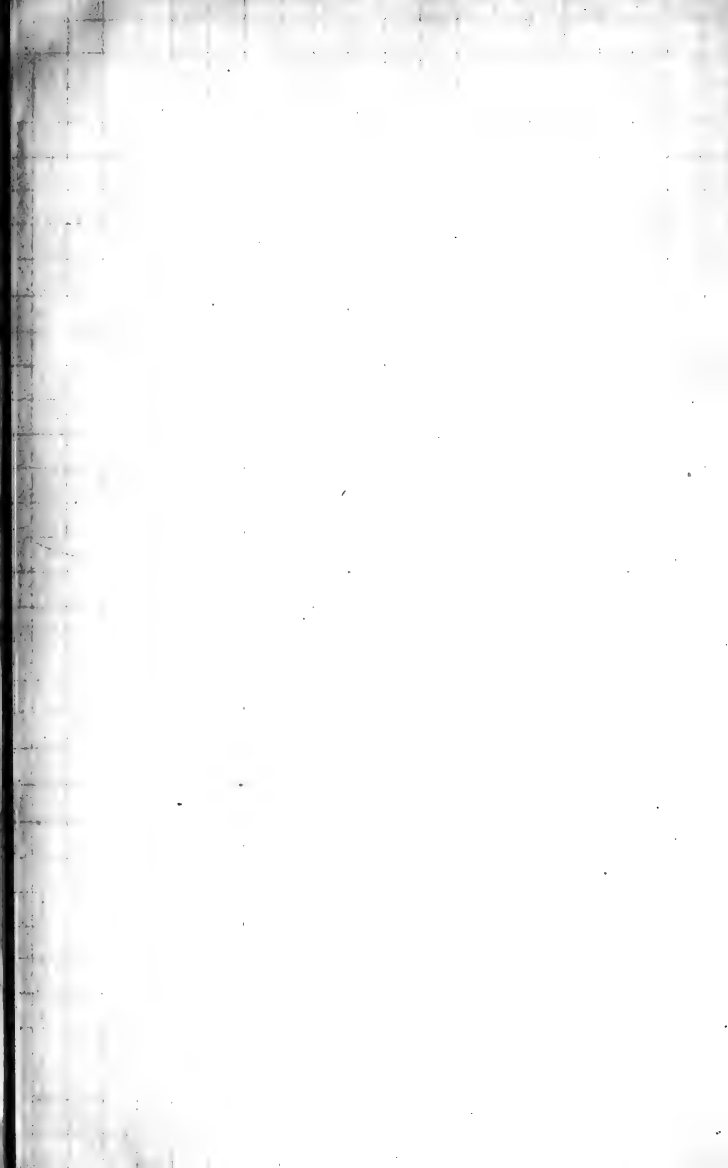


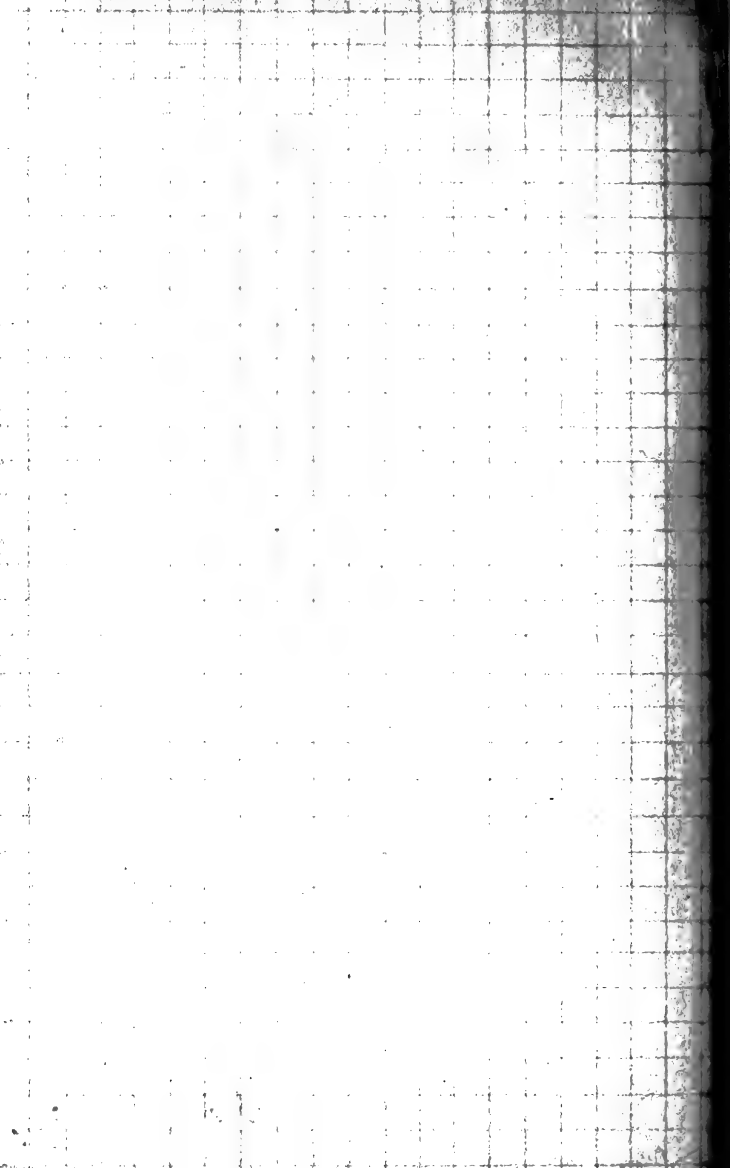


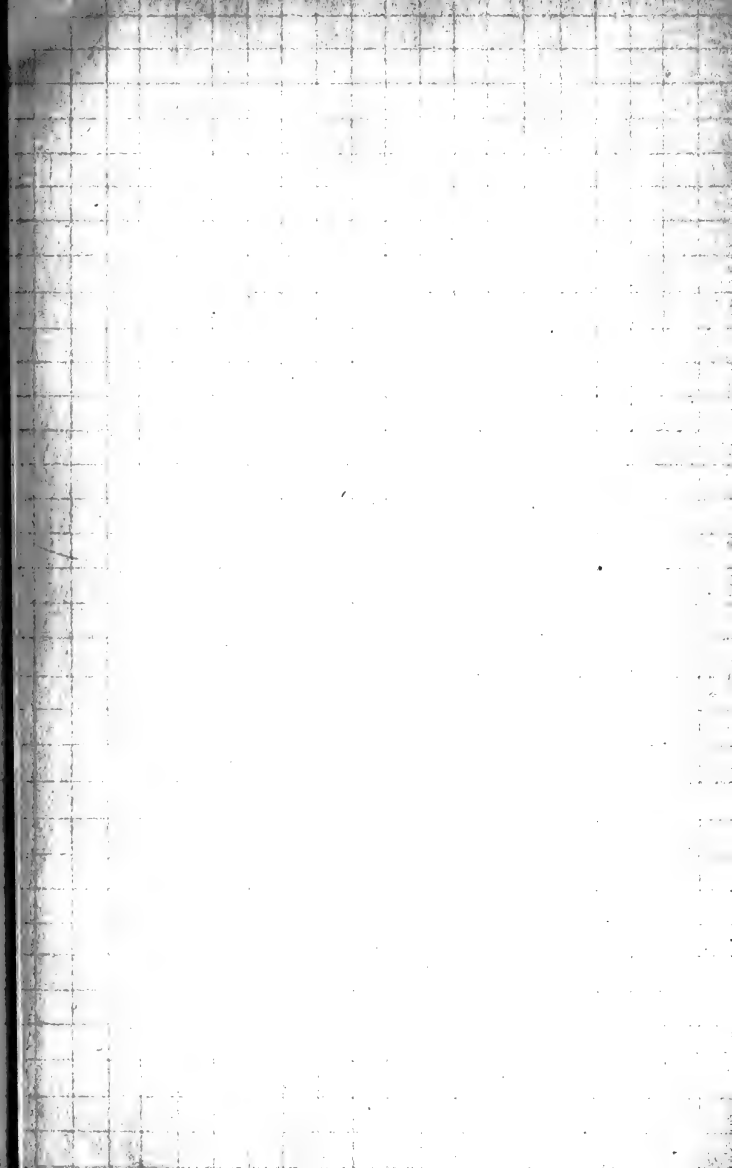


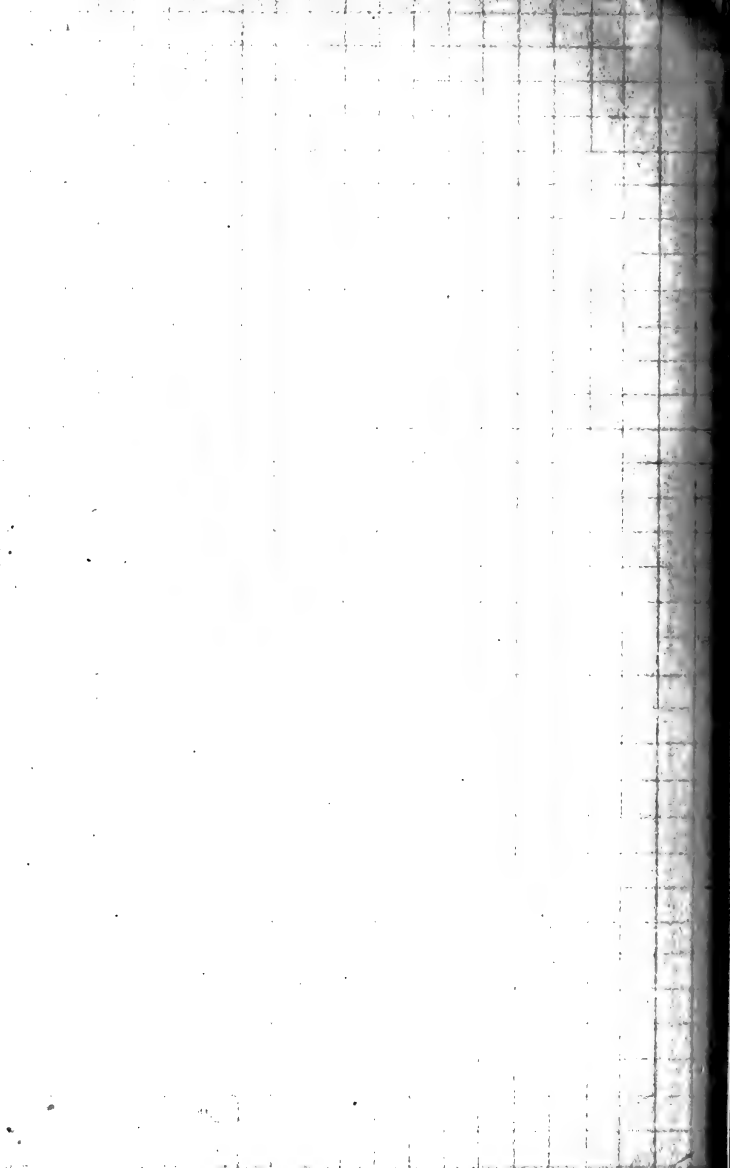


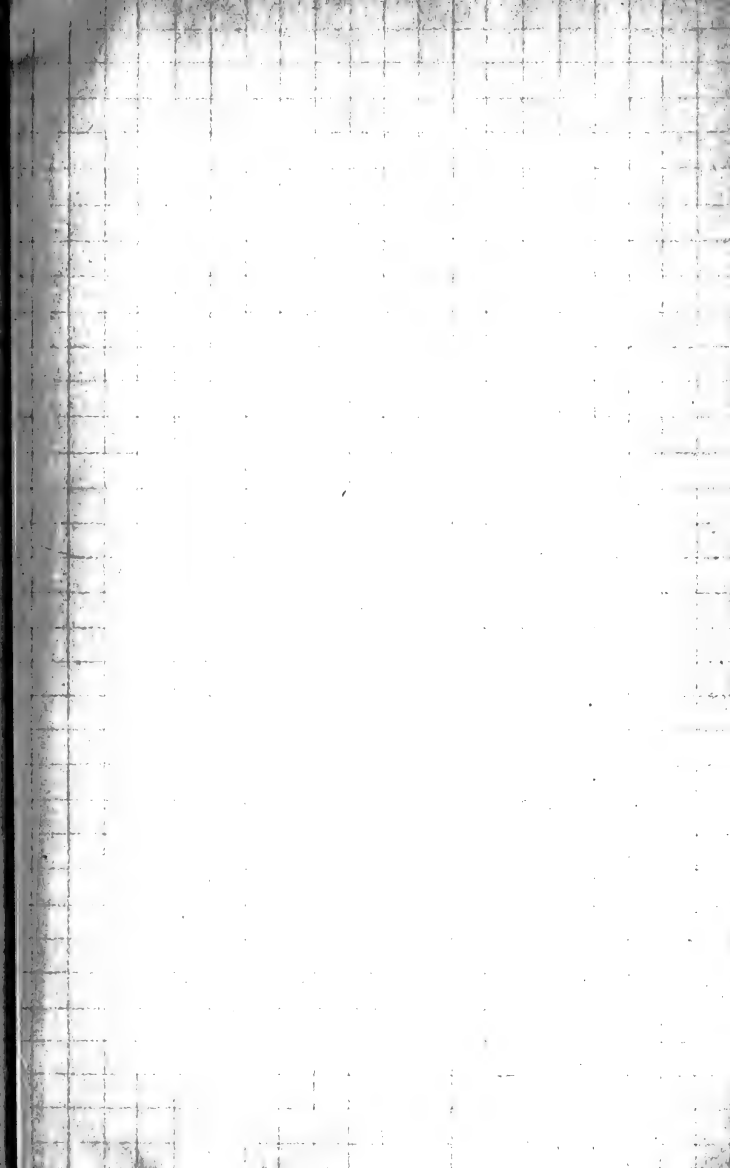


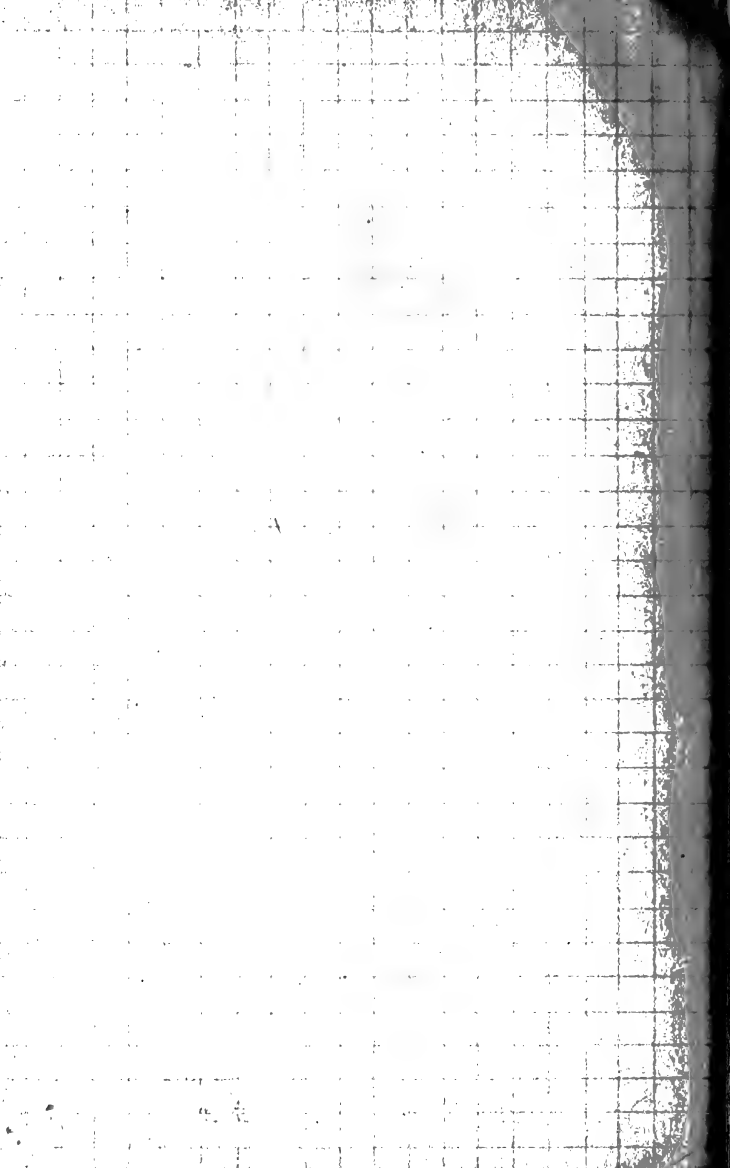




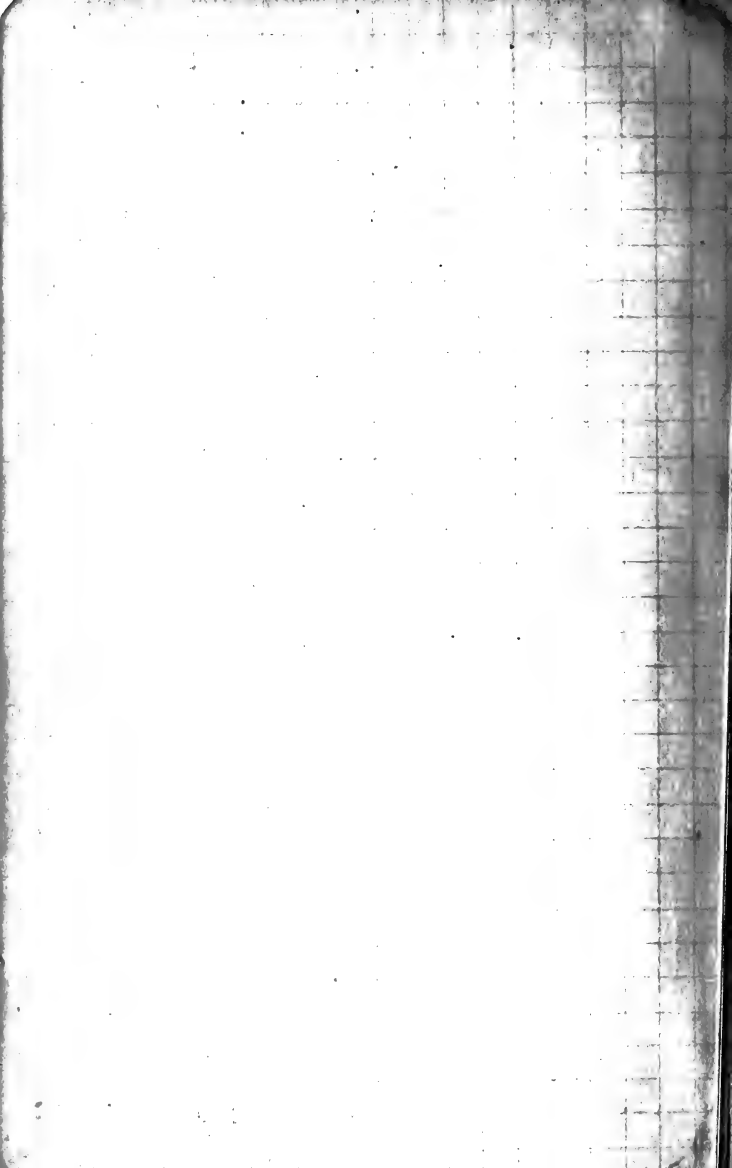












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